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A multi-scale analysis of the different interactions between defects and hydrogen: a review on the contribution of the elastic fields

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Abstract - Hydrogen Embrittlement (HE) is one of the causes mainly evoked in premature rupture of industrial components exposed to an aggressive environment. Many studies have been conducted in order to understand the mechanisms involved during this degradation and the influence of the metallurgical states. Good knowledge of hydrogen interactions with crystal defects is a key element in the understanding of the different damage processes associated with HE in fcc materials. In this state of mind, we have undertaken a systematic study of these interactions in nickel alloys using coupled multi-scale approaches. These latter correspond to the association of atomistic calculations (EAM, DFT) with experimental tests: Electrochemical Permeation (EP), Secondary Ionization Mass Spectrometry (ToF-SIMS) analysis and Thermal Desorption Spectroscopy (TDS) in order to evaluate the hydrogen states in presence of different crystal defects. Among the major results, we focus our attention on the interaction between hydrogen and vacancies in nickel single crystals, the trapping and the segregation of hydrogen for several dislocation distributions (cells, PSB, GBs,...) and the contribution of the grain boundaries (GBs) as well as the precipitates to the hydrogen diffusion and trapping in nanocrystals, polycrystals and bi-crystals. In all the cases, we have questioned the impact of elastic fields associated with the defect to apparent solubility and diffusion of hydrogen. In the second part, we explore the potential impacts of hydrogen on elastic properties and their implication on the mechanisms of plasticity.

### 51 Introduction

52

53 It is now acted that the interactions of the environment with metals are strongly implied in the 54 embrittlement of materials and alloys of the engineering structures and can lead to premature 55 failures [1-5]. Among a large variety of processes which involves a stress/strain state and an 56 aggressive environment, we shall note that the impact of the internal and/or external hydrogen 57 can lead to severe loss of functional properties. A key element for the understanding of 58 hydrogen embrittlement is based on a good knowledge of the interactions between the solute 59 and the metallurgical state of the metal. In particular, hydrogen bonds favorably with defects 60 and affect the physical and chemical properties of metal [6]. Through the so-called trapping 61 phenomenon, the metallurgical state and structural defects can affect the apparent solubility 62 and the diffusion coefficient of the solute which, sometimes, can explain why literature data on the subject exhibit some incoherence. As it has been widely established in literature, the 63 64 electrochemical permeation technique and the thermal desorption spectroscopy can be used to extract and to classify the different hydrogen concentrations based on the difference in 65 binding forces between hydrogen and the trapping sites. The lower, medium and higher 66 67 binding energies correspond to the insertion in the interstitial sites  $C_{L}$  (0.1 to 0.2 eV), in the reversible trapping sites C<sub>Tr</sub> (around 0.3 eV) associated with elastic field near edge 68 69 dislocations network and/or semi-coherent precipitates the insertion in irreversible or deep trapping sites, C<sub>Tir</sub> (0.5 to 0.6 eV) associated with dislocation core and/or vacancy [9,10], 70 71 respectively. In each case, there is a purely mechanical contribution and a contribution of 72 chemical origin that is not always easy to distinguish, especially at the atomic scale. In this 73 work, we restrict our contribution to the question of the multiple interactions between a solute 74 and the elastic stress field at the different microstructural scales and their implications on the 75 apparent solubility and diffusivity of hydrogen. We begin our analysis by a brief presentation 76 of the different techniques used in our work. Then the thermodynamic framework is recalled 77 for an easy questioning of the couplings between mechanics and diffusion. Then, we give a 78 brief reminder of the different origins of the strain fields and their gradients to finally 79 illustrate our discussion on multiple cases recently investigated in our group. 80

81

## 82 **1 – Brief review of the different techniques used**83

84 In this section, we recall briefly the different techniques used in our work to identify on the 85 one hand the various microstructural defects studied and, on the other hand, the experimental 86 and the numerical investigation methods that have been used to characterize the interaction of 87 hydrogen with these defects. Dislocation and vacancy organization in nickel single crystal, bi-88 crystals and polycrystals have been investigated using a JEOL JEM 2011 transmission electron microscope (TEM) operating at 200 kV. Foils for transmission electron microscopy 89 90 (TEM) were thinned in a double twin-jet electro-polisher using electrolytes with the 91 conditions described previously [12]. We focus our attention on differing dislocation features 92 issues to tensile and cyclic loading of (001) single crystal orientation, grain-boundaries with 93 four misorientations and (001) single crystal with different hydrogen charging conditions. 94 Dislocation densities were measured using the standard intersection method from TEM 95 micrographs collected by Digital Micrograph<sup>TM</sup> software [11,12]. The size of vacancies 96 cluster is obtained from classical bright field conditions. The vacancy concentrations have 97 been evaluated using differential scanning calorimetry (DSC) as previously describe [13]. 98 DSC measurements were performed using a Q100 TA Instruments DSC apparatus. The 99 heating of the samples was carried out linearly from 273 to 723 K at a rate of 10 K min<sup>-1</sup>. The existence of an exothermic peak in the evolution of the heat flow as a function of temperature 100

101 is associated with the annihilation of vacancies, and the area of this peak corresponds to the 102 vacancy stored energy. The equilibrium vacancy concentration is obtained using the 103 formation energy of a vacancy deduced from our DFT calculations and exothermic peak (1.49 104 to 1.52 eV between 0 K to 1200 K [14, 15]). The grain-boundary character distribution is 105 investigated using crystallographic orientation mapping data extracted from electron 106 backscatter diffraction (EBSD) analyses as previously proposed (EBSD was carried out using 107 an EDAX/TSL OIM system coupled to a FEI Quanta 200 ESEMFEG scanning electron 108 microscope) [16]. For polycrystalline structure, grain boundaries are categorized into two families: the special GBs ( $\Sigma 29$ ) corresponding mainly to the  $\Sigma^{3n}$  in nickel [16] ( $\Sigma 3$ ,  $\Sigma 9$  and 109  $\Sigma$ 27), and random GBs (> $\Sigma$ 29). For bi-crystals, grain-boundaries with four misorientations 110 111 identified:  $\Sigma 11-50^{\circ}30 < 110 > {311},$  $\Sigma$ 11-129°30<110>{332}, have been Σ3-70°30<110>{111} and  $\Sigma$ 5-37°<100>{310} ( $\Sigma$ x- $\theta$  <hkl>{uvw} with x the index of 112 113 Coincidence Site Lattice (CSL),  $\theta$  the rotation angle, <hkl> the rotation axis and {uvw} the 114 grain boundary plane) [17,18].

115

To quantify the hydrogen concentration and the maximum solubility in nickel, we use 116 117 Thermal Desorption Spectroscopy (TDS, Jobin Yvon Horiba EMGA-621W hydrogen 118 analyzer) composed of an impulsion furnace system coupled with a thermal conductivity 119 detector [9, 15,16]. The procedure consists to measure the hydrogen concentration in the pre-120 charged samples by fusion. The pre-charging conditions are defined in the Volmer domain of cathodic electrochemical potential range in an alkaline solution of 0.1 M NaOH at room 121 122 temperature [15, 16]. According to thermodynamic and kinetic analysis the over potential 123 range explored correspond to a fugacity of 10<sup>5</sup> to 4. 10<sup>7</sup> Pa at 300K [19]. Electrochemical 124 Permeation (EP) is the main technique used to detect the mechanisms of diffusion and 125 trapping of hydrogen in different microstructures in our laboratory [15, 16, 20]. This 126 technique is composed of two cells separated by a membrane with an exposed surface in 127 contact with an electrolytic solution. The charging side or entry side of the membrane is 128 galvanostatically polarized at a constant cathodic charging current density (predefined 129 according to the cathodic polarization curve and fugacity range defined previously) in 0.1 M 130 NaOH (pH ~ 13). The detection side or exit side of the membrane was maintained at a 131 constant anodic potential of ~630 mV/SSE in 0.1 M NaOH (pH ~ 13), and the hydrogen flux (current density) at this side is recorded to study the transport of hydrogen through the 132 133 sample. A constant temperature is maintained between a range of 283 to 313K and both 134 solutions were continuously deaerated by argon gas at 1.4 bar (see the reference [19] and [20] 135 for more details). Using different conditions in term of temperature and cathodic charging 136 current density/potential (equivalent to a specific fugacity), a sequence of charging followed 137 by a sequence of desorption combines with TDS measurements at each step, allow to obtained the apparent diffusion coefficient D<sub>app</sub>, the average concentration of hydrogen on the sample, 138 139 the three different hydrogen concentrations namely interstitial C<sub>L</sub>, reversible trapping C<sub>Tr</sub>, 140 irreversible or deep trapping sites, C<sub>Tir</sub> and their respective energies [9,16]. In the specific case of grain-boundaries, the hydrogen concentration profile maps were obtained from time-141 142 of-flight SIMS measurements (TOF.SIMS5, ION-TOF GmbH, Germany) to elucidate the 143 local distortion around GB impact on hydrogen segregation in polycrystalline structures [21]. 144

The thermodynamic and elastic properties of nickel with hydrogen and/or vacancies were determined from *ab initio* calculations using the framework of the density functional theory (DFT) implemented in the Quantum ESPRESSO package [22]. Details about our calculations and convergence details can be found in our previous studies [14, 23-26]. First, we determine the H and vacancy concentrations at thermodynamic equilibrium with a H<sub>2</sub> gas at the temperature T and secondly the solubility and the jump rates of H in the bulk Ni lattice and in

151 the vicinity of a vacancy core are evaluated in relation with the lattice elastic distortion. For 152 other defects, such as dislocations and grain boundaries, atomistic simulations based on the 153 energy minimization method were performed using the LAMMPS code [27], to compute the 154 structural and defect properties of nickel grain boundaries [17,18,29] and edge dislocation 155 dipoles [30]. The EAM potential developed by Angelo et al. [28] for pure Ni and Ni-H 156 systems has been used for this study. The hydrogen insertion sites that can be found in the GB 157 region or dislocation edge dipole region were examined in terms of energy, excess volume 158 and local stress state [17].

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### 161 **2 - Thermodynamic framework**

163 The influence of the elastic stress/strain field on the chemical potential for solute is treated in 164 the basis of a continuum approach with a thermodynamic framework [15,19, 31, 32]. 165 According to the elastic work associated with the incorporation of the solute from the infinity 166 to the solid, the modification of the chemical potential in an isothermal state can be expressed 167 as :

169 
$$\mu_H(C_H,\bar{\sigma}) = \mu_0(C_{HO},0) + k_B T ln\left(\frac{C_H}{1-C_H}\right) - \Omega_a \sigma_{ij} \varepsilon_{ij}^s + \left[\frac{1}{2}S_{ijkl}\sigma_{ij}\sigma_{kl} + \frac{1}{2}\left(\frac{\partial S_{ijkl}}{\partial C_H}\right)\sigma_{ij}\sigma_{kl}\right]\Omega_a$$

170 (1) 171

172 with  $\Omega_a$  is the atomic volume of the host matrix,  $\mu_0$  and  $C_{H_0}$  the corresponding standard state

chemical potential and the concentration,  $\sigma_{ij}$  the stress tensor,  $S_{ijkl}$  the compliance and  $\mathcal{E}_{ij}^{s}$  the 173 174 strain tensor associated with the insertion of a solute in the crystal lattice, respectively. The 175 first term of equation (1) is the H standard state with the absence of stress, the second one is 176 the solute distribution entropy, the third term is the elastic strain energy associated with the 177 insertion of a solute, and the fourth term is the mechanical energy in the system and its modification in relation with the impact of solute on the compliance tensor  $S_{iikl}$ . In the 178 absence of external stress, the stress state only depends on the elastic energy from the 179 180 insertion of a solute in the crystal lattice (self-stress) or directly on elastic storage energy associated with the "defects" (precipitates, grain boundaries, vacancies, dislocations). 181 182 Considering that the other contributions can be neglected, we can get a simplified form of the 183 chemical potential:

185

184 
$$\mu_H(C_H, \bar{\sigma}) = \mu_0(C_{HO}, 0) + k_B T ln\left(\frac{c_H}{1 - c_H}\right) - \Omega_a \sigma_{ij} \varepsilon_{ij}^s$$
(2)

186

187 Considering the problem of hydrogen incorporation into a crystal lattice is reduced to a 188 spherical inclusion in a homogeneous medium (centrosymmetric problem) with anisotropic 189 elastic properties, the strain induced by the incorporation of solute is expressed as  $\varepsilon_{ij}^S =$ 190  $\frac{1}{3}\varepsilon_H\delta_{ij} = \frac{\bar{V}_H}{3\Omega_a}\delta_{ij}$ . The partial volume of hydrogen  $\bar{V}_H$  (m<sup>3</sup>/at.) is a measurement of the volume 191 variation induced by hydrogen insertion into the interstitial site. According to experimental 192 data and DFT-based atomistic calculations,  $\bar{V}_H$  for nickel is of the order of  $2.1 \times 10^{-3} \pm 10^{-4}$ 193 nm<sup>3</sup>/at [24, 33, 34]. The first order impact in centrosymmetric case of the elastic field 194 associated with defect is then reduced to:

196 
$$\mu_H = \mu_0 + k_B T ln \left[ \frac{c_H}{1 - c_H} \right] + \sigma_m \overline{V}_H$$
(3)

197

198 with  $\sigma_m$  the hydrostatic stress associated with lattice strain induced by the defect.

199 On the other hand, the evaluation of the self-stress including the hydrostatic strain associated 200 with a variation in the composition  $\Delta C_H$  and a component resulting from stress applied by the 201 crystal lattice on the expansion volume, allows to a chemical potential which takes the 202 following form: 203

204 
$$\mu_H(C_H) = \mu_0 + k_B T ln \left[ \frac{C_H}{1 - C_H} \right] - \frac{Y}{9} \bar{V}_H^2 \Delta C_H$$
 (4)

205

Y is an elastic parameter equal to  $-\frac{2E}{(1-\nu)}$  (E is the Young's modulus, v is the Poisson's ratio) when considering isotropic elasticity and takes a more complex form when considering anisotropic elasticity. The latter case depends on the orientation and the components of the stiffness tensor (see the references [15,19] for more details). Consequently, the "apparent hydrostatic self-stress" can be expressed as:  $\sigma_m = -\frac{Y}{9}\overline{V}_H \Delta C_H$ . This approach can be extended to any other centrosymmetric "defects" (vacancy clusters, spherical precipitate, ...) as  $\Delta \mu_H = \sigma_m \overline{V}_d$  and  $\sigma_m = -\frac{Y}{9} \overline{V}_d \Delta C_d$  with  $C_d$  and  $\overline{V}_d$  are the concentration of these defects and their partial volume, respectively.

Based on continuum approach associated with equations (3) and (4), we can reconsider the set of equations which govern the diffusion and the solubility at stationary state first and secondly their impact on the apparent elastic properties (elastic properties of an equivalent homogeneous medium).

218 219

# 3 - Some orders of hydrostatic stress and their impact on apparent hydrogen solubility

For an open system equilibrated with an external system (hydrogen flux equal to zero) and in the Boltzmann approximation, the elastic model derived from the modification of the chemical potential of hydrogen due to the action of a hydrostatic stress allows to define the ratio of the local solubility of a solute under a hydrostatic stress field ( $C_H$ ) to the solubility of the solute in a stress-free crystal ( $C_0$ ) at the temperature T [14]:

$$228 \qquad \frac{c_H}{c_0} = exp\left[\frac{\sigma_m \overline{V}_H}{k_B T}\right]$$

$$229 \qquad (5)$$

230 At room temperature, the theoretical impact of hydrostatic stress on the apparent solubility ratio is illustrated in figure 1. An increase of one decade of hydrogen solubility can be 231 232 predicted for an hydrostatic stress of 5 GPa. The self-stress contribution on the solubility ratio 233 can be neglected because the self-stress stays lower than 5 MPa for an hydrogen content of 7 234 wppm (experimental related solubility at room temperature and atmospheric pressure, 4.15 x 235 10<sup>-4</sup> H/Ni) which allows to a solubility ratio equal to 1.003. Near a basic crystalline defects, 236 the hydrostatic stress induced is in the GPa order range : on the order of 0.5 GPa for 237 octahedral site near a vacancy [14], 1 GPa for interstitial site close to the edge dislocation 238 core [35] and 30 to 50 GPa for some octahedral site in a grain boundary [17, 64, 65] (refer to 239 publications for the calculation of stresses and their location). In all these cases, these values 240 correspond to a maximum obtained for one site and cannot be directly extended at a long-241 range scale without integrate the concentration of defects or solute insertion sites.

243 A recent work, based on DFT calculations and isotropic models [14], have questioned the 244 implications of the elastic strain of the interstitial sites on the hydrogen solubility near 245 vacancy in nickel. It was highlighted that a compressive hydrostatic stress acting, on the first 246 neighboring sites except the octahedral and tetrahedral sites at a position to the center of a 247 vacancy of respectively 0.3948 nm for octahedral site and 0.3848 nm for tetrahedral site. For 248 both sites a local dilatation  $\delta$  equal to 0.24% and 0.33% was identified and conduces to a 249 solubility ratio equal respectively to 1.4 and 1.6. This last effect stays moderate and can 250 partially compensate by electronic contribution ("chemical contribution") [25]. However, for 251 a larger size centrosymmetric defects (cluster of vacancies or semi-coherent precipitates), as 252 sources of long-range residual stress/strain, the intrinsic properties of the solid can be 253 modified (for the diffusion and the elastic properties see the next section). Specifically, it was related recently by TEM observations that the incorporation of hydrogen in nickel single 254 255 crystal induces the formation of vacancy clusters with a spherical volume of 4.2 nm<sup>3</sup> (with 256 T=300 K, C<sub>H</sub>=7 wppm and C<sub>V</sub>=0.15 x C<sub>H</sub>) [15, 26]. This size corresponds to a cluster of 257 around 1000 vacancies which can induce, with the isotropic approximation, a hydrostatic stress in the order of 1.3 GPa ( $\sigma_m = -\frac{Y}{9}\overline{V}_d \Delta C_d$ ) and consequently an increase of the 258 apparent solubility by a factor of 2.5. 259

260

261 For the precipitates, the excess of solubility is mainly related to the elastic strain 262 accommodation associated to strain incompatibility. This last one results to the difference 263 between interatomic distances associated with the precipitates and the matrix, and it is a 264 function of the degree of coherence  $\delta$  of the precipitate/matrix and the volume fraction  $f_V$  of 265 precipitate. The order of magnitude of the excess of solubility is 6 for M<sub>x</sub>C<sub>y</sub> carbides and 300 266 for TiC precipitates in martensitic steel in agreement with experimental data [20, 36]. For 267 nickel base alloys, our recent experimental work with semi-coherent  $\gamma'$  precipitates in 268 Waspaloy and Inconel 718 alloys relates an apparent solubility ratio which can be reach 3.25 269 and 2.36, respectively [37]. Consequently, a large hydrogen content can be stored with the 270 addition of a semi-coherent precipitates. For the other configurations, the chemical and 271 electrical effect (bond change) is also have contribution on ground-state energy around 272 precipitate (short range interaction) in relation with trapping processes (see as example 273 reference [63]).

274

275 Strain incompatibilities between some microstructural components can be also a source of 276 residual stresses which potentially modify the local solubility of hydrogen. When considering heterogeneous distributions of dislocations, long-range internal stresses can develop and 277 278 induce hydrostatic stresses with an amplitude in the order of 0.2 GPa near dislocations walls 279 which allows to an excess of solubility ratio equal to 1.3 [30,38]. The direct relation between 280 long-range internal stresses and the dislocation density suggests a direct proportionality 281 between the excess of the solubility and the dislocation density. However, the experimental data relate only an increase of the apparent solubility of 8% for quenched and tempered 282 martensitic steels [36] and 4% for a density of  $2.5 \times 10^{14}$  m<sup>-2</sup> for nickel single crystal deformed 283 284 in simple tension along the <100> axis [8]. This result highlights the difficulty to extend a 285 local effect to a global measurement, i.e., the impact of the transition scales which integrates 286 the length scale of the elastic strain (from 100 nm to 1 µm for heterogeneous distribution of 287 dislocations). In the other part, the incompatibility of deformation between grains will also 288 result in substantial hydrostatic stresses (in the order of 0.6 GPa [39]) which can lead to an 289 increase of the local solubility to a factor 1.4.

An inclusion state and/or two phases microstructure can induce large stress concentrations near interfaces following a fabrication process and/or under mechanical loading. For instance, in the case of  $\alpha/\beta$  titanium alloys or duplex austeno-ferritic stainless steels, the hydrostatic pressures can reach 1.6 GPa [40,41], for a nodular cast iron is of the order of 0.8 GPa [42], for hydrides is of the order of 0.6 GPa [40, 43] and for oxides and/or sulphides of Manganese is of the order of 0.2 GPa [44]. Consequently, the solubility ratio in these different situations can be reach a maximum value around 2.3.

To conclude, all "macroscopic defects" or particular geometries (cavity, crack, reduction of section, ...) will be the reason for stress concentration that can lead to hydrostatic pressures of several GPa. These hydrostatic pressures directly affect the partial molar volume of hydrogen of metals and alloys, thus providing a non-negligible elastic energy which can promote hydrogen solubility.

302 303

304 4 - The impact of self-stress and point defect stress on the apparent diffusion coefficient
 305

306 The hydrogen flux and the apparent diffusion coefficient can be derived from chemical 307 potential using first and second Fick's laws. According to equations (3) and (4), the hydrogen 308 diffusion properties result to a chemical potential formalization that includes local 309 concentration and hydrostatic stress arise to self-stress and stress induced by point defects. 310 Based on the thermodynamics of irreversible processes, the phenomenological description of 311 the solute diffusion is described by assuming a linear relationship between the flux and the 312 driving forces, which are the concentration and the stress gradient in this present case. The 313 relationship is expressed by an equation related to the gradient of the chemical potential,  $\nabla \mu$ 314 [45,46]:

315

316 
$$\bar{J} = -\bar{L}.\nabla\mu$$
 with  $\bar{L} = \frac{\bar{D}.C_H}{k_B T}$  (6)

317

318  $\overline{D}$  is the diffusion tensor,  $k_B$  is the Boltzmann constant and T is the temperature. The 319 combination of equations (3) and (6), gives a relationship between the hydrogen flux and the 320 apparent diffusion coefficient for a stress state [15,19]:

321

322 
$$\bar{J} = -\bar{L} \cdot \nabla \mu = \bar{L} \cdot \frac{\partial \mu}{\partial C_H} \nabla C_H = -D \left[ 1 + \frac{Y(\bar{n})}{9} \bar{V}_H^2 \frac{C_H}{k_B T} \right] \nabla C_H = -\bar{D}_{app} \nabla C_H$$
(7)

323

324 Consequently the apparent diffusion coefficient  $D_{app}(\bar{n})$  in the direction  $\bar{n}$  is given as :

325 
$$D_{app}(\bar{n}) = D[1 + \beta C_H]$$
 and  $\beta = \left[\frac{Y(\bar{n})\overline{V}_H^2}{9k_BT}\right]$  (8)

This last equation clearly highlights an explicit effect of the solute concentration to the 326 327 diffusion. Additionally, considering the elastic anisotropy, the variation of  $Y(\bar{n})$  as a function 328 of the crystallographic orientation  $\bar{n} = [hkl]$ , allows a direct impact on the apparent diffusion 329 coefficient [15]. Figure 2a illustrates these both effects in the case of the hydrogen self-stress 330 in nickel single crystal. The order of the self-stress implication stays lower than 0.1 for 35 331 wppm (0.025 for 7 wppm) but highlights clearly the potential implication of the hydrogen 332 concentration and the possibility to obtain an anisotropic diffusion behavior in relation with 333 elastic anisotropy.

Experimental data of this anisotropy was initially reported by Brass *et al.* for two crystallographic orientations (<001> and <110>) [47]. More recently, a significant effect of crystallographic orientation on hydrogen diffusivity was observed by Li *et al* for several

crystallographic orientations: (100), (110), (219) and (111) with a hydrogen concentration of 337 338 7 wppm [15]. According to the theoretical approach hydrogen diffusion is the fastest along 339 the (111) orientation and the slowest along the (100) orientation. As reported by Li *et al.*, the 340 experimental data, the apparent diffusion coefficients could be ranked as follows:  $D_{(111)} >$  $D_{(110)} > D_{(219)} > D_{(100)}$  for a same hydrogen content of 7 wppm [15] ( $D_{<111>} = 17.5 \times 10^{-14} \text{ m}^2/\text{s}$ ,  $D_{<110>} = 11.2 \times 10^{-14} \text{ m}^2/\text{s}$ ,  $D_{<219>} = 9.3 \times 10^{-14} \text{ m}^2/\text{s}$  and  $D_{<100>} = 7.1 \times 10^{-14} \text{ m}^2/\text{s}$ ). The impact of 341 342 343 crystallographic orientation on apparent diffusion coefficient is clearly higher than the one 344 predicted by Eq. 8 ( $\Delta D/D=D<111>/D-1$  for the orientation <111> is equal to 4 with  $D=3.5\times10^{-14}$  m<sup>2</sup>/s [25, 48, 49] instead of the modeling prediction: eq. (8) with a value around 345 346 0.02 for 7 wppm, see figure 2a). Moreover, the impact of the hydrogen content on the 347 apparent diffusion coefficient has been experimentally questioned for the orientation <001> in nickel single crystal [15,19]. A linear relation between D<sub>app</sub> and C<sub>H</sub> is related by the authors 348 349 which allows an experimental value of  $\beta$  equal to 0.29 instead of the one predict by the model 350 equal to 0.01 (eq. 8 and figure 2a). The discrepancy between the model and experimental data 351 motivates to reconsider the origin of the impact of solute content on the apparent diffusion 352 coefficient. Based on the fact that hydrogen content promotes the formation of vacancies and 353 vacancy clusters [15,16,26,33,50], we have recently proposed that D<sub>app</sub> is affected more by the 354 355 elastic stress field induced by vacancy clusters than the solute itself [15].

356 From a thermodynamic point of view, DFT calculations have demonstrated that hydrogen decreases the formation energy of vacancies in nickel [24,51,52]. This result is also supported 357 358 by experimental data reported by Fukai et al. [33,50], Oudriss et al. [16], Li et al. [15] and 359 Hachet et al. [26] obtained in Ni single and poly-crystals. Hydrogen incorporated into nickel 360 matrix induces a quite linear increase in vacancy concentration (C<sub>Vac</sub>=k×C<sub>H</sub>). A lower value 361 of k for polycrystalline nickel (k=0.15) than < 001> oriented nickel single crystal (k=1) 362 indicates a significant contribution of the grain boundary to vacancy concentration. Moreover, 363 recent TEM observations relate the formation of vacancy clusters with an average spherical 364 volume of 4.2 nm<sup>3</sup> for 7 wppm of hydrogen in nickel single crystal [26]. Following these 365 observations, equations (2), (4) and (8) are reconsidered to take into account the elastic stress/strain fields arisen from vacancy clusters. According to Li et al.'s [15], the apparent 366 367 diffusion coefficient is determined as a function of the number of vacancies into a cluster nv and the partial molar volume of vacancy  $\overline{V}_{Vac}$ : 368

370 
$$\overline{D}_{app}(\overline{n}) = D[1 + \beta C_H]$$
 with  $\beta = k \left[ \frac{Y(\overline{n})(n_{Vac}\overline{V}_{Vac})^2}{9k_BT} \right]$  (9)

371

As illustrated in figure 2b, the impact of a cluster of vacancies on D<sub>app</sub> is more significant than 372 373 the solute itself and reproduce our experimental data (hydrogen diffusion anisotropy and 374 diffusion dependence on solute content) for a cluster of 40 vacancies and a partial molar volume of vacancy  $\bar{v}_{vac}$  equal to 2.25×10<sup>-6</sup> m<sup>3</sup>/mol [15,24]. If we obtain a same order for the 375 different physical parameters for the continuum thermodynamic model and the experiment, 376 377 this approach remains limited because we do not consider self-interstitial and we have 378 assumed that elastic coefficients are constant and that solute content doesn't modify the 379 electronic contributions to the energy of the system.

To bypass this difficulty and separate chemical and mechanical contributions, we have recently computed the components of the elasto-diffusion tensor  $d_{ijkl}$  [53] from first principles calculations of the elastic dipole tensors  $P_{ij}$  of hydrogen in the interstitial sites of perfect lattice nickel and at the saddle point along the migration path [54]. We have considered vacancies and vacancy clusters, but also the solute itself and self-interstitial, as sources of 385 residual strain in the solid. This last work allows to formalize the impact of stress/strain field 386 of any centrosymmetric defects on the hydrogen diffusion.

387 388

#### **389 5** - Some contributions of self-stress on the hydrogen segregation at grain-boundaries

390 The contribution of self-stress on hydrogen diffusion and segregation processes on non-391 defective lattice has been discussed in the previous sections. More recently, the question of 392 stress/strain energy contribution on the segregation energy of hydrogen on the defective 393 lattice is an interesting challenge [17-19,55]. The grain boundaries offer the opportunity to 394 have a large variety of situations associated with the local distortion of lattice. Following this 395 approach, we have studied grain boundaries differentiated by their energy and excess volume 396 [17-19,29] to explore the diversity of GBs in nickel reported by Olsmted et al. [56]. Atomistic 397 simulations based on the energy minimization method were performed using the LAMMPS 398 code to compute the structural configurations of GBs and segregation energy of hydrogen 399 [17-19]. Based on the fact that the insertion of an atom in lattice site creates a hydrostatic 400 dilatation (hydrostatic strain) and a distortion of the volume (deviatoric strain), we have 401 managed the evaluation of both at atomistic scale. The calculation of the elastic dipole tensor  $P_{ij}$  according to defect force method [17, 27, 62] and the hydrogen atomic volume  $V_H$  at the 402 segregation site in different GBs offer the opportunity to question the impact of elastic energy 403 associated with hydrogen insertion on adsorption energy (or insertion energy)  $E_{H}^{Ins}$  and 404 segregation energy  $E_{H}^{Seg}$ . Thus, the atomic stress  $\sigma_{ii}$  and the elastic strain energy  $E_{el}$  by unit 405 volume induced from the insertion of the hydrogen interstitial are related to the lattice-defect 406 407 elastic tensor [17]:

408

409 
$$\sigma_{ij} = \frac{P_{ij}}{V_H} = \sigma_m \delta_{ij} + \sigma_{ij}^d \text{ and } E_{el} = E_{el}^d + E_{el}^m = \frac{1}{2B} (\sigma_m)^2 + \frac{1}{2G} (\sigma_d)^2$$
 (10)

410

411 where  $\sigma_m$  and  $\sigma_d$  are respectively the hydrostatic stress and the deviatoric stress defined as 412 Von Mises equivalent stress. B and G are the bulk and shear modulus respectively.  $E_{el}^m$  and 413  $E_{el}^d$  represent the dilatational and distortion energies. The insertion energy (or the adsorption 414 energy) of a hydrogen atom in the nickel lattice  $E_H^{Ins}$  and the segregation energy relative to 415 the octahedral site  $E_H^{Seg}$  are given by:

416

417 
$$E_{H}^{Ins} = E_{Ni+H}^{Tot} - E_{Ni}^{Tot} - \frac{1}{2}E_{H_{2}}$$
 and  $E_{H}^{Seg} = (E_{GB+H}^{Tot} - E_{GB}^{Tot}) - (E_{Ni+H}^{Oct} - E_{Ni}^{Tot})$ 

418 (11) 419

where  $E_{Ni+H}^{Tot}$  is the total energy of nickel lattice with a hydrogen atom,  $E_{Ni}^{Tot}$  is the total 420 energy of nickel lattice without hydrogen atom and  $E_{H_2}$  is the chemical potential of the 421 molecular hydrogen.  $E_{GB+H}^{Tot}$  is the total energy of GB with a hydrogen atom,  $E_{GB}^{Tot}$  is the total energy of GB and  $E_{Ni+H}^{Oct}$  is the total energy of the nickel lattice with a hydrogen atom at the 422 423 octahedral site.  $E_H^{Ins}$  expresses the local modification of energy instead of  $E_H^{Seg}$  which relates 424 the global evolution of the energy of the GB. The evolution of the hydrogen energy  $E_H^{Ins}$  as a 425 function of the strain energy  $E_{el}$  from the insertion of a hydrogen atom is illustrated in figure 426 3a. Two distinct linear regimes are observed with a transition around a strain energy density 427 428 about 2 GPa. The total strain energy is dominated by the hydrostatic stress for the first linear regime  $(E_H^{Ins} > -0.5 \text{ eV} \text{ and } V_H < 6.6 \text{ Å}^3)$  while the other linear regime  $(E_H^{Ins} < -0.5 \text{ eV} \text{ and } V_H > 6.6 \text{ Å}^3)$  is due to the contribution of the deviatoric stress. The hydrostatic stress is 429 430

significant for a low volume ( $V_{\rm H} < 6.6 \text{ Å}^3$ ) such as an octahedral site in perfect fcc lattice. At 431 these cubic form or similar sites, the deviatoric stress is low due to the small distortion. 432 433 However, for high volume sites, the hydrostatic stress decreases and, at the same time, the 434 distortion component of the stress is more significant than the hydrostatic volume change [17]. We examine now the correlation between the segregation energy  $E_H^{Seg}$  and the strain energy  $E_{H_2}$  from the insertion of a hydrogen atom (figure 3b). For the first regime defined 435 436 previously (predominance of hydrostatic strain energy and low volume  $V_{\rm H}$  ), a linear relation 437 is obtained which clearly highlights the impact of hydrostatic stress on segregation process in 438 accordance with previous works [17,55]. However, for the second regime ( $E_{el} < 2$  GPa,  $V_{\rm H} >$ 439  $6.6 \text{ Å}^3$ ), we observe some dispersion in our data. This last result illustrates a possible impact 440 of the long range elastic contribution as it has been recently demonstrated [18,19]. Future 441 442 prospects on the subject certainly will highlight the importance to distinguish the contribution 443 of the short and from the long range strain field on solute segregation. Recently, the hydrogen 444 concentration profile maps were obtained from TOF-SIMS measurements [21]. This work 445 highlights for some specific grain-boundaries that a local distortion around GB impacts the 446 hydrogen segregation and consequently supports the idea that long range strain field can be 447 significant on this process.

448 449

## 450 6 - Self-stress and point defect stress impact on the elastic properties451

452 The hydrogen-enhanced localized plasticity (HELP) model is the one of the most significant 453 interpretation of slip localization in the hydrogen embrittlement context [57-59]. The model is 454 based on the reduction of the energy barrier to dislocation motion through an elastic shielding 455 effect induced by hydrogen or any other point defects [57,26]. According to the modification 456 of the elastic properties of the matrix, this screening effect has been introduced into the 457 classical results obtained with the elastic theory of dislocations on the base of a dimensionless 458 "screening coefficient" of the pair interactions [58,59]. Despite the fact that this fundamental 459 approach allows to partially explain some experimental observations [60], a clarification on 460 the influence of hydrogen on the elastic properties has been only proposed recently [26]. A 461 decrease of the Young's modulus of the <001> oriented nickel single crystal with hydrogen 462 concentration has been reported [26]. Additionally, a linear relationship between  $E_{<001>}$  and C<sub>H</sub> is observed:  $E_{<001>}(C_H)/E_{<001>}(0)=1-A\times C_H$  with a slope A equal to 0.036 [26]. By using 463 the equation of the chemical potential (eq. 3), the diffusion equation of hydrogen and the 464 hypothesis of a hydrogen distribution in equilibrium with the local stress gradients, we can 465 466 express the elastic strain due to the incorporation of hydrogen or centrosymmetric defect as 467 follows [57,58, 26]:

468

469 
$$\varepsilon_{ij} = S_{ijkl}^* = \left[S_{ijkl} + \frac{c_d \overline{v}_d^2}{9k_B T}\right] \sigma_{ij} \text{ and } \frac{E_{<001>}^*}{E_{<001>}} = \frac{S_{1111}}{S_{1111}^*} = \frac{1}{1 + \left[\frac{c_d v_d^2}{9k_B T}\right] E_{<001>}}$$
 (12)

470

471 On the concentration range considered of this present work, the last equation can be reduced472 as :

473

$$474 \quad \frac{E_{<001>}^*}{E_{<001>}} = 1 - \left[\frac{E_{<001>}\overline{V}_d^2}{9k_BT}\right]C_d \tag{13}$$

$$475$$

476 Considering only the potential impact of the hydrogen, the vacancies and the cluster of 477 vacancies in the present discussion, we rewrite this equation to include the relation between

- 478 vacancies concentration and hydrogen content ( $C_{Vac}=k\times C_H$ ) and the definition of  $C_d$  and  $V_d$ 479 for the vacancy clusters assuming an additive contribution of monovacancies in an isotropic 480 spherical cluster ( $C_d=C_{Vac}/n_{Vac}$  and  $\bar{V}_d = n_{Vac}\times\bar{V}_{Vac}$ ) introduced by Hachet *et al.* [26] :
- 481

$$482 \quad \frac{E_{<001>}^*}{E_{<001>}} = 1 - \left[\frac{kE_{<001>}n_{Vac}\overline{V}_{Vac}^2}{9k_BT}\right]C_H \tag{14}$$

484 Thus, the experimental slope A can be questioned with theoretical approach for which A is equal to  $\frac{E_{<001>}\overline{V}_{H}^{2}}{9k_{B}T}$  and  $\frac{kE_{<001>}n_{Vac}\overline{V}_{Vac}^{2}}{9k_{B}T}$  for hydrogen and vacancy clusters, respectively. This 485 analytical model has been improved in figure 4a for different situations. The slope A is 486 487 respectively equal to 0.015% for the incorporation of hydrogen, 0.04% for vacancies and 488 0.036 for a cluster of vacancies with 100 vacancies. This last situation is in agreement with 489 experimental observations with a slope of 0.036 (blue dot in figure 4a). Our DFT calculations 490 support the low values obtained for hydrogen and vacancy cases [26]. The size of the vacancy 491 clusters stays lower than the one observed by TEM [26]. Despite this fact, the prediction of 492 the analytical model supports the idea that elastic shielding is more dependent of the 493 superabundant vacancies than of a direct effect of the solute. The clustering of vacancies and 494 the formation of self-interstitials in the conditions previously described are unknown and need 495 further investigation.

496 Recently, we have explored the consequence of the modification of the elastic properties with 497 the addition of hydrogen on edge dislocation dipoles of dislocations (elementary 498 configuration of PSB) using molecular simulation within EAM potential [30,61]. This 499 configuration is fundamental to explain the formation and equilibrium of dislocation pattern 500 obtained under cyclic loading (dipolar walls, persistent slip band, ...). We incorporate 501 successively different hydrogen content, vacancies and cluster of vacancies in the elastic 502 fields of each edge dislocations (in a Cottrell's atmosphere defined for a hydrostatic pressure 503 *P* larger or equal to 10 GPa), then we evaluated the critical passing stress for different dipole 504 configurations. In two last situations, we consider that defects do not trap hydrogen.

505 The contribution of hydrogen and defects on the solid solution strengthening is discussed with 506 the Labusch's theory describing the strengthening due to concentrated, weak obstacles and 507 diluted, strong obstacles distributions. The figure 4b relates the evolution of the increase shear stress due to hydrogen and defects. The insertion of hydrogen to create Cottrell atmosphere 508 509 leads to an increase of the critical passing stress need to break an edge dislocation dipole in 510 accordance with the Labusch's theory. In opposite, the presence of vacancies and vacancy 511 clusters reduces the effect of the solute alone and supports a softening of process. This new 512 result offers the opportunity to revisit the impact of hydrogen on cyclic behavior and it is nice 513 illustration of shielding process induces by point defects [30, 61].

- 514
- 515
- 516

### 517 **Conclusions et prospects**

518

519 A fundamental aspect to elucidate the mechanisms of HE is based on a good knowledge of the 520 interactions between the solute and different defects of the metal. With a review of our recent works, we highlight the importance of the elastic energy associated with the solute and the 521 522 defects to explain some processes implicated on HE. The confrontation of experiment and 523 modelling approaches at different scales offers the opportunity to clearly demonstrate a large 524 contribution of elastic field on the hydrogen solubility, diffusion, segregation and on the 525 modifications of the elastic properties. Moreover, we illustrate that deviatoric stress 526 contribution cannot be neglected in some case in opposite to a common consideration in the 527 literature. The possible contribution of chemical component and the separation of this one to 528 other contributions of the energy stays an interesting challenge.

529

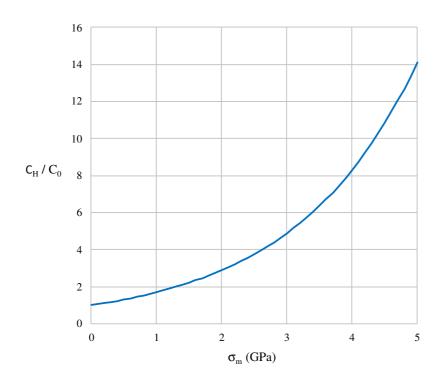
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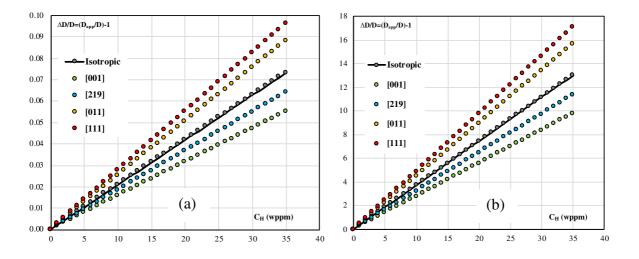
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**Figure 1** : Evolution of normalized hydrogen content with the hydrostatic stress at T=300K according to Eq. 5.



**Figure 2** : Relative variation of the diffusion coefficient with the hydrogen content for different crystallographic orientations: solute impact (a) and vacancy clusters (b) [19].

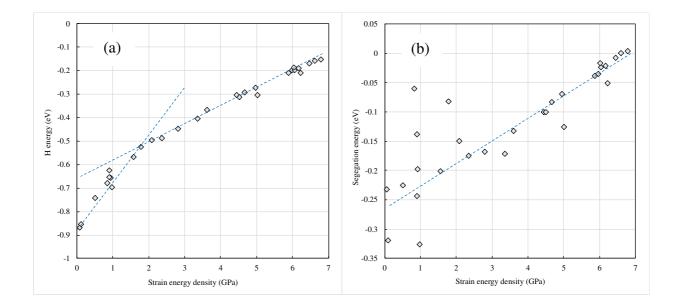


Figure 3 : Hydrogen atom energy (a) and segregation energy (b) as a function of strain energy density in the case of grain boundary in Ni [18,19].

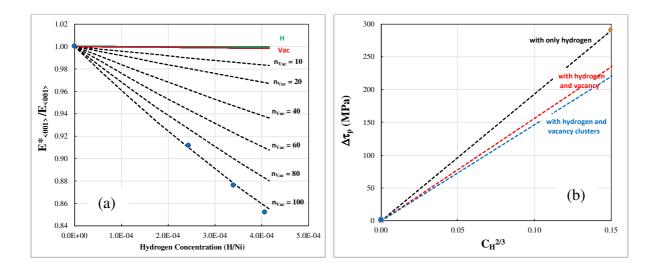


Figure 4 : Decrease of the Ni Young modulus with hydrogen content (blue dotes correspond to experimental data) (a) [26]. Increase of the shear stress due to hydrogen content without and with the addition of vacancies and vacancy clusters (b) [30,61].