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# Enhanced thermal sensitivity of MEMS bolometers integrated with nanometer-scale hole array structures

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## ABSTRACT

We have fabricated two-dimensional nanometer-scale hole array structures on GaAs doubly-clamped microelectromechanical system (MEMS) beam resonators to modulate their thermal properties. Owing to the reduction in the thermal conductance of the MEMS beams by introducing the hole array structures, the nano-porous MEMS bolometers show 2-3 times larger thermal sensitivities than the unpatterned reference sample. Furthermore, since the heat capacitance of the MEMS beams is also reduced by introducing the hole array, the thermal decay time of the patterned MEMS beams is increased only by about 30-50%, demonstrating the effectiveness of the hole array structures for enhancing the thermal sensitivities of bolometers without significantly deteriorating their operation bandwidths.

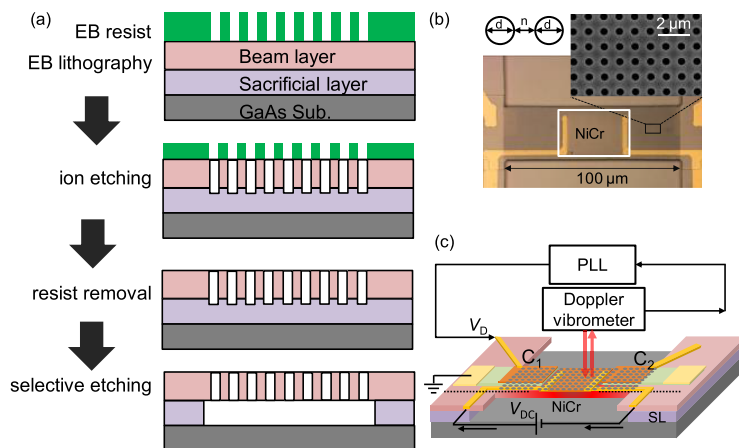
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Micro-electromechanical system (MEMS) resonators<sup>1-3</sup> are very attractive for sensing applications. Owing to their high quality (Q)-factors, the MEMS resonators can detect a small change in the resonance frequencies and can be used to detect changes in mass,<sup>4-8</sup> charge,<sup>9,10</sup> spin orientation,<sup>11,12</sup> and temperature.<sup>13,14</sup> Recently, we have developed an uncooled, sensitive and fast bolometer by using a doubly clamped GaAs MEMS beam resonator for terahertz (THz) sensing applications.<sup>15-17</sup> The MEMS resonator detects THz radiation by measuring the shift in the resonance frequency caused by heating of the MEMS beam.<sup>15-17</sup> Since the responsivity of the MEMS resonators is inversely proportional to the thermal conductance of the MEMS beam,  $G_T$ , it is preferable to decrease  $G_T$  for enhancing the responsivity. On the other hand, the thermal time constant  $\tau_D$  ( $= C_T/G_T$ ;  $C_T$  is the heat capacitance of the MEMS beam) increases when  $G_T$  is decreased, leading to the reduction in the detection speed. This trade-off between the

responsivity and the detection bandwidth exists in all kinds of thermal sensors.

Nano-porous structures such as slabs with one-dimensional (1D)<sup>18</sup> or two-dimensional (2D)<sup>19-21</sup> hole arrays have been proposed to engineer the thermal properties of materials. The hole array structures are promising for improving thermal responsivities of the MEMS resonators; the hole array structure can reduce the thermal conductance,  $G_T$ , of the MEMS beam by decreasing the cross section of the beam. Furthermore, the hole array structure reduces the heat capacitance of the beam,  $C_T$ , by decreasing the material volume. Therefore, the increase in  $\tau_D$  due to the decrease in  $G_T$  is partly compensated by the reduction in  $C_T$  and it is possible to enhance the thermal responsivity, while keeping a fast detection speed of the MEMS thermal sensors.

In this work, we have fabricated 2D nanometer-scale hole array structures on the MEMS beam resonators to modulate their thermal



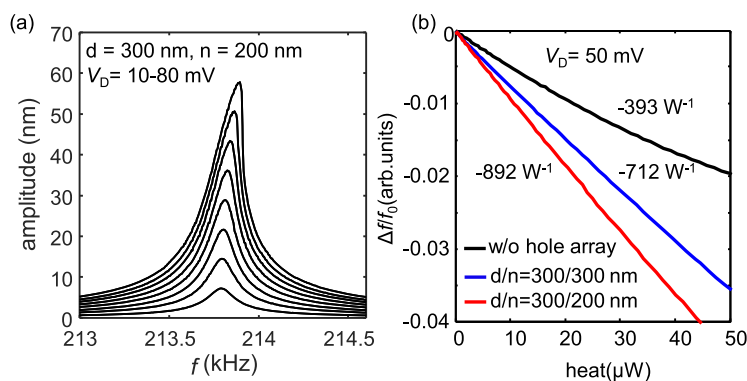
**FIG. 1.** (a) Fabrication processes of a MEMS resonator with a hole array structure. (b) Microscope image of a fabricated GaAs MEMS beam resonator ( $100 \times 30 \times 0.6 \mu\text{m}^3$ ) with a 2D hole array structure of a hole diameter  $d = 500 \text{ nm}$  and a neck size  $n = 500 \text{ nm}$ . The Si-doped GaAs layer and the top gates on both ends of the beam form two piezoelectric capacitors,  $C_1$  and  $C_2$ . A 15-nm-thick NiCr THz absorbing layer was deposited on the beam. This metal film was used also as a heater to calibrate the thermal responsivity of the resonator. The inset shows a blow-up of an SEM image of the hole array structure. (c) Schematic illustration for the measurement setup. An ac voltage was applied to one of the piezoelectric capacitors to drive the beam and the induced beam motion was monitored by a laser Doppler vibrometer. The motion signal is input to a phase locked loop (PLL) to provide a feedback control for maintaining the self-oscillation.

properties. Homogenous hole arrays of square lattices were formed on the GaAs MEMS beams. Owing to the reduction in the thermal conductance of the MEMS beams by introducing the hole array structures, the nano-porous samples shows 2-3 times larger thermal sensitivities than a reference unpatterned sample. Furthermore, because the heat capacitance of the MEMS beams is also reduced by the hole array structures, the thermal decay time of the nano-porous samples is increased only by about 30%~50%, demonstrating the effectiveness of the hole arrays for enhancing the thermal sensitivities of bolometers without deteriorating their operation bandwidths significantly.

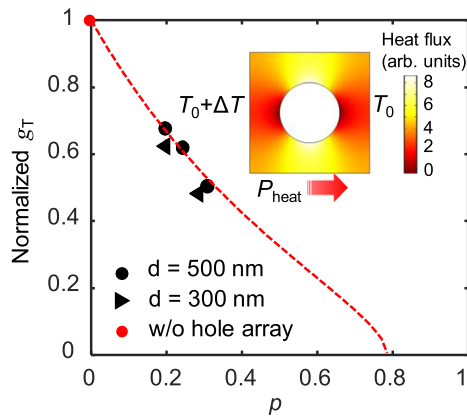
The wafer used for fabricating the doubly clamped MEMS beam resonators was grown by molecular beam epitaxy.<sup>22</sup> After growing a 200-nm-thick GaAs buffer layer and a 3-μm-thick  $\text{Al}_{0.7}\text{Ga}_{0.3}\text{As}$  sacrificial layer on a (100)-oriented semi-insulating GaAs substrate, the beam layer was formed by depositing a 50-nm-thick GaAs layer, a GaAs/ $\text{Al}_{0.3}\text{Ga}_{0.7}\text{As}$  superlattice structure, and a 400-nm-thick GaAs layer. We subsequently grew a 20-nm-thick Si-doped GaAs layer, a 70-nm-thick  $\text{Al}_{0.3}\text{Ga}_{0.7}\text{As}$  layer and a 10-nm-thick GaAs capping layer. The fabrication process for the MEMS resonators with hole array structures were schematically shown in Fig. 1(a). The nanometer-scale hole array structures of the square lattice were patterned on the beam by using electron-beam lithography. The holes were formed by using reactive ion etching with  $\text{Cl}_2$  gas and a rf power of 200 W at  $50^\circ\text{C}$  for 80 s. The suspended beam

structure was formed by selectively etching the sacrificial layer with diluted hydrofluoric acid.<sup>22</sup> Figure 1(b) shows an optical microscope image of a fabricated MEMS beam resonator ( $100 \times 30 \times 0.6 \mu\text{m}^3$ ) with a 2D hole array structure of a hole diameter  $d = 500 \text{ nm}$  and the neck size (the distance between neighboring holes)  $n = 500 \text{ nm}$ . The inset of Fig. 1(b) shows a blow-up of an SEM image of the hole array structure, showing that the fabricated hole array is homogeneous. We fabricated MEMS beams with the hole array structures of various sizes, *i.e.*,  $d/n = 500 \text{ nm}/500 \text{ nm}$ ,  $500 \text{ nm}/400 \text{ nm}$ ,  $500 \text{ nm}/300 \text{ nm}$ ,  $300 \text{ nm}/300 \text{ nm}$ , and  $300 \text{ nm}/200 \text{ nm}$ . In addition, we fabricated a reference sample without a hole array structure. The Si-doped GaAs layer and the top metal gates (15-nm-thick NiCr) on the two ends of the MEMS beam form two piezoelectric capacitors. An ac voltage was applied to one of the piezoelectric capacitors to drive the beam and the induced resonant beam motion was monitored by a laser Doppler vibrometer, as schematically shown in Fig. 1(c). The resonance signal is input to a phase locked loop (PLL) to provide a feedback control for maintaining a self-oscillation, as we reported elsewhere.<sup>17</sup> On the MEMS beam, we deposited a 15-nm-thick NiCr layer as a heater for calibrating the responsivity of the MEMS resonator, whose sheet resistance was  $\sim 500 \Omega/\square$ . All the measurements were performed in a vacuum ( $\sim 10^{-4}$  torr) at room temperature.

Figure 2(a) shows the measured oscillation spectra of a MEMS resonator with a hole array structure ( $d/n = 300 \text{ nm}/200 \text{ nm}$ ) at various driving voltages ( $V_D = 10\text{-}80 \text{ mV}$ ). (b) The normalized frequency shift ( $\Delta f/f_0$ ) as a function of the input heating power,  $P_{\text{in}} = 0\text{-}50 \mu\text{W}$ , for two MEMS resonators with the hole array structures ( $d/n = 300 \text{ nm}/300 \text{ nm}$  and  $300 \text{ nm}/200 \text{ nm}$ ) and that for a reference MEMS resonator. The numbers in the figure are the thermal responsivities  $R \equiv \Delta f/f_0 P_{\text{in}}$  of these three samples determined from the slope of  $\Delta f/f_0$ .



**FIG. 2.** (a) Resonance spectra of a MEMS beam resonator with a hole array structure ( $d/n = 300 \text{ nm}/200 \text{ nm}$ ) measured by using an open-loop circuit (lock-in amplifier) at various driving voltages ( $V_D = 10\text{-}80 \text{ mV}$ ). (b) The normalized frequency shift ( $\Delta f/f_0$ ) as a function of the input heating power,  $P_{\text{in}} = 0\text{-}50 \mu\text{W}$ , for two MEMS resonators with the hole array structures ( $d/n = 300 \text{ nm}/300 \text{ nm}$  and  $300 \text{ nm}/200 \text{ nm}$ ) and that for a reference MEMS resonator. The numbers in the figure are the thermal responsivities  $R \equiv \Delta f/f_0 P_{\text{in}}$  of these three samples determined from the slope of  $\Delta f/f_0$ .



**FIG. 3.** Red dashed line plots the normalized thermal conductance of the unit cell of the square hole array lattice calculated as a function of the porosity of the nano-porous structure for a dimensionless unit cell (see the inset) by using finite element method. The symbols show the normalized thermal conductance of the nano-porous MEMS beams with various  $d$  and  $n$ , derived from the measured thermal decay time of the beams shown in Fig. 4(b), as a function of the porosity of the hole array structure.

capacitor. The resonance frequency,  $f_0$ , was about 213.8 kHz and the Q-factor was about 1,500.  $f_0$  was higher than that of the reference MEMS resonator ( $\sim 167.8$  kHz). This is because the etching of the sacrificial layer develops through the holes for the nano-porous samples, whereas the etching proceeds only from the sides of the beam for the reference sample. This difference in the etching paths makes a difference in the length of the etching undercut, resulting in a shorter effective beam length for the nano-porous samples. When  $V_D$  exceeds 50 mV, the MEMS resonator shows a nonlinear hardening effect.

When an input power to the NiCr film,  $P_{in}$ , is increased from 0 to 50  $\mu$ W,  $f_0$  is reduced due to the thermal stress of the beam. Figure 2(b) shows the normalized frequency shift,  $\Delta f/f_0$ , as a function of the input heating power,  $P_{in}$ , for two MEMS resonators with hole array structures ( $d/n = 300$  nm/300 nm and 300 nm/200 nm) and a reference MEMS resonator without the hole array. From the slope of the frequency shift shown in Fig. 2(b), we determined the thermal responsivity,  $R \equiv \Delta f/(f_0 P_{in})$ , for the samples.  $R$  is increased from  $\sim 393$   $W^{-1}$  for the reference sample to  $\sim 712$   $W^{-1}$  for  $d/n = 300$  nm/300 nm and  $\sim 892$   $W^{-1}$  for  $d/n = 300$  nm/200 nm,

indicating that the hole array is effective in increasing the thermal responsivity of the MEMS detectors.

To back up our interpretation, we have calculated the thermal conductance of the unit cell of the square hole array lattice,  $g_T$ . Here, we introduce the porosity of the beam,  $p$ , which is defined by the ratio of the material volume removed from the beam to the volume of the beam before fabricating hole array structures,<sup>19</sup>

$$p = \frac{\pi d^2}{4(d+n)^2}. \quad (1)$$

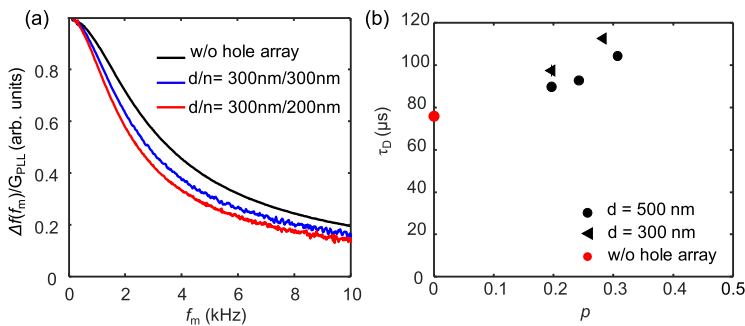
As seen in Eq. (1),  $p$  is determined only by the ratio  $n/d$ . In the calculation, we assumed that the left and right boundaries of the hole array unit cell has a temperature difference,  $\Delta T$ , and we calculated the heat power,  $P_{heat}$ , transmitted through the unit cell.  $g_T$  is defined as  $g_T \equiv P_{heat}/\Delta T$ . The red dashed line in Fig. 3 shows  $g_T$  as a function of the porosity of the hole arrays. The hole array structures fabricated in this work have a porosity of 0.2–0.3 and we expect that  $g_T$  is reduced by 40%–50% in our samples. In the figure, the inverse of the thermal responsivities of the hole array samples normalized by that of the unpatterned sample are also plotted. The measured inverse responsivities are in good agreement with the calculated  $g_T$ , indicating that the enhancement in  $R$  is indeed due to the reduction in  $G_T$  by introducing the hole arrays.

Next, to examine the effect of the hole array structures on the detection speed of the MEMS thermal sensors, we measured the thermal decay time,  $\tau_D$ , of the beam by measuring the heat signal as a function of the modulation frequency,  $f_m$ . We drove the MEMS beam resonator in a self-oscillation mode by using a PLL and applied an ac voltage to the NiCr heater to generate a modulated heat of  $\sim 2.3$   $\mu$ W on the beam. From a simple thermal decay theory, the frequency shift,  $\Delta f$ , and the thermal decay time,  $\tau_D$ , have a relationship expressed by;

$$\Delta f(f_m) = \frac{\Delta f_0}{\sqrt{1 + (2\pi\tau_D f_m)^2}} G_{PLL}(f_m), \quad (2)$$

where  $\Delta f_0$  is the frequency shift when the heat modulation frequency  $f_m = 0$ .  $G_{PLL}(f_m)$  expresses the circuit response of the PLL.

We first characterized  $G_{PLL}(f_m)$  to calibrate the effect of the demodulation bandwidth (BW) of the PLL. We input a frequency-modulated (FM) ac signal (amplitude = 1V, carrier frequency = 200 kHz, and FM depth 1 kHz) to the PLL to simulate the signal from the MEMS bolometer.<sup>17</sup> We swept  $f_m$  and measured the demodulated output of the PLL to obtain  $G_{PLL}(f_m)$ . Then,

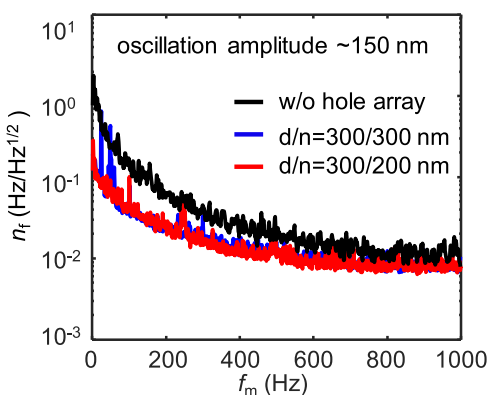


**FIG. 4.** (a)  $\Delta f(f_m)/G_{PLL}$  measured for two nano-porous MEMS resonators ( $d/n=300$ nm/300nm and 300nm/200nm) and a reference sample. (b) Thermal decay time  $\tau_D$ 's of the beams with various hole array structures are plotted as a function of the porosity of the hole array structure.  $\tau_D$ 's were derived from the  $\Delta f(f_m)/G_{PLL}$  spectra.

we can obtain the intrinsic frequency response of the beams as  $\Delta f(f_m)/G_{\text{PLL}}(f_m)$ , which is only determined by the thermal decay process in the MEMS beam. Figure 4(a) plots  $\Delta f(f_m)/G_{\text{PLL}}(f_m)$  for a reference MEMS resonator without the hole array and two typical MEMS resonators with the hole array structures ( $d/n = 300 \text{ nm}/300 \text{ nm}$  and  $300 \text{ nm}/200 \text{ nm}$ ). As seen in the figure, the signals for the nano-porous samples decrease slightly faster than that of the reference sample, indicating that the thermal decay times,  $\tau_D$ , are slightly increased by introducing the hole array structures.

By using numerical fitting of Eq. (2) to  $\Delta f(f_m)/G_{\text{PLL}}(f_m)$ , we obtained  $\tau_D$  for the MEMS beams with the hole arrays and that for the reference MEMS beam. Figure 4(b) plots  $\tau_D$  of the MEMS beams with the hole array structures as a function of  $p$ .  $\tau_D$  is increased from  $\sim 75.8 \mu\text{s}$  for the reference sample to  $\sim 97.4 \mu\text{s}$  for  $d/n = 300 \text{ nm}/300 \text{ nm}$  and  $\sim 112.5 \mu\text{s}$  for  $d/n = 300 \text{ nm}/200 \text{ nm}$ . From Fig. 4(b), we see that the increase in  $\tau_D$  by introducing the hole array structures is typically 30-50%. Compared with the improvement in responsivity (2-3 times), the reduction in the thermal BW is smaller, demonstrating effectiveness of the hole array structures for partly resolving the trade-off between the responsivity and the bandwidth of the thermal sensors.

Finally, we have characterized the noise equivalent power (NEP) of the MEMS beam resonators. We drove the MEMS beam resonators in a self-oscillation mode by using a PLL with a demodulation bandwidth of 1 kHz and measured the frequency noise spectra,  $n_f$ . Figure 5 plots  $n_f$  as a function of  $f_m$  for two MEMS resonators with hole arrays and a reference MEMS resonator. The samples with the hole arrays have slightly smaller frequency noise than the reference sample. Since the NEP of the MEMS resonator is expressed as  $\text{NEP} \equiv n_f/f_0R$ , the NEP is reduced by the enhanced thermal responsivities for the nano-porous samples. The minimum NEP for the reference sample was  $\sim 110 \text{ pW}/\text{Hz}^{0.5}$  at  $f_m = 1 \text{ kHz}$ , whereas the NEP for the sample with  $d/n = 300 \text{ nm}/300 \text{ nm}$  is  $\sim 50 \text{ pW}/\text{Hz}^{0.5}$  and that for the sample with  $d/n = 300 \text{ nm}/200 \text{ nm}$  is  $\sim 40 \text{ pW}/\text{Hz}^{0.5}$ . Since the detector sensitivity is defined by  $1/\text{NEP}$ , the nano-porous MEMS resonators have 2-3 times larger sensitivities than the unpatterned reference sample.



**FIG. 5.** Frequency noise spectra of the nano-porous MEMS resonators ( $d/n = 300 \text{ nm}/300 \text{ nm}$  and  $300 \text{ nm}/200 \text{ nm}$ ) and the reference sample. The spectra were measured when the MEMS resonators were driven in a self-oscillation mode with a resonance amplitude of  $\sim 150 \text{ nm}$  by a PLL with a modulation bandwidth of 1 kHz.

In summary, we have fabricated two-dimensional nanometer-scale hole array structures on GaAs doubly-clamped MEMS beam resonators to modulate their thermal properties. Owing to the reduction in the thermal conductance of the MEMS beams by introducing the hole array structures, the nano-porous samples with the hole array structures show 2-3 times larger thermal responsivities than an unpatterned reference sample. Furthermore, since the heat capacitance of the MEMS beams is also reduced by introducing the hole array structures, the thermal decay time of the nano-porous samples is increased only by about 30%~50%, demonstrating the effectiveness of the hole array structures for enhancing the thermal sensitivities of bolometers without deteriorating their operation bandwidths very much.

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