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# Flow around an oscillating grid in water and shear-thinning polymer solution at low Reynolds number

Tom Lacassagne · Adrien Lyon · Serge Simoëns · Mahmoud EL Hajem ·  
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**Abstract** The study of turbulence in complex fluids is of great interest in many environmental and industrial applications, in which the interactions between liquid phase rheology, turbulence, and other phenomena such as mixing or heat and mass transfer have to be understood. Oscillating grid stirred tanks have been used for many purposes in research involving turbulence. However the mechanisms of turbulence production by the oscillating grid itself have never been studied, and oscillating grid turbulence (OGT) remained undescribed in non-Newtonian, shear-thinning, dilute polymer solutions until recently (?). The aim of this paper is to study the influence of the shear thinning property of dilute polymer solutions (DPS), such as Xanthan Gum (XG), on mean flow, oscillatory flows, and turbulence around an oscillating grid. Liquid phase velocity is measured by Particle Image Velocimetry (PIV) in a vertical plane above the central grid bar. Mean, oscillatory and turbulent components of the velocity fields are deduced by triple Hussain-Reynolds decomposition based on grid phase-resolved measurements. Outside of the grid swept region, the amplitude of oscillatory fluctuations quickly become negligible compared to that of turbulent fluctuations, and the triple and classical Reynolds decomposition become equivalent. Oscillatory jets and wakes behind the grid and their interactions are visualized. Turbulent (Reynolds) and oscillatory stresses are used

to evidence a modification of oscillatory flow and turbulence intensity repartition in and around the grid swept region. Energy transfer terms between mean, oscillatory and turbulent flows are estimated and used to describe turbulence production in the grid swept region. Energy is injected by the grid into the oscillatory component. In water, it is transferred to turbulence mostly inside the grid swept region. In DPS, oscillatory flow persists outside of the grid swept zone. Energy is transferred to turbulence as well, in the grid swept region, and far from the tank's walls, but also to the mean flow, leading to an enhancement of the latter. Mean flow production and enhancement mechanisms are explainable by oscillatory jets variable symmetry and intensity, and by time and space variable viscosity. Backward transfer from turbulence to oscillatory flow is also evidenced in DPS. Finally, using phased root mean square (rms) values of turbulent velocity fluctuations, it is shown that in water, the decay of turbulence intensity behind an oscillating grid can be related to the decay of fixed grid turbulence for specific grid positions, a result no longer valid in DPS.

**Keywords** PIV, Triple decomposition, Oscillating Grid, Shear-thinning, Dilute Polymer

## 1 Introduction

A multitude of environmental phenomenon and industrial processes involve turbulent flows of complex liquid phases such as suspensions (?), multiphase media (?), or liquids with complex rheology. The study of turbulence, already quite complex in itself, becomes even more challenging when it is done in such fluids. In particular, complex rheology liquids, known as non-Newtonian, are present in many industrial and environ-

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mental applications involving turbulent flows, for example in fermentation broths (??). The complete understanding of complex real life situations requires fundamental description and characterization of turbulence properties in such fluids, and thus adequate experimental or numerical simplified cases of study. One of them is that of a rigid grid oscillating in a liquid initially at rest, called oscillating grid turbulence (OGT) (??).

Oscillating grid stirred tanks have been used for many purposes in research on turbulence. Among them is the study of interactions between turbulence and solid impermeable boundaries (??), turbulence and gas-liquid mass transfer at a free surface (????), in stratified media (????), or study the behavior of bubbles, cells, fibers and aggregates suspended in a turbulent liquid phase (????). Apart from fundamental turbulence effect studies, oscillating grids are used as flotation cells (???) in tanks with various shapes (tubular, prismatic...) and with various number of grids.

Such devices are said to generate quasi homogeneous and isotropic turbulence in horizontal planes (parallel to the grid, when it oscillates vertically), and to yield theoretically no mean flow, which is a major advantage compared to fixed grid setups in channels. The absence of a strong mean shear avoids some destruction of complex fluids' components (fibers, polymer chains, cells) that is sometimes observed in fixed grid turbulence (?). The fact that turbulent eddies are theoretically not advected by a strong mean flow makes them more easily observable and traceable by optical techniques such as Particle Image Velocimetry (PIV) and Planar Laser Induced Fluorescence (PLIF): seeding particles or tagged fluorescent molecules stay for longer times in the region of interest.

However, the mechanisms of turbulence production by the oscillating grid itself have never been studied. It is commonly said that turbulence arises from the *interaction of jets and wakes* (?) behind grid holes and bars, but the exact interactions of these jets and wake, and the way they merge to generate homogeneous turbulence remained unobserved, even in water, until recently (?).

Regarding oscillating grid turbulence in non-Newtonian liquids, only a few studies can be found in the literature (???), focused on purely elastic fluids, and none of them seems to tackle the effects of variable viscosity on either the mechanisms of turbulence generation, or the mean flow and turbulence properties mapping in the whole tank. This has only been described in a recent study by ?.

Studies of periodic and turbulent flows in non-Newtonian polymer solutions yet suggest that the presence of a minute amount of polymer in the liquid phase,

conferring it either shear-thinning and/or viscoelastic properties, may significantly alter the energy distribution and exchanges between mean flow structures, oscillatory fluctuations and turbulence in the flow (???)

The aim of this paper is to study the influence of a shear thinning behaviour on mean flow, oscillatory flows, and turbulence around an oscillating grid. This study is meant to bring additional information on both oscillating grid turbulence generation mechanisms, and on the fundamental effect of polymer induced shear-thinning property on oscillatory flows and turbulence.

The shear thinning properties is given to an initially Newtonian fluid, water, by addition of a minute amount of polymer (Xanthan Gum, XG). Fluid velocity measurements are achieved using PIV in and around the region of the grid oscillations (grid swept zone). A triple decomposition methodology (?), already used in industrial impeller-stirred tank studies (?), is applied to reconstruct mean flows, oscillatory/periodic fluid motion, and turbulent velocity fluctuations. Oscillating grid flow in water is compared to a single polymer concentration case at the upper limit of the dilute regime.

The rest of present paper is organised in four sections. In the background section, the basis of oscillating grid turbulence in water are presented, the influence of polymer on turbulence in general and on grid turbulence (mostly for fixed grids) is described, and finally the triple decomposition method is introduced. In the "material and methods" section ??, the properties of polymer solutions used in this study are introduced and the oscillating grid setup is described. PIV measurements and image and data processing stages are also detailed. The "results" section ?? first focuses on the decomposition of the velocity fields in mean, oscillatory and turbulent components, and on turbulent and periodic fluctuation properties. Energy transfers between flow components are then discussed, and further details on mean flow and turbulence generation are provided. Previous results are evidenced again by a viscosity estimation approach. In the conclusion, the mechanisms of flow generation by the oscillating grid in water are summarized, and the observed effects of polymer addition on the flow are listed.

## 2 Background

### 2.1 Oscillating grid turbulence in water

The principle of Oscillating Grid Turbulence (OGT) is to produce turbulence in a fluid initially at rest by making a grid oscillate, usually vertically, at a frequency  $f$  and with an amplitude or stroke  $2S$ . It is commonly said that the jets and wakes behind the grid's holes

and bars interact to generate turbulence (????), which then diffuses away from the grid. It is of great interest for turbulence study since it theoretically creates almost no mean flow and therefore allows to study the effects of turbulence alone, which is not the case for fixed grid systems. OGT is also supposed to yield a quasi-homogeneous and isotropic turbulence in horizontal planes when measured far enough from the grid's top position.

The first oscillating grid apparatus was designed by ? to study turbulent diffusivity across a density stratification layer located above the grid and consisted in a square mesh grid in a cylindrical tank. Later, ? performed hot-fiber velocity measurements of grid generated turbulence in water, using a perforated plate as an oscillating grid. A full characterization of OGT in prismatic tanks came with the pioneer works of ? and ?. ? studied several types of grids with different mesh sizes  $M$  and different bar shapes, and showed that the best homogeneity and intensity of turbulence was achieved with square section bars and a solidity parameter  $\Xi = \frac{d}{M} (2 - \frac{d}{M})$  lower than 0.4,  $d$  being the width of grid bars. ? added that the walls of the tank should be planes of symmetry for the grid, in order to minimize the recirculation effects in the tank. For the same reason, the grid's average position should be at least  $2.5 \times M$  above the bottom of the tank (?). Horizontal homogeneity of turbulence is reached when the distance from the grid's mean position is greater than an empirically determined value  $Z_h$  expressed in numbers of mesh parameter, with  $2M < Z_h < 4M$  depending on the study. Since the ultimate interest is to achieve turbulence homogeneity, many studies of OGT use this  $Z_h$  parameter as a critical minimal distance at which the grid has to be placed from the item one wants to study the interaction with turbulence. Only recently, ? evidenced the spatial homogenisation of turbulence from the grid's swept zone to the  $Z_h$  region. Once the far-grid, homogeneity region is reached, turbulence properties can be described by various evolution laws, first derived by ? and ? and later completed by other studies (?????). These turbulence decay relationships are well described for water, but not in shear-thinning polymer cases. This yet will not be discussed in the present paper, as it is the subject of another work that has been published separately (?). It is worth noting that OGT has almost never been simulated numerically. Only the recent work by ? presents a Lattice Boltzmann simulation of OGT and numerically visualizes the interactions between jets and wakes behind the grid bars and holes leading to turbulence generation.

At first, the concept of OGT generating no mean flow but only isotropic and homogeneous turbulence was rather well believed. Yet with the development of PIV techniques allowing further investigations of the flow inside OGT tanks, it became clear that mean flow exist even when matching the requirements detailed above. ? studied the mean flows in an oscillating grid tank using PIV and showed that persistent mean flow cells always existed, with relative high kinetic energy level as compared to the turbulent kinetic energy. Moreover, these mean flows seem to be poorly reproducible and strongly dependent on initial conditions (?). It is therefore really hard to predict the mean flow that could occur in the oscillating tank during a specific measurement, and this is one of the main limitations of OGT systems.

A method for reducing mean flows in OGT is to use an inner box placed inside the stirred tank to separate the wall-induced vortices from the rest of the flow (???). The complementary work previously referred to (?) also suggests that the mean flow may be enhanced by the presence of polymer in the dilute entanglement regime. Investigations of flow properties in the grid region may allow to explain the origin of this mean flow both in water and in shear thinning polymer solutions.

## 2.2 Turbulence and grid turbulence in polymer solutions

The influence of non-Newtonian behaviour on grid turbulence has been mainly studied for fixed grid configuration and viscoelastic fluids (??????). Recently, ? used PIV measurements to look at turbulent spectra and scales in grid turbulence of dilute viscoelastic polymer solutions and evidence elastic modifications of turbulence. In their experiments, they found that both the shape of the energy spectrum and the elastic scale evolved with time, which they explained by the destruction of polymer chains by the strong shears in the vicinity of the grid. This shows one of the limits of fixed grid devices for the study of turbulence in polymer solutions: reaching high levels of turbulence requires high flow rate which causes important degradation of the polymer throughout the measurements. Moreover, turbulent velocity fluctuations are even smaller when compared to mean flow velocities than for the water case. One may thus prefer using OGT rather than fixed grid.

The first study of OGT in viscoelastic dilute polymer solutions (PEO) was made by ?, who observed the propagation velocity of the boundary between turbulent and non-turbulent regions in the tank, at the first instants after the onset of the grid's oscillations. They found that the turbulent/non-turbulent interface

moved globally faster in dilute polymer solution than in water. ? and ? later used a two oscillating grid system to study the viscoelastic effects of surfactants and dilute polymers on coherent structures. Using proper orthogonal decomposition (POD), they show that the addition of polymer tends to decrease the small scale effects of turbulence, and that this decrease can not only be attributed to the overall viscosity increase, since it is not associated with a decrease of the turbulent kinetic energy (TKE). Hence the non-Newtonian property of the flow seems to strongly modify the spectrum behaviour of the turbulent structures. They show promising results for the use of this method to analyse OGT flow properties in complex fluids such as DPS.

### 2.3 Triple decomposition of turbulence in periodic flows

In some cases, a flow may display a periodic behaviour due to external forcing or waves. Blade motion in stirred tanks (?), periodic vortex shedding at rigid boundaries in free surface flows (?), or pulsating flow in blood vessels induced by periodic heartbeats (?) are good examples of flows in which an oscillatory/organised/periodic effect is present. Oscillating grid turbulence used in this work is another one. In such flows, the time average of the oscillatory component of the flow is nil. Hence when using classical Reynolds decomposition to describe them, periodic fluctuations are included considered together with while they are not strictly speaking turbulent fluctuations.

To be able to distinguish turbulence from organised motion, ? proposed a triple decomposition of the velocity field, that will be called triple decomposition hereinafter. The total instantaneous velocity field is this time written as the sum of the average velocity  $\bar{U}$ , the periodic fluctuation  $u^*$  and the turbulent fluctuation  $u'$ .

$$U(M, t) = \bar{U}(M, t) + u^*(M, t) + u'(M, t) \quad (1)$$

Pressure decomposes the same way, with  $\overline{u^*} = 0, \overline{u'} = 0, \overline{p^*} = 0, \overline{p'} = 0, \overline{u^*u'} = 0$  and  $\overline{p^*p'} = 0$ . Turbulent, mean and oscillatory kinetic energies can be defined respectively as  $k' = \frac{1}{2}\overline{u'_i u'_i}$ ,  $K = \frac{1}{2}\overline{U_i U_i}$  and  $k^* = \frac{1}{2}\overline{u_i^* u_i^*}$ . ? derived the following governing equations for respectively  $k'$ ,  $k^*$  and  $K$ :

$$\begin{aligned} \frac{\partial k'}{\partial t} + \bar{U}_j \frac{\partial k'}{\partial x_j} &= - \frac{1}{\rho} \frac{\partial}{\partial x_j} \left[ \overline{u'_j \left( p' + \frac{1}{2} \rho u'_i u'_i \right)} \right] \\ &+ \underbrace{\left( -\overline{u'_i u'_j} \right)}_{(4)} \frac{\partial \bar{U}_i}{\partial x_j} + \underbrace{\left( -\langle u'_i u'_j \rangle_\phi \frac{\partial u_i^*}{\partial x_j} \right)}_{(5)} \\ &+ \underbrace{u_j^* \frac{\partial}{\partial x_j} \left\langle \frac{1}{2} u'_i u'_i \right\rangle_\phi}_{(6)} + \underbrace{\nu \frac{\partial}{\partial x_j} \left[ u_i^* \left( \frac{\partial u'_i}{\partial x_j} + \frac{\partial u'_j}{\partial x_i} \right) \right]}_{(7)} \\ &- \underbrace{\frac{\nu}{2} \left( \frac{\partial u'_i}{\partial x_j} + \frac{\partial u'_j}{\partial x_i} \right)^2}_{(8)} \end{aligned} \quad (2)$$

Where (1) is the accumulation term, (2) is advection by the mean flow, (3) (6) and (7) are diffusion terms, term (8) dissipation, and terms (4) and (5) are exchanges with mean and oscillatory components.  $\langle a \rangle_\phi$  is the phase averaged quantity of  $a$  (see section ??).

$$\begin{aligned} \frac{\partial k^*}{\partial t} + \bar{U}_j \frac{\partial k^*}{\partial x_j} &= - \frac{1}{\rho} \frac{\partial}{\partial x_j} \left[ \overline{u_j^* \left( p^* + \frac{1}{2} \rho k^* \right)} \right] \\ &+ \underbrace{\left( -\overline{u_i^* u_j^*} \right)}_{(4)} \frac{\partial \bar{U}_i}{\partial x_j} - \underbrace{\left( -\langle u'_i u'_j \rangle_\phi \frac{\partial u_i^*}{\partial x_j} \right)}_{(5)} \\ &+ \underbrace{\nu \frac{\partial}{\partial x_j} \left[ u_i^* \left( \frac{\partial u_i^*}{\partial x_j} + \frac{\partial u_j^*}{\partial x_i} \right) \right]}_{(6)} - \underbrace{\frac{\nu}{2} \left( \frac{\partial u_i^*}{\partial x_j} + \frac{\partial u_j^*}{\partial x_i} \right)^2}_{(7)} \end{aligned} \quad (3)$$

Where term (1) is the accumulation term, term (2) is advection by the mean flow, terms (3) and (6) are diffusion, term (7) is dissipation, and terms (4) and (5) are exchanges with mean and turbulent components.

$$\begin{aligned}
\underbrace{\frac{\partial K}{\partial t}}_{(1)} + \underbrace{\bar{U}_j \frac{\partial K}{\partial x_j}}_{(2)} = & - \underbrace{\frac{1}{\rho} \frac{\partial \bar{U}_i \bar{P}}{\partial x_i}}_{(3)} - \underbrace{\left( -\overline{u'_i u'_j} - \overline{u_i^* u_j^*} \right) \frac{\partial \bar{U}_i}{\partial x_j}}_{(4)} \\
& - \underbrace{\frac{\partial}{\partial x_j} \left[ \bar{U}_i \left( -\overline{u'_i u'_j} - \overline{u_i^* u_j^*} \right) \right]}_{(5)} \\
& + \nu \underbrace{\frac{\partial}{\partial x_j} \left[ \bar{U}_i \left( \frac{\partial \bar{U}_i}{\partial x_j} + \frac{\partial \bar{U}_j}{\partial x_i} \right) \right]}_{(6)} \\
& - \underbrace{\frac{\nu}{2} \left( \frac{\partial \bar{U}_i}{\partial x_j} + \frac{\partial \bar{U}_j}{\partial x_i} \right)^2}_{(7)} \quad (4)
\end{aligned}$$

Where term (1) is the accumulation term, term (2) is advection by the mean flow, term (3) is the pressure velocity correlation, terms (5) and (6) are diffusion terms, term (7) is dissipation, and term (4) is the transfer to other components' kinetic energy. From equations (??), (??) and (??), it is possible to extract the exchange terms (respectively numbered (5), (4) and (5), and (4)) and identify the expression of the kinetic energy transfer between each components of the velocity field (?):

Mean to turbulent energy transfer:

$$\mathcal{T}_{mt} = -\overline{u'_i u'_j} \frac{\partial \bar{U}_i}{\partial x_j} \quad (5)$$

Mean to oscillatory energy transfer:

$$\mathcal{T}_{mo} = -\overline{u_i^* u_j^*} \frac{\partial \bar{U}_i}{\partial x_j} \quad (6)$$

Oscillatory to turbulent energy transfer:

$$\mathcal{T}_{ot} = \overline{\left( -\langle u'_i u'_j \rangle_\phi \frac{\partial u_i^*}{\partial x_j} \right)} \quad (7)$$

Each of these transfer terms is a product of a gradient of mean or oscillatory motion and a stress term of organized and turbulent motion. The direct transfer from mean flow to turbulent motion  $\mathcal{T}_{mt}$  is equivalent to the turbulence production by mean flow in Reynolds classical decomposition. However in the present case, the mean flow also transfers part of its energy to the periodic one ( $\mathcal{T}_{mo}$ ) and part of the turbulent kinetic energy production comes from the organized motion ( $\mathcal{T}_{ot}$ ). In order to fully understand turbulence in oscillatory flows, the knowledge of these transfer terms is required. It is worth noting that all of the above equations reduce to the ones obtained using the classical Reynolds decomposition when  $u^* \ll u'$ , i.e. in case of negligible oscillatory flow influence.

### 3 Material and methods

#### 3.1 Polymer solutions

Shear-thinning properties are conferred to the liquid by addition of a minute amount of a polymer, Xanthan Gum (XG), into distilled water. Here XG produced by Kelco under the commercial name Keltrol CG-T is used. Its average molar mass is  $M_w = 3.4 \times 10^6$  g.mol<sup>-1</sup> and its polydispersity equal to 1.12 (?). XG is chosen for its high resistance to strong shears and extreme temperature and pH conditions (?). Such features are useful when using it nearby a rigid oscillating grid. XG yields optically clear non-Newtonian solutions once dissolved in aqueous media. This allows the use of optical methods for liquid phase velocity measurements. This polymer is commonly utilized as a flow additive for non-Newtonian fluid mechanics experiments, but also in the food, process, and oil and gas industries (?). Its rheology and its properties have been widely studied in the literature (???). Depending on the polymer concentration  $C_{XG}$ , one may distinguish between three entanglement regimes: dilute, semi-dilute, and concentrated (?). In the last two cases, the flow behaviour is defined by fluid-polymer but most importantly polymer-polymer mechanical or electrical interactions. In this work the focus is made on the dilute regime, for which polymer molecules only interact with the flow and not between each other. It concerns the  $C_{XG} \leq 100$  ppm concentration range (?). Here the working concentration is  $C_{XG} = 100$  ppm. This last concentration is chosen so that the solution is still in the dilute regime for entanglement, with the strongest possible concentration effects within that regime. One then talks about a dilute polymer solution (DPS). The shear-thinning behaviour of aqueous XG DPS can be modelled by a Carreau-Yasuda (CY) equation

$$\frac{\mu - \mu_\infty}{\mu_0 - \mu_\infty} = (1 + (t_{CY} \dot{\gamma})^a)^{\frac{n-1}{a}} \quad (8)$$

With  $\mu_0 = 32.8$  mPa.s and  $\mu_{inf} = 1.1$  mPa.s the zero shear rate and infinite shear rate Newtonian plateau,  $t_{CY} = 1.58$  s a characteristic timescale of the polymer,  $(n-1) = -0.5$  the shear thinning power law exponent, and  $a = 2$  a parameter for the transition between power law and Newtonian behaviours (all values given for  $C_{XG} = 100$  ppm). The evolution of viscosity with the nominal shear rate is shown on figure ???. Vertical lines indicates estimate of i) the typical shear rates caused by the grid (full line, based on its frequency), and ii) the maximum shear rates caused by mean, oscillatory and turbulent motions (based on data shown in figure ??). Viscoelasticity is checked to be negligible

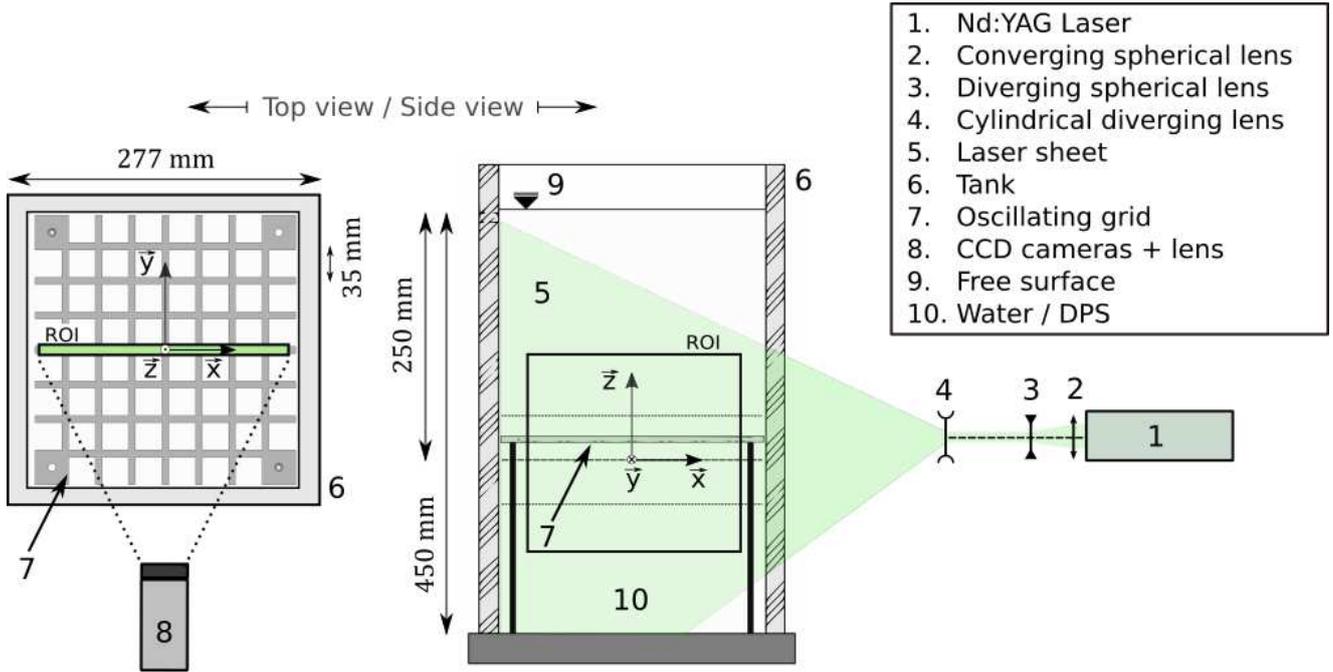


Fig. 1: Sketch of the oscillating grid and PIV setup.

for such a XG concentration. Steady shear rheological measurements performed before and after experiments allow to check that polymer chains are not destroyed by grid oscillations, or at least that destruction does not affect the shear thinning property (see ?, figure 3.10).

### 3.2 Oscillating grid setup

Turbulence is generated in a transparent prismatic tank of  $L^2$  inner cross-section with  $L = 277$  mm. The fluid height is set at  $H=450$  mm and the distance between the surface and the average grid position is 250 mm. The vertical axis, oriented upwards, is noted  $Z$ , and  $X$  and  $Y$  are the axis defined by the grid bar (see figure ??). The origin of the reference frame is placed at the grid average position ( $Z=0$ ) at the crossing between the two central bars. In this study only polymer concentration is varied and all oscillation parameters are kept constant. The grid bars are  $d = 7$  mm thick and the mesh parameter is  $M = 35$  mm. The frequency is fixed at 1 Hz and the amplitude at  $2S = 5$  cm. This allows to define a grid based Reynolds number using the definition of ?, but based on the zero shear rate viscosity  $\mu_0$ :

$$Re_g = \frac{\rho f (2S)^2}{\mu_0} \quad (9)$$

The density  $\rho$  of the fluid is assumed equal to that of water, because of the very small mass of polymer added.

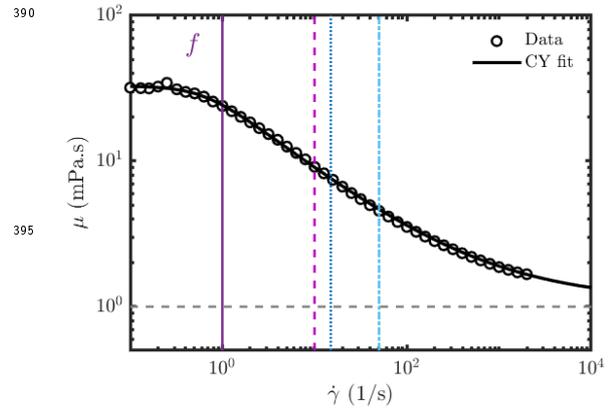


Fig. 2: Viscosity data points (circles) and Carreau-Yasuda fitting (line) for the 100 ppm XG solution. The horizontal dashed line denotes the viscosity of water. The vertical full line is the nominal shear rate corresponding to the grid frequency. Vertical dashed, dotted, and mixed lines show respectively the order of magnitude of the maximum mean, oscillatory, and turbulent velocity gradients. They thus indicate the range of viscosity variations induced by all three types of flow.

Here one gets  $Re_g = 2500$  for water and  $Re_g = 76$  for the polymer case. In order to quantify the ratio between the polymer relaxation time scale and the grid forcing

time scale the grid based Deborah number  $De$  is defined as

$$De = \frac{t_{CY}}{T} = t_{CY} f \quad (10)$$

with  $T$  the period of oscillations. Here  $De = 1.58$ .

### 3.3 PIV Measurements

Liquid phase velocity measurements in the tank are achieved by Particle Image Velocimetry (PIV). The experimental setup is sketched in figure ?? . The region of interest (ROI) is a vertical rectangle, in a plane normal to the central bar of the oscillating grid. Its width is close to that of the tank, and it is vertically centred around the grid swept zone. The cameras used is a double frame LaVision SCMOS sensors of 2560 by 2160 pixels, equipped with a 50 mm focal macro lens. A pulsed Quantel Nd:YAG laser emitting at  $\lambda = 532$  nm is used to illuminate 50  $\mu\text{m}$  diameter polyamid particles. Double frame PIV at an acquisition frequency  $f_{acq}$  of 10 Hz is performed. The time interval between laser pulses is  $\Delta t = 4$  ms. Vector fields are computed with DaVis 8 software using a multipass processing: a first pass with 48 by 48 pixels and 2 following passes with 24 by 24 pixels round Gaussian weighted interrogation windows, at a maximum of 50% overlapping. Spurious vectors are removed from PIV fields by applying a threshold of 1.2 on the peak ratio, and replaced using median filtering.

The final spatial resolution achieved is 3.4 mm. The smallest Kolmogorov length scale and Taylor micro scales of turbulence are supposed to be found in the water case, for which the viscosity is always the lowest. The Kolmogorov and Taylor length scales are evaluated to be respectively of about 0.47 mm and 3.17 mm for water. For 100 ppm XG solutions, using a constant viscosity equal to  $\mu_\infty$ , they increase to 0.23 mm and 3.25 mm, and up to 6.45 mm and 18.17 mm when using  $\mu_0$  as the scale viscosity. The 3.4 mm spatial resolution is thus quite coarse and would unfortunately not allow to evidence energy variations at large wave numbers characteristic of viscoelastic turbulence. We shall thus discuss only the inertial and large scale effects.

Measurements performed here are planar (2D PIV) and give access to only two components of the velocity field. As a consequence, it is not possible to compute all the terms of the governing equations introduced in section ?? , but only a part of the terms involving the components and their gradients along  $X$  ( $i$  and/or  $j$  equal to  $x$ ) and  $Z$  ( $i$  and/or  $j$  equal to  $z$ ). In what follows, analysis of the velocity fields is carried out as if the flow was two dimensional, assuming that velocities

and gradients along the  $y$  direction are nil. This is a strong and reductive hypothesis. In order to perform a complete analysis of the production, dissipation, and transfer terms of turbulence of the governing equations in the whole volume of interest, full three dimensional three component velocity data would be required.

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### 3.4 Grid detection and phase resolved statistics

#### 3.4.1 Grid masking and tracking

As measurements are focused around the swept zone, the oscillating grid is visible on the recorded images (figure ?? a)), which is an asset for grid tracking but problematic for the velocity field calculation. The grid has therefore to be first removed from images for velocity calculation and then isolated for the grid tracking step. Grid masking is achieved using DaVis software from LaVision. At first, an horizontal median filter is applied on every recorded image (figure ?? b)). These images are then binarized using an arbitrary threshold based on the image gray level values such that the pixel corresponding to the grid are set to zero and the rest of the image to one (figure ?? c)). Each mask image is then applied to the corresponding image when calculating the velocity field. One effect that can not be easily corrected with this procedure is the shaded area visible on the left part of figure ?? a) under the grid. Here the PIV laser sheet was directed so that it always met the grid from the top, and the shaded region was always under the grid. In doing so, the region above the grid is always well lighted, and measurements can always be considered reliable there. The shaded particle region is represented by a gray zone on each PIV-deduced fields at specific grid positions in the following figures, to recall that this region is prone to errors.

Grid tracking is performed by a Matlab custom script. It also starts by an horizontal median filtering step to smooth particles off the image. Gray level intensity is then horizontally averaged on the whole image width, and the peaks of width averaged intensity gradients are used to detect grid boundaries (figure ??). Finally, the grid position is defined at equal distance from the two peaks. Once the grid tracking step is made, every pair of PIV frames and the corresponding vector field can be associated to a grid position. The grid direction (going up or going down) for each instantaneous fields can be found using the difference in detected grid position on frame 1 and 2.

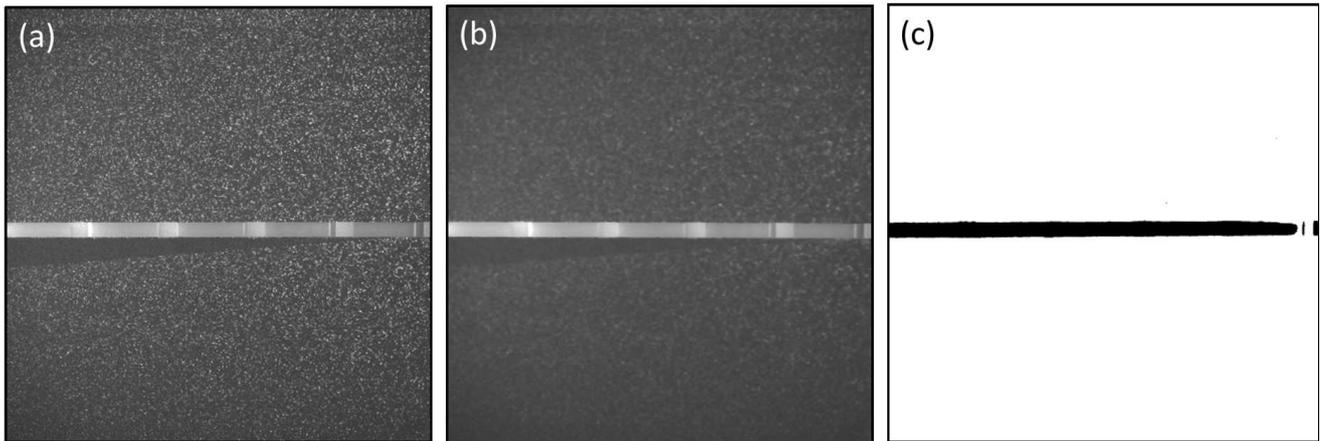


Fig. 3: Grid masking procedure. (a) Recorded image showing both the grid and PIV particles, (b) particles smoothed out by applying an horizontal median filter, (c) Mask obtained using an arbitrary intensity threshold. The laser sheet comes from the right, as sketched in figure ??.

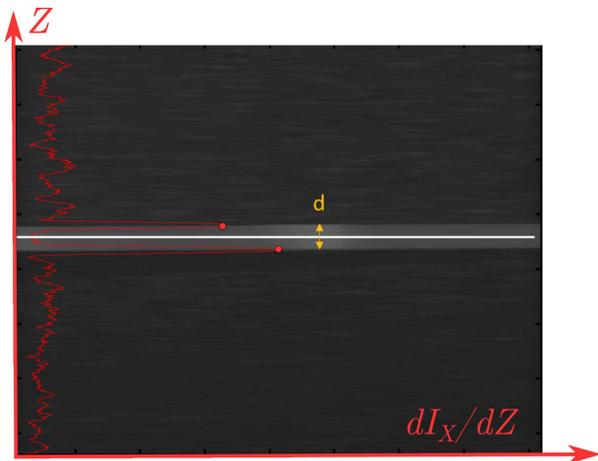


Fig. 4: Grid tracking procedure: The red curve is the vertical gradient of horizontally averaged intensity  $I_X$ . The two red dots correspond to the maximum gradient peak detected. It is checked that the distance between the two peaks is equal to the grid thickness  $d$  (orange). The white line shows the detected grid position.

### 3.4.2 Conditional averaging and triple decomposition

As mentioned in section ??, a triple decomposition of the velocity field into mean, oscillatory, and turbulent components is a useful tool to study the dynamics of flows which exhibit a periodic pulsation or sustained by a periodic forcing. ? detailed a method to extract mean, oscillatory and turbulent component of the flow from statistical analysis of non time resolved 2D-PIV measurements synchronized on blade motion. The main idea was to perform different sets of PIV measurements corresponding each to a different but known

position of the blade (or here the grid), the synchronization between blade/grid position and measurement being enforced by an outside detection system. Here the method used to achieve phase resolved measurements is not based on an external trigger but rather on image processing of a collection of randomly sampled instantaneous fields. The main principle of statistical estimation of the triple decomposition component still stays the same, and is detailed in what follows.

**Sampling of the grid stroke:** A conditional averaging of velocity fields is performed based on the grid position previously detected. To that end, the total measured amplitude is sampled into  $N_p$  parts of constant size  $\Delta S$  such that  $2S = N_p \times \Delta S$ . Based on its measured grid position, each instantaneous field is then associated to the slice it lies into, and is thus affected to a closest matching sample grid position. Phase averaging is performed by averaging all the velocity fields stored at a given sampling grid position (*i.e.* in a given slice). Ultimately, the typical period of oscillation is described using  $2 \times N_p - 1$  point in time ( $N_p$  for the grid going up, same for the grid going down, minus the starting point).  $N_p$  is chosen as the best compromise between high period sampling and convergence of each position's velocity statistics. Indeed if  $N_p$  is too large, each slice may not include enough instantaneous field to achieve statistical convergence (see the next paragraph). On the other hand if  $N_p$  is too low, one may not be able to describe accurately oscillatory velocity fields around the grid, and results can not be considered phase-resolved. The results presented hereinafter are for  $N_p = 12$ . This induces every slice to always store at least 250 instantaneous data fields, which has proven to be sufficient for

phase-averaged velocity fields calculation (see figure ?? and following paragraphs).

**Flow statistics:** Knowing the phase averaged velocity fields, it is then possible to perform a triple decomposition of the velocity field as proposed by ? and explained in section ?. It is worth noting that triple decomposition has never been applied to the study of oscillating grid turbulence despite its obvious oscillatory behaviour.

Here for a velocity component  $i$ , the mean velocity field is taken as the ensemble average of all velocity fields:

$$\bar{U}_i = \frac{1}{N} \sum_{p=1}^N U_i^p \quad (11)$$

Where  $N$  is the total number of instantaneous velocity fields. Phase averaged velocity for a given grid position  $k$  is defined as

$$\langle U_i \rangle_\phi^k = \frac{1}{N_k} \sum_{p=1}^{N_k} U_i^p \quad (12)$$

With  $N_k$  the number of instantaneous fields  $U^p$  at grid position  $k$  ( $U^{p=k}$ ) in the phase.

The oscillatory component at this same grid position is the phase averaged velocity from which the mean component is removed:

$$u_i^{*k} = \frac{1}{N_k} \sum_{p=1}^{N_k} (U_i^p - \bar{U}_i) \quad (13)$$

The turbulent fluctuation accounting for the grid position  $k$  is thus :

$$u_i'^k = U_i - \bar{U}_i - u_i^{*k} \quad (14)$$

The phase root mean square (rms) velocity can then be defined as the root mean square of turbulent fluctuations at position  $k$ :

$$\langle u_i' \rangle_{\phi,rms}^k = \sqrt{\frac{1}{N_k} \sum_{p=1}^{N_k} (u_i'^p)^2} \quad (15)$$

It can be used to estimate the intensity of turbulence at position  $k$ , and will be later referred to as "phased rms" Finally, the non phase-averaged rms of oscillatory

and turbulent velocity fluctuations are defined respectively as

$$\langle u_i^* \rangle_{rms} = \sqrt{\frac{1}{N_p} \sum_{p=1}^{N_p} (u_i^{*p})^2} \quad (16)$$

and

$$\langle u_i' \rangle_{rms} = \sqrt{\frac{1}{N} \sum_{p=1}^N (u_i'^p)^2} \quad (17)$$

They quantify for a given Eulerian probing point the intensity of respectively oscillatory and turbulent fluctuations at a fixed location in the flow.

**Statistical convergence and data weight/size:** For all quantities, it has to be checked that statistical convergence is reached. The number of independent instantaneous fields used for average or rms computation on the whole set of data ( $N$ ) or at the  $k$  position ( $N_k$ ) should be large enough for the computed quantity to be independent of it. This is verified by computing the sliding statistics using larger and larger  $N$  until the chosen indicator for statistical convergence reaches a constant value <sup>1</sup>. For non time resolved PIV measurements of turbulent flows, it is commonly said that a few hundreds of independent fields are sufficient to reach convergence of averaged quantities, and about 1000 is required for second order statistical quantities (rms for example). This criterion is yet arbitrary, so statistical convergence has been checked for our measurements. Our phase resolved measurement provide uncorrelated fields for phase rms computation, since two fields recorded at the same grid position are separated by a minimum amount of time of 1 s corresponding to at least one grid period. In order to perform phase averaged statistical analysis, a minimum of a few hundreds of images is needed for each grid sample position. The typical total number of images recorded here to fulfil this requirement is thus around 10 000, with a number of images per grid position  $N_k$  laying between 250 and 500. Here  $N_k$  is a consequence of the true grid frequency, the acquisition frequency of the PIV system, the lag between these two frequencies and the accuracy of the grid detection procedure.

Statistical convergence is checked at all grid sample positions. To that end, the average and rms values are plotted as a function of the sample size  $N$  or  $N_k$  for

<sup>1</sup> A more rigorous approach could be lead via an ensemble probability estimation method (?), in which the amount of independent field needed to achieve statistical convergence pre-determined by the analysis of the expected shape of concentration fluctuations PDF.

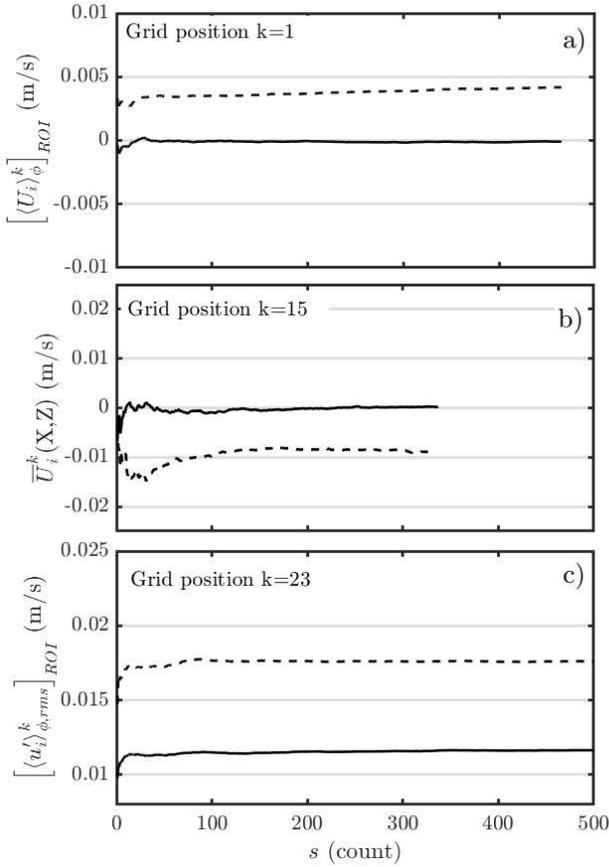


Fig. 5: Example of graph of convergence of statistical quantities (water).  $s$  is the size of sample used for statistical analysis. a) Convergence of the phase averaged velocity values, spatially averaged over the whole ROI. b) Statistical convergence of the same quantity at a given probing location  $(X,Z)$  of the ROI (here  $X=0$ ,  $Z/S=2$ ). c) Convergence of the phase rms velocities, averaged over the ROI. Full lines are for horizontal velocity components and dashed lines for vertical velocity components. Examples are provided for three grid positions ( $k=1$  for a),  $k=15$  for b) and  $k=23$  for c)) but similar results are achieved for all  $2Np - 1 = 23$  possible grid sampling positions with all three (a,b,c) indicators and for both fluids.  $[\cdot]_{ROI}$  denotes a spatial average over the full ROI.

all velocity components (along  $X$  and  $Z$ ), at several random locations in the ROI or spatially averaged over the whole ROI. An example of a convergence graph is shown in figure ???. Globally, all indicators are found to converge in all ROIs and planes.

## 4 Results and discussion

### 4.1 Flow visualization

#### 4.1.1 Instantaneous velocity fields and flow decomposition

An example of instantaneous velocity field for each fluid is pictured in figure ?? for a bottom grid position. In this figure as for all following fields, the  $Z$  dimension is scaled by the stroke  $S$ , and the  $X$  dimension by the semi width of the tank  $L/2$ . In both cases, the wake of the grid is evidenced by a series of counter rotating vortices behind each grid bars. DPS visually exhibits stronger but larger vortices than water. Using the grid detection procedure presented in section ??, each instantaneous field is associated to a specific grid position. The mean velocity field is computed by averaging all instantaneous velocity fields, and phase averaged velocity fields by averaging all instantaneous velocity fields at the same grid position, as explained in section ??. The oscillatory component is deduced by removing the mean velocity field from phase averaged velocity field at each grid position, and fluctuating velocity fields are derived by subtraction of mean and oscillatory fields to each instantaneous field.

Figure ?? gathers, for the two studied fluids, their mean velocity field, a phase averaged and oscillatory velocity field at a given grid position (bottom position), and the fluctuating velocity field corresponding to instantaneous fields that are shown in figure ??. The background color represents the vorticity of each velocity field, respectively  $\overline{\Omega}$ ,  $\langle \Omega \rangle_\phi$ ,  $\Omega^*$  and  $\Omega'$  for the average, phase averaged, oscillatory and fluctuating vorticity. The averaged fields show two side vortex above the grid swept zone. They seem stronger in DPS than in water, and accompanied, in DPS only, by an enhanced up-going motion above the swept zone centred around  $X = 0$ . This specific mean flow enhancement is described in ?. Phase average velocity field exhibit more clearly the grid bar wakes, together with the side vortices. The oscillatory component mostly displays the wakes, since it is the result of the subtractions between phase averaged measurement and mean flow. A new interesting difference between water and DPS appears when comparing the oscillatory components at the low grid position: DPS fields display two symmetric pairs of vorticity patches at the edges of the ROI above the grid swept zone, which are not visible for water. Finally, the fluctuating velocity fields allow to see the turbulent structures produced behind the grid. Eddies are created close to the grid and interact so that turbulence diffuses towards the bulk.

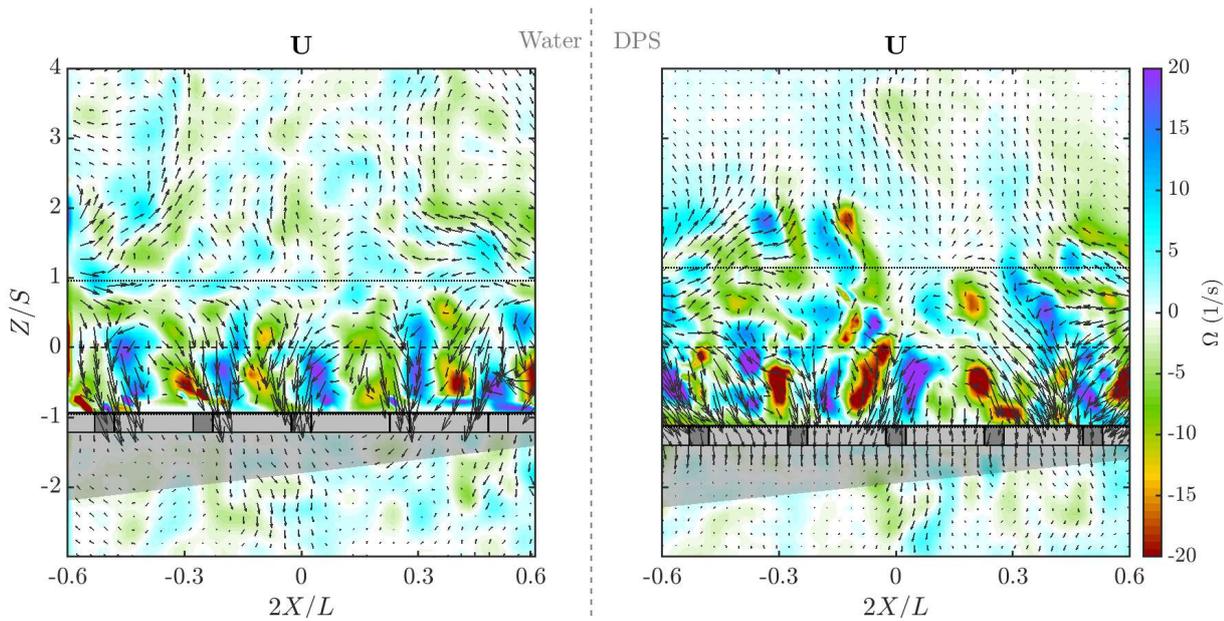


Fig. 6: Example of close grid instantaneous velocity and vorticity fields in water (left) and dilute polymer solution (DPS) (right). The colorbar represents the out-of-plane vorticity of  $U$ . The gray area under the grid represents the area of the ROI for which the laser sheet was shaded by the grid and were measurements could be inaccurate. For figure's clarity, only one every two vector in both dimensions is plotted.

#### 4.1.2 Typical period of oscillations

The typical period of oscillations can be described by considering the phase averaged velocity field  $\langle U \rangle_\phi$  (and its associated vorticity), to which we subtract the mean flow  $\bar{U}$  (and its vorticity). Figure ?? displays a typical period of oscillations for the resulting oscillatory flow illustrated by the the oscillatory component of the vorticity field. Five successive grid positions  $k = p$  are sketched (a snapshot has already been presented in figure ?? for the lower grid position). The instantaneous relative grid altitude  $Z_g$  corresponding to each snapshot is shown on the sinusoidal plot. Positions are numbered from  $p = 1$  to  $p = 5$ . Trailing vortices behind grid bars are evidenced again, and their growth and decay can be visualized as a function of the grid position. In DPS, a periodic vortex shedding is observed on both sides of the ROI, specifically in the region where the two mean vortices are formed. The shed vortex are those previously evidenced on figure ?? third line.

### 4.2 Turbulence, oscillatory motion, and mean flow analysis

#### 4.2.1 Reynolds and oscillatory stresses

In order to quantify the relative intensity of oscillatory versus turbulent fluctuations in both fluids, the

root mean square (rms) over the whole set of instantaneous fields of oscillatory and turbulent fluctuations (regardless of the grid position), defined at equations (??) and (??) respectively, are represented on figure ?? . The Reynolds and "oscillatory" stresses  $\overline{u'_i u'_j}$  and  $\overline{u_i^* u_j^*}$  are shown in figures ?? and ?? respectively. In these figures and the grid is sketched at its mean position ( $Z = 0$  mm). The shaded area is not represented since these fields are statistical quantities involving several grid positions. The stresses for which  $i = j$  are referred to as "normal" stresses, and the other ones as "tangential" stresses.

All turbulent fluctuations are logically much higher in the swept region of the grid around  $Z = 0$ . They also exist at a lower level outside of the stroke region in both water and DPS (non zero RMS of turbulent fluctuations). The RMS of the oscillatory component is strong in the grid swept region, as also suggested by the snapshots of typical oscillation period shown in figure ?? and ??, but quickly vanishes when moving away from the grid. In DPS, the RMS of oscillatory motion is slightly increased outside of the grid region compared to water. Figure ?? thus shows that the amplitude of oscillatory component of the flow is mostly significant in the swept region of the grid, and quickly becomes negligible compared to turbulence outside of this region. The effect of DPS seems to be an enhancement of

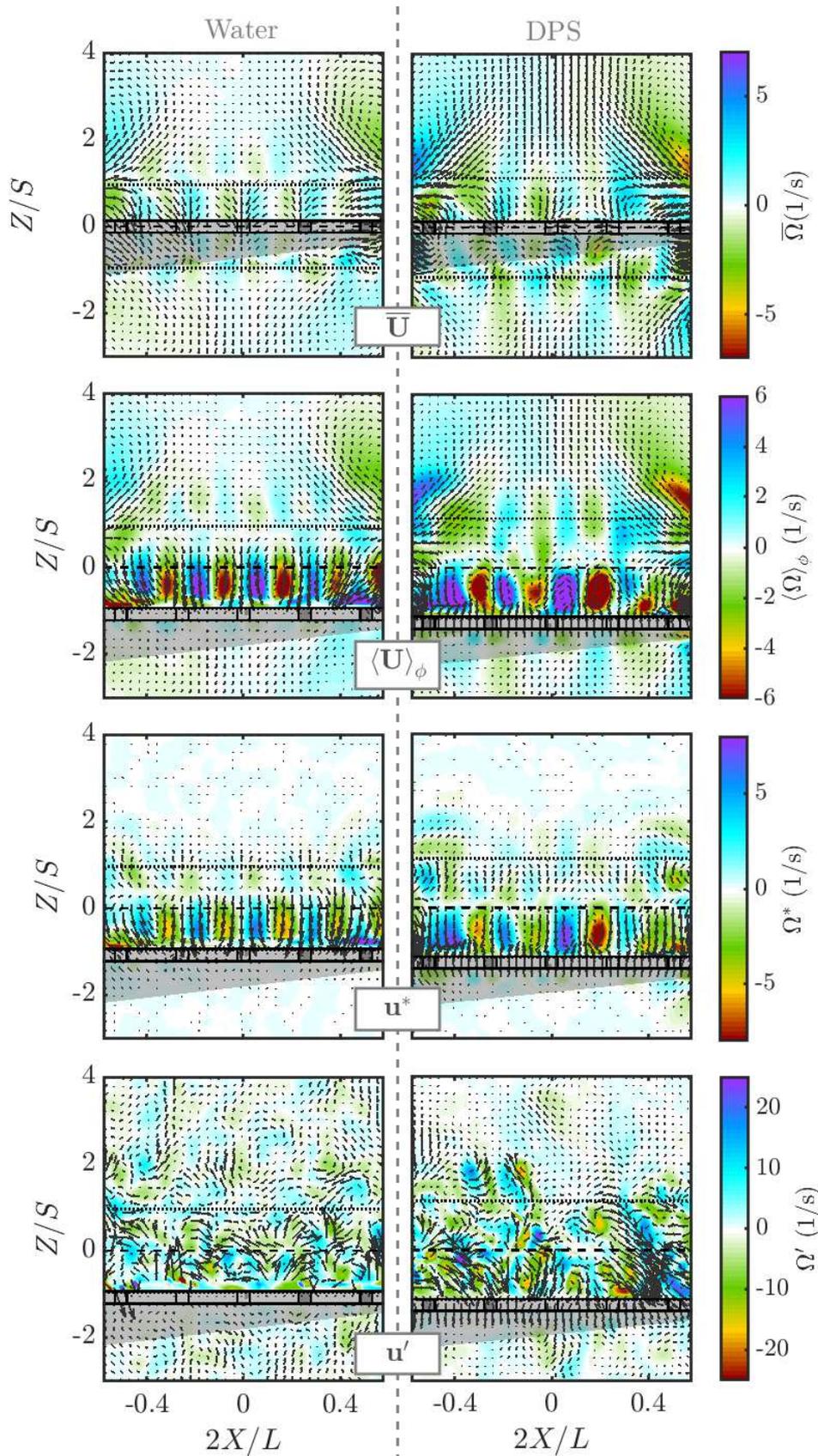


Fig. 7: Ensemble average (first line), phase average for a given grid position (second line), oscillating component for a given grid position (third line) and turbulent fluctuating component example at the same grid position (fourth line) for velocity and vorticity fields, in water (left column) and DPS (right column).

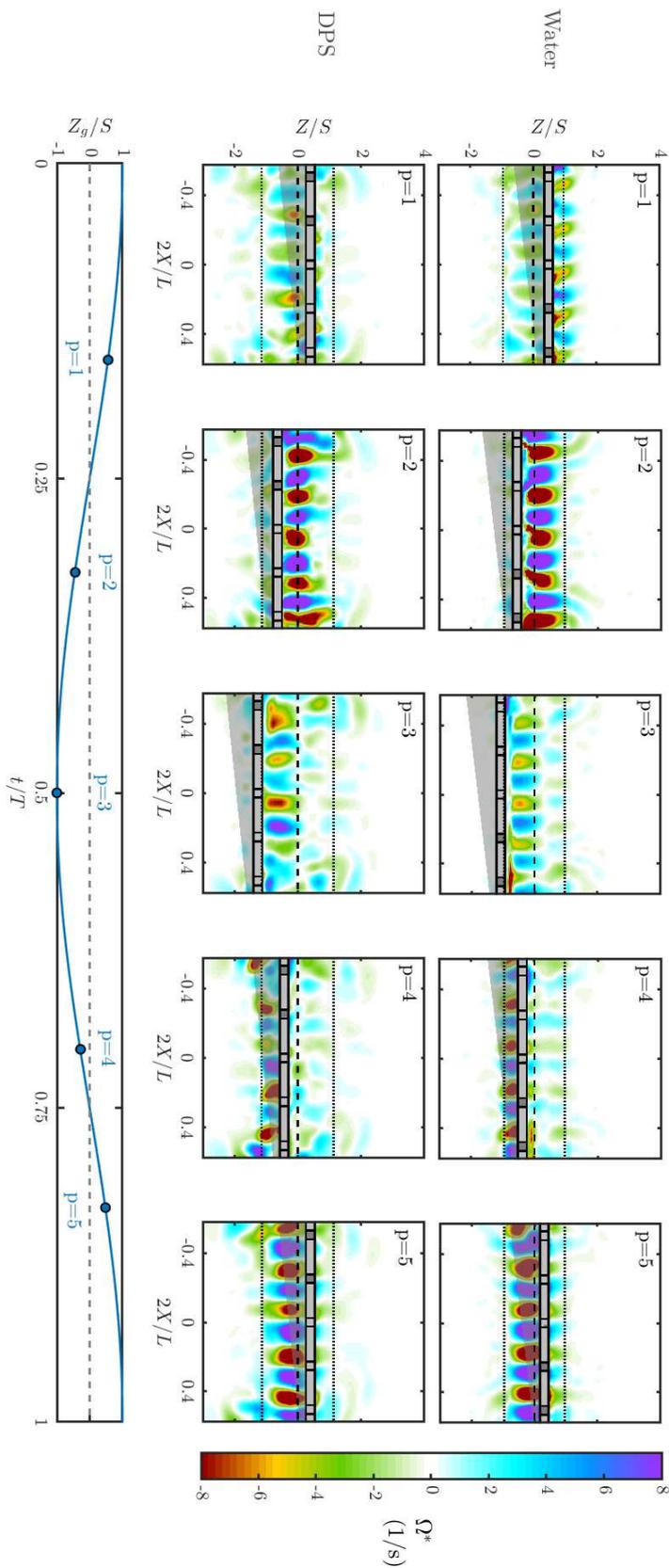


Fig. 8: Oscillating vorticity  $\Omega^*$  field in (1/s) at different grid positions in the close grid region for water and DPS. The sampling of the grid period is sketched alongside the figure, on the  $Z_g/S$  versus  $t/T$ , where  $Z_g$  is the distance from the grid to its mean position, and  $t$  the time over a grid period  $T$ .

the oscillatory fluctuations intensity and a modification of their spatial distribution.

Similar conclusions can be drawn from figures ?? and ??: Reynolds stresses and oscillatory stresses are high in the swept region for both water and DPS. They decrease when moving away from this region, and oscillatory stresses rapidly become nil. The presence of polymer tends to increase the spatial decay of Reynolds stresses, but slightly decrease that of oscillatory stresses, especially for the normal horizontal ones. Stress fields yet allow to make a few more observations. First, both the Reynolds and oscillating stresses seem to be increased at  $Z = 0$  mm in DPS compared to water. Second, the intensity of normal Reynolds stress in DPS is enhanced at the center of the ROI whereas that of oscillatory stress is larger on the sides of the ROI. Finally, the two side vortices evidenced from the mean flow study are found to correspond to two patches of tangential Reynolds stress with a significant magnitude, and that for both water and DPS, as visualized on figure ?? second row.

#### 4.2.2 Energy transfers

The transfer terms have been defined in section ??, equations (??), (??) and (??). The  $\mathcal{T}_{mt}$  (mean to turbulence),  $\mathcal{T}_{mo}$  (mean to oscillatory) and  $\mathcal{T}_{ot}$  (oscillatory to turbulence) fields for water and DPS are shown in figure ?. Noticing the scales of each colorbars, one sees that in order of magnitude,  $|\mathcal{T}_{mt}| < |\mathcal{T}_{mo}|$ ,  $|\mathcal{T}_{mt}| < |\mathcal{T}_{ot}|$ , and  $|\mathcal{T}_{mo}| \approx |\mathcal{T}_{ot}|$ . In water it appears that  $|\mathcal{T}_{mo}| < |\mathcal{T}_{ot}|$ , but in the polymer case  $|\mathcal{T}_{mo}| > |\mathcal{T}_{ot}|$ .

From the topology of these fields, several observations can be made:

- The variations of transfer terms are larger in DPS than in water. Since transfer terms are a product of stress and spatial gradient, the origin of these variations may come from both of these parameters. Reynolds and oscillatory stresses spatial variations are more important in DPS than in water (see figure ?? and ??). Mean and oscillatory flows are enhanced by the presence of polymer (as shown in figure ??), and their gradients are sharper.
- All the transfers mostly occur within the grid swept region. The only small but noticeable exception is observed for  $\mathcal{T}_{mt}$  fields in DPS, just above the grid's top position, where two weak mean to turbulence transfer regions are observed on both sides of the ROI (evidenced by dashed circles on figure ??, first line of sub figures). They correspond to the mean flow vortices observed previously. This is the blueprint of a secondary turbulence production region, the strength of which is enhanced by the pres-

ence of polymer. It was also evidenced by the enhancement of  $\overline{u'_x u'_z}$  Reynolds stresses in the same region in figure ??.

730 –  $\mathcal{T}_{mo}$  seems stronger in the DPS than in the water case, as illustrated by the second row of the figure. This underlines the increased importance of the oscillatory field in DPS. In particular, two highly negative  $\mathcal{T}_{mo}$  patches appear on the top part of the swept zones at the sides of the ROI (hence near the walls). Negative  $\mathcal{T}_{mo}$  means that energy is transferred from the oscillatory motion to the mean flow. The location of this patches corresponds quite well to that of enhanced mean flow structures observed in figure ?? first line. Energy transfer terms thus bring the additional information that this mean flow enhancement comes from the mean flow production by oscillatory flow at the walls.

– In water,  $\mathcal{T}_{ot}$  mostly occurs in vertical regions aligned with the grid bars, and the transfer term is always positive, so that oscillatory motion seems to always transfer energy to turbulence and not the other way around. In DPS, the pattern of the  $\mathcal{T}_{ot}$  field is more elaborated and both positive and negative regions exist, which means that energy transfer is a two way process. This is consistent with the two-way flow-polymer interaction process evidenced by ? in viscoelastic turbulence.

Figure ?? summarizes figures ??, ?? and ?? in terms of vertical profiles of Reynolds and oscillatory stresses and transfer terms. All curves have been obtained by width averaging the corresponding fields over the  $-50 < X < 50$  mm range. Only the values for  $Z > 0$  are shown.

These curves confirm and complete the earlier observations. Oscillatory and Reynolds stresses are maximum in the core of the grid swept region, close to  $Z = 0$ . Oscillatory stresses decay much faster than the Reynolds stresses with increasing  $Z$ , and are negligible compared to the Reynolds stresses outside of the swept region, by at least a factor 10. For a given fluid and a given type of fluctuations, the vertical stress is always larger than the horizontal one. This is obviously because of the vertical grid displacement. This effect is all the more important for the oscillatory stresses which are directly due to this grid motion. The presence of polymer slightly increases the Reynolds stress value at the origin, but also the decay rate of the stresses with  $Z$ . In other words, DPS tends to concentrate the effects of turbulence in the swept region. As for the effect of polymer on the oscillatory component, it was previously observed that DPS solutions showed enhanced oscillatory structures outside of the swept region on the sides of the ROI. However this effect was found to be related

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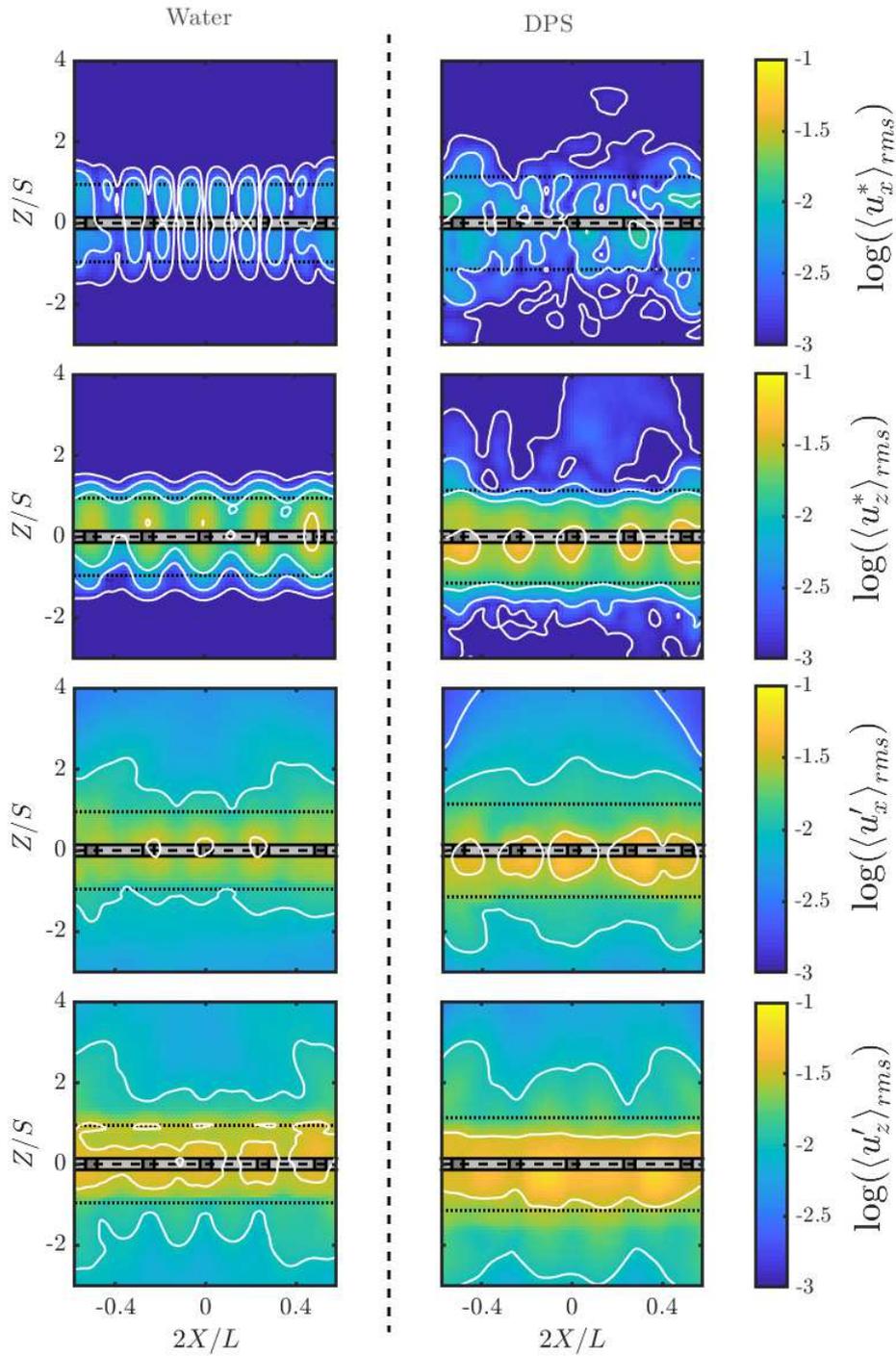


Fig. 9: RMS of oscillatory (lines 1 and 2) and turbulent (lines 3 and 4) velocity fluctuations along the horizontal (lines 1 and 3) and vertical (lines 2 and 4) directions, in water and DPS. Velocities are expressed in m/s and displayed in log scale. Isovalue lines are drawn in white full lines at log values of -3, -2.5, -2, -1.5 and -1 on each sub-figure.

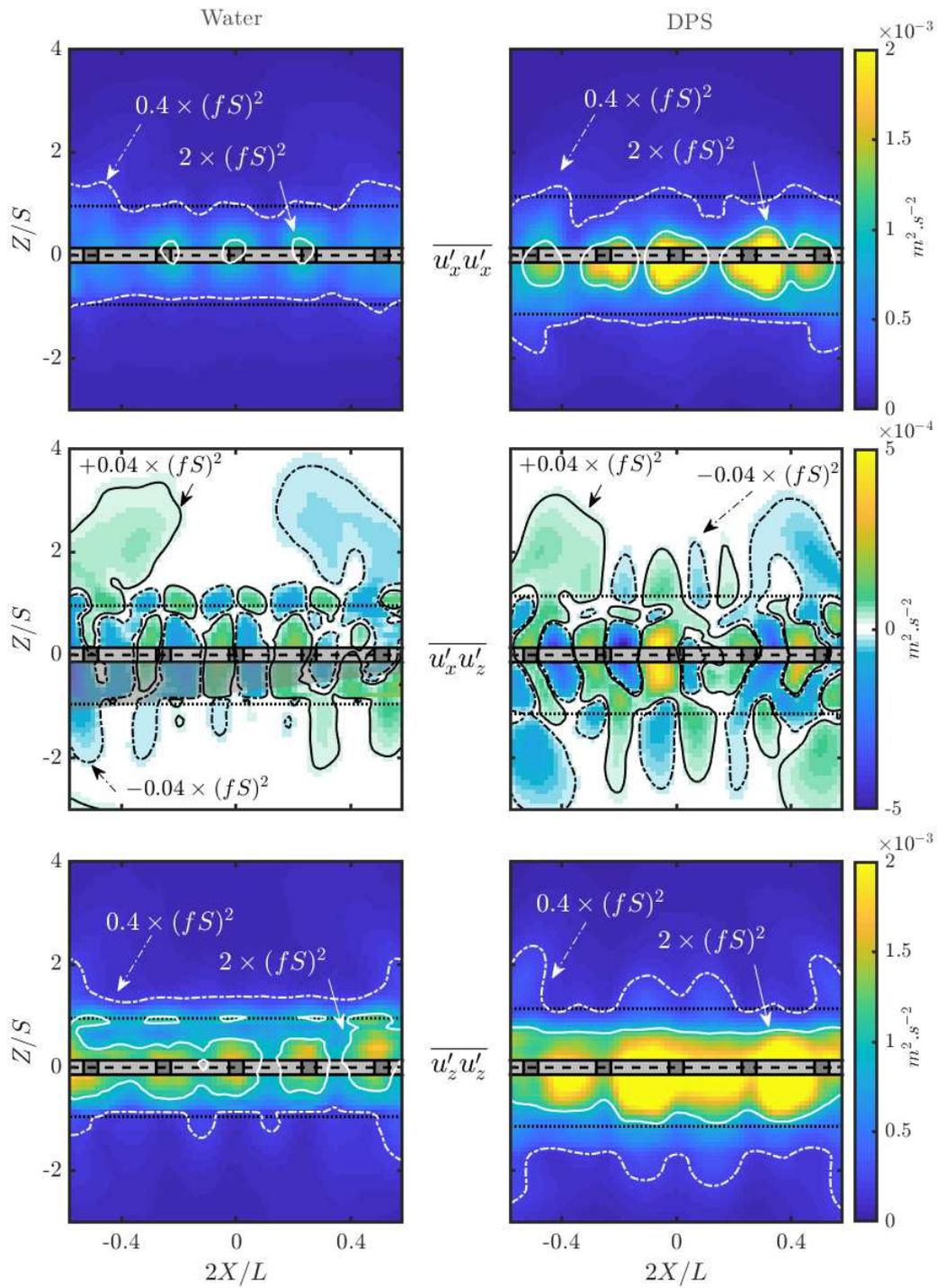


Fig. 10: Reynolds stresses in water and DPS. Isovalue lines are plotted in full or dashed-dotted lines and their values are indicated by arrows on the figure.

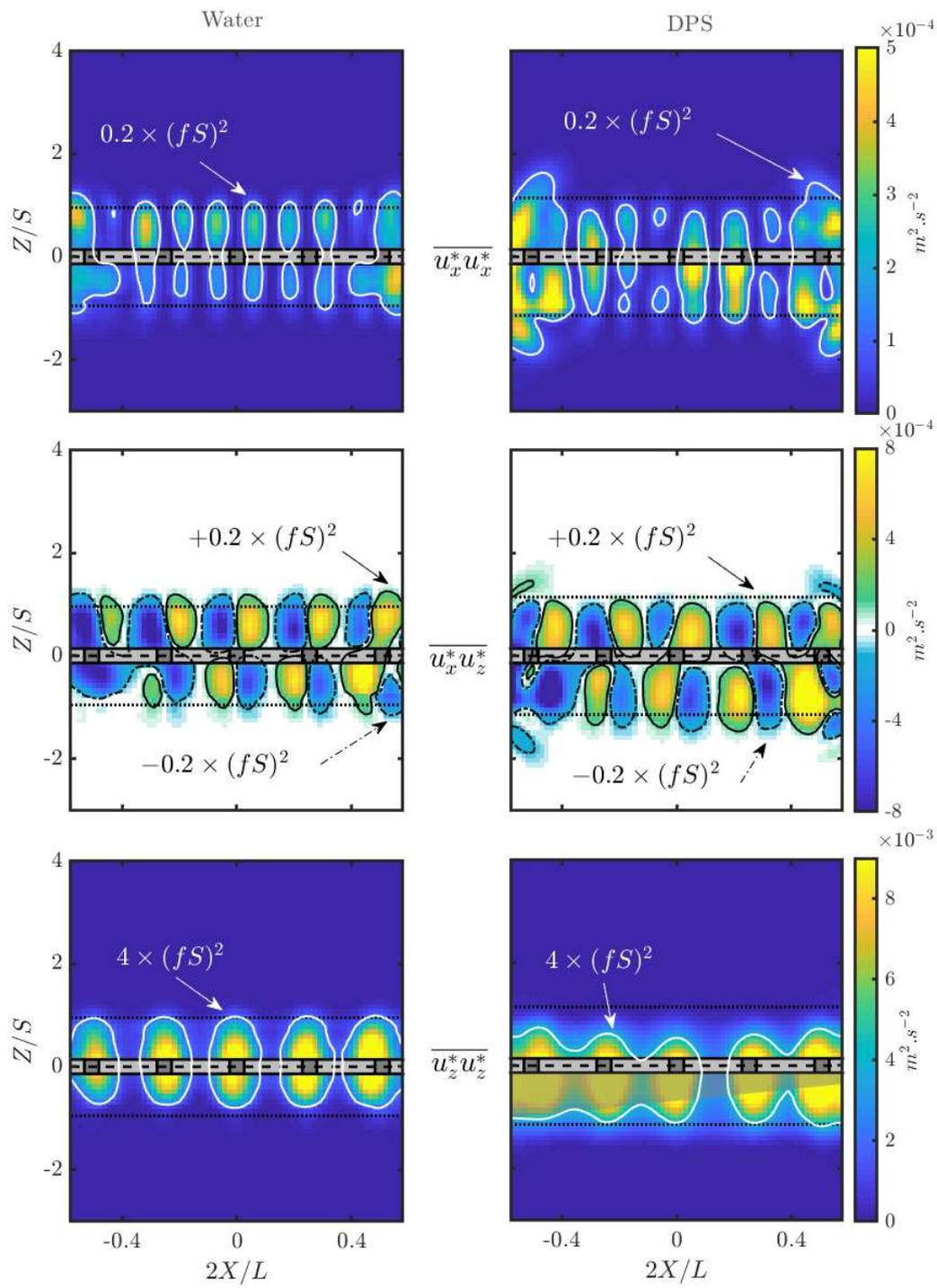


Fig. 11: Oscillatory stresses fields induced by the periodic velocity fluctuations in water and DPS. Isovalue lines are plotted in full or dashed-dotted lines and their values are indicated by arrows on the figure.

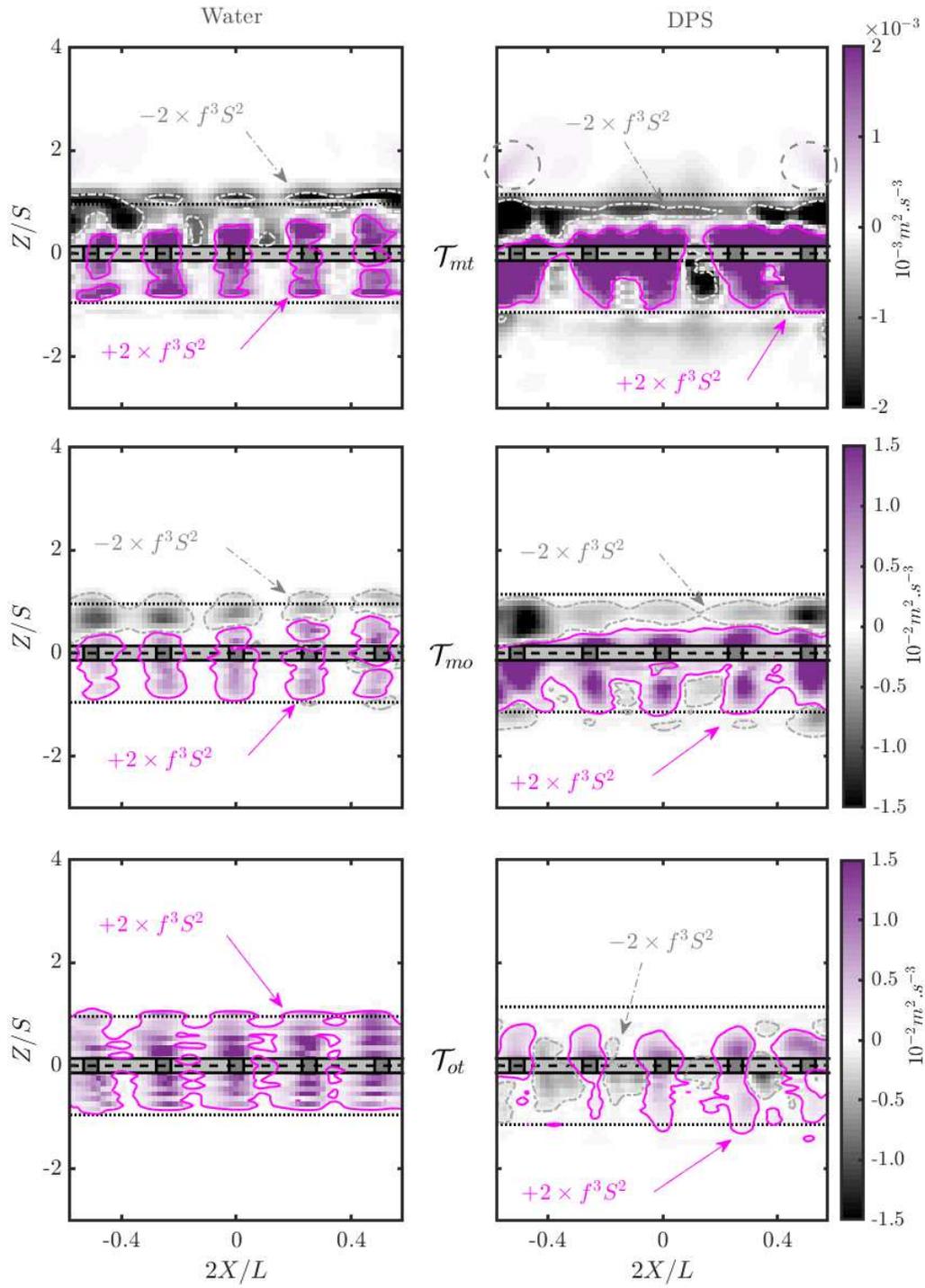


Fig. 12: Triple decomposition transfer terms  $\mathcal{T}_{mt}$  (mean to turbulent),  $\mathcal{T}_{mo}$  (mean to oscillatory or periodic) and  $\mathcal{T}_{ot}$  (oscillatory to turbulent) in water and DPS. Transfer terms are expressed in  $m^2 \cdot s^{-3}$ . Isovalue lines are plotted in full or dashed-dotted lines and their values are indicated by arrows on the figure.

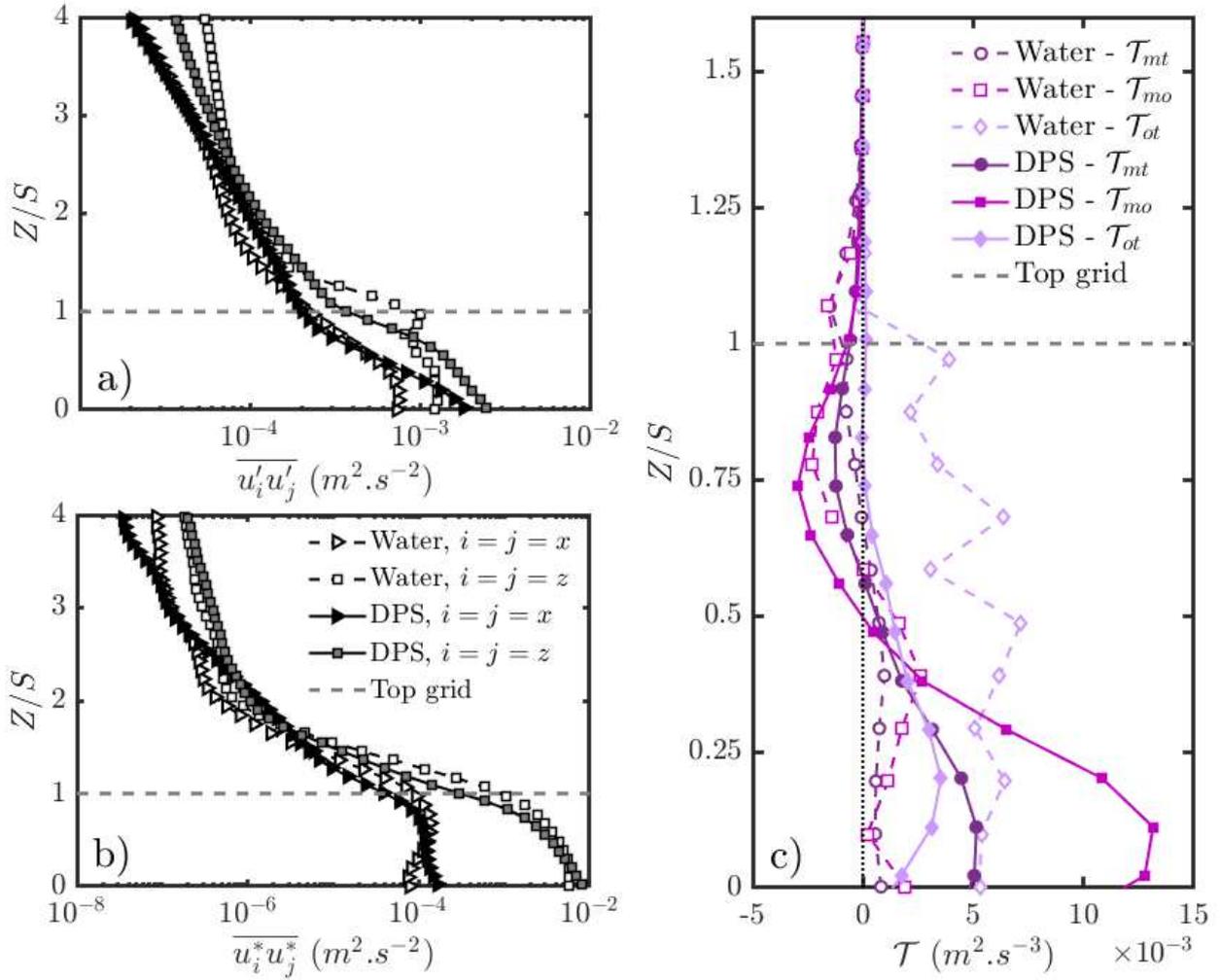


Fig. 13: Vertical profiles (width-averaged over the ROI) of a) Reynolds normal stresses, b) oscillatory normal stresses, c) transfer terms, for water and DPS.

to tangential stresses and not to normal ones, hence it is not visible on the  $\overline{u_i^* u_i^*}$  fields and on their vertical profiles.

As for energy transfers, the vertical variations of transfer terms is increased in DPS as compared to water in the swept region. This is supposedly due to both the enhancement of oscillatory and Reynolds stresses and to the spatial gradients of mean and oscillatory velocities. Such results suggest that gradient-based models could be good candidates at closure relationships for the estimation of these transfer terms. In the core of the swept region, all width averaged transfer terms are positive for water and DPS: energy is transferred from the mean and oscillatory flows to turbulence. At the edge of the grid swept zone,  $\mathcal{T}_{mo}$  and  $\mathcal{T}_{mt}$  profiles

become negative suggesting a feeding of the mean flow, that is further enhanced in DPS.

An important conclusion of the present work is thus that, outside of the grid swept zone, oscillatory, grid correlated, fluctuations quickly vanish in front of random turbulent ones with increasing  $Z/S$ . Despite its enhancement upon polymer addition previously mentioned, the oscillatory motion's intensity (quantified by the rms of oscillatory fluctuations, figure ??, or by oscillatory stresses, figure ??) is one to several orders of magnitude lower than turbulence intensity. This legitimates the use of the classical Reynolds decomposition outside the grid swept zone when working in a fixed, tank attached reference frame (as done in ?), since the oscillatory fluctuations can be assumed negligible there. However it must be kept in mind that any study

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presenting turbulence properties inside the swept zone from a classical Reynolds decomposition implicitly includes oscillatory motion into either mean flow or turbulent fluctuations.

#### 4.2.3 About mean flow generation

One of the key questions regarding OGT is the existence of mean flows, often an unwanted feature of the device. Its origin is most of the time attributed to misalignment or default in symmetry between the grid and the tank (?). ?, based on the older work by ? advance a possible source for the establishment of mean flow in the tank. They state that *mean flow is induced in OGT when there is a significant difference in the relative strength of the jets produced by the oscillating grid in different regions of the tank, and suggested the Coanda effect (applied on jets closest to the tank's wall) to be the dominant mechanism for this.* Indeed as argued by ?, jets close to the wall are necessarily non symmetric fashion, their growth being inhibited in the wall-normal direction. Compared to central jets, they should spread at higher grid distances in the wall-tangential, grid-normal direction, and consequently be less likely to merge with their neighbours. They are thus more likely to reach the outside of the grid swept zone and to give rise to a persistent flow on the sides of the tanks, resulting in the mean recirculation structures observed in several studies (????).

The previous description applies quite well in the present case, for both water and DPS: figure ??, ?? and ?? show that the side jets at  $|2X/L| > 0.4$  are significantly non symmetrical compared to central jets. This is correlated to persistent mean flow structures on the sides of the ROI at similar  $|2X/L|$  values (figure ??, first line). Moreover, figure ?? lines 3 and 4 shows that higher turbulent velocity rms values are reached in the trails of grid bars at the center of the ROI, compared to grid bars closer to the wall. The relative variation of jet strengths (in addition to the asymmetry) is thus also confirmed.

One striking results is that the addition of polymer seems to enhance the intensity of the mean flow. As previously mentioned, side vorticities seem stronger in DPS than in water, and accompanied in DPS only by an enhanced up-going motion above the swept zone. Looking back at figures ??, ??, ?? and ??, one sees that all the features characteristic of mean flow production as described by ? and ? are even more obvious and enhanced in DPS compared to water. Asymmetry of the side jets is enhanced, and jets at the center of the tank have even higher intensities with respect to the side ones when considering rms fields (figure ??).

The description of the mechanisms of mean flow production by ? thus seems to hold in water and DPS, since an enhancement of jet asymmetry and intensity variations leads to a stronger mean flow. This yet does not explain *why* asymmetry and relative intensity variation is enhanced in DPS. We infer that in DPS, the Coanda effect should also be accompanied by shear-thinning variable viscosity actions. Indeed, jets close to the walls are in a region for which the fluid is submitted to a sustained high shear rate. The imposed velocity gradient is strong since the grid forces a periodic velocity, the velocity at the wall is nil and the variations between the two boundary constrained velocities happen within the very small gap between the grid and the wall (typically 1 mm here between the edge of a grid bar and the wall). Since the shear rate is high, viscosity should be low in this region. However when moving away from the walls, the imposed periodic shear rate is decreased and viscosity thus increases. The consequence is that side jets are inherently coupled with an horizontal viscosity gradient, increasing their asymmetry and the non horizontally homogeneous repartition of intensities in the jets. Such a behaviour would thus tend to enhance mean flows as described by ? and ?.

Additional information can be brought to this mechanism by the present data, regarding the distance from the grid at which mean flow enhancement occurs. Indeed, figure ?? shows the profiles of width averaged energy transfer terms  $\mathcal{I}_{mo}$ ,  $\mathcal{I}_{mt}$  and  $\mathcal{I}_{ot}$ . Considering that the energy inputs, by the grid, are made towards the oscillatory component, mean flow production should thus be a consequence of energy transfers from oscillatory motion to mean flow, evidenced by negative  $\mathcal{I}_{mo}$  values. This is achieved in the  $0.5 < Z/S < 1$  region, *i.e* inside but at the outer part of the grid swept zone in both water and DPS. In the DPS case, the  $\mathcal{I}_{mo}$  reaches more negative values, confirming and enhanced mean flow production. Moreover, one notices that in the water case, the  $\mathcal{I}_{ot}$  term is always positive, and significantly higher than in the DPS case. This means that in water, most of the energy input at the oscillatory level is used to generate turbulence, and only a smaller part of it creates mean flow:  $|\mathcal{I}_{ot}/\mathcal{I}_{mo}|$  is typically equal to 1.5 at  $Z/S = 0.75$ . In DPS, a more significant part of the oscillatory energy is transferred to the mean flow:  $|\mathcal{I}_{ot}/\mathcal{I}_{mo}|$  falls to 0.03 at the same altitude <sup>2</sup>.

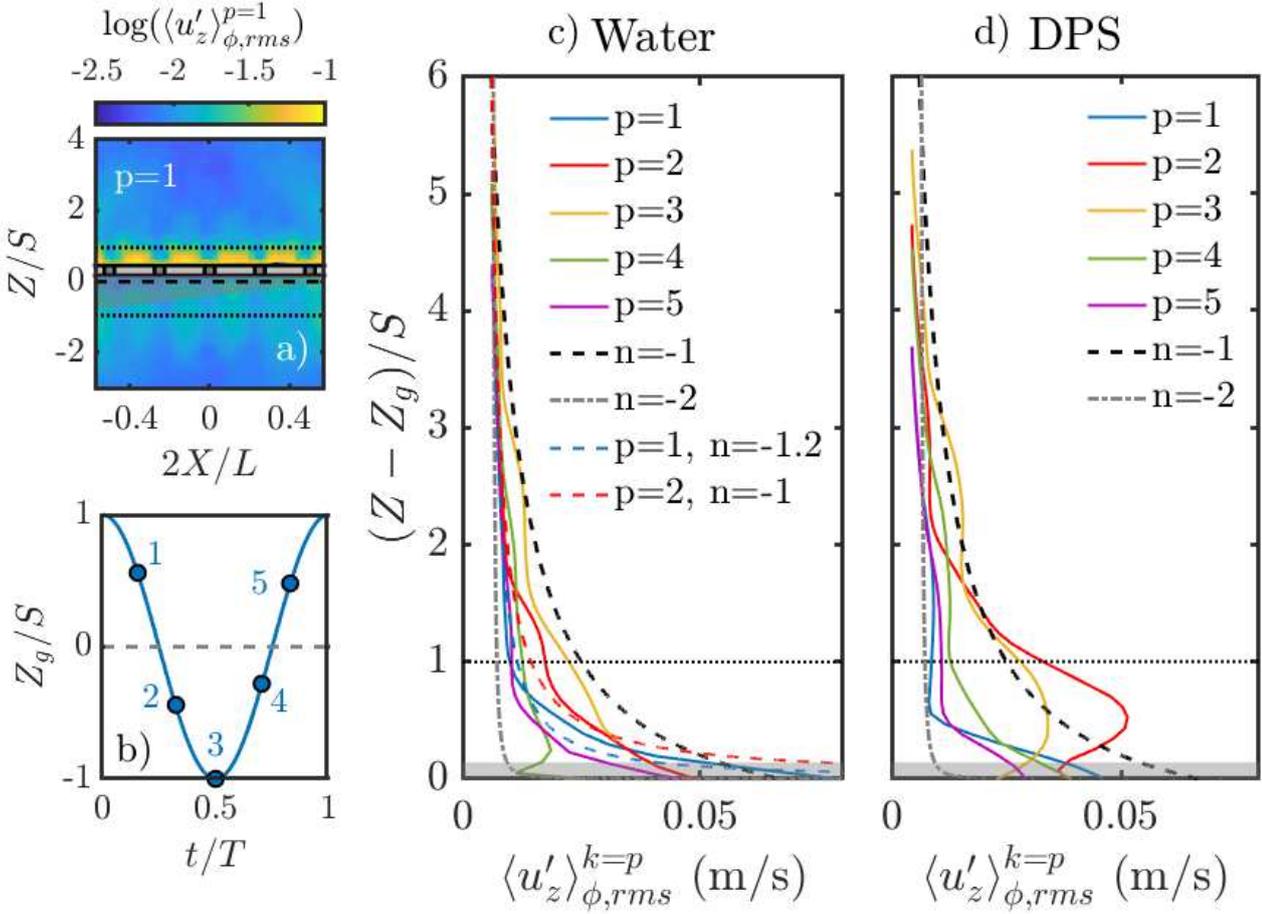


Fig. 14: Phase rms of velocity fluctuations. a) Phase rms field for the vertical velocity fluctuation  $\langle u'_z \rangle_{\phi, rms}^{k=p}$  at sketch position index  $p = 1$ , in log color scale. b) Sketch of the sampled grid positions numbered 1 to 5. c) and d) Profiles of phase rms plotted as a function of the instantaneous grid distance normalized by the grid stroke  $(Z - Z_g)/S$  for respectively water and DPS, at the 5 sampled positions sketched on subfigure b). The dashed black line and dashed-dotte gray line illustrate respectively  $(Z - Z_g)^{-1}$  and  $(Z - Z_g)^{-2}$  trends. Dashed color lines on sub-figure c) are least square fittings of  $p = 1$  and  $p = 2$  curves by power laws. The grayed region represents half the width of the grid bar along  $(Z - Z_g)/S$ .

### 4.3 Phase turbulence

Another way to describe the periodicity of turbulence property is to compute rms values of velocity fluctuations not on the full set of data, but for each specific grid position. Such so-called phase rms  $\langle u'_z \rangle_{\phi, rms}^k$  are defined at equation ???. An example of phase rms field for water for a given grid position is given in figure ?? a), the log-scaled colorbar representing the magnitude of  $\langle u'_z \rangle_{\phi, rms}^{k=p=1}$  in m/s. One can clearly evidence the wake of the grid by high turbulent intensity patches. We should

stress that the following analysis is not performed in the global Eulerian frame of the tank, for which oscillatory flow has already been considered through non-phased rms of oscillatory fluctuations, or oscillatory stress fields. This time, we are looking at oscillatory flow in a grid-attached Eulerian frame: the oscillatory aspect of the flow is intrinsically accounted for by defining turbulence based on the grid position.

It is interesting to notice that the higher turbulent intensity regions are found to correspond to grid holes. Previously, it was observed that normal Reynolds stresses (figure ??) and non-phased rms fields (figure ??) where maximal above grid bars. Tangential Reynolds stresses were themselves maximal above grid

<sup>2</sup> The consequence of this enhancement in terms of mean flow properties is described in ?, for various polymer concentrations

holes. Here we understand that for a given grid position, turbulence is high where the wakes of grid bars meet, *i.e.* in the jets behind the holes. In this region, both vertical and horizontal fluctuations are found since structures are the result of a lateral collision of structures, advected by the oscillatory trailing vortices shown in figure ?? . This thus explains the mapping of tangential Reynolds stresses. Vertical Reynolds stresses, as for rms of  $u'_z$ , are maximal in the region where turbulence production is the result of vertical sweeping by bars only.

In the rest of this paragraph, five different sampling grid positions are considered (already used in figure ?? for the visualisation of a typical vorticity phase). They are represented on a grid period in time and space in figure ?? b). Position 1 correspond to a grid accelerating downwards, position 2 to a grid still going downwards, but decelerating. Position 3 is the extreme low position at  $Z = -S$ , where the velocity is nil and the acceleration maximal and oriented upwards. Positions 4 and 5 are for the grid going upwards and respectively accelerating and decelerating. For each grid sampling position  $k = p$ , phase rms fields are averaged over the horizontal dimension  $X$ . The width-averaged profiles of  $\langle u'_z \rangle_{\phi, rms}^{k=p}$  are plotted versus the instantaneous distance from the grid  $Z - Z_g$  normalized by  $S$  in figure ?? c) (water) and d) (DPS).

For almost all grid positions and for the two fluids considered (except  $p = 2$  and  $p = 3$  in DPS as discussed later), rms profiles roughly follow power law decay trends such that  $\langle u'_z \rangle_{\phi, rms}^p \sim (Z - Z_g)^n$ . All curves are included inside an envelope defined by  $n = -2$  and  $n = -1$  trends. The  $n = -1$  value happens to be the usual exponents of the decay law for oscillating grid turbulence evidenced by ? when plotting non phased rms profiles of  $\langle u'_z \rangle_{rms}$  as a function of the dimensional  $Z$ . We see that here, once phased to the grid motion, the decay profiles of each grid positions has a  $n$  value lower than -1, but higher than -2.

In water, one could probably expect that when phasing turbulence with the grid position, the decay exponents characteristic of fixed grid turbulence could be retrieved for well chosen grid positions. Indeed, one can consider an Eulerian description on the flow in a reference frame attached to the grid and no longer to the tank. When the grid is going down (respectively up), the configuration for each grid position that of a fixed grid with flow passing through in the  $+Z$  (respectively  $-Z$  direction), with a relative fluid velocity equal to the grid's velocity. For fixed grids, ? and many more recent works (listed in ?) evidenced decay exponents for the turbulent kinetic energy in the  $[-1.4, -1]$  range. For the streamwise velocity fluctuations considered here, this should yield decay exponents in the  $[-1.2, -1]$  range.

Here curves for position  $p = 1$  and  $p = 2$  in figure ?? c) correspond to the situation analog to that of a fluid flowing upwards through a fixed grid, and should be comparable to fixed grid scaling laws. They are fitted by expressions of type  $\langle u'_z \rangle_{rms} = a * (Z - Z_g)^n$ . Values of  $n$  obtained for  $p = 1$  and  $p = 2$  are respectively equal to -1.2 and -1, with a better fitting for  $p = 1$ .

This phase analysis suggests that original mechanisms of turbulence generation by the oscillating grid are in fact quite comparable to those behind a fixed grid in a mean flow, at least as a first approximation: a grid moving in a fluid quite logically generated turbulence in a similar fashion that when a fluid moves across a fixed grid. Yet the fundamental difference between the two setups is that turbulent structures generated at previous grid positions are still present in the flow at following grid positions and may interact with the newly generated structures. This is one of the possible reason why the fitting for the  $p = 2$  position is less efficient, and why the decay exponent varies between -1.2 and -1. Indeed, for  $p = 1$  most of the  $Z - Z_g > 0$  region lays outside of the grid swept zone, while for  $p = 2$ , low  $Z - Z_g$  values are found inside this grid swept zone, when pre-existing turbulent structures interact with the  $p = 2$  jets and wakes.

All of the above is valid for water. When considering DPS (figure ?? d)), the first observation is that profiles no longer follow single exponent power law trends, at least in the vicinity of the grid. For  $p = 1$  and  $p = 5$ , a two-slope trend is visible with a change of slope at  $(Z - Z_g)/S \simeq 0.5$ . For  $p = 2$  and  $p = 3$ , a peak of  $\langle u'_z \rangle_{rms}$  is observed at the same scaled distance. This shift in decay rate concerns top grid positions, and evidences a boundary between high turbulent intensity, near grid region and the rest of the flow above the swept zone that for grid positions. The second behaviour, namely the rms peak, is characteristic of a turbulent patch shedding by the grid: at bottom grid positions ( $p = 2, 3$ ) and with a grid going down, previously generated turbulent structures are advected away from the grid by the hole jets. Since the grid is slowing down ( $p = 2$ ) or even stopping ( $p = 3$ ), turbulence generation is less efficient and up-going turbulent patches break away from the near-grid region. This is no longer observed for ( $p = 4$ ) since the grid is going up and *catches back* on the shed turbulent patches. We thus see again an enhanced importance of flow periodicity in term of turbulence generation for the DPS case.

It is worth mentioning that this phase rms study can be another way of describing the periodicity of the flow induced by the grid. It is here addressed not in terms of periodic flow structures produced, but as a periodic behaviour of turbulent properties. Figure ??

shows that if this periodicity of turbulence is significant in the swept zone (see sub-figure a as an illustration), it reduces when moving away from the grid, as evidenced by the asymptotic collapse of all curves for  $(Z - Z_g)/S > 3$ . This seems to indicate that outside of the grid swept zone, turbulent properties are also not periodic. However, clearer evidence could be brought by performing time resolved measurement of turbulence generated by the grid and studying the temporal periodicity of correlation functions of turbulent correlations to themselves (or turbulent time-scales) in the Eulerian tank-attached frame.

#### 4.4 Viscosity estimation and statistics

A fast approach for studying polymer influence on the origins of OGT is an estimation of the local viscosity field and its statistics. The main idea is to derive local shear rate fields from instantaneous, phase averaged or time averaged velocity fields. Local shear rate values are then used to estimate an apparent viscosity through the constitutive equation of the polymer, here a CY law for the rheological behaviour derived in section ?? (equation ??, figure ??).

This method is limited because the velocity data is only 2D and lacks the third velocity component. Shear rate values can thus only roughly approach the real local shear rate, and no precise quantitative study can be performed. However the method allows to qualitatively estimate the viscosity variations in a plane of measurement.

In practice, the apparent instantaneous shear rate is computed as

$$\dot{\gamma}_{app} = \sqrt{\left(\frac{\partial U_x}{\partial z}\right)^2 + \left(\frac{\partial U_z}{\partial x}\right)^2} \quad (18)$$

an the instantaneous apparent viscosity as

$$\mu_{app} = f_{CY}(\dot{\gamma}_{app}) \quad (19)$$

with  $f_{CY}$  the Carreau-Yasuda function defined in equation (??), and using fitting parameters obtained in section ?. Statistics for viscosity are then obtained by ensemble averaging over the whole set of field for  $\bar{\mu}_{app}$ , or grid position by grid position for  $\mu_{app}^*$  exactly like what is done for the velocity field.

Figure ?? shows the fields of ensemble average viscosity  $\bar{\mu}_{app}$ , ensemble rms of turbulent viscosity fluctuations  $\langle \mu_{app}' \rangle_{rms}$  and fields of maximum and minimum viscosity values over time  $\mu_{app,max}$  and  $\mu_{app,min}$ . All values are scaled by the  $\mu_0$  maximum viscosity.

Estimating the uncertainty on instantaneous viscosity field is quite arduous since one would need to

know the uncertainty on instantaneous velocity fields and instantaneous local shear rates. However, another approach can be used to evaluate the error associated to this viscosity estimation process. From statistical convergence analysis (see figure ??) we estimate the uncertainty on velocity statistics convergence to be at worst of 5%. Uncertainty propagation on velocity gradient and shear rates can be performed to quantify the resulting relative uncertainty on apparent shear rate, which may be up to 30%. From this value, the CY law (equation ??, figure ??) can finally be used to assess uncertainty on calculated apparent viscosity at each shear rate value. This last uncertainty is maximal when the slope of the curve in figure ?? is the steepest, i.e at the lowest effective flow index (as defined in ?). This is here the case for shear rates around  $4 \text{ s}^{-1}$ . At this worst-case shear-rate, the relative uncertainty of apparent viscosity is found to be 14%.

The first sub-figure of figure ?? shows that average viscosity is minimal close to  $Z = 0$  inside the swept grid region. It then increases when moving away from  $Z = 0$  until it reaches its zero shear rate plateau value at  $Z/S > 3$ . The maximum of rms velocity fluctuations is found just above the grid's top and bottom positions, around  $X = 0$ . Here the viscosity varies from a value close to its zero shear rate plateau when the grid is on the other side of its stroke, to a much lower value when the grid departs from this position and releases high shearing eddies. Vertical trails of high viscosity rms are also observed in regions associated to grid holes. Since this plot represents the rms of turbulent viscosity fluctuations, it means that these trails are not due to oscillatory motion, but rather to strong fluctuations of the shear rate fields because of turbulent structures in those regions. The central high viscosity fluctuation path in the  $X = 0 \text{ mm}$ ,  $Z/S = 1.5$  region confirms the existence of preferential paths for turbulence. Turbulent fluctuations are more likely to be found at the center of the ROI above the swept zone. The minimum viscosity fields shows that viscosity is always higher than the infinite shear rate viscosity, which means that during the experiments, no shear rate (mean, oscillatory or turbulent) is high enough for the fluid to behave like a low viscosity Newtonian fluid, even locally. Finally, the maximum viscosity field shows that almost everywhere in the fluid, the maximum viscosity value may be reached at a time, i.e that almost everywhere in the fluid, at some time, the shear rate is almost nil. The only locations where this is not the case are just above the grid swept region. Here lower maximum viscosity patches are found which correspond to the shape and location of the mean flow vortices.

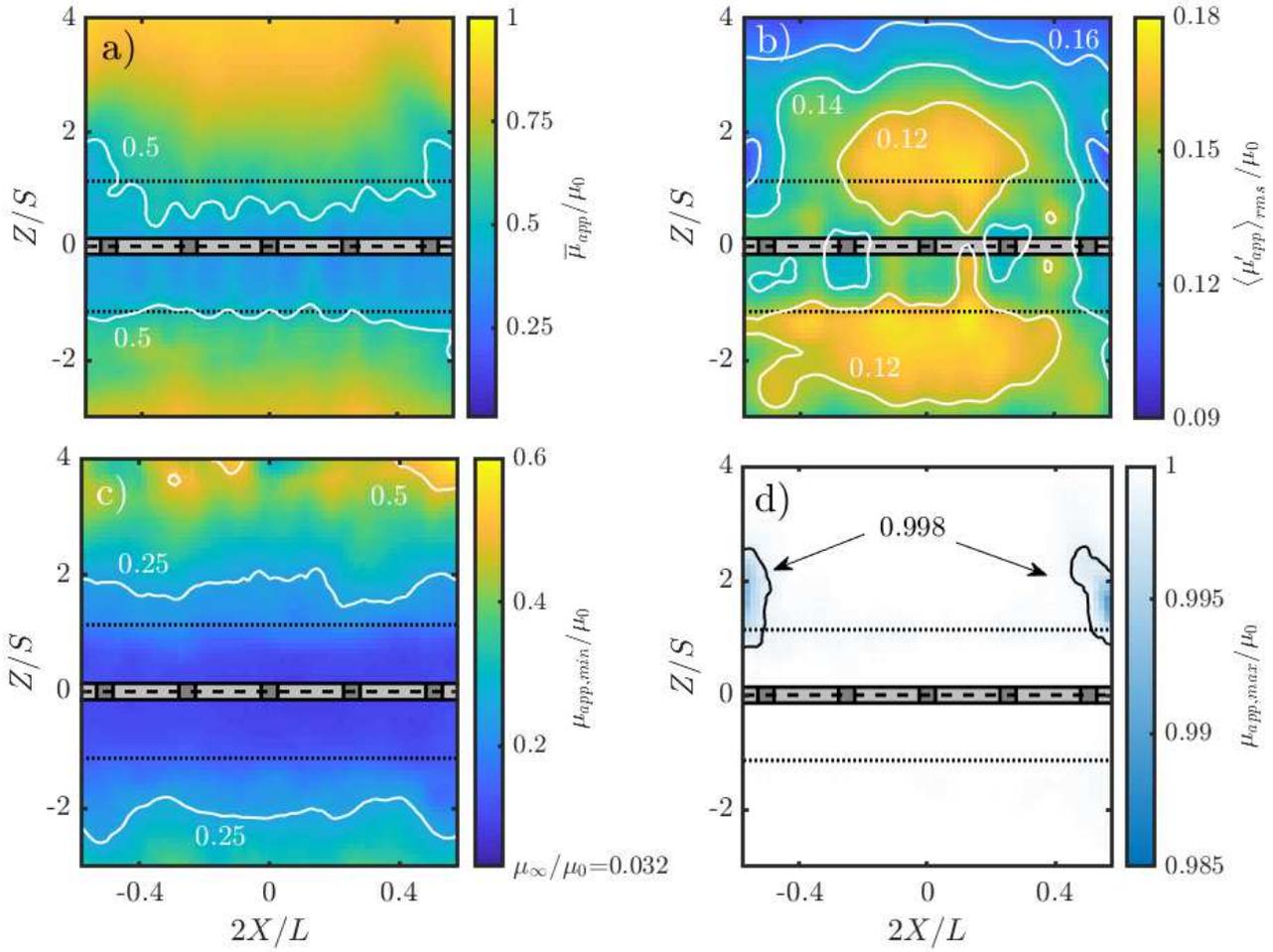


Fig. 15: Local statistics of apparent viscosity: average (a), rms of turbulent fluctuations (b), minimum (c) and maximum (d). The zero shear rate viscosity in 100 ppm XG solutions is 32.78 mPa.s and the infinite shear rate viscosity is 1.05 mPa.s. Isovalue lines are represented by full lines on each sub-figures, with values indicated nearby.

## 5 Conclusion

In this last section, the main conclusions are summarized, first the key features of the flow around a grid oscillating in water are described. The effects of polymer addition are summarized in a second paragraph. Finally the generalisation of the present results and perspectives for future works are discussed.

### 5.1 OGT in water

The grid periodic motions create oscillatory vortices behind the grid bars. At the walls (on both sides of the ROI), these periodic, non symmetric vortices feed the large mean flow eddies. Oscillatory component is strong within the grid swept region, but quickly vanishes when moving away from the grid's action. This suggests that a classical Reynolds decomposition can

equally be used to describe turbulence properties in the bulk flow. Turbulence is created mostly by oscillatory flows in the swept region. It is highly anisotropic, with a much higher intensity along the vertical direction, as imposed by the grid motion. When turbulent intensity is computed in phase with the grid position, its decay law with the distance to the grid can be compared to fixed-grid correlations for well chosen grid positions. The global mechanisms of turbulence and mean flow production by the oscillating grid is the following: the grid introduces turbulence in the oscillatory fields, which transfers energy to the mean flow and to turbulence.

### 5.2 Effects of polymer addition

Polymer addition has several effects on the flow structure and energy exchanges around the grid. The first

one is an enhancement of the oscillatory flow on the sides of the ROI near the walls. This leads to a periodic vortex shedding that feeds the mean recirculation and increase its intensity, thus possibly explaining the mean flow enhancement. The second effects is a modification of the spatial distribution of turbulence. Reynolds stress and turbulence intensity are increased in the core of the swept region close to  $Z = 0$ , and decrease quicker with increasing  $Z$  magnitude. Turbulence is enhanced at the center of the ROI (far from the walls), both in the swept region and far from the grid. Finally, the transfer from oscillatory to turbulent fluctuations seems more complex in DPS than in water, and suggests that oscillatory motion may locally both give and take energy from turbulence, which was not the case for water. Another visualisation of the same phenomenon was made possible by an estimation of viscosity from PIV measurements and its statistical analysis.

### 5.3 Perspectives

It is worth reminding that a limitation of the previous analysis is the fact measurements are planar and do not account for the highly three-dimensional behaviour of turbulence. Results may be different when considering for example a plane of measurement not coincident with a grid bar, but with a set of grid holes, (*i.e.* translated of  $M/2$  in the  $Y$  direction, see figure ??). With similar 2D PIV measurements in additional planes, and under a specific set of symmetry hypothesis, it would be possible to estimate kinetic energy budgets along  $Z$  directions at specific  $X$  and  $Y$  values, and go further in the modelling of transfer terms and turbulence production. However, three dimensional three component measurements of the velocity fields would ultimately be required to measure the total energy transfer terms, or the actual local viscosity mappings. Being now confirmed that the spatial heterogeneity of oscillatory flow is a possible cause of mean flow generation, and that this heterogeneity is induced by spatial confinements effects, further study of the influence of this confinement (e.g. through the  $M/L$  ratio) on the flow would be of great interest.