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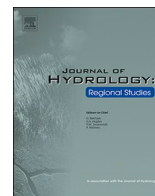
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Hydraulic characterization and identification of flow-bearing structures based on multi-scale investigations applied to the Lez karst aquifer

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ABSTRACT

Study Region: The Lez aquifer is a Mediterranean karst system located in southern France, which supplies groundwater to the Montpellier urban area.

Study Focus: Multi-scale hydrodynamic investigations were carried out in a fractured and karstic aquifer in order to identify the flow-bearing structures and evaluate their hydraulic properties. The study is based on an extensive dataset developed from several hydraulic tests, performed at different spatial and temporal scales. The scales ranged spatially from a few meters to more than 15 km and temporally from a few minutes to a few months.

New Hydrological Insights for the Region: The data analysis shows that the hydraulic connectivity at both local and regional scales is mainly due to sub-horizontal flow-bearing structures, in which a conduit network has developed. This structure appears mainly to be located at the interface between two stratigraphic units, at the transition between Jurassic and Cretaceous limestones (Kimmeridgian-Berriasian interface). At the regional scale, this flow-bearing structure plays a major role in large-scale connectivity since a compartmentalization of the Lez aquifer appears where the continuity of this structure disappears. The hydraulic properties estimated appear to be strongly dependent on the investigated geological structures and on the different hydrogeological methods used for the borehole, local and regional scale of investigations.

1. Introduction

Karst aquifers, which are generally very productive, constitute important groundwater resources for approximately a quarter of the global population (Ford and Williams, 2007). These aquifers can be conceptualized by three levels of porosity: the primary porosity of the rock matrix; the secondary porosity of fractures, which includes various fracture types or joints at several scales (cracks, joints including bedding-planes and faults); and the third porosity resulting from the dissolution of the bedrock along the fracture or joint surfaces (Worthington, 1999; Ford and Williams, 2007). The permeability of the system is generally dominated by the second and third porosity types (Worthington et al., 2000; Worthington and Ford, 2009). In fractured rocks, flow channeling generally occurs at fracture and fracture-network scales (de Dreuzy et al., 2012) but this process may be stronger in karstic reservoirs (Worthington and Ford, 1995). This behavior may be enhanced by the presence of complex networks of enlarged fractures due to wall dissolution, and to the development of karst conduits over several kilometers (Palmer, 1991; Worthington, 1999). Groundwater

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quality and quantity in karst aquifers are therefore highly variable due to the strong heterogeneity and anisotropy of the fractured and karstic networks (Worthington, 2011). The management of these groundwater resources are thus particularly challenging and require detailed characterization of hydraulic heterogeneity, which are extremely variable and difficult to determine (Bakalowicz, 2011).

In fractured-karstic reservoirs, the degree of detail in the hydraulic heterogeneity depends on the spatial extent of the investigation and on the specificity of the hydraulic experiments (Shapiro et al., 2015). For instance, hydraulic tomography provides important details of spatial hydraulic heterogeneity but requires multiple cross-hole hydraulic tests, which are generally made at a limited scale of investigation to allow monitoring of hydraulic responses (Ackerer and Delay, 2010; Wang et al., 2017; Fischer et al., 2017). However, hydraulic tomography still remains a challenge to be conducted at regional scale (i.e., aquifer/watershed scale) due to, for instance, the technical difficulty to investigate significant volumes of the aquifer, a limited number of observation wells distributed over the entire system, or simply to an impossibility to provide responses at each observation well during sequential pumping tests. At regional scale, groundwater flow and hydraulic property estimates in karstic systems are classically investigated with spring-discharge hydrographs (Baedke and Krothe, 2001; Kovács et al., 2005; Fiorillo, 2014), by hydraulic head data analyses (Sauter, 1991; Renard and Jeannée, 2008; Galvão et al., 2016) or, more rarely, by long-term pumping test analysis (Maréchal et al., 2008).

To obtain more details on hydraulic heterogeneity and connectivity at larger scale, which could be helpful to improve groundwater management, another approach consists in a multidisciplinary framework. This requires consequently intensive investigations to identify and characterize the relevant flow structures such as faults, joints, bedding-planes and karstic features. Such investigations can be made by measurements at several scales of investigation in order to connect all the information and provide a consistent interpretation. At the borehole scale, flowing fractures or karstic features can be localized and characterized through different methods such as temperature logging (Chatelier et al., 2011; Klepikova et al., 2011), packer testing (Quinn et al., 2012) or flowmeter testing (Paillet, 1998; Day-Lewis et al., 2000). At the local scales, cross-hole hydraulic tests, such as pumping tests, can be used to identify the flow pattern to provide information on reservoir geometry, in addition to its hydraulic properties (Gringarten, 2008). At the regional scale, water-level monitoring in several observation wells appropriately distributed across the system can be used, for instance, to identify potential compartments under different hydrological conditions (Guihéneuf et al., 2014). Even though such approach is challenging and requires numerous data, it remains necessary to identify geological structures relevant for groundwater flow at larger scales and estimates their hydraulic properties.

The objective of this study is to identify and characterize the properties of the main flow-bearing structures in a karst aquifer, based on geological information and a multi-scale hydraulic investigation. These intensive investigations were conducted in the Lez aquifer, a Mediterranean karst aquifer located in southern France, near the metropolitan area of Montpellier. Investigations were performed at regional scale (i.e., the watershed scale), local scale using an experimental site (i.e., the Terrieu experimental site) and borehole scale with specific measurements in some boreholes. Detailed knowledge of the aquifer characteristics remains of major importance for the Lez aquifer management, because groundwater is intensively pumped for water supply to the Montpellier metropolitan region. Such detailed information on reservoir heterogeneities may also be helpful for any future predictive modeling related to groundwater management and protection.

2. Study site: the Lez aquifer

This large karst system located in the Mediterranean basin, South East of France, is referred to as the Lez aquifer because it feeds the Lez spring. The Lez aquifer supplies some 30 million m³ of water per year to the metropolitan area of Montpellier. The area is characterized by a typical Mediterranean climate with dry summers and rainy autumns. The mean temperature is about 22 °C in summer, and about 5 °C in winter. The intense rainfall events in autumn are the main contributors to the annual recharge. Annual rainfall occurs primarily from September to December and to a lesser extent from March to May. The mean annual precipitation ranges from about 600 mm (dry years) to more than 1500 mm (wet years). Rainfall is also spatially variable with an increase from south to north due to the rising topography and the proximity of the Cevennes hills (Mazzilli, 2011). The recharge area of the Lez spring is estimated about 150 km², corresponding to the surface area where limestone directly outcrops. The exact boundaries of the aquifer area are poorly known, but it is estimated of more than 250 km². In the following sections, the hydrogeological context of the Lez aquifer, details concerning the Terrieu experimental site, and the strategy adopted for this study are presented.

2.1. Hydrogeological context

The Lez aquifer is composed mainly of Upper Jurassic and Early Cretaceous limestone. These sedimentary rocks overlie the Callovian–Oxfordian marls (Jurassic) and may locally be covered by a thick succession of Early Valanginian (Early Cretaceous) marls and marly limestone (Fig. 1a). The aquifer is divided by NE-SW normal faults related to the Pyrenean orogeny (Eocene) and later impacted by the oligocene extension phase (Séranne et al., 1995; Benedicto et al., 1999). The Matelles-Corconne fault, which is one of the main faults, divides the reservoir into two compartments. The western compartment contains the Upper Jurassic limestone at the outcrop while the eastern compartment primarily contains cretaceous formations of the Early Valanginian at the outcrop (Fig. 1a). The Lez aquifer shows a high degree of karstification developed during different geological periods, from the Middle Cretaceous to the current period (Leonardi et al., 2011). In particular, the possibility of deep karstification is attributed to the Messinian salinity crisis (about 5.5 My ago) when the sea-level of the Mediterranean Sea dropped by more than 1000 m due to the closing of the Gibraltar straits (Audra et al., 2004; Clauzon et al., 2005).

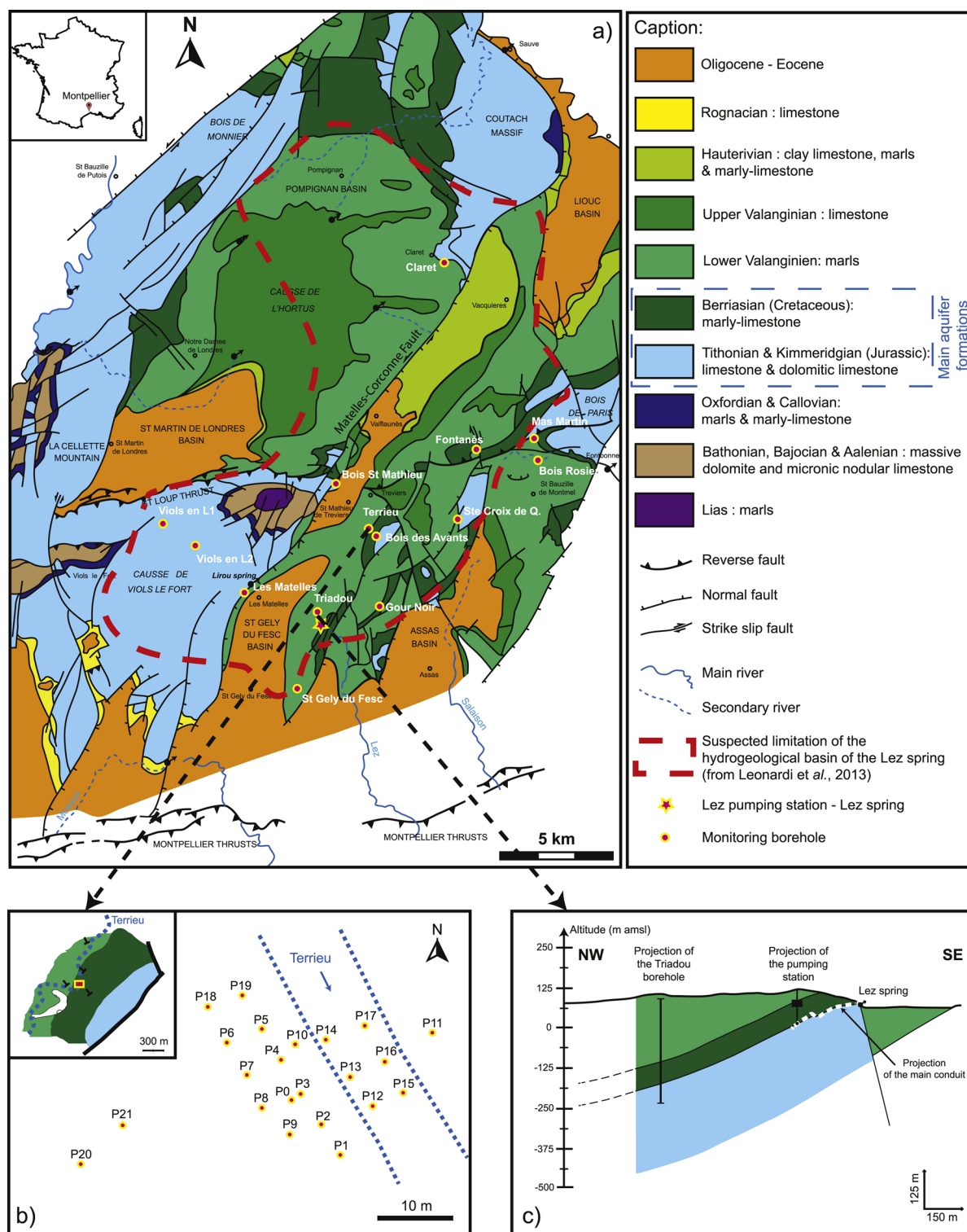


Fig. 1. a) Regional geological map with the position of the monitoring network of the Lez aquifer (modified from Marjolet and Salado, 1975); b) Geological location of the Terrieu experimental site and spatial distribution of boreholes; c) Simplified geological cross-section through the Lez spring and the Triadou borehole (modified from Leonardi et al., 2013).

An extensive fracture dataset was collected at different spatial scales from 2D patterns observed at the Lez aquifer. Data available come from the geological map at a scale of 1:250 000 (Tissier, 2009), from assembled aerial photographs at a scale of 1:25 000 (Durepaire, 1985) and from *in situ* outcrop measurements at the Terrieu experimental site (Droque and Grillot, 1976; Jazayeri Noushabadi, 2009). Statistical analyses revealed different preferential orientations of the fracture sets depending on the scale of analysis (Leonardi et al., 2011; Dausse, 2015). At the regional scale (1:250 000), the main orientations of the faults are from N010 to N040, with over 50% of fractures oriented in this direction. At the 1:25 000 scale, the results are highly heterogeneous, depending on the selection of the geographic zones (Dausse, 2015). Three main fracture sets show the N040-N045 direction (the main representative ones are related to the NE-SW direction of the Matelles-Corconne fault), the N-S direction and the E-W direction. At the local scale (i.e., the Terrieu experimental site), from Cretaceous limestone outcrops, two main families of fractures with the N070 and N140 directions have been identified (Wang et al., 2014). According to the scale of observation and to the locations chosen for fracture trace maps analyzed, the impact of the variability of the fracture networks is significant on the estimated apparent connectivity, ranging from well- to poorly-connected (Lei and Wang, 2016). The connectivity of fracture networks organizes the groundwater flow and could influence the karstification of the carbonate reservoir. The organization of the karstic networks is related to both the fracturing and the direction of the hydraulic gradient, whereas close to major faults, this organization is controlled by the juxtaposition of different units and by the tectonic regime (Leonardi et al., 2011). The karstic network is preferentially oriented along the NE-SW main faults, but in poorly-deformed areas, the network is mainly oriented in the NS-EW direction (Leonardi et al., 2011). Husson et al. (2018) demonstrated that the varying karstification distribution of the Lez aquifer can be related to the presence or absence of impervious formations covering the carbonate strata. In particular, carbonates located under impervious marly formations (Early Cretaceous) appear mostly preserved from dissolution processes and are less karstified (Husson et al., 2018).

The reservoir discharges into several seasonal overflowing springs. The main outlet, the Lez spring, is located near Saint-Clément-de-Rivière, about 15 km north of Montpellier. This spring is of a Vaclousian-type with a maximum discharge of approximately $15 \text{ m}^3 \text{ s}^{-1}$. However, the discharge at the Lez spring is generally small or nil due to the active pumping management of the aquifer, which also reduces downstream floods (Jourde et al., 2014). Since 1980, the water supply of the metropolitan area of Montpellier has been provided by the underground Lez pumping station installed 250 m upstream of the Lez spring (Fig. 1c). The water is pumped from the main karst conduit leading to the spring, around 50 m below the spring level (i.e., 15 m above mean sea level (ams)). The maximum cumulative pumping rate is about $6120 \text{ m}^3 \text{ h}^{-1}$. The water levels at the Lez catchment are monitored through numerous observation wells distributed from a few meters to several kilometers (i.e., 15 km) from the pumping station (Fig. 1a). One of these observation wells, the Triadou, is located 580 m upstream of the Lez pumping station (Fig. 1c), and was drilled to a depth of 330 m for the purpose of this work. Geophysical and hydraulic characterizations in this borehole are presented below in the section “Borehole scale investigations”.

2.2. The Terrieu experimental site

The Terrieu experimental site is located at the east of the Matelles-Corconne fault, in the eastern compartment of the reservoir, 4.6 km north of the Lez spring (Fig. 1a). This site is located in a NE-SW monocline of the Early Cretaceous marly limestone and the Upper Jurassic limestone, dipping NW from 15 to 20°. It is composed of 22 shallow boreholes (about 60 m deep), with a diameter of 115 mm (except P0, P8, P21 with a 216 mm diameter), grouped in a network with a spacing of about 5 to 7 m over the 1500 m^2 surface area of the site (Fig. 1b). Groundwater level usually fluctuates from 35 to 75 m above mean sea level (i.e., around 50 to 10 m below ground surface) depending on the hydrological conditions. Under exceptional meteorological conditions artesianism has been observed on the site. Most of the boreholes are not cased (except P18 and P19 with cased screen) and intersect two main lithologies. The upper part of the boreholes (length of about 30–40 m) crosscuts inter-bedded marly limestone, which corresponds to the Berriasian limestone. The lower part of the boreholes (length of about 20–30 m) crosscuts more massive limestone. This change of lithology may be attributed to the transition between Cretaceous (Berriasian) and Jurassic (Kimmeridgian) limestones.

Fracture analyses were conducted at the Terrieu site on the outcrops as well as in several boreholes from video logs (Droque and Grillot, 1976; Jazayeri Noushabadi, 2009). At the outcrops, two main fracture directions were observed, N070 and N140 (Wang et al., 2014). From video-log investigations, the fractures oriented N070 are preferentially open (Jazayeri Noushabadi, 2009). This is consistent with the orientation of the observed karst conduits (Jazayeri Noushabadi et al., 2011). The karstification at this site appears moderately developed with a preferential karstification at the intersections between fractures and bedding-planes (Droque and Grillot, 1976).

Various hydrogeological studies have been performed at the Terrieu experimental site. The first pumping tests conducted at the site in the 1980s has shown that the flow is preferentially oriented N070, which is well correlated with one of the main fracture orientations (Droque and Grillot, 1976). The correlation with the fracture orientations has also been confirmed by numerous short-term (several minutes) pumping tests conducted at different pumping boreholes (Jazayeri Noushabadi et al., 2011; Wang et al., 2016). The pumping tests analyses provided transmissivity values ranging from 3.7×10^{-7} to $2.0 \times 10^{-2} \text{ m}^2 \text{ s}^{-1}$. Single-borehole electromagnetic flowmeter measurements from three boreholes (P2, P5, P16) estimated transmissivities ranging from 3.7×10^{-7} to $1.6 \times 10^{-4} \text{ m}^2 \text{ s}^{-1}$ (Lods, 2000). These estimates show a strong variability of the transmissivity at the site scale due to a strong heterogeneity of the karst reservoir. In addition, the single-borehole flowmeter tests revealed only two or three main flow zones per borehole, which is also confirmed by temperature logging (Droque, 1985; Malard et Chapuis, 1995; Jazayeri Noushabadi, 2009; Dausse, 2015). The strong anomalies in temperature loggings measured at some boreholes (i.e., P2, P8, P11, P12, P15, P20) suggested flow zones of higher permeability related to karstified fractures and karst conduits developed along a bedding-plane (Jazayeri Noushabadi et al., 2011). Because its extensive network of boreholes, the experimental site is also appropriate to conduct hydraulic

tomography studies. Recently, sequential short-term pumping tests (Wang et al., 2016, 2017; Fischer et al., 2017) and sequential harmonic pumping tests (Fischer et al., 2018a, b) have been performed to characterize the spatial distribution of field transmissivity and imaging karstic features. The inversions of the hydraulic data were based on a two-dimensional conceptual model derived from field investigations (Jazayeri Noushabadi, 2009; Dausse, 2015).

2.3. Multi-scale investigations strategy

The multi-scale investigations of the Lez aquifer are based on an analysis of extensive dataset collected at different spatial scales, from a few meters to more than 15 km; and temporal scales, from a few minutes to a few months. Three main scales have been defined according to the methodology applied and spatial investigation: regional, local and borehole scales. The regional scale, presented in section 3, mainly focuses on the large influence of the Lez pumping on water levels. Water levels have been monitored at several location using numerous observation boreholes distributed across the watershed, including the Terrieu boreholes. Daily and seasonal variations on water levels have been analyzed to extract hydraulic properties. At the Terrieu experimental site, which represents the local scale presented in section 4, a cross-hole pumping test was performed to estimate local properties. Since high flow rate pumping at the Lez station have a large impact on the hydrodynamics of the Terrieu experimental site, the regional interferences observed during hydraulic tests at this site have been removed to analyze independently the hydrodynamic response to the local perturbation. This influence was thus filtered in order to provide a consistent interpretation of the long-term pumping test performed at local scale. In section 5, the borehole scale investigations are presented. These includes specific measurements (i.e., packer tests, temperature and electrical conductivity logging) conducted in some Terrieu boreholes and the Triadou borehole, which has been implemented for this study. In addition to cuttings analysis, geophysical resistivity logging was performed at the Triadou borehole to characterize properly the geology with depth. In order to identify the main flow zones in this borehole and estimate their transmissivity, temperature and electrical conductivity logging as well as borehole flowmeter tests were realized.

3. Regional scale investigations

3.1. Materials and methods

For the water supply of the metropolitan area of Montpellier, the pumping rates vary daily according to the water demand and impact the aquifer over several kilometers. Discharge rates are continuously monitored with high-frequency measurements (1 minute timestep). Water level variations were recorded at high-frequency with pressure transducers (TD-Diver® and CTD-Diver®, Schlumberger) at the Lez station and in 14 observation boreholes distributed at different places over the karst catchment (red dots in Fig. 1a). The seasonal variations due to the long-term pumping, later referred to as “seasonal drawdowns”, were observed in most observation boreholes. Only a few of them are sensitive to daily variations, called “daily drawdowns”. Seasonal and daily variations were both used to characterize the hydrodynamic properties of the reservoir. The hydraulic properties were first derived by the classical Cooper and Jacob's (1946) and Theis' (1935) solutions for seasonal and daily responses, respectively. The limitations of applying the Theis' solution or its Cooper-Jacob's approximation to model the Lez pumping responses are obvious based on their assumptions (e.g., fully penetrating well, homogeneous and confined aquifer of infinite extent), which cannot account for karst complexity. However, these reference models can be useful to estimate aquifer hydraulic properties using late-times drawdown data and may provide a good estimate of the effective transmissivity in heterogeneous media (Meier et al., 1998; Sánchez-Vila et al., 1999; Knudby and Carrera, 2006). The transmissivity estimates using these simple approaches for seasonal and daily responses are next validated using the radial composite model of Butler (1988), which allows to simulate consistently the global behavior of the regional drawdowns.

3.2. Results

3.2.1. Seasonal drawdowns analysis

The continuous water level monitoring in several boreholes demonstrates strong temporal and spatial variabilities (Fig. 2a). During the rainy periods, water levels react rapidly to rainfall, rising from a few meters to several tens of meters. When water level at the Lez spring is higher than the outlet altitude (i.e., 65 m amsl), the Lez spring starts flowing. However, the spring does not always discharge after significant rainfall events because of the Lez pumping influence, inducing strong decrease in water level. During dry periods (negligible or no rain), the pumping stops the natural flow at the Lez spring and decreases the water levels over several kilometers. The resulting drawdowns were analyzed over three months during the dry season (from June to August 2012). The different types of drawdowns were organized in five groups according to their behaviors (Fig. 2b, c and d). These responses do not appear dependent of the distance between the borehole and the pumping station (Fig. 1). Indeed, some boreholes displayed similar drawdown responses while they are located at different radial distances from the pumping station (see Fig. 2b and c). A summary is provided in Table 1 with the different response categories detailed below.

Fig. 2b presents two categories of drawdown responses. One category groups boreholes with daily responses (i.e., Triadou, Claret, and Terrieu). All boreholes at the Terrieu site react similarly to the Lez pumping and thus can be considered as a single point at the regional scale. Interestingly, daily responses measured at the P20 Terrieu borehole have lower amplitudes once the water level decreases below 45 m amsl (see zoom at Fig. 2a). The amplitude of the average daily drawdowns suddenly changes from 1.7 m to 0.3 m in this borehole. The second category groups boreholes with a similar trend and amplitude but without daily variations (i.e.,

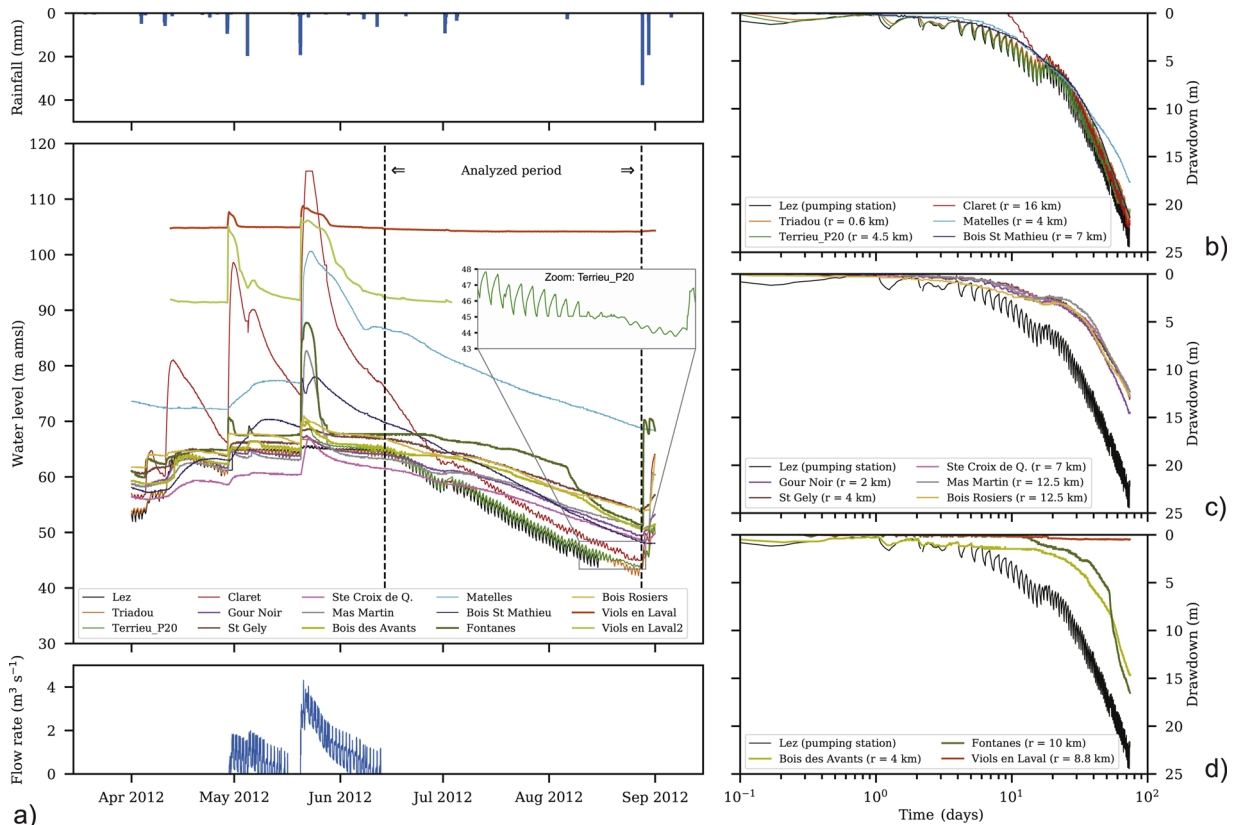


Fig. 2. a) Rainfall, borehole water levels and flow rate at the Lez spring from April to September 2012. During the 2012 dry period, the two dotted lines limit the period during which the regional drawdown due to pumping (average $Q_{\text{pumping}} = 4134 \text{ m}^3 \text{h}^{-1}$) at the Lez station were analyzed. b) Typical hydrodynamic responses at the different boreholes that exhibit a drawdown similar to the drawdown at the Lez station pumping well (black line). c) Typical hydrodynamic responses at the different boreholes that exhibit similar shape responses but with smaller amplitude. d) Boreholes that exhibit complex drawdown responses and borehole without any influence from the pumping at the Lez station.

Matelles and Bois de Saint Mathieu). Fig. 2c presents a borehole category with a similar shape compared to that of the Lez station, but without daily variations and with smaller amplitude (i.e., Gour Noir, Saint Gely, Sainte Croix de Quintillargues, Mas Martin, and Bois des Rosiers). Fig. 2d shows two other borehole categories. One is characterized by a different behavior (i.e., different inflexion) than that of the Lez station and groups Bois des Avants and Fontanès. Note that Bois des Avants presents a combined behavior: during the first four days, the response was impacted by daily pumping, then it changed to follow the general decrease in water level with a different shape. The last category represented by the two boreholes located at Viols en Laval (only one is shown) is characterized by almost no response to the pumping. Note that these last boreholes cross-cut only the Kimmeridgien limestone in the western compartment of the Lez system (Fig. 1).

The late times drawdown responses were interpreted with Cooper and Jacob's (1946) method and the results are presented in Table 1. The values of transmissivity range from 3.8×10^{-3} to $7.8 \times 10^{-3} \text{ m}^2 \text{s}^{-1}$ and are characterized by a geometric mean of $6.0 \times 10^{-3} \text{ m}^2 \text{s}^{-1}$. This mean value is fully consistent with previous estimates at the Lez station, which range between 6.0 and $6.9 \times 10^{-3} \text{ m}^2 \text{s}^{-1}$ whichever period is considered (i.e., 1986, 1987, 1998, 2002, 2003, 2005, 2006) (Jourde et al., 2011). The storativity values are more variable and range between 8.2×10^{-5} and 6.3×10^{-2} , which is classically observed from the analysis of pumping tests in heterogeneous reservoirs using this method (e.g., Meier et al., 1998; Sánchez-Vila et al., 1999; Bodin et al., 2012) and can be related to the heterogeneous diffusivity of the karst aquifer.

3.2.2. Daily drawdowns analysis

Daily water-level variations due to the pumping cycles can be clearly observed at the Triadou, Terrieu and Claret boreholes (Fig. 2b) and for few pumping cycles at the Bois des Avants borehole (Fig. 2c). Fig. 3a shows water levels at the Triadou borehole from April to July 2012. The Lez spring altitude (65 m amsl) is represented by the blue dotted line. When the water level is above that of the spring, the Lez spring discharges, but, when the water level is below that of the spring, the discharge stops (Fig. 3b). The variable drawdown responses are highlighted for 21 daily pumping cycles in June 2012 (Fig. 3b and c).

For similar durations and pumping rates at the Lez station, the variability of the daily drawdown shapes appears strongly correlated to the natural flow discharge at the Lez spring (Fig. 3b). The slopes and amplitudes of the drawdowns were smaller when the natural discharge at the Lez spring was higher than the pumping rates (highlighted in green in Fig. 3b and green curves in 3c). The

Table 1

Characteristics of the seasonal pumping responses at regional scale over 74 days of the pumping at the Lez station in June–August 2012 (at low water level conditions with no flow discharge at the Lez spring) with average pumping rate of $4134 \text{ m}^3 \text{ h}^{-1}$ ($1.15 \text{ m}^3 \text{ s}^{-1}$). “Distance” refers to the radial distance between the Lez pumping station and each observation well and “ Δs ” refers to the maximum drawdowns during the analyzed period. The transmissivity (T) and storativity (S) were estimated from Cooper-Jacob’s method.

Drawdowns description compared to the pumping well response	Location	Distance (km)	Δs (m)	T ($\text{m}^2 \text{ s}^{-1}$)	S (–)	D = T/S ($\text{m}^2 \text{ s}^{-1}$)
Pumping well	Lez pumping station	0	22.1	6.3×10^{-3}	–	–
Similar trend and amplitude + daily responses observed	Triadou	0.6	20.6	6.1×10^{-3}	6.3×10^{-2}	0.1
	Terrieu site (P20)	4.5	20.6	6.1×10^{-3}	1.1×10^{-3}	5.8
	Claret Brissac	16	20.6	6.1×10^{-3}	8.2×10^{-5}	74.4
Similar trend and amplitude	Les Matelles	4	17.7	7.8×10^{-3}	1.9×10^{-3}	4.1
	Bois de Saint Mathieu	7	21.4	5.7×10^{-3}	4.7×10^{-4}	12.1
Similar shape but smaller amplitude	Gour Noir	2	14.4	6.1×10^{-3}	9.0×10^{-3}	0.7
	St Gely du Fesc	4	12.8	6.6×10^{-3}	2.3×10^{-3}	2.9
	Ste Croix de Quintillargues	7	12.8	6.8×10^{-3}	8.0×10^{-4}	8.5
	Mas de Martin	12.5	12.3	7.2×10^{-3}	2.6×10^{-4}	27.7
	Bois des Rosiers	12.5	12.8	7.3×10^{-3}	2.4×10^{-4}	30.4
Drawdowns with different inflexion	Bois des Avants	4	14.7	4.2×10^{-3}	1.8×10^{-3}	2.3
	Fontanès	10	16.5	3.8×10^{-3}	2.8×10^{-4}	13.6
No drawdown response	Viols en Laval 1	8.8	–	–	–	–
	Viols en Laval 2	6.7	–	–	–	–
Geometric mean				6.0×10^{-3}	1.1×10^{-3}	5.6

slopes and amplitudes of the drawdowns increased when the natural discharge at the Lez spring decreased (highlighted in blue and orange in Fig. 3b, and blue and orange curves in 3c). Once the discharge at the Lez spring had stopped, the slope and the amplitude of the daily drawdowns stabilized, while the water level continued to decrease (highlighted in red in Fig. 3b, and red curves in 3c). As illustrated in Fig. 4, similar drawdown behaviors can be observed at the Terrieu and Claret boreholes that follow the drawdowns at the Lez pumping station. Bois des Avants borehole only presents daily responses under high water level conditions.

The hydrological conditions (*i.e.*, high and low water levels) related to the Lez spring flow conditions (*i.e.*, overflow or no overflow) have a strong impact on hydraulic responses due to the daily pumping tests at regional scale (Figs. 3 and 4). Drogue and Delaunay (1992) previously demonstrated that the singular evolutions of the hydraulic heads are related to the transition from a flow with pseudo-constant head (overflow) to a flow with variable head (no overflow) as a consequence of the pumping. When the discharge at the Lez spring is higher or equal to the pumping rate (green and blue cycles on Fig. 3), the daily drawdowns appear strongly impacted by boundary effects due to the Lez spring, which do not allow proper application of classical radial flow solution such as Theis (1935) or the Cooper-Jacob’s approximation. Accordingly, pumping test analysis was performed only for the period during which the discharge at the Lez spring was lower than the pumping rate (*i.e.*, $Q_{\text{spring}} < Q_{\text{pumping}}$; orange cycles) or when the discharge at the Lez spring was zero (red cycles). In these cases, the spring effect was negligible or nil and the drawdown derivatives obtained using the method of Bourdet et al. (1989) seem to tend to radial flow, even though the derivative may be not stabilized because of the short duration of the daily pumping (Fig. 5). Because Theis’ (1935) model can properly reproduce this behavior (Fig. 5), this solution was used to estimate the transmissivity. The use of a more complex model cannot be justified from this drawdown behavior, although the system is heterogeneous. Therefore, the interpretation using Theis’ (1935) model was focused on six pumping periods without impact of the discharge flow at the Lez spring (orange and red cycles on Fig. 3). Table 2 presents the hydraulic properties estimated for these pumping cycles at the Triadou and Terrieu (P17) boreholes. The estimated transmissivities, which are relatively constant and similar for these boreholes, are characterized by a geometric mean of $1.0 \times 10^{-1} \text{ m}^2 \text{ s}^{-1}$ for the Triadou borehole and $1.1 \times 10^{-1} \text{ m}^2 \text{ s}^{-1}$ for the Terrieu borehole. The estimated storativities are also relatively constant between the different pumping cycles analyzed, but different between the boreholes. The geometric means of estimated storativity are 4.4×10^{-3} for the Triadou borehole and 5.5×10^{-5} for the Terrieu borehole.

3.2.3. Radial composite flow model

The previous interpretations using the classical radial flow solution at early (*i.e.*, daily responses analysis) and late times (*i.e.*, seasonal responses analysis) highlighted some changes in the hydraulic properties with the duration of the pumping and therefore with the investigation scale. To consider this observation, hydrodynamic responses at the Lez aquifer were analyzed with a radial composite flow model. This interpretation has been performed using the semi-analytical solution of Butler (1988), which assumes nonuniform aquifer with a pumping well located at the center of a first domain embedded within an infinite second domain of different hydraulic properties. This simple configuration does not pretend to discretize the high level of heterogeneity of the karst

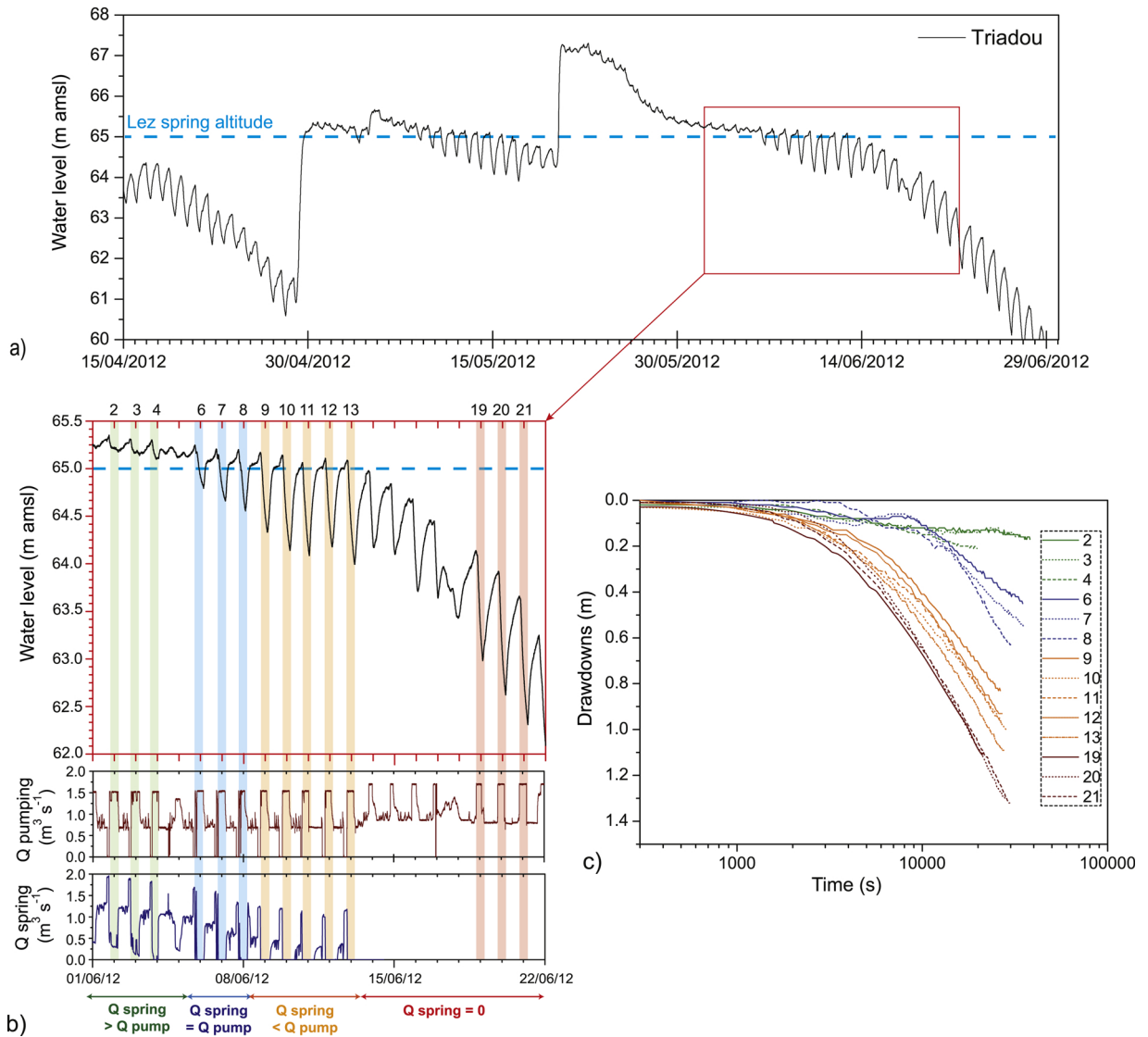


Fig. 3. Influence of the hydrological conditions on the hydrodynamic response at the Triadou borehole: a) Hydrodynamic behavior of the Triadou borehole from April to June 2012; b) Drawdown at the Triadou borehole in response to daily pumping rate variations at the Lez station (red line) and evolution of the natural discharge at the Lez spring (blue line); c) semi-log plot of the drawdown observed at the Triadou borehole for each pumping cycle (For interpretation of the references to colour in this figure legend, the reader is referred to the web version of this article).

aquifer, but can properly reproduce the global behavior of the pumping responses (see Fig. 6).

Fig. 6 shows, in log-log and semi-log plots, the measured drawdowns and the modeling using the composite model of Butler (1988) for the Lez pumping station, and the observation borehole Bois de Saint Mathieu. This observation borehole presents a similar behavior of the pumping well but without daily variations (see Fig. 2b). The drawdown derivative is represented in green for the data and with a continuous black line for the model. Note that the drawdown derivatives were noisy, especially at the Lez station, and has been strongly filtered to improve clarity. One can observe here that the radial composite flow model of Butler (1988) can properly describe the observed regional drawdown behavior in agreement with the transmissivities obtained from daily and late times seasonal responses analyses using Theis' and Cooper-Jacob's methods, respectively.

The estimated hydraulic parameters obtained with the composite model are presented in Table 3. A radius of 5 km was fixed for the first domain extension with the transmissivity T_1 of $5.0 \times 10^{-1} \text{ m}^2 \text{ s}^{-1}$, close to the estimates obtained from daily drawdown analyses using Theis' (1935) model. The second domain had a transmissivity T_2 of $6.0 \times 10^{-3} \text{ m}^2 \text{ s}^{-1}$ corresponding to the geometric mean of the transmissivity estimates obtained from late times analyses of the seasonal drawdowns using Cooper-Jacob's method. The storativity estimate of the first domain (S_1) ranges from 7.5×10^{-4} to 6.5×10^{-3} and the storativity estimate of the second domain (S_2) ranges from 5.0×10^{-5} to 1.0×10^{-4} .

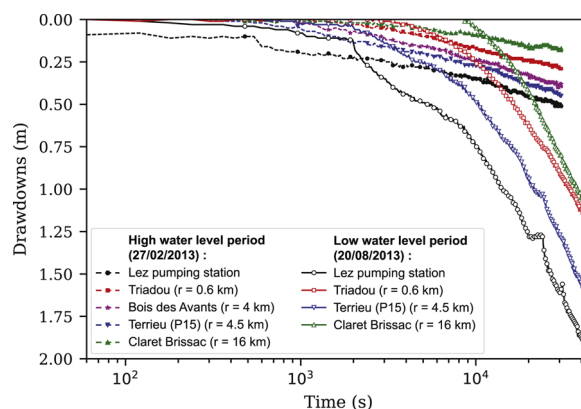


Fig. 4. Semi-log plot of the drawdowns observed at the Lez pumping station and at the observation boreholes Triadou, Bois des Avants, Terrieu (P15) and Claret Brissac in response to the daily pumping variations at the Lez station during high water levels (flow discharge at the Lez spring) and during low water levels (no discharge at the Lez spring).

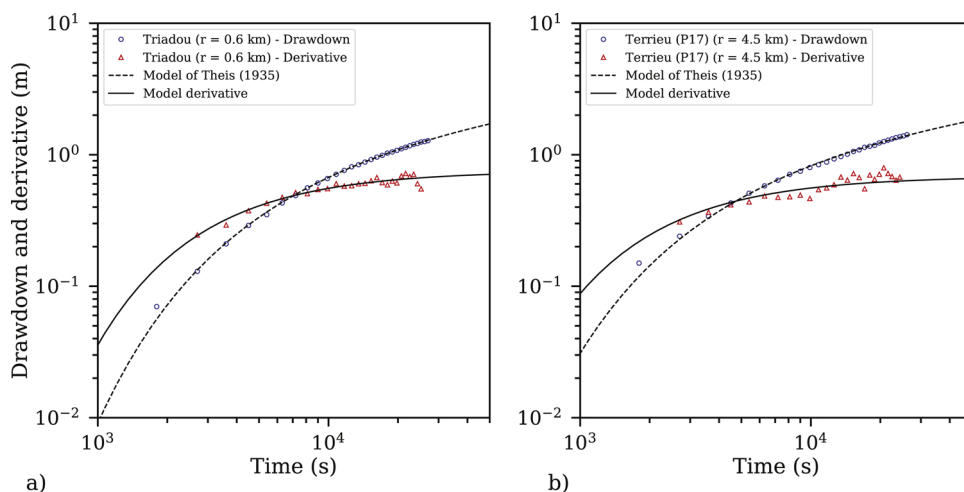


Fig. 5. Diagnostic plots of daily drawdown monitored at a) Triadou and b) Terrieu (P17) boreholes and its logarithmic derivative for the daily pumping cycle in June 20, 2012 (Fig. 3). The model of Theis (1935) is represented by a black dashed line for the drawdown curve and by a continuous black line for the derivative curve.

Table 2

Characteristics of the daily pumping responses at the Triadou and Terrieu (P17) boreholes due to the regional pumping at the Lez station, with no impact of discharge flow at the Lez spring (orange and red cycles in Fig. 3). The transmissivity (T) and storativity (S) were estimated from Theis' (1935) model.

Cycles	Duration (h)	$Q_{ave.}$ ($m^3 s^{-1}$)	Δs (m)		T ($m^2 s^{-1}$)		S (-)	
			Triadou	Terrieu (P17)	Triadou	Terrieu (P17)	Triadou	Terrieu (P17)
9	8.5	0.81	0.83	0.89	1.2×10^{-1}	1.3×10^{-1}	5.4×10^{-3}	6.7×10^{-5}
10	8	0.85	0.99	1.10	1.1×10^{-1}	1.2×10^{-1}	5.1×10^{-3}	5.7×10^{-5}
11	7.25	0.82	0.95	1.10	9.4×10^{-2}	1.2×10^{-1}	5.1×10^{-3}	5.5×10^{-5}
12	7	0.82	0.92	0.98	9.9×10^{-2}	1.1×10^{-1}	5.0×10^{-3}	6.7×10^{-5}
13	7.5	0.93	1.08	1.22	1.2×10^{-1}	1.2×10^{-1}	4.4×10^{-3}	5.7×10^{-5}
19	6	0.90	1.11	1.24	9.6×10^{-2}	1.0×10^{-1}	3.6×10^{-3}	4.8×10^{-5}
20	7.25	0.90	1.30	1.42	9.5×10^{-2}	1.0×10^{-1}	3.5×10^{-3}	4.2×10^{-5}
21	7.75	0.90	1.32	1.47	9.7×10^{-2}	9.5×10^{-2}	3.6×10^{-3}	4.9×10^{-5}
			Geometric mean		1.0×10^{-1}	1.1×10^{-1}	4.4×10^{-3}	5.5×10^{-5}

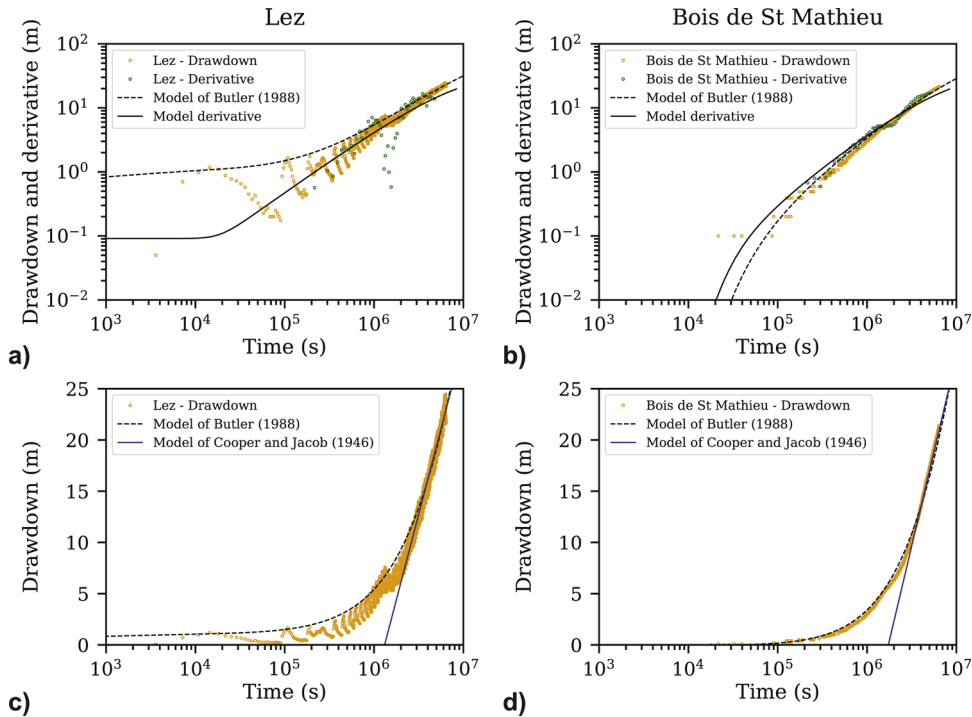


Fig. 6. Log-log plots of drawdown and drawdown derivative at a) the Lez pumping station and b) at the observation borehole Bois de Saint Mathieu. The radial composite flow model of [Butler \(1988\)](#) is represented by a black dashed line for the drawdown curve and by a continuous black line for the derivative curve. The semi-log plots of the drawdowns observed and modeled c) at the Lez pumping station and d) at the observation borehole Bois de Saint Mathieu is provided to compare with the Cooper-Jacob's approximation method applied previously.

Table 3

Hydraulic properties estimated with the radial composite flow model of [Butler \(1988\)](#) for the long-term pumping test at the regional scale (a fixed radius of extension for the first domain: $R = 5000$ m and average pumping rate of $4134 \text{ m}^3 \text{ h}^{-1}$ ($1.15 \text{ m}^3 \text{ s}^{-1}$) have been considered).

Wells	r (km)	Domain 1			Domain 2		
		$T_1 (\text{m}^2 \text{ s}^{-1})$	$S_1 (-)$	$D_1 (\text{m}^2 \text{ s}^{-1})$	$T_2 (\text{m}^2 \text{ s}^{-1})$	$S_2 (-)$	$D_2 (\text{m}^2 \text{ s}^{-1})$
Lez pumping station	0	1.0×10^0	3.0×10^{-3}	333	6.0×10^{-3}	1.0×10^{-4}	60
Triadou	0.6	5.0×10^{-1}	3.3×10^{-3}	153	6.0×10^{-3}	1.0×10^{-4}	60
Terrieu site (P20)	4.5	5.0×10^{-1}	3.0×10^{-3}	168	6.0×10^{-3}	1.0×10^{-4}	60
Claret Brissac	16	5.0×10^{-1}	7.5×10^{-4}	668	6.0×10^{-3}	5.0×10^{-5}	120
Les Matelles	4	5.0×10^{-1}	4.0×10^{-3}	125	6.0×10^{-3}	1.0×10^{-4}	60
Bois de Saint Mathieu	7	5.0×10^{-1}	2.7×10^{-3}	185	6.0×10^{-3}	6.0×10^{-5}	100
Gour Noir	2	5.0×10^{-1}	5.5×10^{-3}	91	6.0×10^{-3}	1.0×10^{-4}	60
St Gely du Fesc	4	5.0×10^{-1}	6.5×10^{-3}	77	6.0×10^{-3}	5.0×10^{-5}	120
Ste Croix de Q.	7	5.0×10^{-1}	4.8×10^{-3}	104	6.0×10^{-3}	1.0×10^{-4}	60
Mas de Martin	12.5	5.0×10^{-1}	3.2×10^{-3}	156	6.0×10^{-3}	5.0×10^{-5}	120
Bois des Rosiers	12.5	5.0×10^{-1}	2.7×10^{-3}	185	6.0×10^{-3}	5.0×10^{-5}	120
Bois des Avants	4	5.0×10^{-1}	5.7×10^{-3}	88	6.0×10^{-3}	5.0×10^{-5}	120
Fontanès	10	5.0×10^{-1}	2.7×10^{-3}	185	6.0×10^{-3}	5.0×10^{-5}	86
Geometric mean		5.4×10^{-1}	3.7×10^{-3}	193	6.0×10^{-3}	7.4×10^{-5}	91

4. Local scale investigations

4.1. Materials and methods

A pumping test was performed at the Terrieu experimental site ([Fig. 1b](#)) at borehole P0 during four days in April 2013 with a discharge rate of $50 \text{ m}^3 \text{ h}^{-1}$. Fifteen observation boreholes and the pumping well were monitored with TD and CTD-Diver transducers. The test was performed under high water level conditions with an initial water level at about 66.5 m amsl. Under these conditions, the daily interferences related to the pumping at the Lez station were minimized (see previous section) but still visible and superimposed on the local pumping test ([Fig. 7](#)). Pre-test water-level measurements have been used to identify and correct the regional effects (*i.e.*, regional pumping interferences and water-level trend). In order to remove the influence of these regional

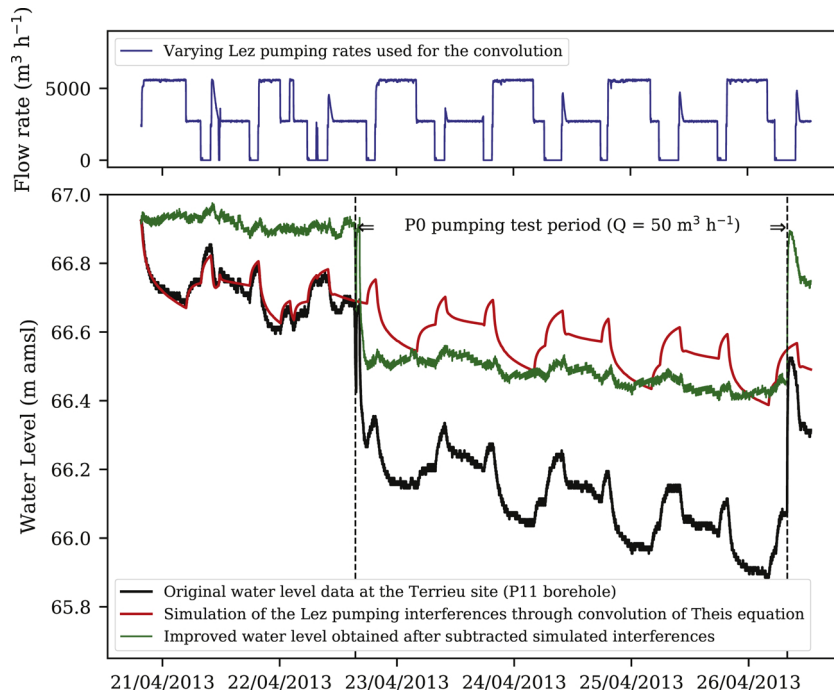


Fig. 7. Example of P11 water-level data processing (green curve) to improve the P0 pumping test analysis. The Lez pumping interference at the Terrieu site (red curve) was simulated by convolving the Theis' (1935) solution with the varying Lez pumping rates (blue curve), also accounting for the regional water-level trend with a linear coefficient correction, and then subtracted from the original data (black curve) (For interpretation of the references to colour in this figure legend, the reader is referred to the web version of this article).

interferences, the superposition principle in time and space was used (Reilly et al., 1984; Olsthoorn, 2008). First, the responses to the Lez pumping variations observed a few days before the P0 pumping test were used to estimate the hydraulic properties with Theis' (1935) solution for each observation well. Second, using the estimates of the hydraulic properties related to the Lez pumping and by convolution of the Theis' (1935) solution with the flow rate variation at the Lez station (Olsthoorn, 2008), the theoretical responses to the Lez pumping cycles obtained in the Terrieu observation boreholes were predicted throughout the measured period, *i.e.*, before and during the P0 pumping test. Third, the simulated interferences were subtracted from the data with a linear coefficient to correct the regional water level recession trend observed for this period (Fig. 7). This procedure made possible a drawdown derivative analysis in order to identify the flow regimes and thus improve the choice of the solution (Bourdet et al., 1989; Gringarten, 2008; Renard et al., 2009).

4.2. Results

The pumping test carried out at P0 in Terrieu induced significantly different drawdowns in all the nearby boreholes. The drawdown map clearly showed two main flow directions oriented at N070 and N160 (Fig. 8a). These features are well-known and were found consistently throughout the pumping tests conducted at the site. This is related to the structure of the reservoir, *i.e.*, the main fracture directions, which control the flow around the boreholes (Droque and Grillot, 1976; Jazayeri Noushabadi et al., 2011).

Fig. 8b shows, in log-log plot, the drawdown and derivative curves obtained for the P4 borehole for the pumping test at P0, after removing most of the regional influences of the Lez pumping. At early times, the drawdown derivative reflects the behavior of the local main flow zone with a short radial flow response; then, the drawdown derivative decreases between 2×10^3 and 2×10^4 seconds and then increases again. All the boreholes present the same kind of response characterized by a similar V-shape minimum on the drawdown derivative, typically associated with a double-porosity behavior (Gringarten, 1987; Renard et al., 2009). We thus considered that the flow regimes can be described through the double-porosity model of Moench (1984). This model is based on the concept of a fractured system embedded within blocks of lower permeability, characterized by a matrix specific storage (S_{sm}) and a matrix hydraulic conductivity (K_m). The flow occurs from the fractures to the pumping well and the water stored in the matrix blocks contributes to the flow in the fractures. A fracture skin is considered, which provides a resistance to flow from matrix to fractures (Moench, 1984). This transient analytical solution is derived for fully penetrating wells including wellbore storage and wellbore skin.

Table 4 presents the results obtained using the least-squares method to fit the model to the data (Fig. 8c). A constant fracture skin factor was set to fit the data using $s_f = 1$. The transmissivity values obtained for the fractured system range from 2.7×10^{-3} to $1.3 \times 10^{-2} \text{ m}^2 \text{ s}^{-1}$, and the storativity values range from 1.9×10^{-3} to 1.3×10^{-1} . The block matrix presents variable hydraulic conductivity ranging between 4.6×10^{-10} and $5.6 \times 10^{-6} \text{ m s}^{-1}$ and specific storage ranging between 3.5×10^{-6} and $8.2 \times 10^{-1} \text{ m}^{-1}$. The diffusivity values estimated for the fracture system ($D_f = T_f/S_f$) are about 7000 times greater than for the

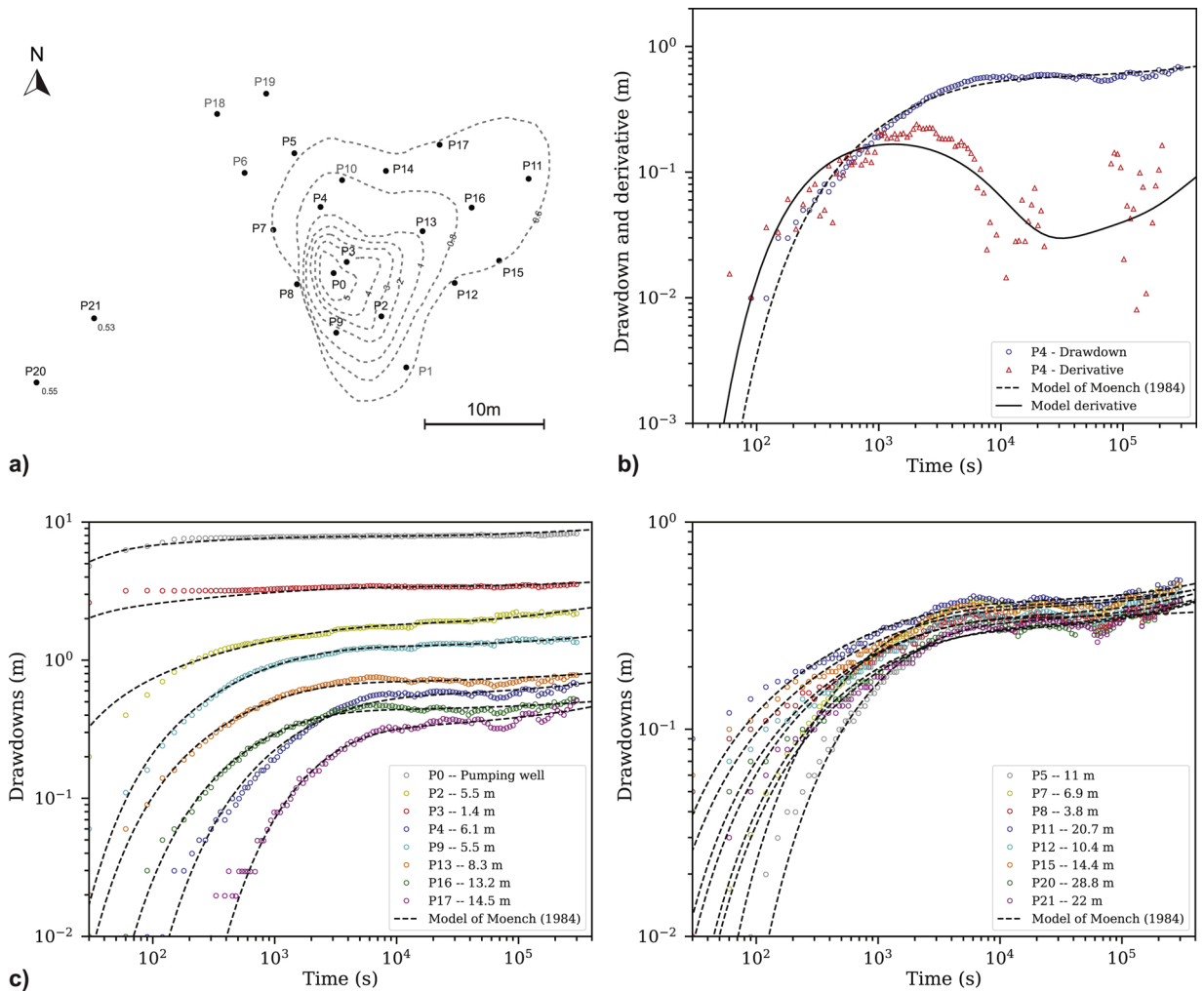


Fig. 8. Hydrodynamic responses during the long-term pumping test at the Terrieu site: a) Map of drawdowns measured at different boreholes 80 h after the beginning of the pumping test in P0; b) Diagnostic plot of drawdown monitored at P4 and its logarithmic derivative. The V-shape derivative is characteristic of double-porosity behavior. The Moench (1984) model is represented by a black dashed line for the drawdown curve and by a continuous black line for the derivative curve; c) Drawdowns and fit obtained with the Moench's (1984) solution using the least-squares method. Estimated parameters corresponding to the displayed matching curves are given in Table 4.

matrix blocks ($D_m = K_m/S_{sm}$).

5. Borehole scale investigations

5.1. Materials and methods

5.1.1. Methodology applied to the Terrieu boreholes

In order to locate the main flow zones along the boreholes, temperature and electrical conductivity loggings were performed under ambient conditions in several boreholes at the Terrieu site. Such logs may provide information on the location of the main flow zones if, at depth, fluid conductivity and temperature variations or anomalies are encountered that are likely to be related to water circulation in the borehole between the main flow zones (Drury, 1984; Keys, 1990; Chatelier et al., 2011; Klepikova et al., 2011). For a precise comparison, only the logs carried out at the same time are presented here (*i.e.*, P3, P5, P11, P13, P15, P17, P20). The temperature was measured with an accuracy of ± 0.1 °C and the electrical conductivity was accurate to $\pm 1\%$ of the reading. On average, the logs were made with 25 measurement points per meter.

To provide an estimate of the transmissivity of the main flow zones as well as of the surrounding fracture network and fissured matrix, 15 straddle-packer injection tests were made in P2, P5, P13 and P15 (Fig. 1b). To improve the estimate of the depth of the main flow zones in each borehole, borehole video logs were also used to control the borehole conditions before installing the packer system. Straddle packers were inflated at pressures from 7 to 12 bars depending on the water column above, in order to minimize the

Table 4

Computed hydraulic parameters with the [Moench's \(1984\)](#) model for the long-term pumping test at the local scale in borehole P0 at Terrieu (fixed parameters for skin well: $s_w = 1$, skin fracture $s_f = 1$, aquifer thickness: $e = 100$ m, and slab blocks thickness: $b = 10$ m).

Wells	r (m)	Fracture system			Blocks parameters		
		T_f ($\text{m}^2 \text{s}^{-1}$)	S_f (–)	D_{fracture} ($\text{m}^2 \text{s}^{-1}$)	K_m (ms^{-1})	S_{sm} (m^{-1})	D_{blocks} ($\text{m}^2 \text{s}^{-1}$)
P0	0	2.7×10^{-3}	$1.3 \times 10^{-5*}$	207.35*	2.9×10^{-9}	6.3×10^{-6}	4.6×10^{-4}
P2	5.54	3.7×10^{-3}	2.0×10^{-3}	1.85	1.1×10^{-7}	3.1×10^{-4}	3.5×10^{-4}
P3	1.44	4.7×10^{-3}	$7.5 \times 10^{-6*}$	623.38*	4.6×10^{-10}	3.5×10^{-6}	1.3×10^{-4}
P4	6.09	4.4×10^{-3}	1.3×10^{-1}	0.03	5.6×10^{-6}	1.3×10^{-1}	4.3×10^{-5}
P5	11	6.5×10^{-3}	4.8×10^{-2}	0.14	5.6×10^{-6}	7.5×10^{-2}	4.6×10^{-5}
P7	6.91	6.4×10^{-3}	6.6×10^{-2}	0.10	5.6×10^{-6}	2.0×10^{-2}	2.9×10^{-5}
P8	3.78	1.3×10^{-2}	1.1×10^{-1}	0.11	5.6×10^{-6}	8.2×10^{-1}	6.8×10^{-6}
P9	5.5	2.8×10^{-3}	1.6×10^{-2}	0.17	1.4×10^{-6}	3.5×10^{-2}	4.1×10^{-5}
P11	20.7	1.2×10^{-2}	1.9×10^{-3}	6.51	1.1×10^{-7}	1.1×10^{-3}	1.1×10^{-4}
P12	10.4	1.2×10^{-2}	1.8×10^{-2}	0.66	1.1×10^{-6}	8.6×10^{-3}	1.2×10^{-4}
P13	8.3	4.3×10^{-3}	1.5×10^{-2}	0.29	1.5×10^{-6}	7.4×10^{-2}	2.1×10^{-5}
P15	14.4	1.3×10^{-2}	5.4×10^{-3}	2.37	2.9×10^{-7}	2.7×10^{-3}	1.1×10^{-4}
P16	13.2	5.1×10^{-3}	1.5×10^{-2}	0.34	1.6×10^{-6}	1.5×10^{-1}	1.1×10^{-5}
P17	14.5	3.4×10^{-3}	5.9×10^{-2}	0.06	3.4×10^{-6}	9.2×10^{-2}	3.7×10^{-5}
P20	28.8	1.2×10^{-2}	3.4×10^{-3}	3.48	2.3×10^{-7}	1.8×10^{-3}	1.3×10^{-4}
P21	22	1.2×10^{-2}	6.6×10^{-2}	1.81	3.6×10^{-7}	2.7×10^{-3}	1.3×10^{-4}
Geometric mean		6.3×10^{-3}	1.6×10^{-2}	0.42	4.5×10^{-7}	7.1×10^{-3}	6.3×10^{-5}

* value not representative because of the effect of the P0 pumping well.

short-circuiting in the open borehole above and below the test interval. The hydraulic tests were conducted by injecting water into the 32 mm diameter inner pipes (NPS 1 ¼") from a water tank at the surface to the 0.7 m interval by means of a pump. The injection rate was measured with a flow meter (with a range of 0.01 L s^{-1} to 1.8 L s^{-1}) and the water pressure was monitored inside, as well as above and below the test interval, to identify potential short-circuiting. The injection reached quasi-steady state conditions after a few seconds or a few minutes, depending on the tested zone. A quasi-steady state was assumed to be reached when the pressure in the tested interval and the injection rate were both relatively constant. The transmissivity values were calculated by the Thiem's method for steady-state flow in a confined aquifer ([Bear, 1979](#); [Quinn et al., 2012](#)).

5.1.2. Methodology applied at the Triadou borehole

A 330 m deep borehole of 165 mm in diameter was drilled in the Valanginian, Berriasian and Kimmeridgian carbonates 580 m upstream of the Lez pumping station ([Fig. 1c](#)). In addition to cuttings analyses and video logs, rock resistivity measurements were carried out in the Triadou borehole to obtain a detailed characterization of the lithology and of the fractured zones ([Fig. 11a](#) and [b](#)). Many flow zones were first identified by air-lift during the drilling (black arrows in [Fig. 11b](#)). In order to localize precisely and estimate the transmissivity of the main flow zones, single-borehole flowmeter tests in combination with temperature and electrical conductivity loggings were performed under both ambient and pumping conditions. Comparisons between the ambient and pumping flowmeter logs allow estimates of the transmissivity of the inflow zones ([Paillet, 1998](#); [Le Borgne et al., 2006](#); [Lods, 2000](#)). These measurements were carried out for a few hours on July 2, 2012, *i.e.*, under low water level conditions. The vertical flowmeter profiles were obtained using a micro-impeller flowmeter, which can measure velocities to a minimum of 3 cm s^{-1} . The flow profile under pumping condition was conducted at approximately $16.8 \text{ m}^3 \text{ h}^{-1}$ (280 L min^{-1}) once the drawdown was relatively stable. The FLASH program developed by [Day-Lewis et al. \(2011\)](#) was used for the analysis of the vertical flow logs. The model is based on an analytical solution for steady-state multi-layer (or discrete fractures) radial flow to a borehole ([Paillet, 1998](#)).

5.2. Results

5.2.1. At the Terrieu boreholes

The temperature and electrical conductivity logs obtained at the Terrieu site revealed at least one major flow zone. [Fig. 9](#) presents the temperature and electrical conductivity profiles in P3, P5, P11, P13, P15, P17, and P20 and shows variation from 13°C to 14°C for the temperature and from 500 to $900 \mu\text{S cm}^{-1}$ for the electrical conductivity. These logs present one or two inflections with one located near the water table at around 60 m amsl and the other located between 45 and 50 m amsl depending on the borehole location. The second inflection is more or less marked but appears in all the boreholes. This flow zone determined from the temperature and electrical conductivity logs can be visible through borehole video investigations, and confirms the presence of an active karst conduit in some boreholes (*i.e.*, P0, P8, P11, P12, P15).

The 15 straddle-packer injection tests conducted in the boreholes P2, P5, P13 and P15 reveal a strong variability of the transmissivity over five orders-of-magnitude, ranging from 7.2×10^{-8} to $5.2 \times 10^{-3} \text{ m}^2 \text{s}^{-1}$. All results are presented in [Table 5](#). The transmissivity values obtained for the major flow zone also show a variability ranging from 1.3×10^{-6} to $5.2 \times 10^{-3} \text{ m}^2 \text{s}^{-1}$ depending on the location of the borehole. Some previous estimates of the transmissivity from single-hole vertical flow measurements with an electromagnetic flowmeter ([Lods, 2000](#)) conducted in boreholes P2, P5 and P16 (see [Table 5](#)), appear very consistent for this

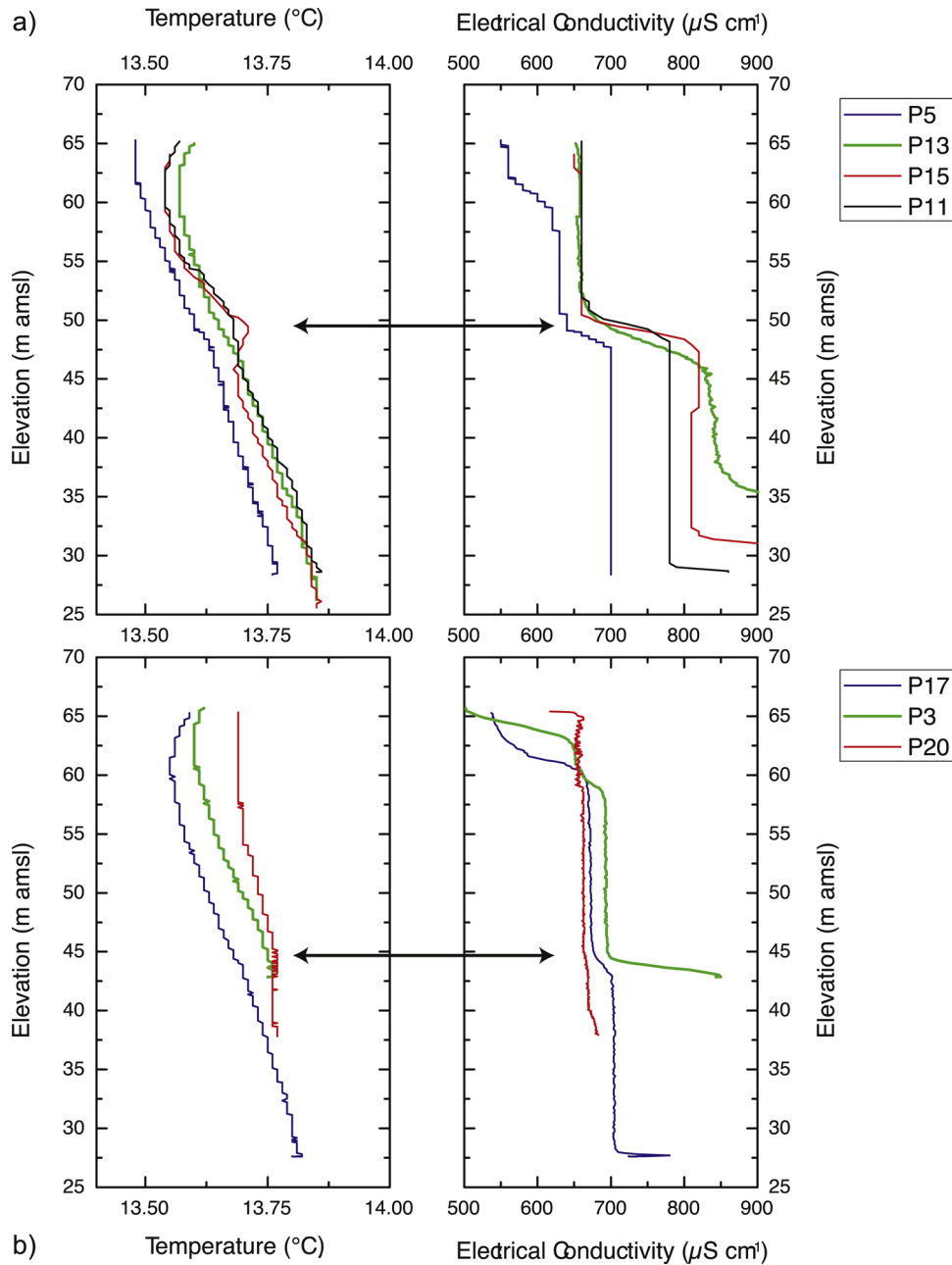


Fig. 9. Temperature and electrical conductivity logs in the P5, P13, P15, P11 boreholes at the Terrieu experimental site, made in June 2012 (a) and February 2013 (b). The main flow zone appears to be located between 45 and 50 m amsl (black arrows).

main flow zone. Interestingly, a passive observation at the P15 borehole using a straddle-packer system positioned in front of this main flow zone (*i.e.*, karst conduit) shows a strong influence by the Lez pumping in the isolated interval while observations above and below the packer system did not show a significant one (Fig. 10). This main flow zone located at around 50 m amsl corresponds to the elevation of the stratigraphic interface between marly limestone and hard limestone, potentially related to the Berriasian-Kimmeridgian transition (Fig. 10b). Remember that the continuous water level monitoring at the P20 borehole (Fig. 2a) showed that the amplitude of daily drawdowns due to the Lez pumping strongly decreases at the Terrieu site when the water levels are below 45 m amsl corresponding to the elevation of this main flow zone (Fig. 9b).

5.2.2. At the Triadou borehole

Fig. 11 shows the different logs registered at the Triadou borehole. Electrical resistivity log (Fig. 11a) shows clear lithology transitions with depth between the Valanginian, the Berriasian and the Kimmeridgian carbonates. The electrical resistivity increases

Table 5

Characteristics of the hydraulic tests at the borehole scale with the transmissivities obtained for the different tested zones in the boreholes of the Terrieu experimental site and the Triadou borehole. Data in bold represent the position and the transmissivity values of the main tested flow path. Details and complementary information about the different tests and analytical methods can be found in Lods (2000) and Dausse (2015).

Well	Hydraulic tests	Interpretation method	Elevation of the tested zones (m amsl)	T (m ² s ⁻¹)
P2 Terrieu	Constant head injection tests (Lods, 2000)	Lods' (2000) solution*	Full length	1.8×10^{-4}
	Single-hole electromagnetic flowmeter tests (Lods, 2000)	Lods' (2000) solution*	60.6 - 56.6	2.0×10^{-5}
	Straddle-packer injection tests (Dausse, 2015)	Thiem's equation	46.6 - 45.6	1.6×10^{-4}
			59.9 - 59.2	$2.6 \times 10^{-5**}$
			59.6 - 58.9	$6.1 \times 10^{-7**}$
			53.3 - 52.6	5.7×10^{-6}
			52.3 - 51.6	1.4×10^{-6}
			47.0 - 46.3	$1.4 \times 10^{-5**}$
			42.8 - 42.1	1.0×10^{-7}
			32.4 - 31.7	$7.0 \times 10^{-6**}$
P5 Terrieu	Constant head injection tests (Lods, 2000)	Lods' (2000) solution*	Full length	3.8×10^{-6}
	Single-hole electromagnetic flowmeter tests (Lods, 2000)	Lods' (2000) solution*	62.5 - 60.5	7.5×10^{-7}
			49.5 - 48.5	7.4×10^{-7}
			48.5 - 47.5	2.1×10^{-6}
	Straddle-packer injection tests (Dausse, 2015)	Thiem's equation	62.5 - 61.8	$1.9 \times 10^{-7**}$
			49.2 - 48.5	1.3×10^{-6}
P13 Terrieu	Straddle-packer injection tests (Dausse, 2015)	Thiem's equation	48.5 - 47.8	1.1×10^{-6}
			47.0 - 46.3	1.5×10^{-6}
P15 Terrieu	Straddle-packer injection tests (Dausse, 2015)	Thiem's equation	37.7 - 37.0	7.2×10^{-8}
			58.7 - 58.0	1.1×10^{-7}
			50.8 - 50.1	$3.1 \times 10^{-8**}$
			50.3 - 49.6	$5.2 \times 10^{-3**}$
P16 Terrieu	Constant head injection tests (Lods, 2000)	Lods' (2000) solution*	Full length	8.7×10^{-6}
	Single-hole electromagnetic flowmeter tests (Lods, 2000)	Lods' (2000) solution*	63.2 - 62.2	3.7×10^{-7}
			56.2 - 52.2	8.2×10^{-6}
Triadou	Single hole pumping test (Dausse, 2015)	Theis' (1935) solution	Full length	1.5×10^{-3}
	Single-hole spinner flowmeter tests (Dausse, 2015)	FLASH (Flow-Log Analysis of Single Holes) program based on the solution of Paillet (1998)	(2): 37 - 32	1.7×10^{-4}
			(3): -128 - -133	4.8×10^{-4}
			(4): -140 - -146	1.6×10^{-4}
			(5): -172 - -178	5.1×10^{-4}
			(6): -237 - -240	1.5×10^{-4}

* Lods (2000): solution for steady-state radial flow included non-linear skin effects.

** Average values from 2 or 3 tests performed on the same zone.

because of decreasing clay content in these carbonate facies. The borehole crosses first 200 m of Early Valanginian marls and marly limestone, before crossing 70 m of Berriasian (Early Cretaceous) limestone and 60 m of Upper Jurassic limestone (Fig. 11b).

The temperature and electrical conductivity logs show inflections that are characteristics of the main flow zones (Fig. 11c and d). The vertical flowmeter profiles (Fig. 11e) are fully consistent with the temperature and electrical conductivity logs. Six important flow zones, which are numbered in the Fig. 11, have been revealed by all the logs. In ambient condition, flow measurements were between 20 L min⁻¹ and 53 L min⁻¹. The downward flow observed in this condition could be attributed to the Lez pumping that significantly impacts the Triadou borehole (Fig. 3). Interestingly, two major outflows are located in the Berriasian limestone (zones 3 and 5) where one is located at the interface between the Berriasian and the Kimmeridgian limestones (Fig. 11). Under pumping conditions, these two major flow zones contribute to the flow by 65% of the total pumping rate. The estimated transmissivities using the FLASH program (Day-Lewis et al., 2011) range from 1.5×10^{-4} to 5.1×10^{-4} m² s⁻¹ (Table 5) where the transmissivity in zone (5) is the highest one.

6. Discussion

6.1. Hydraulic properties of the Lez aquifer

The numerous hydraulic tests performed at different spatial scales, from a few meters to more than 15 km, and temporal scales, from a few minutes to a few months, displayed a strong hydraulic property variability of the Lez karst aquifer (see Tables 1–5). The synthesis of these hydraulic properties is provided in Fig. 12.

The transmissivity values obtained at the borehole scale are, as expected, strongly variable and range from 3.1×10^{-8} to 5.2×10^{-3} m² s⁻¹. This large range is mainly due to the methods used, which allow to discretize and investigate low to high permeability features corresponding to fissured matrix and fractured-karstic network, respectively. Straddle-packer injection tests

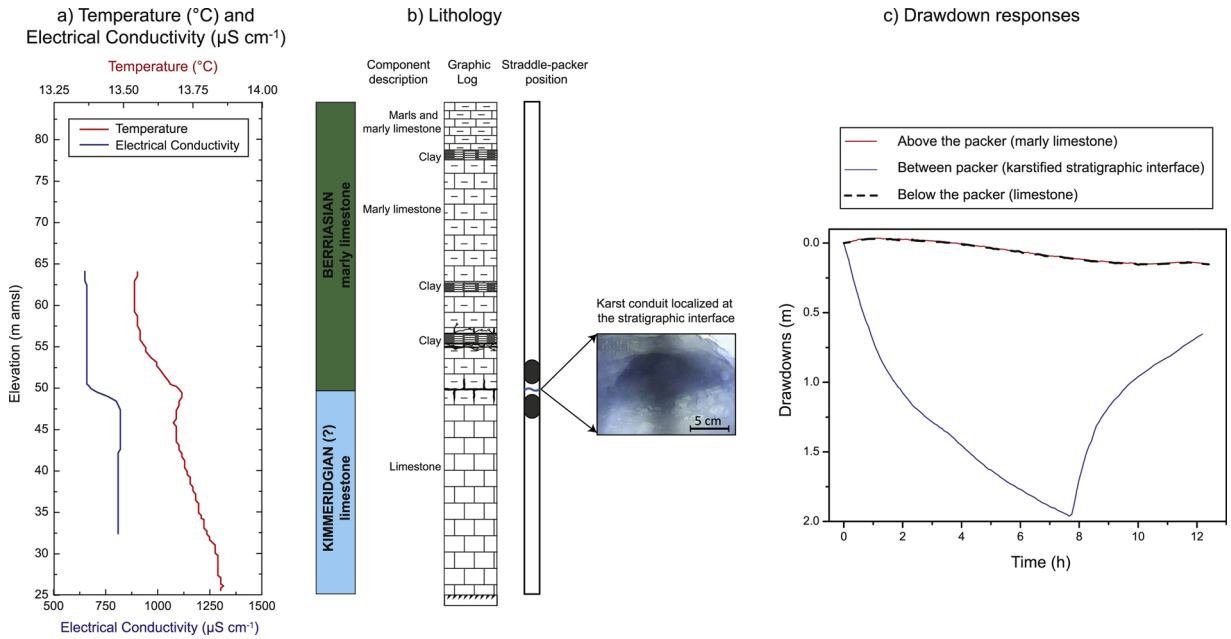


Fig. 10. Main karstic flow paths into borehole P15: location of the preferential flow path using a) The temperature and electrical conductivity logs; b) Lithology log from interpretation of drill cuttings (modified from Pitard, 1976) with position of the straddle-packer isolating the karst conduit at 50 m amsl; c) Drawdown responses in P15 above, between and below the straddle-packer in response to pumping at the Lez station.

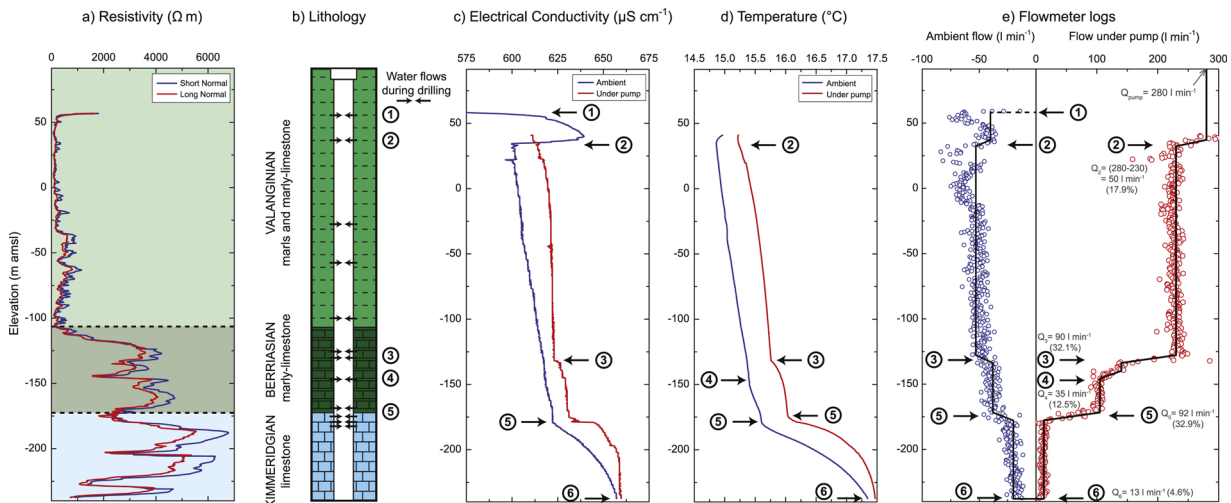


Fig. 11. Geological and hydrogeological logs in the Triadou borehole. a) The resistivity log of the formation has a wide range of values between a lithology rich in clay minerals (Valanginian marls) and more resistive Berriasian marly-limestone and Kimmeridgian limestone; b) Lithology log from interpretation of drill cuttings and resistivity logs; several water inflows were observed during drilling; c) Electrical conductivity; d) Temperature; e) Flowmeter logs measured under ambient and pumping conditions. The straight black line represents the flow modeled with the Paillet's (1998) solution. Six preferential flow zones, identified by number 1 to 6 in logs, were located into the Triadou borehole.

cover a broad range of transmissivity values, with some low estimates related to the fissured rock matrix while the impeller flowmeter instrument detects higher-permeability zones, generally related to the fracture network or karstic features (Fig. 11). At the local scale (P0 pumping test), the transmissivities appear less variable compared to straddle-packer tests and range from 2.7×10^{-3} to $1.3 \times 10^{-2} \text{ m}^2 \text{ s}^{-1}$, with a geometric mean value of $6.3 \times 10^{-3} \text{ m}^2 \text{ s}^{-1}$. The geometric mean transmissivity value obtained by pumping tests may correspond to the effective transmissivity of the investigated volume of the reservoir (Meier et al., 1998). Note that the transmissivity estimates can also be influenced by the location of the pumping well (e.g., Jazayeri Noushabadi et al., 2011). At the regional scale, the transmissivity values obtained using the Cooper-Jacob's method to analyze the long-term behavior (i.e., late times drawdown data of the seasonal pumping) also appear less variable and range from 3.8×10^{-3} to $7.8 \times 10^{-3} \text{ m}^2 \text{ s}^{-1}$. Interestingly, the geometric mean transmissivity value of $6.0 \times 10^{-3} \text{ m}^2 \text{ s}^{-1}$ (Table 1) appears similar to the mean transmissivity value

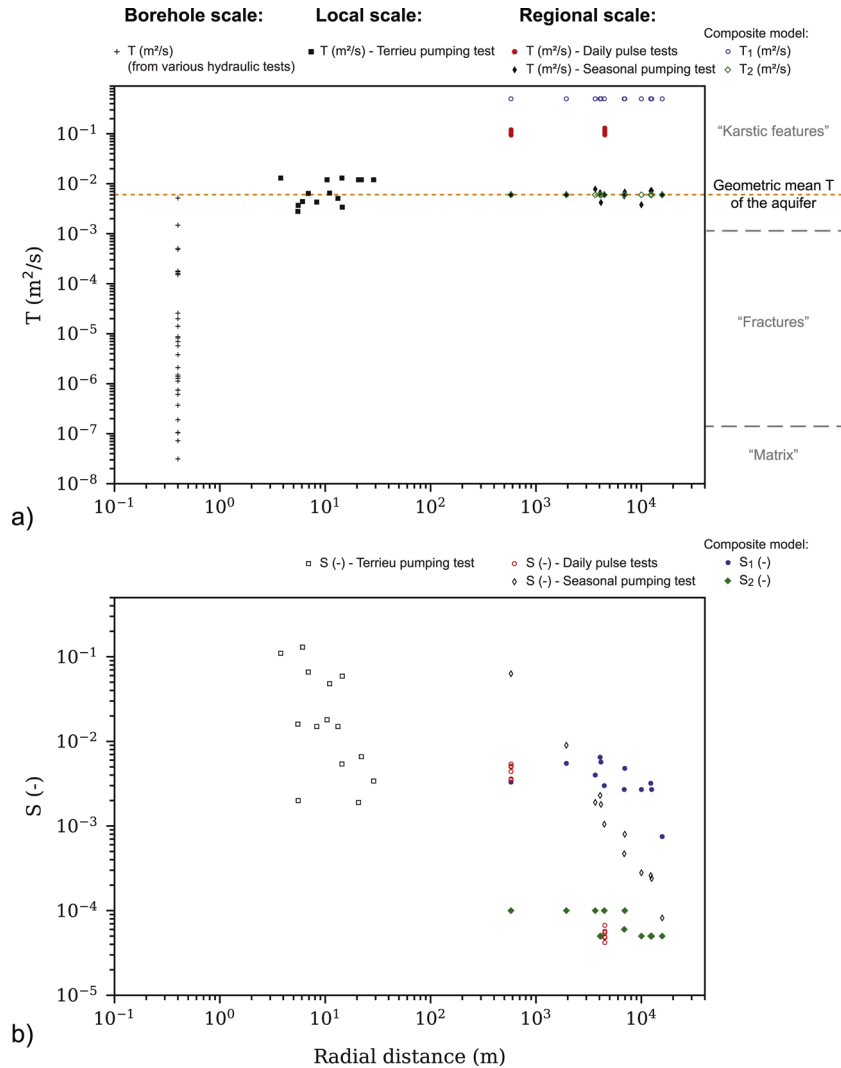


Fig. 12. Synthesis of hydraulic parameters of the Lez aquifer estimated at borehole scale (Table 5), local scale (Table 4) and regional scale (Tables 3 and 2 and 1): a) Transmissivity, b) Storativity.

obtained at the local scale by P0 pumping test, which might suggest that the geometric mean transmissivity of the reservoir is about $6.1 \times 10^{-3} \text{ m}^2 \text{ s}^{-1}$. The interpretation of the daily drawdown observations showed higher values of transmissivity, with a geometric mean value of $1.0 \times 10^{-1} \text{ m}^2 \text{ s}^{-1}$ (Table 2), suggesting a higher hydraulic connectivity between the observation boreholes and the main pumped karstic drain. Daily pumping tests may be comparable to high-frequency hydraulic periodic tests (*i.e.*, in this case pulse tests), which appear more sensitive to local heterogeneity (Cardiff et al., 2013; Gultinan and Becker, 2015) and to the main flow path network composed of highly conductive features (Fischer et al., 2018b). Indeed, sensitivity of observed drawdown to aquifer heterogeneity are known to be different related to the period of the pumping test (Cardiff et al., 2013). Proximity of the pumping well to higher permeable zone may cause a local increase in transmissivity estimated at shorter periods of pumping (Gultinan and Becker, 2015). The daily responses related to short periods of pumping are thus mainly impacted by the high transmissivity of the terminal karst conduit where the pumping well is located. The seasonal responses are related to long period of pumping test that investigate larger volume of the aquifer. The seasonal pumping effects appear to better integrate all the components of the reservoir that may contribute to flow. The long-time behaviors are known to be independent of the local heterogeneities (Butler and Liu, 1991). The lack of sensitivity to pumping well position is thus expected because transmissivity is derived from the late times behavior of the seasonal drawdowns. The different level of heterogeneity (*i.e.*, contrasted transmissivity) can be here represented at the first order using the radial composite flow model of Butler (1988), which allows to simulate the global behavior (early and late times) of the regional drawdowns. The interpretation using this model considers a first domain of high transmissivity (relatively similar to the mean transmissivity estimated from daily drawdowns analysis) embedded in a second domain of lower transmissivity corresponding to the mean transmissivity estimated from late times of seasonal drawdowns analysis.

Many investigations of karst aquifers point to increasing transmissivity as a function of the measurement scale (*e.g.*, Király, 1975;

Sauter, 1991; Rovey and Cherkauer, 1995; Schulze-Makuch and Cherkauer, 1998). The effect of scale on the transmissivity is often explained by an increase of the connectivity of preferential flow paths (Király, 1975; Sánchez-Vila et al., 1996; Le Borgne et al., 2006; Illman, 2006). However, the high transmissivity often estimated at larger scale may be biased as cross-hole tests are generally performed in the most permeable zones (Guimerà et al., 1995). The multi-scale investigations of the Lez karst aquifer confirm that any apparent scale dependency of the transmissivity is mainly related to the tested geological structures and strongly depends on the methodology used to investigate these structures.

Compared to seasonal responses, the lower values of storativity estimated for the Triadou and Terrieu boreholes from daily responses also confirm a better hydraulic connectivity to the Lez pumping station. Indeed, the storativity obtained using a radial flow model can be used as an indicator of the hydraulic connectivity in heterogeneous media (Meier et al., 1998; Sánchez-Vila et al., 1999; Knudby and Carrera, 2006). The use of simple classical solutions of Theis (1935) and its approximation of Cooper and Jacob (1946) to analyze short (daily pumping) and late times of the regional drawdown data provided a high variability of storativity, which ranges from 4.2×10^{-5} to 6.3×10^{-2} . The apparent correlation of these estimates with the distance observed in Fig. 12b can be attributed to the use of homogeneous radial flow model in heterogeneous reservoirs (Meier et al., 1998). The analyses with the composite model of Butler (1988) may provide better storativity estimates, with storativity ranging from 7.5×10^{-4} to 6.5×10^{-3} for the first domain and from 5.0×10^{-5} to 1.0×10^{-4} for the second domain. The values obtained at the local scale (*i.e.*, Terrieu site), which range from 1.9×10^{-3} to 1.3×10^{-1} , might be here representative of the effective porosity due to strong local hydraulic connectivity.

6.2. Importance of karst bedding-plane structures on groundwater flow

In addition to faults and karstic features, the multi-scale observation also suggests the presence of a sub-horizontal structure, which seems to significantly impact the hydraulic connectivity and the flow organization of the reservoir. At the Terrieu site, temperature and conductivity logs collected in several boreholes displayed one main flow zone throughout the site. By isolating this zone with straddle-packers, pressure responses related to the regional pumping clearly indicated localized flow within the structure (Fig. 10c). This behavior is confirmed by the decreases in amplitude of the daily influences when the water levels at the Terrieu site reach levels below this zone (see zoom at Fig. 2a). Although this structure was cross-cut by all the boreholes, its transmissivity appears strongly variable and ranges from 1.3×10^{-6} to $5.2 \times 10^{-3} \text{ m}^2 \text{ s}^{-1}$. Note that the highest estimated transmissivity corresponds to the karstic conduit observed at the site. This sub-horizontal structure may be related to the bedding-plane between the marly-limestone and massive limestone, which potentially corresponds to the transition between Cretaceous (Berriasian) and Jurassic (Kimmeridgian) limestones. This Kimmeridgian-Berriasian interface follows the NE-SW monocline dipping $15\text{--}20^\circ$ towards the WNW at the Terrieu site (Jazayeri Noushabadi et al., 2011). The main karst conduit observed at this site appears as preferentially developed at the intersection between this interface and the fractures (Droque and Grillo, 1976; Jazayeri Noushabadi et al., 2011). This preferential karstification seems to be controlled mainly by interactions between bedding-planes and fractures as shown in former studies (Lauritzen and Lundberg, 2000; Filipponi et al., 2009).

At the regional scale, the Viols en Laval boreholes, located to the West of the Matelles-Corconne fault, were not influenced by the Lez pumping to the East of the fault whereas all the other boreholes were impacted. This behavior suggests a compartmentalization of the reservoir either by the presence of the Matelles-Corconne fault or by the absence of connected structures, which can be linked to the absence of the Kimmeridgian-Berriasian interface in this compartment. The second hypothesis, which is also consistent with the observation at the Terrieu site, is supported by several indications. First, the impeded cross-fault flow generally occurs where the permeability of the fault core is reduced (Bense et al., 2013). However, the Matelles-Corconne fault seems to be permeable enough to transmit the signal of the Lez pumping to the Claret Brissac borehole (Fig. 2b). Second, the flowmeter tests carried out at the Triadou borehole have shown a significant flow zone located at the contact between the Kimmeridgian and the Berriasian stratigraphic units. The importance of this flow zone is highlighted by the downward flow observed under ambient conditions, which suggests the influence of the Lez pumping that tends to withdraw water and localized flow in this structure. This is further consistent with the ability of the radial composite flow model to represent the global hydrodynamic behavior (early and late times responses) at regional scale, which suggests flow within a 2D structure. Finally, the main karst conduit at the pumping station was mainly developed along the discontinuity between the Kimmeridgian and the Berriasian units (Fig. 1c) as shown by Marjolet and Salado (1975) and Leonardi et al. (2013). Thus, the Kimmeridgian-Berriasian interface appears to be an important structure for the groundwater flow at the Lez reservoir and may control the connectivity of the fault and karstic conduits networks at the regional scale. The presence of a large and sub-horizontal structure appears to increase the hydraulic connectivity of the fracture network and may contribute to develop the karstic network. Indeed, speleogenesis studies conducted in other carbonate reservoirs have demonstrated that most karstic conduits mainly follow bedding-plane structures (Palmer, 1991; Filipponi and Jeannin, 2008; Filipponi et al., 2009). Galvão et al. (2016) also showed for the aquifer of Sete Lagoas (Minas Gerais, Brazil) that the localized development of the sub-horizontal karstic bedding dissolution controlled the aquifer permeability at both local and regional scales.

To summarize all the observations, Fig. 13 presents a 3D hydrogeological conceptual model of the Lez aquifer. As mentioned previously, the Berriasian and the Kimmeridgian limestones constitute the main aquifer formations where fractures and karstic networks are well developed. The major NE-SW faults illustrated in Fig. 13 significantly influence groundwater flow at the regional scale. As in the case of the karstic network, these faults may strongly channelized flow over several kilometers. As demonstrated by isotopes and geochemical tracer analyses, these faults also contribute to water mixing by connecting shallow and deeper zones (Bicalho et al., 2012, 2017). The contact between the Berriasian and the Kimmeridgian is shown to have a significant influence for flow at the regional scale. The multi-scale hydrogeological investigations carried out here suggest the importance of this structure. The flow appears likely to be localized at this interface and in its absence, the reservoir is compartmentalized. In this reservoir, flow

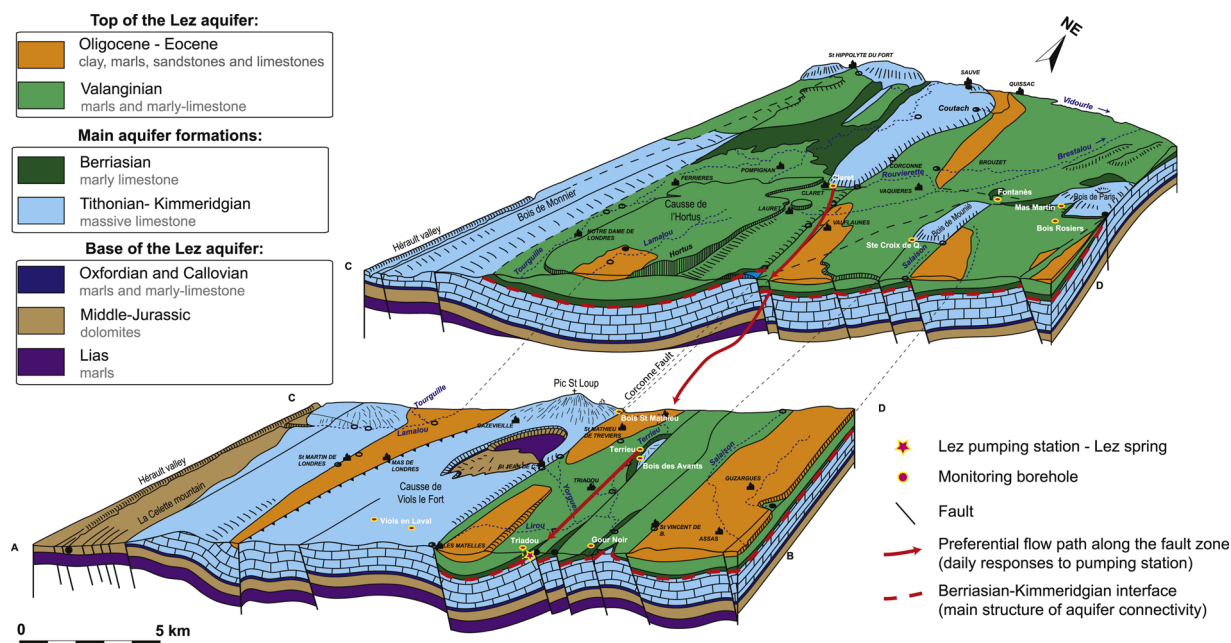


Fig. 13. Three-dimensional conceptual model of the main hydraulic connectivity structures of the Lez aquifer (modified from Paloc, 1979).

ranking appears very important and confirmed by the distribution of transmissivity, which is below $10^{-7} \text{ m}^2 \text{ s}^{-1}$ for the matrix, varies from 10^{-7} to $10^{-3} \text{ m}^2 \text{ s}^{-1}$ for the fracture network, and above $10^{-3} \text{ m}^2 \text{ s}^{-1}$ for the karstic features (Fig. 12). Even though karstic conduits and fault zones provide locally large transmissivities, the sub-horizontal 2D interface may constrain the hydraulic connectivity of the reservoir. The hydraulic connectivity at the regional scale appears to be based on the contact between the Berriasian and the Kimmeridgian, which contributes to drain the surrounding fracture network where flow may be more diffuse. Note that the bedding-plane structures do not always have the same transmissivity, which results in strong heterogeneity as observed at the Terrieu site.

7. Conclusions

The multi-scale hydraulic investigations performed at the Lez karst aquifer illustrated a strong variability of hydraulic properties as well as a clear flow ranking. The transmissivity of the Lez aquifer obtained by several methods provide values below $10^{-7} \text{ m}^2 \text{ s}^{-1}$ for the matrix alone, ranging from 10^{-7} to $10^{-3} \text{ m}^2 \text{ s}^{-1}$ for the fracture network, and above $10^{-3} \text{ m}^2 \text{ s}^{-1}$ for the karstic features. A large sub-horizontal flow-bearing structure, here the contact (*i.e.*, the bedding-plane) between the Kimmeridgian and Berriasian limestone units, appears to significantly impact the hydraulic connectivity of the reservoir at the regional scale. The other structures of the reservoir, *i.e.*, the faults, the karst conduits and the fracture network, may be well connected to this interface. In the absence of the interface, the reservoir seems to be compartmentalized (loss of connectivity), which highlights the fact that this flow-bearing structure plays a major role in large-scale connectivity of the aquifer. The flow appears strongly localized within this structure despite the strong heterogeneity of the reservoir. Because this structure seems to insure the connectivity of the reservoir at larger scales, it allows large volumes of water to be drained out of the karst aquifer, which insures the sustainability of the water supply.

Such spatial characterization of hydraulic heterogeneity and identification of the main flow-bearing structures is of prime importance for groundwater resources management and protection. The influence of bedding-plane structure on connectivity and groundwater flow, highlighted for the Lez aquifer, may also be valid in other karstic areas in the world. The fact that flow appears strongly localized at this interface may be critical for groundwater exploitation and vulnerability. Indeed, short transit time of contaminants transport would be expected due to strong channelized flow. Such phenomena could also be enhanced by the development of karst conduits at the intersection between interfaces and major fractures. These flow-bearing structures appear thus to be critical in predictive modeling of contaminant transport in such aquifers.

Declaration of Competing Interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

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Appendix A. Supplementary data

Supplementary material related to this article can be found, in the online version, at doi:<https://doi.org/10.1016/j.ejrh.2019.100627>.

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