

# High amplitude/high frequency acoustic field effects on coaxial inkection

J.B. Blaisot, Antonio Ficuciello, Christine Richard, Marie Théron, Françoise

Baillot

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# High amplitude/high frequency Cnes acoustic field effects on coaxial injection



# 1. Introduction

High-frequency thermoacoustic instabilities are one of the biggest issue limiting liquid rocket engines (LREs) reliability.

Pressure fluctuations produced by combustion can couple with the resonant mode of the combustion chamber, leading to the modulation of the local instantaneous rate of the heat release.

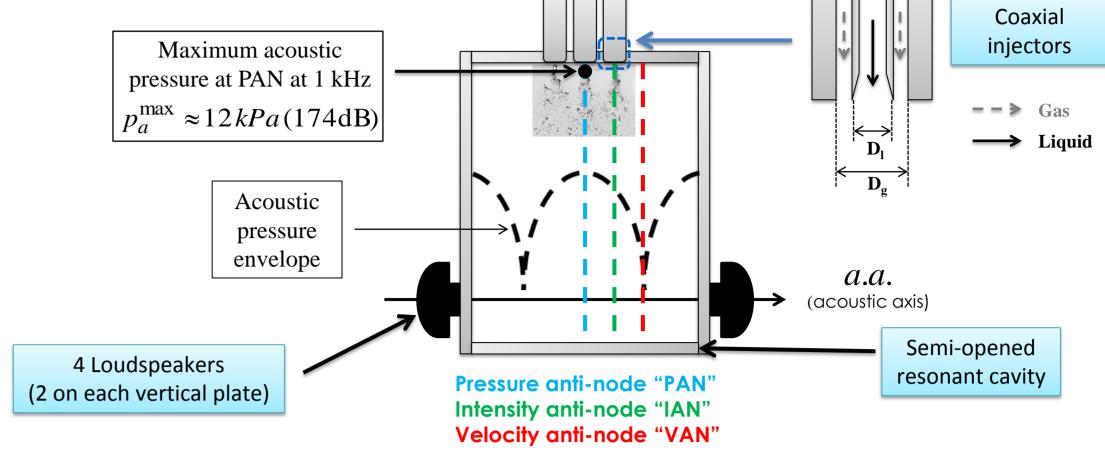
Despite many years of research, the understanding and the capacity of predicting combustion instabilities are still limited. Due to the complexity and multiplicity of the processes involved, a global approach cannot identify the dominant mechanisms and a local approach is needed.

# 2. Objectives

- Investigation of **air-assisted liquid jets response** to the acoustic perturbation
- Validation of a theoretical model based on non-linear acoustics describing jet dynamic

# 3. Experimental setup and acoustic field

- Semi-opened resonant cavity + compression drivers to reproduce acoustic field similar to what can be found in a combustion chamber
- The acoustic field can be approximated as the 2<sup>nd</sup> transverse mode of the resonant cavity.



# 4. Air-assisted jets response to the acoustic field

Jet response depends on the position in the acoustic field

## **NO EFFECTS AT PAN**

## **JET DEVIATION AROUND IAN** Low Weber - $We_g = 9$ High Weber - $We_g > 100$ with ac with ac w/o ac w/o ac o o oWe = 262 - Re = 3900**0.07** \* \* We = 104 - Re = 3900• • • We = 225 - Re = 2500 $\cdots$ Exponential fitting 0.05 \_\_\_\_\_ 0.04 ب<sub>n</sub> 1 0.03 0.02 0.01 10 000 12 000 14 000 8 000 $p_a [Pa]$ See theoretical model in §5 $\widetilde{\mu}_m$ : droplet spatial distribution mean value **ATOMIZATION PROCESS IMPROVEMENT AROUND VAN** Low Weber - $We_{o} = 9$ High Weber - $We_g > 100$ with ac with ac w/o ac w/o ac - - - B $PR = N_{d,ac} / N_{d,0}$ 47.1° 76.9° Position Membrane Fiber $(We_g = 100, Re_l = 2200)$ $(We_g = 220, Re_l = 2500)$

Anti-node: spatial location where the amplitude of fluctuations of the considered acoustic quantity (e.g. pressure, velocity or intensity) is maximum.

# 5. Theoretical model

**Nonlinear acoustic** model for cylindrical or spherical objects based on:

- **Radiation pressure** distribution:
- Radiation force effects:

on:  

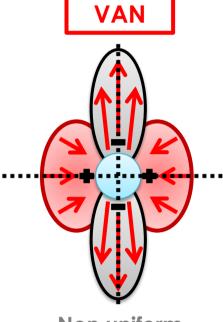
$$P_{rad} = \frac{\left\langle p_a^2 \right\rangle}{2\rho_g c^2} - \frac{\rho_g}{2} \left\langle \substack{\rho, \rho' \\ u u} \right\rangle$$

$$\int_{F_{rad}}^{\rho} F_{rad} \cdot \stackrel{\rho}{ndS} = Gf(\eta) \frac{p_a^2}{4} \sin 2kh e^{\rho}$$

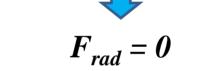








Uniform distribution of p<sub>rad</sub> acts like a pressurized environment



Model validation

**NO DEVIATION NO DEFORMATION** 



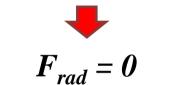
 $F_{rad} \neq 0$ 

DEVIATION

AND

DEFORMATION

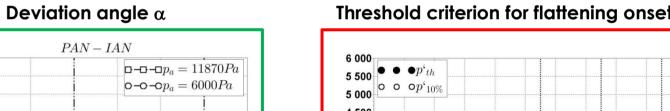
Non uniform distribution of p<sub>rad</sub>



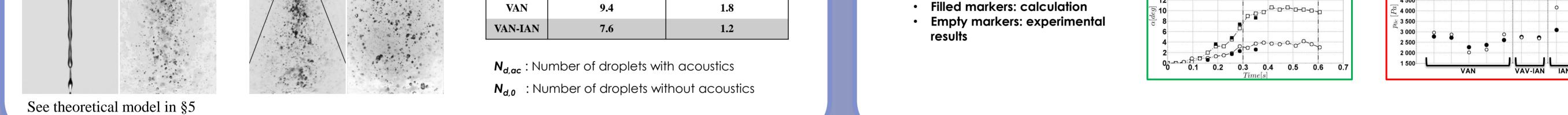
**NO DEVIATION** DEFORMATION



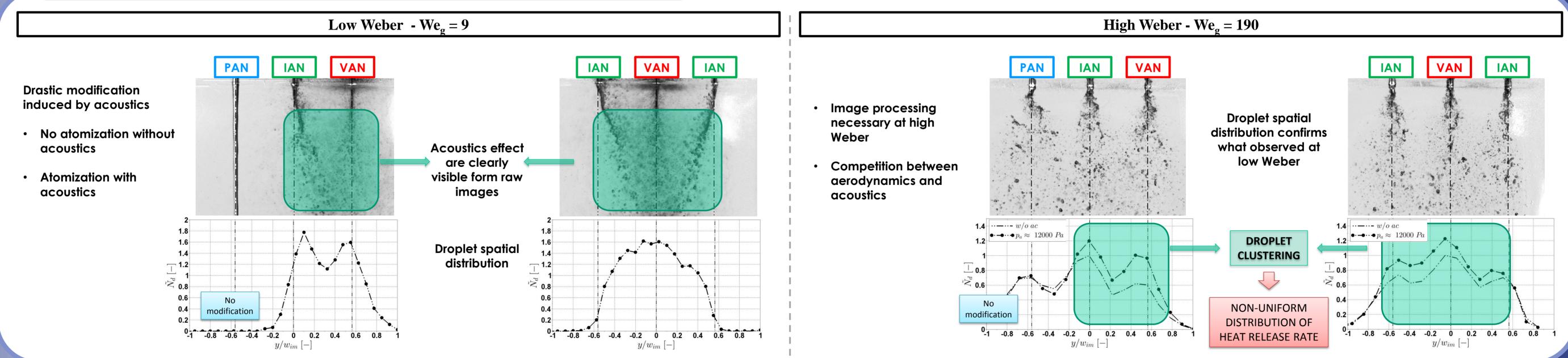
12



6 000			 
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# 6. Droplet spatial distribution: clustering effect



## 7. Conclusions

• Acoustics can drastically affect jet dynamics according to the position of the injector w.r.t. the acoustic field.

Two main phenomena have been observed:

• An intensification of the atomization process, particularly strong at VAN;

Droplet clustering in the region

• A deviation toward the velocity anti-node, nearby IAN.

around IAN and VAN

□ Theoretical model based on radiation pressure and radiation force distribution well describe jet behavior.

> The model must be completed to take into account different object geometries and the energy balance between flattening and deviation.

# References

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<sup>1</sup> Normandie Université, UNIROUEN, INSA Rouen, CNRS, CORIA, 76000 Rouen, France <sup>2</sup> LMRS, UMR 6085, CNRS-Université de ROUEN, BP 12, 76801 Saint Etienne du Rouvray, France <sup>3</sup> CNES Launchers Directorate, 52 rue Jacques Hillairet, 75612 PARIS Cedex, France

