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Vehicle platooning schemes considering V2V communications: A joint communication/control approach

Tiago R. Gonçalves¹, Vineeth S. Varma², and Salah E. Elayoubi¹

Abstract—This article addresses communication and control aspects of platooning systems with the related challenges introduced by the overlap of both areas. The main objective is to provide a dynamic control mechanism where the parameters of the well-known Predicted Cooperative Adaptive Cruise Control (PCACC) are adapted based on the observed quality of the V2V (Vehicle-to-Vehicle) communication links. Different from the state of the art, our main design goal is the minimization of intervehicular distances while being robust in terms of an extremely low probability of emergency braking. A new adaptive control scheme based on the offline optimization of the control gains is proposed. We evaluate the new approach in a highway scenario and show the improvements obtained by the dynamic adaptation of the control parameters over static control strategies.

Index Terms—Vehicle platoons, cooperative adaptive cruise control (CACC), wireless communication.

I. INTRODUCTION

During the last decades, several approaches have been developed to deal with autonomous vehicles. Among some of the control technologies that were deployed to help the drivers' safety and increase their driving experience, one can cite the Cruise Control (CC) as a precursor of autonomous cars. However, the first meaningful step to allow the implementation of platoons in the vehicular environment was the establishment of the Adaptive Cruise Control (ACC). It was first introduced by Ioannou and Chien [1] and it consists of an autonomous control scheme based on constant time headway safety distance. Essentially, it allows autonomously to keep a certain desired distance from the preceding vehicle due to onboard sensors such as camera, radar, and lidar. A more sophisticated approach based on a coordinated exchange of information supported by wireless communication was early provided by [2] and it is known as Cooperative Adaptive Cruise Control (CACC). However, as CACC technology relies on other's vehicle information it is vulnerable to inherent communication aspects such as packet loss and latency. Our particular interest in the platooning system is because it is designed to take advantage of the particular distribution of a convoy in order to increase road capacity and to decreased fuel consumption that is achievable by gathering vehicles close together in order to reduce the air resistance of the

platoon's members. The exchange of information is crucial to the deployment of platoons as it allows taking control actions based on the most up-to-date information about the road and traffic status.

We consider in this paper the V2V communication method in platoons as illustrated in Figure 1. V2V enables communication between vehicles as long as they are in a certain range. This is the case of the IEEE 802.11p and 3GPP C-V2X Mode 4 technologies. The former is an adapted version of the IEEE 802.11a to suit vehicular applications [3], while the latter is the direct communication interface standardized by the 3GPP. Notice that the network-based communication approach of the 3GPP standard, known as 3GPP C-V2X Mode 3, is not considered here. [4] conducted simulations to show a comprehensive analysis of the advantages of the performance of C-V2X Mode 4 over the 802.11p. Similarly, [5] used a simulation environment to compare the communications performance of both modes 3 and 4 of C-V2X with the 802.11p standards. More recently, [6] adopted an analytic approach to describe the C-V2X Mode 4 performance. However, these works were limited to the telecommunication aspects and did not consider the control aspects of the platooning problem.

Another set of works considered the platooning scenario under different communication approaches. For instance, [7] used the 802.11p technology to evaluate the communication performance under a CACC controller in platoons. Likewise, [8] has adopted both wireless technologies (802.11p and C-V2X) and compared their performances in terms of the intervehicular distance of the platoon. [9] proposed a control strategy for graceful degradation based on estimating the preceding vehicle's acceleration in case of packet losses, but it mainly deals with extreme cases like complete link failure or lack of a wireless device on one of the vehicles. Different from the aforementioned article, we propose an online adaptation of the control parameter based on the observed quality of the communication link determined by the distance to the transmitter and the level of interference caused by other vehicles. More recently, [10] introduced a string stability analysis for a CACC alternative control design, in this paper called Predicted Cooperative Adaptive Cruise Control (PCACC).

The novelty in this paper is the introduction of a dynamic control mechanism where some of the parameters of the PCACC controller are adapted based on information about V2V communication. In particular, we adapt the parameter that is responsible to weigh the influence of the leader's

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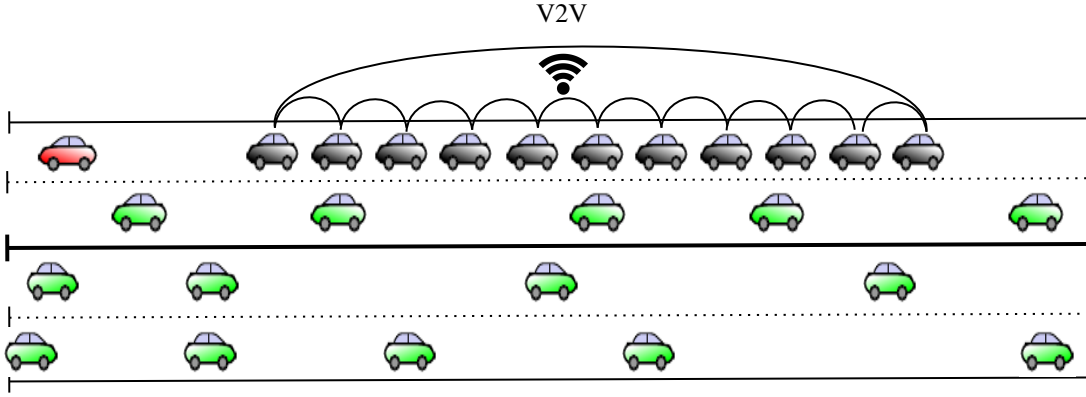


Fig. 1. Traffic scenario including a platoon with V2V communication approach.

broadcasted messages in the control algorithm, as well as the target distance between vehicles, based on the communication links qualities. Keeping in mind the above discussion and the results available in the literature on cooperative platooning systems, the following are the main contributions of this paper:

- 1) Evaluation of the robustness of the platooning mechanism under severe conditions for V2V communications, expressed in long bursts of losses and in difficult traffic jamming conditions on the road.
- 2) Offline optimization of the platooning control parameters based on extensive simulations of a highway scenario.
- 3) Online adaptation of the control parameters based on the observed communication link quality and on the results of the offline optimization.
- 4) Adoption of safety as a primary performance metric, quantified in terms of avoiding emergency braking. This translates to robustness constraints, where the inter-vehicle distance in the platoon is set so that *emergency braking is avoided in 99,999% of the cases*.

The paper is organized as follows. An overview of the control and communication aspects is presented in Section II, and the proposed scheme is described. Section III presents the system model, introduces the robustness case scenario and discusses the performance evaluation. Section IV includes considerations for future work and concludes the paper.

II. CONTROL AND COMMUNICATION PLATOONING SCENARIOS

The objective of this section is to present the control schemes and their interaction with algorithms performance, and to introduce the proposed scheme based on PCACC.

A. Adaptive Cruise Control

The ACC scheme autonomously allows the equipped vehicle to keep a certain desired distance apart from the preceding vehicle. This is possible because of the adoption of cameras, radars, and lidars that measure in real-time the preceding vehicle's position and velocity. Different spacing policies can

TABLE I
COMMUNICATION AND CONTROLLER PARAMETERS

| Communication | | Controller | |
|----------------|---------------|--------------------------------|----------|
| Parameter | Value | Parameter | Value |
| Channel | Highway NLOS | Leader factor (C_1) | Adaptive |
| Path loss | Winner+B1 LOS | Desired distance (D_{des}) | Adaptive |
| Noise power | -174 dBm/Hz | Damping ratio (ξ) | 2 |
| Tx power | 22.5 dBm | Bandwidth (ω_n) | 0.5 Hz |
| MCS | QPSK, R=1/2 | Time gap (h) | 1.4 s |
| CAM size | 500 bytes | Vehicle length (L) | 16.5 m |
| CAM interval | 100 ms | Actuator lag (τ) | 500 ms |
| Radar interval | 60 ms | Lane width | 5 m |
| Process delay | 1 ms | | |

be used such as Constant Spacing (CS) and Constant Time-Gap (CTG) policy, for instance, see [11]. Briefly, the controller on the former scheme aims to keep a constant distance of the preceding vehicle while on the latter one it aims to control the clearance, or time gap, between the host vehicle and the preceding vehicle. In this paper, the CTG policy is applied with the following control law introduced by Ioannou and Chien [1]

$$a_{i_des} = \ddot{x}_{i_des} = -\frac{1}{h}(\dot{\varepsilon}_i + \lambda\delta_i) \quad (1)$$

where

$$\varepsilon_i = x_i - x_{i-1} + L_{i-1} \quad (2)$$

$$\delta_i = \varepsilon_i + h\dot{x}_i \quad (3)$$

are the inter-vehicle spacing and the spacing error, respectively. The index i symbolizes the vehicle index, the first vehicle being numbered 0. x_i denotes the position of vehicle i , L_i its length and a_i its acceleration. h is the time-gap parameter and λ is the design gain parameter. The control input is calculated based on the difference of its own velocity and position with the preceding vehicle, (\dot{x}_i, x_i) and (\dot{x}_{i-1}, x_{i-1}) respectively. Note that in platooning systems, the ACC control law is always adopted by the leader since it is preceded by a vehicle that is not subject to the platooning controller.

B. Predictive Cooperative Adaptive Cruise Control

PCACC, introduced in [10], implies that the control effort, the desired acceleration, of the leader and of the preceding

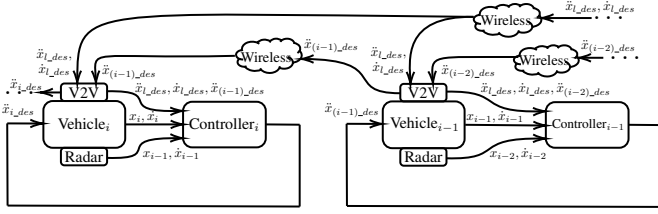


Fig. 2. Block diagram of the platoon system with a PCACC control between vehicle $i - 1$ and vehicle i .

vehicle are available to the following vehicle and its control law is given by

$$\begin{aligned}
 a_{i_des} = \ddot{x}_{i_des} = & (1 - C_1)\ddot{x}_{(i-1)_des} + C_1\ddot{x}_{l_des} \\
 & - (2\xi - C_1(\xi + \sqrt{\xi^2 - 1}))\omega_n\dot{\epsilon}_i \\
 & - (\xi + \sqrt{\xi^2 - 1})\omega_n C_1(\dot{x}_i - \dot{x}_l) - \omega_n^2\epsilon_i \quad (4)
 \end{aligned}$$

where

$$\epsilon_i = x_i - x_{i-1} + L_i + D_{des} \quad (5)$$

$$\dot{\epsilon}_i = \dot{x}_i - \dot{x}_{i-1}. \quad (6)$$

L_i is the length of the vehicle and D_{des} is the desired inter-vehicular distance that we want to minimize. The control parameters to be tuned are C_1 , ξ and ω_n . The parameter C_1 takes on values $0 \leq C_1 < 1$ and is responsible to weigh the contribution of the leader's speed and acceleration. ξ is the controller damping ratio and ω_n is the controller bandwidth. The adopted control parameters are shown in Table I. Such improvement of this fully predictive cooperative control is due to the fact that it allows the communication between all the vehicles in the platoon including the leader as shown in Fig. 2. Fig. 2 also illustrates the input signals required by the PCACC controller and the respective segments (V2V radio, vehicle dynamics, and radar equipment) that provide them. In other words, the CACC sends the actual acceleration, which is measured after the actuation lag, while the PCACC is able to propagate the actual values that will become effective after the actuation lag. The PCACC is expected to be superior to CACC because the actuation lag of the system does not affect directly the control effort, which is a big limiting factor for achieving short inter-vehicle distances [8].

C. Semi-Autonomous Control

This is a particular class of control that allows the system to achieve string stability with a constant space control strategy without direct communication from the leading vehicle. The control strategy can be obtained with a simple change in one of the control parameters of the CACC control scheme. Therefore, $C_1 = 0$ yields

$$a_{i_des} = \ddot{x}_{i_des} = \ddot{x}_{i-1} - 2\xi\omega_n\dot{\epsilon}_i - \omega_n^2\epsilon_i. \quad (7)$$

The control law is based on one vehicle look-ahead communication topology, which means that only preceding vehicle's information is required. In this case, its acceleration, velocity,

and position $(\ddot{x}_{i-1}, \dot{x}_{i-1}, x_{i-1})$ are necessary, but without any information from the leader. As proven in [12], this particular control law is only string stable when the control effort is always available which means when there is no delay in the process. In the control field, the concept of string stability is recurrently mentioned when it comes to platoon systems. A string stable platoon means that any acceleration or braking in the first vehicle is not going to cause an amplification of the error along the tail of the platoon. In other words, as long as the first vehicle is able to avoid a collision all others will be able too. In [11], there is more information about mathematical definitions and conditions to ensure the string stability.

D. Proposed dynamic scheme based on PCACC

In contrast to existing works that assume a fixed control strategy, our main contribution is to propose an approach that will adapt the control parameters based on the communication link quality characterized by the packet error rate from the leader to the last vehicle (defined as PER_{LLV}). We aim to keep a homogeneous control strategy in the whole platoon. In particular, among the control inputs, the pair (C_1, D_{des}) has the most substantial impact on the performance of the system. As mentioned before, C_1 is responsible to weigh the influence of the leader's message in the control algorithm while D_{des} is the desired inter-vehicular distance that we want to set, but due to actuator lag and delay in the process it does not correspond to the actual average inter-vehicular distance (D_{avg}). The following algorithm based on PCACC controller is proposed.

- **Step 1:** Update the traffic density range limits (PER_{LLV}).
- **Step 2:** Vary the C_1 parameter while minimizing D_{des} and register the average inter-vehicular distance D_{avg} for each PER_{LLV} inside the range of Step 1.
- **Step 3:** Consider the minimum D_{avg} result with no collision and identify its correspondent pair of $(C_1(PER_{LLV}), D_{des}(PER_{LLV}))$ to build the optimum lookup table $(C_1^*(PER_{LLV}), D_{des}^*(PER_{LLV}))$.
- **Step 4:** Observe the current communication link and adapt the control inputs (C_1, D_{des}) accordingly based on the optimum lookup table of Step 3.

Therefore, we conduct an offline heuristic optimization to determine the best control parameters (C_1, D_{des}) , in terms on minimum inter-vehicular distance without collisions, for any given value of PER_{LLV} (which is the result of the traffic density and the resulting interference). We build a $(C_1^*(PER_{LLV}), D_{des}^*(PER_{LLV}))$ lookup table that will serve as an optimum reference for each PER_{LLV} value.

Many existing works on CACC and PCACC mention the minimum distance possible assuming a certain level of interference or traffic on parallel lanes, however, it is not clear what should be done in practice where these parameters will evolve over time in an unknown manner. We propose to apply an online adaptation of the parameters (C_1, D_{des}) based on the observed PER_{LLV} and on the results of the offline optimization. Note that due to actuator lag and delay the string stability is not guaranteed for all platoon sizes other than those evaluated.

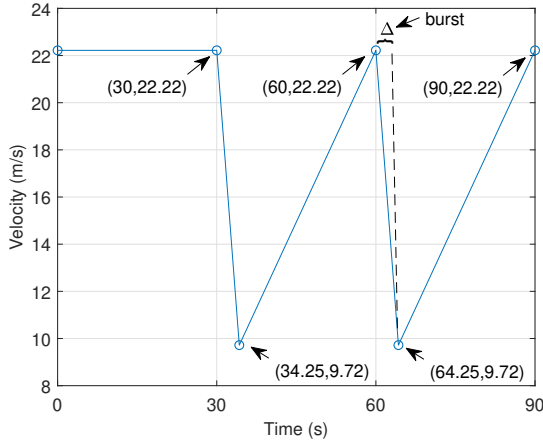


Fig. 3. Illustration of the jammer velocity profile adopted with 2 cycles.

III. SIMULATION ASSUMPTIONS AND PLATOON MODEL

In this section, we present the system model, the control and communication parameters, and the simulation tool adopted.

A. Vehicle dynamics

The vehicle dynamics is modeled as first-order low pass filter due to the actuator lag. So the transfer function is modeled in the frequency-domain as

$$G(s) = \frac{A_i(s)}{A_{i_des}(s)} = \frac{1}{\tau s + 1} \quad (8)$$

where τ is the time constant of the first-order low pass filter. A_i is the output, which can be interpreted as the actual vehicle acceleration, whereas A_{i_des} is the vehicle input, which can be seen as the desired acceleration. Note that, $\cdot(s)$ denotes the Laplace transform of the corresponding time-domain variable. The idea is to approximate the dynamics of the throttle body and vehicle inertia in order to avoid instantaneous response. In this paper, we assumed a lag of $\tau = 0.5$ s as in [11].

B. Platoon Scenario and Robustness Criterion

The system consists of a platoon of 10 automated vehicles following the leader. The simulated scenario takes place in a four-lane highway, as illustrated in Fig. 1, with a maximum traffic density of 20 interfering vehicles/km. The vehicles of all other lanes are not in platoons (green vehicles) and a jammer (in red) precedes the platoon leader. In the offline optimization section, the speed of the jammer (vehicle outside of the platoon) follows a preset sequence, adapted to only two cycles from [8], as shown in Fig. 3. The main reason for this jammer velocity profile is to study the capacity of the platoon system to avoid a collision in risky scenarios such as when the vehicle outside of the convoy suddenly applies the maximum brake capacity. Furthermore, different from the previous articles so far that just do Monte-Carlo simulations (100 or 1000 iterations of normal conditions), we have considered a burst of packet losses. While bursts are rare events, they may occur and impact the safety of the platoon,

but are not well reflected in the numerical analysis of most previous works like [7]- [13]. In this sense, the robustness treated here is related to the following worst-case event: the jammer brakes at some time ($t = 60$ s in our simulation) and this braking coincides with a burst of packet losses (complete interruption of the transmitted signal) during the following interval $t + \Delta$ also illustrated in Fig. 3.

In order to be conservative, we consider long bursts of packet losses that occur with a probability of 10^{-5} . Denoting by PER the probability of packet loss taking into account the channel model and packet collisions and T the time sampling interval for vehicle information, the burst size Δ (in seconds) can be calculated as

$$\Delta = -5/(\log_{10}\text{PER})T \quad (9)$$

In our simulations, we have considered the sampling rate of $T = 100$ ms as advocated by the ETSI EN 302 637-2 standard.

C. Simulation tool

We used the MATLAB/Simulink environment to model the vehicle dynamics and to implement the control law. Furthermore, we adopted the WLAN Toolbox of MATLAB to implement the channel configuration for a 802.11p transmission in order to obtain the Packet Error Rate (PER) taking into account the V2V fading channel aspects, the additive white Gaussian noise, the packet collisions and others communication parameters as in Table I. The mobility behavior of vehicles is also observed in the MATLAB/Simulink environment as we consider a traffic scenario as in Fig. 1. So at the beginning of each simulation step, from the ‘‘Radar’’ module the ‘‘Controller_i’’ is able to update the velocity and the position of the preceding vehicle (\dot{x}_{i-1}, x_{i-1}) as in Fig. 2. Also, the block ‘‘Vehicle_i’’ provides the vehicle’s dynamics, thus its own velocity and position (\dot{x}_i, x_i), to the ‘‘Controller_i’’ module. Furthermore, the controller reads the leader’s acceleration and velocity and the preceding vehicle acceleration ($\ddot{x}_l, \dot{x}_l, \ddot{x}_{i-1}$) from the ‘‘V2V’’ module. Recall that in the leader vehicle we implement an ACC controller, so the ‘‘V2V’’ module is responsible only to broadcast its acceleration and velocity since the ACC controller does not require any other inputs as those provided by the modules ‘‘Radar’’ and ‘‘Vehicle’’. Based on the inputs mentioned, the ‘‘Controller_i’’ module is able to calculate the desired acceleration (\ddot{x}_{i_des}) in order to keep a certain desired distance (D_{des}) from the preceding vehicle. Thus, the ‘‘Vehicle_i’’ module, responsible to approximate the dynamics of the vehicle, applies the desired acceleration and provides as output the vehicle’s position and velocity at the next simulation step.

The WLAN Toolbox is used to simulate the wireless condition for a 802.11p transmission. We adopted two different packet error rate parameters. The first one is related to the packet error rate between two successive vehicles and defined as $\text{PER}_{i,i+1}$ along the article. We adopted an Highway line-of-sight (LOS) profile as vehicles in the platoon are close enough to justify the usage. The second one is the packet error rate between the leader to the last vehicle that was defined as

PER_{LLV} . In this case, we used the Highway non line-of-sight (NLOS) profile in the toolbox since in this case the leader is less likely to be in the LOS with the last vehicle in the platoon. Furthermore, we stochastically calculated the SINR (Signal to Interference and Noise Ratio) for each of the vehicles in the platoon considering Winner-II Path Loss Model (B1 scenario) [14] and the interference from other vehicles.

IV. PERFORMANCE EVALUATION

The leader is equipped with an ACC control to be in accordance with the recommended safety time interval gap of the respective local law while the platoon is equipped with fully predictive cooperative control. The focus is to apply a longitudinal control in the platoon through V2V communication technology and analyze the system stability by means of vehicle collisions in some robust and worst-case scenarios. We considered the zero-order hold mechanism as the holding strategy for the control signal during the periods of packet losses. Furthermore, in all simulations, we focus on obtaining the minimum feasible inter-vehicular distance in the platoon with a emergency breaking probability no more than 10^{-5} . Note that we implemented a safety gap distance of 0.5 m for the emergency braking actuation to avoid collisions in practical settings.

The control strategy demands relative position and longitudinal velocity of the preceding vehicle so we assumed that the measurements are sampled each 60 ms with 1 ms delay and done by a long-range radar as in [8]. All the vehicles in the platoon broadcast a 500 bytes message on a 10 MHz channel bandwidth. Neighbouring vehicles are subject to a Highway LOS channel model [15] and our simulations provide a $PER_{i,i+1} \in \{0.006, 0.0245\}$ for the cases without interference and with interference, respectively. We have adopted $PER_{i,i+1} = 0.0245$ as the default value. As of the leader communication, the leader broadcasts a message to all other vehicles that is subject to a Highway NLOS channel [15] with $PER_{LLV} \in \{0.2, \dots, 0.7\}$, depending on the interference conditions.

A. Offline optimization

We start by performing an offline optimization of the control parameters (C_1, D_{des}). Fig. 4 illustrates the substantial impact of C_1 parameter on the average inter-vehicular distance (D_{avg}) for different PER_{LLV} values. Thus, from Fig. 4 we can retrieve the C_1^* optimum that minimizes the inter-vehicular distance for each PER_{LLV} evaluated, which is illustrated in Fig. 5 on the left. Similarly, the optimum D_{des} values were established as shown in Fig. 5 on the right. In this figure, $C_1 = 0.3$ represents the best alternative in the robust scenario for low PER_{LLV} values. While, $C_1 = 0.2$ indicates to be the best value for mid-range values as $0.2 \leq PER_{LLV} \leq 0.4$. For higher $PER_{LLV} \geq 0.5$ the best parameter values is $C_1 = 0$ which is the case of semi-autonomous control.

B. Online adaptation of the control parameters

We now move to the online adaptation of the control parameters, where the whole platoon adapts the control inputs

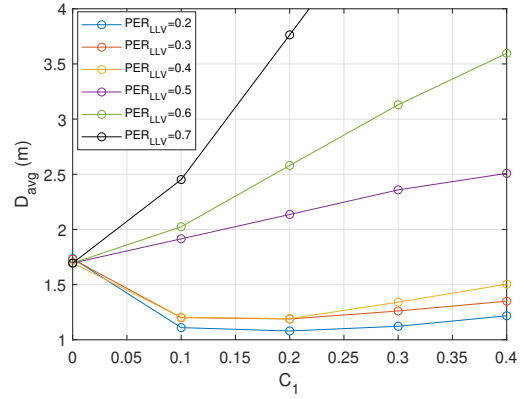


Fig. 4. Illustration of the average inter-vehicular distance with $PER_{i,i+1} = 0.0245$ for different C_1 values.

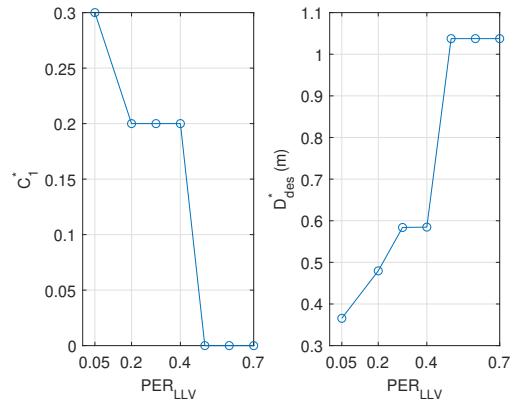


Fig. 5. Illustration of the optimum C_1 and D_{des} parameters for different PER_{LLV} values.

(C_1, D_{des}) corresponding to the optimal values computed in the offline optimization based on the packet loss observed on the communication link by the leader and the last vehicle (PER_{LLV}). For comparison purposes, we also simulated cases with fixed control parameters. The idea is to inspect the occurrence of collisions and to compare the inter-vehicular distance of the platoon in a long simulation of 25 minutes in three different cases defined as follows:

- Case 1 - PCACC with fixed $C_1 = 0.2$. In this case, we apply the D_{des} correspondent to the average PER_{LLV} . We aim to treat the case where the system operates in a moderate scenario where it's not too conservative.
- Case 2 - Semi-autonomous ($C_1 = 0$). In order to have a robust controller, we apply the D_{des} corresponding to the worst-case PER_{LLV} .
- Case 3 - The proposed dynamic scheme where the control parameters are based on the observed PER_{LLV} .

In all cases, we considered the jammer profile as the pattern from Fig. 3 repeated 50 times. Another important factor is the traffic density that generates interference and changes the PER. In order to have a fair comparison between all cases, we apply a predefined traffic density in the simulation. The range of the traffic densities varies from 0 vehicle/km to 20 vehicle/km

TABLE II
CASE COMPARISON FOR THE ONLINE IMPLEMENTATION.

| | Parameters | Case 1 | Case 2 | Case 3 |
|------------|---------------|--------|--------|---------|
| Controller | C_1 | 0.2 | 0 | Dynamic |
| | D_{des} (m) | 0.5847 | 1.0375 | Dynamic |
| Outputs | D_{avg} (m) | 1.2103 | 1.6785 | 1.3823 |
| | D_{min} (m) | 0.2537 | 0.6297 | 0.5233 |
| | Collisions | 8 | 0 | 0 |

that corresponds to $PER_{LLV} = 0.2$ and $PER_{LLV} = 0.7$ for a 11 platoon vehicle in the considered scenario, respectively. The predefined traffic densities starts from $PER_{LLV} = 0.2$ and during each 2 minutes (4 cycles) it adds 0.1 in the PER_{LLV} up to the maximum $PER_{LLV} = 0.7$. Then, with the same logic, it decreases to the minimum $PER_{LLV} = 0.2$ and then increases again until $PER_{LLV} = 0.4$ where its elapsed time reaches 25 min. Notice that the traffic density changes linearly and less frequently than the jammer incidents. We applied the burst as in (9) in each 6 min of simulation in the 9th vehicle in the platoon to simulate the burst of packet losses in the most critical moment.

From Table II, we notice that Case 1 exhibited 8 collisions while cases 2 and 3 had none. The former case comprises the event where the system is assumed to operate in an average traffic condition such as $PER_{LLV} = 0.4$. However, it can be seen that this is not a safe approach since it does not guarantee a secure outcome. Case 2 corresponds to the case where the optimum (C_1^*, D_{des}^*) control parameters are set for higher PER_{LLV} values (worst case). Note that this corresponds to the adoption of the semi-autonomous control as $C_1 = 0$. The idea behind this scenario is to have a robust and safe outcome. Despite no collisions, it exhibited an increase of 21% in the inter-vehicular distance when compared to the suggested Case 3 approach. Figure 6 shows the average inter-vehicular distance and the correspondent PER_{LLV} value of the suggested approach for the considered simulation. Therefore, the proposed method is demonstrated to be the best option so that platoon remains safe and robust while reducing the inter-vehicular distance.

V. CONCLUDING REMARKS

This paper studies the design of the platoon control algorithm based on the V2V communication quality. We started by devising the optimal parameters of the controller for different communication qualities, namely the weight given to the information broadcast by the platoon leader (C_1 parameter), and the desired distance (D_{des}) between vehicles. We then proposed a new dynamic approach based on the offline optimization of the control parameters (C_1, D_{des}). In this dynamic scheme, the quality of the communication link is continuously monitored and the control parameters updated accordingly based on the results of the offline optimization. Our simulation results show that, if the control parameters *are not adapted to the channel quality*, the *semi-autonomous control* performs best. However, with the *proposed adaptive control, using leader information results in a better performance*. In future work, combin-

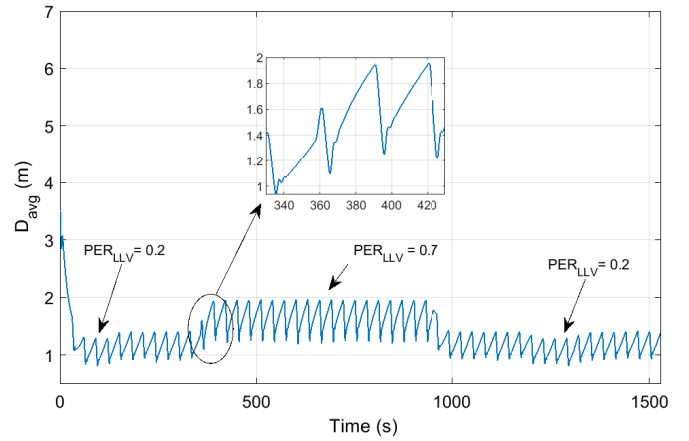


Fig. 6. Illustration of the average inter-vehicular distance of the Case 3 simulation and the correspondent boundaries of PER_{LLV} .

ing different wireless technologies, such as V2N (Vehicle-to-Network) and VLC (Visible Light Communication), is a promising means for enhancing the robustness of the platoon while reducing the inter-vehicle distance.

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