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# Strain-Enhanced Charge-to-Spin Conversion in Ta/Fe/Pt Multilayers Grown on Flexible Mica Substrate

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Recent demonstration of magnetization manipulation has been focused on the utilization of pure spin current converted by charge current in nonmagnetic materials with strong spin-orbit coupling (SOC), which stimulates intensive studies on the exploration of materials with larger SOC, such as heavy metals and topological insulators. We suggest an alternative approach for enhancing the effective charge-to-spin conversion efficiency by applying strain in Ta/Fe/Pt films grown on flexible mica substrates. We experimentally demonstrate a large and tunable charge-to-spin conversion efficiency in Ta/Fe/Pt films by applying compressive strain within a flexible substrate, and over 50% enhancement of effective spin Hall angle  $\Theta_{\text{SHE}}^{\text{eff}}$  of up to approximately 0.2 is achieved in a 6.26‰ strained film. Our findings may spur further work on the integration of flexible electronics and SOC and may potentially lead to the innovation of alternative flexible spintronics devices.

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## I. INTRODUCTION

The integration of an electronic system with a flexible substrate has received considerable attention due to the appealing applications in alternative devices such as flexible display, electronic skin, and wearable devices [1–5]. The fantastic property of such flexible electronics also triggers numerous research efforts in the spintronics field on the flexible strain effects of spin-dependent phenomena such as exchange bias [6,7], interlayer coupling [8], and perpendicular magnetic anisotropy (PMA) [9]. In recent years, the focus of modern spintronics has been shifted to the generation and manipulation of pure spin currents through spin-orbit coupling (SOC) in nonmagnetic systems [10–12], the studies of which even give birth to an emerging field, that is, spin orbitronics [13]. However, the integration of pure spin currents in flexible electronics remains largely unexplored.

As a flow of angular momentum that does not accompany a charge flow, pure spin currents carry information with minimum power dissipation [14]. More importantly, similar to spin-polarized current, pure spin

currents are capable of manipulating the magnetization of ferromagnetic elements, showing promising application perspectives in alternative information recording and data processing devices such as spin orbital torque magnetic random access memory (SOT MRAM) [15] and spin Hall nano-oscillators [16]. In a ferromagnetic-nonmagnetic (FM/NM) bilayer system, pure spin currents can be converted by charge current flowing through NM with strong spin orbit coupling (spin Hall effect), then propagate into the adjacent FM, thereby affecting the magnetic fluctuation, magnetization dynamics, and even magnetization switching [17–19]. In consideration of the FM-NM interface spin loss during the injection of spin currents, the effective charge-to-spin conversion is quantified by the effective spin Hall angle  $\Theta_{\text{SHE}}^{\text{eff}}$  [20, 21]. As such, optimizing the effective spin Hall angle  $\Theta_{\text{SHE}}^{\text{eff}}$  for specific applications is of immense importance and has been achieved by various strategies, including exploring NM with large spin orbital coupling such as heavy metals [18,20,22,23], topological insulators [19,24] and more recently, the antiferromagnetic material [25, 26], engineering the FM-NM interface for greater spin transparency [27], or reducing interfacial spin memory loss [20]. Here, we report the observation of a large and tunable  $\Theta_{\text{SHE}}^{\text{eff}}$  in mica//Ta/Fe/Pt by applying mechanical strain in a flexible mica substrate during film deposition.

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## II. EXPERIMENTAL PROCEDURES

### A. Film deposition

A series of Ta(4 nm)/Fe (4 nm)/Pt(5 nm) multilayers are deposited on flexible mica substrates, with the 4-nm Ta employed as a buffer layer to reduce the roughness of the flexible substrates. Before the deposition, the substrates are cleaned with ethyl alcohol in an ultrasonic cleaner for 10 min and then dried with nitrogen gas. During the deposition, the substrates are bent and fixed on a homemade convex aluminum alloy mold, as shown in Fig. 1(a). Thus, a longitudinal compressive strain is induced in the films when flattening the substrate after the deposition and the strain direction is shown in Fig. 1(b). By changing the curvature radii of the mold, Ta/Fe/Pt multilayers with compressive strain  $\varepsilon$  of 0 to approximately 6.26% are obtained. The magnitude of such induced strains is estimated by  $\varepsilon = T/2R$ , where  $R$  is the curvature radii of the mold and  $T$  is the total thickness including both the substrate and multilayers [28].

### B. Device fabrication

The microstrips for measurements are patterned with the long axis parallel to the strain directions by standard UV lithography and have lateral sizes of  $20 \times 90 \mu\text{m}^2$ . Ti/Au electrodes are deposited on the edge of the microstrip by the lift-off technique to form a ground-signal-ground (GSG) contact that guides the radio frequency (rf) current into the sample. We also prepare a control sample with the long axis perpendicular to the strain direction for the multilayer with a compressive strain of 6.26%.

## III. RESULTS AND DISCUSSION

### A. ST FMR measurements

Spin-torque ferromagnetic resonance (ST FMR), [also referred to as spin-orbit ferromagnetic resonance, that is, SO FMR] [22,29] measurements are performed to evaluate the efficiency of charge-to-spin conversion for all the microstrip devices, and the schematic of the measurement setup is illustrated in Fig. 1(c). A rf charge current  $J_c$  with a power of 10 dBm is injected into the microstrip in the presence of an external field  $H$  that is applied in plane at  $45^\circ$  with respect to the microstrip, as shown in Fig. 1(d). Note that for all the measurements, the rf current is flowing along the long axis of the microstrip devices with a frequency ranging from 5–20 GHz. A transverse spin current is then converted by the rf current in Pt due to the spin Hall effect, which manipulates the magnetization precession of Fe by exerting two orthogonal torques, namely, a dampinglike torque ( $\tau_D$ ) and a fieldlike torque ( $\tau_F$ ). Owing to the anisotropic magnetoresistance (AMR) effect, the oscillating magnetization gives rise to a time-dependent resistivity, which mixes with the rf current and results in a rectified dc voltage.

Figure 2(a) shows the dc voltage signal for a Ta/Fe/Pt device with compressive strain of 6.26%, measured by spin-torque ferromagnetic resonance under a configuration of  $J_c \parallel \varepsilon$ . It is notable that the resonance field shifts toward higher fields as the rf current frequency increases, which is consistent with the Kittel model [30]. Here, the measured dc voltages are a mixture of a symmetric Lorentzian component  $V_{\text{sym}}$  due to the dampinglike torque and an antisymmetric one  $V_{\text{anti}}$  arising from the fieldlike torque,

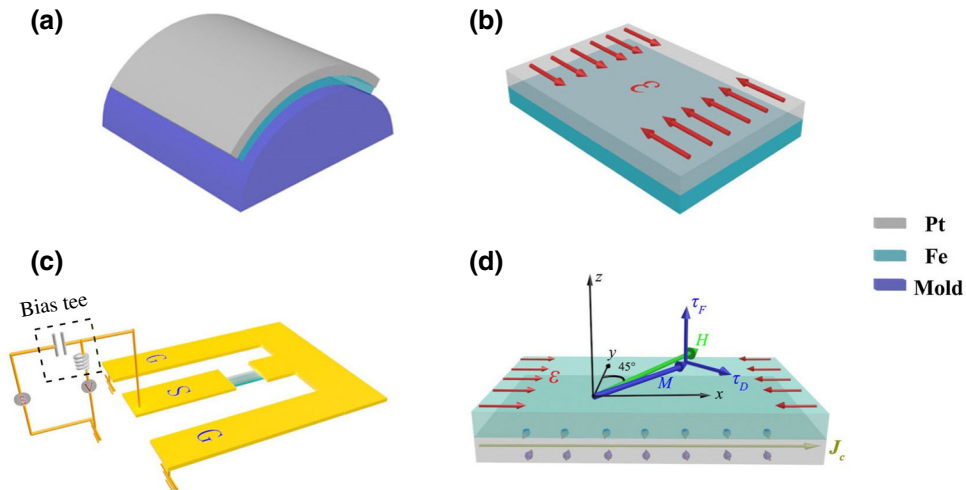


FIG. 1. (a),(b) Schematic illustration of the strain application process. The fix of mica on a convex aluminum alloy mold during the film deposition and the flattening afterward induced a compressive strain  $\varepsilon$  in the films with direction shown in (b). (c) Schematic representation of the ST FMR experimental setup. (d) Sketch of the ST FMR experimental configuration showing the spin-transfer torques  $\tau_F$  and  $\tau_D$ , magnetization  $M$ , and external field  $H$ . Here, the charge current  $J_c$  is parallel to the strain  $\varepsilon$  direction.

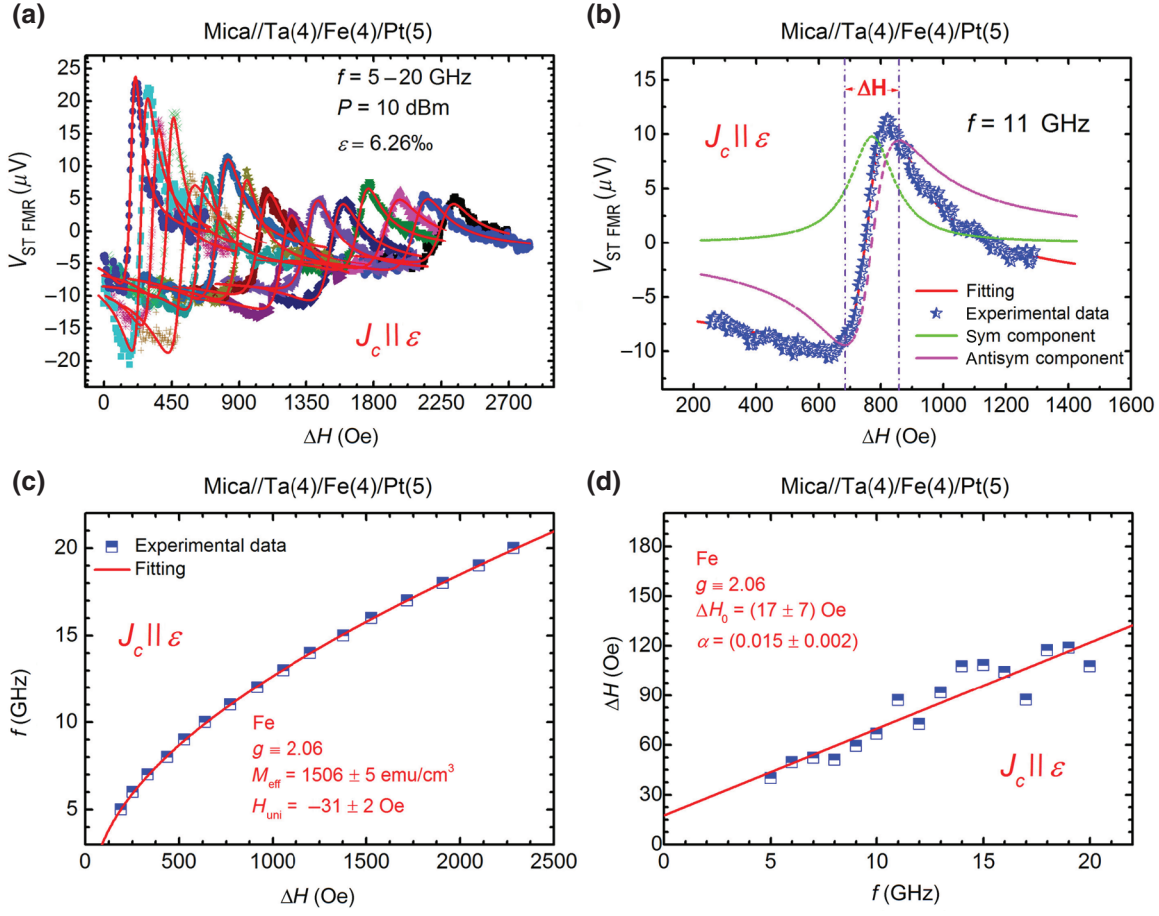


FIG. 2. ST FMR data for the 6.26‰ strained film. (a) The measured ST FMR signals at different frequencies, the red lines are the fittings according to Eq. (1). (b) Single ST FMR spectrum measured at 11 GHz. The red solid line represents the fit to the Lorentzian function. The green and purple dash-dotted lines represent symmetric and antisymmetric voltage components, respectively. (c) The fitting of frequency dependence of the resonance field from which we can obtain the value of  $M_{eff}$ . (d) Effective damping determination from the fitting of frequency dependence of the line width.

in a first approximation for the level of thicknesses in our samples [22,31,32]. We extract the symmetric and antisymmetric voltage contributions by fitting the spin-torque ferromagnetic resonance spectra with the following equation, also considering an off-set  $V_{off}$  [32]

$$V_{dc} = V_{off} + V_{sym} \frac{\Delta H^2}{\Delta H^2 + (H - H_{res})^2} + V_{anti} \frac{(H - H_{res})\Delta H}{\Delta H^2 + (H - H_{res})^2}, \quad (1)$$

where  $H$ ,  $H_{res}$ , and  $\Delta H$  are the applied field, the resonance field, and the resonance line width, respectively. Figure 2(a) shows the fitting result and Fig. 2(b) shows the fitting detail of a ST FMR spectrum measured at a frequency of 11 GHz. Both agree well with the experimental data. We extract the resonance fields and plot them against the resonance frequency  $f_{res}$  in Fig. 2(c), in which the resonance field dependence of the frequency can be well fitted

by the Kittel formula

$$f_{res} = \frac{\gamma}{2\pi} [(H_{res} + H_{uni})(H_{res} + 4\pi M_{eff} + H_{uni})]^{1/2}, \quad (2)$$

where  $\gamma$  and  $H_{uni}$  are the gyromagnetic ratio and the in-plane uniaxial magnetic anisotropy field, respectively.  $4\pi M_{eff} = 4\pi M_s - H_k$  is the effective magnetization,  $M_s$  is the saturation magnetization, and  $H_k$  is the perpendicular anisotropy field. The value of  $M_{eff}$  for all the samples is obtained from the fitting and the strain dependence of  $M_{eff}$  and is shown in Fig. 2(c). It is notable that  $M_{eff}$  slightly increases with the increasing of strain regardless of the strain direction, which probably stems from the increase of  $H_k$  due to an out-of-plane stretch of the lattice by the in-plane compressive strain.

## B. Strain dependence of magnetic damping

The ST FMR measurements also allow us to evaluate the effective magnetic damping  $\alpha$  by fitting the

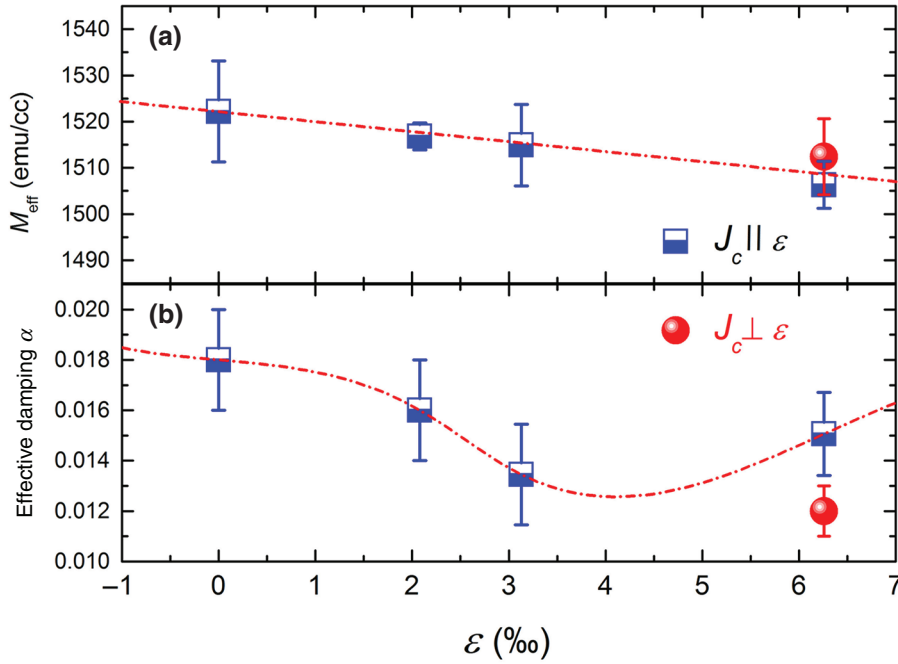


FIG. 3. Strain dependence of  $M_{\text{eff}}$  (a) and effective damping (b). The dash-dotted lines represent a guide to the eyes. The red circle data point corresponds to the control device where  $J_c$  is perpendicular to  $\epsilon$ . We can observe in (a) that  $M_{\text{eff}}$  is the same in both devices for the higher  $\epsilon$  we have measured. This is an indication that the Fe layer is isotropic in the film plane. We can observe in (b) that the total damping when  $J_c$  is perpendicular to  $\epsilon$  is lower than the one with  $J_c \parallel \epsilon$ . This is an indication of a more efficient spin pumping contribution when  $J_c \parallel \epsilon$ .

frequency dependence of the resonance line width with equation  $\Delta H = \Delta H_0 + 2\pi f \alpha / \gamma$ , where  $\Delta H_0$  is the frequency independent contribution due to the inhomogeneity of the films. A fitting example is shown in Fig. 2(d) and a linear dependence can be observed. Figure 3(b) shows the strain dependence of  $\alpha$ . It is interesting to find that rather than the monotonous behavior of  $M_{\text{eff}}$ ,  $\alpha$  depends on the strain direction and it decreases first then increases with the increasing of strain for a  $J_c \parallel \epsilon$  configuration. We will explain this anomalous behavior in the discussion of  $\Theta_{\text{SHE}}^{\text{eff}}$  below.

### C. Strain-enhanced charge-to-spin conversion

The spin Hall angle  $\Theta_{\text{SHE}}^{\text{eff}}$  is the ratio of spin current density  $J_s$  to the rf current density  $J_c$ , which in the simplest model is proportional to the ratio of the symmetric voltage component over the antisymmetric one  $V_{\text{symm}}/V_{\text{anti}}$ . When the resonance field is larger than the saturation field ( $H_{\text{res}} > H_{\text{sat}}$ ), the precession of magnetization is considered to be uniform, as such  $\Theta_{\text{SHE}}^{\text{eff}}$  can be obtained by the following equation [11,22,31,32]

$$\Theta_{\text{SHE}}^{\text{eff}} = \frac{J_s}{J_c} \cong \frac{V_{\text{symm}}}{V_{\text{anti}}} \frac{e\mu_0 M_s t_{\text{Fe}} t_{\text{Pt}}}{\hbar} \left[ 1 + \frac{4\pi M_{\text{eff}}}{H_{\text{res}}} \right]^{1/2} \times \frac{1}{1 + (H_F/H_{\text{Oe}})}, \quad (3)$$

where  $\mu_0$  is the permeability in vacuum and  $t_{\text{Fe}}$  and  $t_{\text{Pt}}$  are the thicknesses of the Fe and Pt layers, respectively. The last factor in Eq. (3) takes into account a possible contribution  $H_F$  due to fieldlike spin orbit torque and  $H_{\text{Oe}}$  is the Oersted field arising from the rf current. Here, we

ignore the contribution of the Oersted field from the Ta layer due to the small current density in Ta, considering the much larger resistivity in Ta ( $200 \mu\text{W cm}$ ) than that in Pt ( $24 \mu\text{W cm}$ ). We have estimated the value of the Oersted field ( $H_{\text{Oe}} \sim 1.5 \text{ Oe}$ ) and the field due to the fieldlike spin orbit torque ( $H_F \sim 0.15 \text{ Oe}$ ) in our samples according to the method given by Refs. [31] and [33]. Thus, we can neglect the factor  $H_F/H_{\text{Oe}}$  in Eq. (3). Figure 4(a) shows the effective spin Hall angles  $\Theta_{\text{SHE}}^{\text{eff}}$  for Pt in the Ta/Fe/Pt system without and with a strain of 6.26% at varying  $J_c$  frequencies from 6 to 20 GHz, from which a significant increase of  $\Theta_{\text{SHE}}^{\text{eff}}$  by strain is noted. To further confirm the strain effect on  $\Theta_{\text{SHE}}^{\text{eff}}$ , we also show the  $\Theta_{\text{SHE}}^{\text{eff}}$  comparison derived from the ST FMR measurements with  $J_c$  flowing along and perpendicular to the strain direction in Fig. 4(b). It is worth noting that in both cases, Figs. 4(a) and 4(b), the value of  $\Theta_{\text{SHE}}^{\text{eff}}$  is increased when  $J_c \parallel \epsilon$  and when the magnitude of  $\epsilon$  increases. The strain dependence of  $\Theta_{\text{SHE}}^{\text{eff}}$  is shown in Fig. 4(c), indicating the increase of  $\Theta_{\text{SHE}}^{\text{eff}}$  from  $0.12 \pm 0.02$  to  $0.20 \pm 0.02$  by the increase of strain when  $J_c \parallel \epsilon$ . On the contrary,  $\Theta_{\text{SHE}}^{\text{eff}}$  is almost constant ( $\Theta_{\text{SHE}}^{\text{eff}} = 0.12 \pm 0.02$  and  $0.11 \pm 0.02$  for  $J_c \perp \epsilon$  and  $\epsilon = 0$ , respectively) when  $J_c$  is not flowing along strain direction. It should be mentioned that the measured  $\Theta_{\text{SHE}}^{\text{eff}}$  is larger compared to that reported previously (around 0.05) [20,22,32], and we ascribe this to the presence of the Ta buffer layer, which has a negative spin Hall angle [17,18] thereby also contributing to the spin current density  $J_s$ . Even if we do not consider the thickness of Ta, the calculated “effective” value involves the contribution of Ta. Thus, it explains the large value, approximately 0.12, we obtain in our devices without any strain. Similar enhancements of effective values in trilayers have also

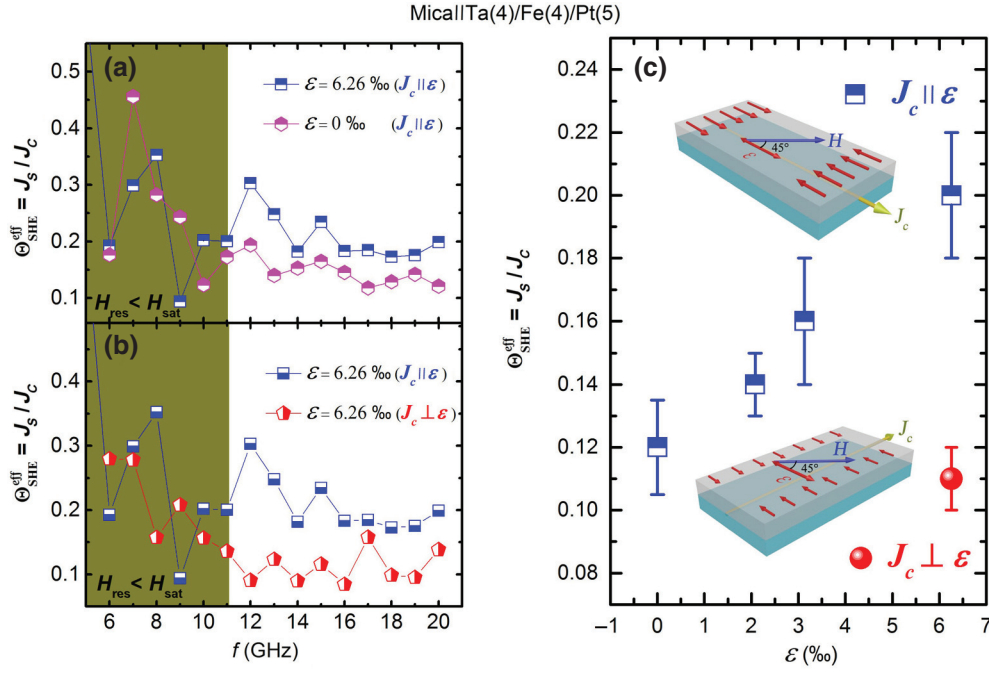


FIG. 4. (a),(b) Determination of the effective spin Hall angle according to Eq. (3), which is reliable only when  $H_{\text{res}} > H_{\text{sat}}$  [32]. (c) Strain dependence of the effective spin Hall angle.

been observed in W/(Co, Fe)B/Pt [31] and Pt/Co/Ta [34] systems.

The strain dependence of  $\Theta_{\text{SHE}}^{\text{eff}}$  can also be verified by the anomalous behavior of effective damping  $\alpha$  as we mentioned in Fig. 3(b). Here, we consider two damping mechanisms contributing to the effective damping  $\alpha$ : one is the intrinsic damping of magnetic layer, which decreases with increasing compressive strain, as reported previously [6]. The other is an additional damping due to spin pumping into the heavy metal, Pt and Ta, layers. Note, however, that the enhancement of damping due to the Ta layer is much smaller than that of Pt [18]. Thus, the clear increase of  $\Theta_{\text{SHE}}^{\text{eff}}$  suggests more efficient spin pumping into the heavy metal (HM) layers, thus a larger  $\alpha$  for the Fe layer, which agrees with the damping measurements for the two devices with a compressive strain of 6.26%. Despite the different rf current orientation, the Fe layers in both devices undergo the same magnitude of strain (6.26%) and magnetic field configuration ( $H$  is applied  $45^\circ$  in plane to the strain direction), thus the intrinsic damping of Fe is identical. Consequently, the effective damping is mainly determined by the additional damping due to spin pumping. In contrast, for the devices with different strain,  $\alpha$  decreases first then increases with the increase of strain. This can be explained by the competition of strain effect on the intrinsic damping of Fe and the enhancement of spin pumping due to the larger  $\Theta_{\text{SHE}}^{\text{eff}}$ .

Finally, we discuss the possible mechanism accounting for the observed strain-dependent  $\Theta_{\text{SHE}}^{\text{eff}}$ . It is well known that a magnetoelastic anisotropy will be induced due to strain in the magnetic layer, and in our case, the easy axis of the magnetoelastic anisotropy is in-plane perpendicular

to the compressive strain direction [6,28]. However, the observed strain-dependent  $\Theta_{\text{SHE}}^{\text{eff}}$  is unlikely due to the strain-induced anisotropy, since different  $\Theta_{\text{SHE}}^{\text{eff}}$  are still obtained in the 6.26% strained devices in which the same orientation ( $45^\circ$ ) between the magnetic field and strain direction is given. We note that the variation of  $4\pi M_{\text{eff}}/H_{\text{res}}$  [factor in Eq. (3)] due to strain is less than 1%, thus it cannot account for the 50% variation of the effective spin Hall angle. Moreover, magnetic anisotropy independent  $\Theta_{\text{SHE}}^{\text{eff}}$  is also observed in epitaxial Fe/Pt [32] and an exchange-biased NiFe/IrMn system [35]. The increase of SOC in Pt(Ta) is another reason to be ruled out since SOC is dominated by the atomic number of Pt(Ta), which cannot be changed by the strain. A possibility for the strain-dependent  $\Theta_{\text{SHE}}^{\text{eff}}$  is the decrease of spin-current dissipation at the interface due to the flexible substrate-induced strain, which may improve the interfacial disorder. More detailed theoretical and experimental investigations are needed to explore the exact microscopic mechanism of the enhanced  $\Theta_{\text{SHE}}^{\text{eff}}$  given the complex nature of the system.

#### IV. CONCLUSION

With the ST FMR technique, we show a large and tunable charge-to-spin conversion efficiency in compressive strained Ta/Fe/Pt films grown on flexible mica substrates, and the effective spin Hall angle  $\Theta_{\text{SHE}}^{\text{eff}}$  is significantly enhanced over 50% from  $0.12 \pm 0.02$  to  $0.20 \pm 0.02$  by the flexible substrate-induced strain of 6.26%. The demonstrated strong strain dependence of charge-to-spin conversion efficiency paves an alternative way for the manipulation of spin current, and we anticipate the results can be

used for the application of alternative spin memory or logic devices as well as the development of flexible electronics.

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