

Optimization of ciprofloxacin degradation in wastewater by homogeneous sono-Fenton process at high frequency

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Katia González-Labrada, Diana Rosa Alcorta Cuello, Israel Saborit Sánchez, Marise García Batle, Marie-Hélène Manero, et al.. Optimization of ciprofloxacin degradation in wastewater by homogeneous sono-Fenton process at high frequency. Journal of Environmental Science and Health, Part A, 2019, pp.1-10. 10.1080/10934529.2018.1530177 . hal-02354658

HAL Id: hal-02354658 https://hal.science/hal-02354658

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González-Labrada, Katia[®] and Alcorta Cuello, Diana Rosa and Saborit Sánchez, Israel and García Batle, Marise and Manero, Marie-Hélène[®] and Barthe, Laurie[®] and Jáuregui-Haza, Ulises Javier *Optimization of ciprofloxacin degradation in wastewater by homogeneous sono-Fenton process at high frequency.* (2019) Journal of Environmental Science and Health, Part A. 1-10. ISSN 1093-4529

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1	Optimization of ciprofloxacin degradation in wastewater by homogeneous sono-Fenton
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20	Abstract
21	Emerging pollutants such as pharmaceuticals have been focusing international attention for a
22	few decades. Ciprofloxacin (CIP) is a common drug that is widely found in hospital and
23	wastewater treatment plants effluents, as well as in rivers. In this work, the feasibility of CIP
24	degradation by ultrasound process at high frequency is discussed and sonolysis, sonolysis
25	with hydrogen peroxide and sono-Fenton are evaluated. The amounts of hydrogen peroxide

and ferrous ions (Fe^{2+}) needed were optimized using response surface methodology. Best 26 27 results were obtained with the sono-Fenton process resulting in a total pharmaceutical degradation within 15 minutes and a mineralization greater than 60% after one hour. Optimal 28 29 conditions were tested on a real matrix from a municipal wastewater treatment plant. Even if 30 the degradation of the pollutants by sono-Fenton was hampered, the removal efficiency of 31 both CIP and total organic carbon (TOC) is interesting as an increase in the biodegradability 32 of the wastewater is found. These results show that sono-Fenton oxidation can be a promising 33 pre-treatment process for pharmaceutical-containing wastewaters.

34

KEYWORDS: Advanced oxidation processes, pharmaceuticals, optimization, sono-Fenton,
 ultrasound, wastewater treatment

37 Introduction

38 The use of thousands of tons of pharmaceuticals to treat human and animal illnesses, but also 39 in farming and aquaculture has become a serious problem for environment and human health. ^[1-4] They could be toxic to aquatic life when released in the environment ^[5-9], even at very 40 low concentrations (parts-per-trillion to parts-per-billion) in aquatic systems. ^[10, 11] Depending 41 42 on the drugs, up to 95% of the administered dose can be excreted unchanged or as active metabolites and enter the environment altering rivers, lakes and groundwater. ^[1-4,12] Most 43 44 drugs are designed so that they keep their chemical structure long enough to exert their 45 therapeutic effect. This property, combined with their continuous input into the ecosystem, may enable them to persist for an extended period of time. ^[13] Antibiotics are of particular 46 concern because their presence in natural waters could contribute to the rise of antibiotic 47 resistance in microorganisms. [14-19] 48

Fluoroquinolones are a group of antibiotics widely used in human and animal therapy. Among
 them, ciprofloxacin (1-cyclopropyl-6-fluoro-4-oxo-7-piperazin-1-ylquinoline-3-carboxylic

51 acid, CIP) is a non-biodegradable antibiotic that has been detected in wastewater treatment 52 plant effluents in concentrations from 5.6 μ g L ⁻¹ to 6.5 mg L⁻¹. ^[21, 22] The molecular structure 53 of CIP is shown in figure 1.

54 Conventional wastewater treatment processes such as biological degradation or adsorption have been verified to be ineffective for the removal of most antibiotics. ^[17, 20]In recent years, a 55 considerable interest has been shown in the development and application of Advanced 56 57 Oxidation Processes (AOPs) for the treatment of pharmaceutical contaminants in water. ^[7, 23] 58 Several techniques such as ozonation, photocatalysis or UV/H₂O₂ have been the focus of a 59 great deal of research. More recently, ultrasonic irradiation has received significant attention thanks to its ability to promote the fast degradation of environmental pollutants in water. ^{[24,} 60 ^{25]} The mechanism of sonolysis is based on cavitation, which is the formation, growth, and 61 62 sudden collapse of bubbles in liquids. The collapse of these bubbles leads to extremely high 63 local temperatures and pressures. These localized hot spots were estimated to have temperatures of roughly 5200 K, pressures of about 500 atm and lifetimes of a few 64 microseconds. ^[26-28] Two possible degradation routes are usually proposed. First, the 65 66 contaminant can undergo thermal degradation inside the cavity and in the interfacial region 67 (cavity-liquid). Second, formed free radicals (mainly OH[•]), can react with the contaminant in the interfacial region or in the bulk solution. ^[29] This route allows sonolysis to be considered 68 69 as an AOP. High frequency ultrasound (US) generally raises the amounts of free radicals 70 because there are more cavitational events which subsequently lead to an increase in 71 contaminant degradation. However, an optimum frequency maximizes the degradation rate of 72 pollutant. The same phenomenon occurs with the ultrasound power. An increase of ultrasound 73 power could improve the degradation of pollutants; the rates of degradation may decrease 74 with further increase in power that is beyond its optimum value due to bubble cloud formation on the ultrasonic probe surface.^[30] The addition of strong oxidants such as hydrogen peroxide 75

or Fenton reagent to sonolysis can be used to improve the biodegradability of a real
 pharmaceutical wastewater. ^[23, 31, 32]

There are not many previous studies concerning the sonolysis of CIP and its combination with 78 79 H₂O₂ and the Fenton reagent. The influence of operational parameters in the sonolysis on CIP degradation and CIP initial concentration was studied by De Bel and collaborators.^[33] Xiao et 80 al. ^[11] studied the role of matrix organic compounds on the sonolysis of CIP in aqueous 81 82 solutions. The effective destruction of CIP at the frequencies of 20 and 620 kHz has been 83 proven. It was also demonstrated that a larger size and lower concentration of matrix organics 84 in water have a smaller impact on the CIP degradation as compared to a smaller size and higher concentration of matrix organics.^[11] A report on ultrasound assisted Laccase catalysed 85 degradation of CIP at low frequency, 22 kHz, showed a maximum degradation of 51% at 86 0.02% (wt v⁻¹) enzyme loading. As compared to conventional method, this technique not only 87 increases CIP degradation rate but also reduces degradation time. ^[34] Moreover, it was 88 observed that pH affected the ultrasonic degradation rate of aqueous CIP solution.^[35] 89

In previous studies, Quesada et al. ^[30] showed that the integration of AOPs with the use of oxidants such as hydrogen peroxide and Fenton's reagent improved the degradability of pharmaceutical pollutants in water. They reported the use of H_2O_2 as a radical promoter to the sono-degradation of paracetamol and levodopa. It has been also reported that the Fenton chemistry combined with ultrasound treatment remarkably enhanced the sulfadiazine ^[36] and paracetamol ^[32] degradation when concentrations of H_2O_2 and Fe²⁺ are optimized.

In this study, the application of sonolysis for the degradation of CIP in water is examined. The intensification of the oxidation with H_2O_2 and the Fenton reagent under acidic conditions on the CIP degradation rate is studied. Moreover, the hydrogen peroxide concentration and relation between $c(H_2O_2)/c(Fe^{2+})$ in the sono-Fenton process are optimized using surface response methodology (SRM). In addition, the best sono-Fenton conditions were evaluated on a real matrix from a municipal wastewater treatment plant (WWTP).

102 Materials and Methods

103 Reagents

All solutions were prepared by dissolving CIP (Sigma-Aldrich, 99%) in distilled water. The pH adjustment was carried out using 1 M solution of H₂SO₄, which was prepared with concentrated sulfuric acid (95–97% purity) from Sigma-Aldrich. For high-performance liquid chromatography (HPLC) analysis, acetonitrile (HPLC quality) and o-phosphoric acid (85%) from Merck and Fisher, respectively, were used. The other chemicals employed were FeSO₄·7H₂O (99.5%), potassium iodide (99.5%), sodium hydroxide (99%) and sodium sulfite (98%) obtained from Sigma-Aldrich, and hydrogen peroxide (30% wt v⁻¹), from Fluka.

111 Sonication experiments

112 An US multifrequency generator (Meinhardt Ultraschall technik) operating in continuous 113 mode at frequencies of 580 and 862 kHz and variable electric power output was connected to 114 a stainless steel transducer (E 805/T/M, Ø 40 mm) for the sonication experiments. Actual 115 power dissipated into the liquid was measured by the standard calorimetric method according to procedures detailed in other studies. ^[26, 27] Reactions were performed in a 0.5 L cylindrical 116 117 glass reaction vessel (internal \emptyset 75 mm) with the transducer placed at the bottom of the vessel 118 in direct contact with the solution, at a depth of 57 mm from the liquid surface. Cooling of the 119 reaction mixture was achieved by circulating water through the vessel jacket, to maintain an 120 average temperature of 30±1°C, monitored by a thermometer immersed in the solution. The 121 experimental set-up is shown in figure 2. Solution pH was adjusted to the initial value (pH 3), but not controlled over reaction time due to the particularities of the reactor. All US 122 123 experiments were performed with 250 mL of aqueous solutions containing CIP at 100 mg L^{-0} . Sono-Fenton experiments were carried out with a relation of concentrations of H₂O₂/Fe²⁺ 124 125 between 2-6.

126 The best conditions obtained for the sono-Fenton experiment were tested in a real matrix. Influent samples were collected from WWTP "María del Carmen", in Boyeros, Havana City, 127 128 Cuba, (W 82.40; N 23.04). Samples were collected in 2.5 L amber glass bottles and 129 transferred from the WWTP to our laboratory in cooled box and then kept refrigerated (+4 130 °C). Wastewater samples were filtered after reaching room temperature using medium density 131 cellulose filter. The samples were then acidified to pH 3 by adding H₂SO₄. The wastewater 132 was characterized by Standard Method for the examination of water and wastewater.^[37] In 133 all experiments, liquid samples periodically were drawn from the reaction vessel for chemical 134 analyses; the total volume withdrawn during a single experiment was less than 6% of the total reacting volume. A solution containing KI, Na₂SO₃, and NaOH (each 0.1 M) was used to 135 136 quench the reaction in the samples when H_2O_2 and the Fenton reagent were used. The 137 obtained precipitate was removed on a 0.45 µm RC syringe filter prior to chemical analyses.

138

139 Chemical analysis

140 An HPLC system (SHIMADZU Prominence High Pressure model), involving a two solvent 141 delivery pump, UV/VIS diode array detector (SHIMADZU SPD-M20A model) and an 142 autosampler was used to follow the concentration-time profiles of CIP. The antibiotic was 143 analyzed at 40°C using a RP18 column (Super Sphere 100 model, 250 mm×4.6 mm; 5 µm) 144 with acetonitrile/ acidified water 13/87% (v/v) at 1.5 mL min⁻ⁱ as the mobile phase. The injection volume was 20 µL, and detection was set at 278 nm. The CIP retention time was 145 146 about 9 min. The calibration curve ($R^2 = 0.999$) was obtained from external standards prepared with known concentrations of the target compound. 147

A total organic carbon (TOC) analysis was performed using a TOC-LCPN Shimadzu analyzer
equipped with a non-dispersive infrared detector. The injection volume was 50 μL. The

150 combustion reaction was achieved in a quartz pipe at 680 °C with a regular platinum catalyst. *151* The carried flow was oxygen at 150 mL min⁻¹.

152 Degradation experiments were performed at an initial CIP concentration of 100 mg L^{-t} , 30°C,

153 pH 3, and frequencies of 580 and 862 kHz and at three different ultrasonic powers. The

154 degradation of CIP by the US–process, D, is defined by Equation 1.

$$D(\%) = \frac{Co - C}{Co} * 100$$
(1)

155 where C_o represents the initial concentration of CIP and C is the concentration of CIP at time 156 t. The mineralization (M) of CIP in the US-process, based on TOC concentration, was 157 calculated by Equation 2.

$$M(\%) = \frac{TOCo - TOC}{TOCo} * OCo$$
⁽²⁾

158 where TOC_o represents the initial concentration of the total organic carbon and TOC is the 159 concentration of total organic carbon at time t.

160 For checking the reproducibility of the evaluated processes, some experiments were161 triplicated. The observed relative error was less than 5% for CIP concentration and TOC.

162

163 Results and discussion

164 Influence of ultrasonic frequency and power

165 The most important parameters in the sonolysis process are ultrasound power and frequency.166 The sonochemical degradation of CIP at different powers was investigated using a 2x3

167 experimental design (Table 1), for two ultrasonic frequencies: 580 and 862 kHz. Figure 3 168 shows the influence of ultrasonic frequency and power on CIP degradation and mineralization 169 at 100 mg L^{-0} initial concentration, 30°C and pH 3. The best mineralization and degradation 170 correspond to the highest power for both values of frequency studied. Figure 3 shows that the 171 highest efficiency on CIP degradation after 120 min was obtained at 580 kHz.

172 US power affects cavitational activity and has a significant influence on TOC removal (22%) 173 mainly at the lowest frequency. In these experimental conditions, the initial removal rates 174 increased with the power. Similar results were obtained for US degradation of levodopa and 175 paracetamol at 574 and 860 kHz, but significantly lower removals were reported, 66 and 67% respectively, at the highest frequency 1,134 kHz. ^[30] De Bel et al. ^[33] found that the lowest 176 frequency, 544 kHz, proved to be the most favorable on CIP degradation. The ultrasonic 177 178 frequency significantly affects sonolysis due to both the critical size and lifetime of cavitation bubbles, which consequently affects the number of cavitation bubbles, the violence of the 179 bubble collapse and the OH• radical production. ^[11, 38, 39] Higher ultrasound frequencies are 180 more effective for generating hydroxyl radicals owing to the rapid microbubble collapse. 181 182 However, a maximum frequency should not be exceeded to avoid affecting degradation rates 183 and cavitation effects. Actually, the rarefaction cycle of the sound wave produces a negative 184 pressure and the compression cycle occurs faster than the time needed for the microbubble to collapse. Therefore, fewer HO[•] radicals are released. ^[39] Other authors have reported faster 185 degradation of organic compounds at 200-600 kHz frequencies.^[11, 39-42] In any case, the 186 operating frequency must be optimized for the particular US-driven treatment process. 187 188 However, due to the formation of highly hydrophilic by-products during the process, poor 189 mineralization is usually observed using this process alone. ^[43]

Table 2 shows the pseudo first-order rate constant as a function of US frequency and power.
The degradation of CIP by the US–Sy the ada consistent with pseudo-first-order kinetics, as
follows:

193

$$\frac{-dc}{dt} = kc; \ \ln\frac{c_0}{c} = kt \tag{3}$$

194

195 De Bel et al. ^[33] found comparable results for CIP sono-degradation at 25°C as the production 196 of HO[•] radicals was the highest at 544 kHz (k_1 equal to 0.0067 min⁻¹), in comparison with 801 197 kHz ($k_1 = 0.0055 \text{ min}^{-1}$) and 1081 kHz ($k_1 = 0.0018 \text{ min}^{-1}$).

198 Sonochemical reactions would be favored by an increase in US power at a fixed frequency. It 199 is widely accepted that higher ultrasonic power input increases the frequency of cavitation, 200 the number of active cavitation bubbles, the size of individual bubbles, as well as the rate of generation and concentration of hydroxyl radicals. ^[44] During ultrasonic irradiation, two main 201 202 reactions occur: (1) pyrolysis due to the high temperature and pressure in the gas phase, and 203 (2) hydroxyl radical attack in the bubble-liquid interface and/or in the bulk liquid. Gas phase 204 pyrolytic reactions are considered to play a minor role in the case of non-volatile solutes. According to its low volatility (Henry's law constant = -18.3 atm.m³ mol⁻¹ at 25°C^[11]) and 205 low water solubility (Log $K_{ow} = 0.28$ ^[45]), it has been demonstrated that the attack of hydroxyl 206 207 radicals on CIP molecules is the dominant reaction. [33, 35] Recent studies revealed the intensification of the sonochemical degradation of levofloxacin at 20 kHz using carbon 208 tetrachloride as a rate enhancer. ^[44] The formation of °Cl radicals will lead to a series of 209 210 recombination reactions conducting to the formation of additional active species, such as 211 HClO, Cl₂ and chlorine-containing radicals (Cl[•], CCl₃[•] and :CCl₂), having strong oxidizing 212 property, which will markedly accelerate the degradation of levofloxacin in aqueous solution.

213 ^[44] It was reported^[46] that the improvement of US power had a positive effect on the 214 degradation rate of the antibiotic, until an optimal power dissipation. Beyond this value, 215 cavitational activity and pollutant degradation, are either slightly affected or decreases. This 216 optimal power is dependent on the reactor configuration and on the particular 217 system/pollutant.

The values obtained for pseudo first-order rate constant (Table 3) are in the range which have been previously reported by other authors for CIP degradation by several AOPs ^[33, 35, 47-49]. The highest pseudo first-order rate constant obtained in this work is comparable with the reported value by De Bell and collaborators. ^[33]

Two regression models were adjusted to evaluate the influence of both the frequency and ultrasonic power on the degradation and mineralization of CIP according to Equations 4 and 5. The regression and variance analysis for both models are shown in Tables 1S and 2S (supporting information). Figure 4 shows the response surface models of degradation (a) and mineralization (b) for 2x3 experimental design. It is observed that increasing power is favorable, in both cases. Both lineal models confirm that ultrasonic power is the most influent variable for both the degradation and mineralization rate (Eq. 4 and 5).

$$deg = -6.032 + 0.021 F - 0.004 F * P + 2.612 P + 0.039 P * P \qquad R^2 = 99.73\%$$
(4)

$$\min = -3.249 + 0.007 F - 0.002 F * P + 1.949 * P + 0.017P * P \qquad R^2 = 99.49 \%$$
(5)

229 Intensification of CIP sono-degradation with the oxidant H₂O₂ as a radical promoter

230 Few reports about the combination of ultrasound with H_2O_2 on the fluoroquinolones 231 degradation have been found. ^[48] It is well documented in the literature that during aqueous 232 sonolysis, hydroxyl radicals are produced and recombined into H_2O_2 at the bubble-liquid 233 interface and/or in the bulk liquid. ^[50, 51] In general, H_2O_2 is expected to promote degradation since it may be decomposed by US and/or react with H[•] generated by water sonolysis thus generating additional HO[•] according to Equations 6 and 7. $^{[7, 52]}$ For this reason, the degradation of organic compounds maybe augmented by an increase in the H₂O₂ dose. $^{[53]}$

237
$$H_2O_2+))) \to 2 HO^{\bullet}$$
 (6)

$$238 \qquad \text{H}_2\text{O}_2 + \text{H}^\bullet \to \text{HO}^\bullet + \text{H}_2\text{O} \tag{7}$$

where))) refers to the ultrasonic irradiation.

Hydroxyl radicals can (i) degrade organic compounds, (ii) react with H_2O_2 (especially when they are in large excess) forming less active species according to Equation 8 ^[36, 54, 55] (iii) or recombine with different radicals according to Equations 9-11. ^[56-58]

$$243 \qquad \text{H}_2\text{O}_2 + \text{HO}^\bullet \to \text{HOO}^\bullet + \text{H}_2\text{O} \tag{8}$$

$$244 \quad \text{HO}^{\bullet} + \text{HO}^{\bullet} \to \text{H}_2\text{O}_2 \tag{9}$$

$$245 \quad \text{HO}^{\bullet} + \text{H}^{\bullet} \to \text{H}_2\text{O} \tag{10}$$

$$246 \quad \text{HO}^{\bullet} + \text{HOO}^{\bullet} \to \text{H}_2\text{O} + \text{O}_2 \tag{11}$$

Then, another set of experiments was carried out in order to study the effect of H_2O_2 addition on CIP sonolysis. The stoichiometric amount of the required H_2O_2 for the complete oxidation of CIP in aqueous solution was calculated according to Equation 12:

250
$$C_{17}H_{18}FN_3O_{3(aq)} + 47 H_2O_{2(aq)} = 3HNO_{3(aq)} + HF_{(aq)} + 17CO_{2(g)} + 54H_2O_{(l)}$$
 (12)

After one hour of reaction under stoichiometric conditions, a low CIP degradation was found: 5.9% under silent conditions . The influence of the oxidant concentration on CIP degradation and mineralization was studied to understand the phenomena better. Experimental runs were conducted with different concentrations of H_2O_2 corresponding to 0.5, 1, 5, 10, and 15 times the stoichiometric amount (Figure 5). No increase in the CIP degradation was observed with the addition of H_2O_2 . This was verified by comparing the means of CIP degradation by Student test (for α =0.05). When ultrasound is applied without H₂O₂ the degradation and mineralization (35.8% and 22.6% respectively) were similar to the results obtained for one time the stoichiometric amount of H₂O₂ (36.5% and 24.4% respectively), the highest values obtained when hydrogen peroxide was added. In some of the experiments, the addition of H₂O₂ showed a detrimental effect on US-driven CIP degradation in comparison to the performance of the ultrasound-driven process alone.

263 As previously stated here, despite the generation of hydroxyl radicals by its own sonolysis, 264 the hydrogen peroxide can act as a hydroxyl radical scavenger, producing the much less reactive hydroperoxyl radicals (Eq. 8). The hydroxyl radicals in excess will be recombined 265 266 forming water or hydrogen peroxide (Eqs. 9-11). At pH 3, the addition of different 267 stoichiometric amounts of H₂O₂ does not improve the CIP sonolysis process. Several authors reported this negative influence of H_2O_2 in organic pollutant sonodegradation. ^[36, 52] 268 Manousaki et al. ^[52] studied the degradation of sodium dodecvl benzene sulfonate in water 269 by ultrasonic irradiation at 20 and 80 kHz and found a detrimental effect of hydrogen 270 271 peroxide on the substrate degradation, besides the above-mentioned scavenging effect: the 272 pollutant removal occurred mainly in the interfacial region, and thus the beneficial effect of 273 extra hydroxyl radicals (Eq. 7) would be of marginal importance, even close to the cavitation 274 bubbles, due to the thermal decomposition of hydrogen peroxide molecules to oxygen and 275 water. Nevertheless, other authors claim that the addition of H_2O_2 has a positive effect on the degradation of various organic compounds. ^[30, 32, 48, 59-61] The presence of an optimal amount 276 277 of H₂O₂ for the sonochemical degradation of the target compounds can occur, but it is difficult to determine the optimal concentration for each compound. ^[59, 60, 62] It is because the 278 experimental conditions varied widely and a very limited range of H₂O₂ concentrations was 279 used in most previous studies. ^[61] Under our experimental conditions, this optimum amount of 280 281 H_2O_2 was not found.

282 Optimization of the sono-Fenton degradation of CIP

283 The combination of ultrasound with Fenton reagent is an alternative way to increase the 284 generation of free radicals in the ultrasonic system. As previously said, H₂O₂ can be generated during ultrasonic treatment thanks to the recombination of hydroxyl radicals. Therefore, the 285 286 addition of an iron salt can initiate the Fenton reaction during the sonolysis under acidic 287 conditions. This coupling of ultrasonic irradiation and Fenton oxidation (i) promotes faster pollutant conversion/mineralization due to a higher generation of hydroxyl radicals according 288 to Equations 6 and 13^[63]; (ii) improve mixing and contact between hydroxyl radicals and 289 pollutant ^[46, 64], (iii) and enhanced regeneration of ferrous ions according to Equation 14 ^[65], 290 in comparison with an uneasy regeneration of Fe²⁺ by conventional homogeneous Fenton 291 reaction according to Equations 15 and 16. 292

$$293 \qquad \mathrm{Fe}^{2+} + \mathrm{H}_2\mathrm{O}_2 \to \mathrm{Fe}^{3+} + \mathrm{OH}^- + \mathrm{HO}^{\bullet}$$
(13)

$$294 \quad \text{Fe-OOH}^{2+} +))) \rightarrow \text{Fe}^{2+} + \text{HOO}^{\bullet}$$
(14)

$$295 \qquad \text{Fe}^{3+} + \text{H}_2\text{O}_2 \leftrightarrow \text{Fe}\text{-OOH}^{2+} + \text{H}^+ \tag{15}$$

$$296 \quad \text{Fe-OOH}^{2+} \to \text{HOO}^{\bullet} + \text{Fe}^{2+} \tag{16}$$

Table 3 shows the results of ultrasonic degradation of CIP (initial concentration 100 mg L⁻¹, 297 F=580 kHz, P = 30.6 W, T = 30°C, pH= 3) at different concentrations of H₂O₂ and Fe²⁺ 298 corresponding to a H_2O_2/Fe^{2+} ratio between 2 and 10, following a 3^2 factorial experimental 299 300 design (rows 3-11). Sono-Fenton resulted, in all cases, in high CIP degradation (ten times 301 more) within the first 15 min of treatment (higher than 89%) compared to the results obtained during sonolysis alone (row 1, 9.3% of degradation at 15 minutes and 17.4% of 302 303 mineralization in one hour) and those obtained with the addition of hydrogen peroxide without Fe²⁺ (row 2, 9.5% of degradation at 15 minutes and 24.4% of mineralization in one 304 305 hour).

306 An additional ultrasonic experiment was carried out, to evaluate the effect of adding only iron, using 2.37 mM of Fe²⁺ without additional amount of hydrogen peroxide. In this 307 308 condition the CIP degradation at 15 minutes was 18.5%, higher than the value obtained in 309 single sonication experiment but much lower than in the case of hydrogen peroxide was also 310 added together with ferrous salt (98.4%, row 7 table 3). This result can be explained by the 311 formation of hydrogen peroxide during sonication in water. However, it is known that the 312 amount of generated H₂O₂ is not significant comparing with those added as Fenton reagent. [66, 67] 313

314 The mineralization for the sono-Fenton process was also higher than for ultrasonic oxidation 315 alone (row 1 in Table 3) and for sonolysis with hydrogen peroxide (rows 2 in Table 3). The best mineralization was obtained when 14.2 mM of H_2O_2 and H_2O_2/Fe^{2+} ratio 6 (row 7 in 316 317 Table 3) were used. An additional experiment was carried out at the same conditions of row 7 318 (Table 3) without ultrasound (Fenton reaction). It can be seen, that at 15 min the degradation 319 of the sono-Fenton process was practically the same for both processes. With regard to the 320 mineralization, sono-Fenton gave better results than the Fenton process: for example at 60 321 min, the mineralization rate was 30 % higher for sono-Fenton than for Fenton alone (62 vs. 322 30.3). This result shows that ultrasonic radiation combined with Fenton reagent enhances the 323 mineralization of aqueous solution.

324 A mathematical model describing the mineralization behavior at 60 min as a function of H_2O_2 325 concentration and H_2O_2/Fe^{2+} concentration ratio is proposed as follows:

$$\min = -13.2 + 3.12c(H_2O_2) + 13.86 \frac{c(H_2O_2)}{c(Fe^{2+})} - +3c(H_2O_2)^2$$

$$+ 0.007c(H_2O_2) * \frac{c(H_2O_2)}{c(Fe^{2+})} - + \cdot \left[\frac{c(H_2O_2)}{c(Fe^{2+})}\right]^2$$
(17)

The above model describes adequately the experiment with $R^2 = 81.52\%$, a standard error of 326 327 estimation of 8.1 % and a mean absolute error of 3.9 %. The regression and variance analysis 328 for the model are shown in Table 3S (supporting information). Figure 6 shows the response 329 surface model of mineralization, where an optimum of mineralization of 56.78% is observed for hydrogen peroxide concentration of 18.5 mM (stoichiometry of 1.3) and H_2O_2/Fe^{2+} ratio 330 331 of 6. This value of mineralization is higher than those obtained by several AOPs, O_3 (30.5%), UV (18%), UV/H₂O₂ (42%) and is of the same order of magnitude as UV/H₂O₂/Fe²⁺ (63.3%) 332 reported by Bobu and colaborators.^[68] 333

334 Influence of a real waste water matrix on CIP removal

335 The water treatment by AOPs can be affected by the presence of inorganic and organic components in the water matrix, significantly slowing the degradation of the target pollutants. 336 ^[70-71] Several authors have reported the role of organic components on the sonochemical 337 338 degradation of persistent contaminants that appears to be a complex task which need to be experimentaly verified for different systems. ^[7, 72-77] On the one hand, the presence of an 339 340 organic matrix reduces the sonochemical degradation of target contaminants.^[7, 72-74] On the 341 other hand, the presence of organic matter did not affect the sonochemical degradation of methyl tert-butyl ether, ^[76] perfluorooctane sulfonate and perfluorooctanoate. ^[77] In order to 342 343 investigate the efficiency of the sono-Fenton degradation of CIP in real application, some 344 experiments with a real wastewater matrix (WW) were performed. In the case of Fenton 345 chemistry, the presence of organic and inorganic compounds in WW may hamper this reaction by scavenging hydroxyl radicals and/or forming iron complex. ^[7, 78] A positive effect 346 347 has also been reported, phenolic compounds that WW may contain could reduce ferric ion to ferrous ion and thus enhance Fenton reaction.^[76] 348

349 Table 4 shows the physicochemical characteristics of the WW influent from the WWTP 350 "María del Carmen" before (WW-01) and after addition of CIP at 100 mgL⁻¹ and pH 351 adjustment to 3 (WW-02). As CIP is the major organic compound in this matrix, biochemical 352 oxygen demand (BOD₅), chemical oxygen demand (COD) and TOC concentration increased 353 when it was added. However, the BOD₅/COD ratio decreased from 0.33 to 0.21 showing a 354 decrease in the biodegradability of CIP-dopped matrix WW-02. De Bel et al.^[35] experimentally demonstrated the low degradability of the 15 mgL⁻¹ CIP aqueous solution with 355 356 BOD₅/COD ratio of only 0.06. The suspended solid concentration in WW-02 also decreased, 357 due to the solubility of some solids with pH decreasing. The real matrix was treated by the 358 sono-Fenton process. Two different series of experiments were carried out: (i) under the best 359 conditions obtained during CIP degradation in aqueous solution (14.2 mM H₂O₂ and H_2O_2/Fe^{2+} ratio of 6), (ii) recalculating the amount of hydrogen peroxide to be added, taking 360 361 into account the increase in COD to keep the same H₂O₂/COD ratio as in the study with the synthetic solution (31.8 mM H_2O_2 and H_2O_2/Fe^{2+} ratio of 6). 362

363 Figure 7 shows the CIP degradation and mineralization ([CIP]₀: 100 mg L⁻¹, T: 30°C, pH₀=3) 364 by the sono-Fenton process in a real WW matrix for both series of experiments. The 365 degradation and mineralization of CIP are higher when a higher concentration of hydrogen 366 peroxide is used. Nevertheless, even under this condition in a real matrix WW-02, 367 degradation of both CIP and TOC by sono-Fenton is significantly hampered in WW. The 368 degradation of CIP at 15 min and mineralization at 60 min are less important in real 369 conditions (13.6% and 18.9%), than for synthetic water. This result shows the inhibition of 370 CIP degradation and mineralization in a real WW matrix, as reported before for the sonolysis of CIP and other persistent pollutants in different organic matrices. ^[7, 70-72] 371

372 Although the sonochemical degradation of CIP is less efficient for the real matrix, the 373 pollutant degradation and mineralization is still quite adequate: 97.1% of CIP degradation is 374 reached after 60 min (Fig. 7), which practically guarantees the complete elimination of the 375 antibiotic from WW. This is an important environmental issue in the fight against antibiotic 376 resistance in natural systems. On the other hand, in the best cases, the BOD₅ removal was 377 14.2% (Table 4), the COD and TOC removal were higher than 50% and the BOD₅/COD ratio 378 increased from 0.21 to 0.36, showing an increase in biodegradability. ^[35] This result is very 379 promising because it opens the perspective of using ultrasound and sono-Fenton as a 380 pretreatment of biological process in a WWTP for eliminating persistent organic pollutants.

381 Conclusion

High frequency ultrasound guarantees the degradation of the antibiotic CIP following pseudo first-order reaction kinetics. It was verified that the ultrasonic power had a greater influence on CIP degradation than the frequency, at the values studied, in this field of investigation. Higher CIP percent removals and removal rates were observed for the lowest operating frequency studied (580 kHz) and higher ultrasonic power. Practically the total degradation of pharmaceutical was obtained in 15 min for all concentrations of hydrogen peroxide and ferrum salt studied.

389 The addition of hydrogen peroxide, as a radical promoter, does not markedly improve the 390 sonolysis process in the range of operating studied conditions. In contrast, CIP degradation 391 and mineralization are highly improved in the case of the US/Fenton system. The optimal conditions of the sono-Fenton process are 14.2 mM H_2O_2 and H_2O_2/Fe^{2+} ratio of 6, ensuring 392 393 at least a 60%. mineralization rate. The degradation of both CIP and TOC by sono-Fenton 394 was significantly hampered in a real waste water matrix. However, the pollutant degradation, 395 COD and TOC removals can be considered as efficient in the real matrix, with an increase in 396 the biodegradability of the wastewater. These results show that sono-Fenton oxidation can be 397 considered as a promising pretreatment process for wastewater containing pharmaceutical 398 compounds.

399 Acknowledgements

400 This research was supported by the project TATARCOP of Instituto Superior de Tecnologías 401 y Ciencias Aplicadas (InSTEC)-University of Havana. The authors would also like to express 402 their gratitude to the Colaboration Services of the French Embassy in Cuba for the financial 403 support and to the Laboratory of Environmental Analysis of InSTEC-University of Havana 404 for the analytical support of wastewaters.

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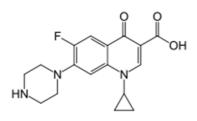
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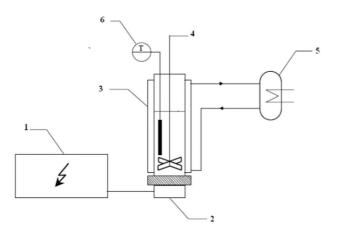
- 623 List of Figure Captions
- 624 Figure 1. Molecular structure of CIP
- 625 **Figure 2.** Experimental set-up: 1 –ultrasonic generator, 2 transducer, 3 glass reactor, 4 –
- 626 stirrer, 5 –thermostat, 6 temperature measurement
- **Figure 3.** Influence of ultrasonic frequency and actual ultrasonic power on CIP degradation and mineralization after 120 min. Open markers with solid line represent degradation and filled markers with dash line represent mineralization. Experimental conditions: ([CIP]_o: 100 mg L⁻¹, T: 30 °C, pH_o=3)
- *Figure 4.* Response surface as a function of ultrasonic power. Degradation (a) andmineralization (b) of CIP
- 633 **Figure 5.** Degradation and mineralization trend in the US/H₂O₂ process (F = 580 kHz y P = 634 21.7 W, pH = 3, t = 60 min)
- 635 **Figure 6.** Response surface as a function concentration of $[H_2O_2]$ and the relation of 636 $c(H_2O_2)/c(Fe^2)$
- 637 **Figure 7.** CIP degradation and mineralization by sono-Fenton process in a real WW matrix.
- 638 Open markers with solid line represent degradation and filled markers with dash line mean
- 639 mineralization for two different H₂O₂ concentrations: 14.2 mM (\circ/\bullet) and 31.8 mM (\Box/\blacksquare).
- 640 Experimental conditions: ([CIP]_o: 100 mg L^{-1} , T: 30 °C, pH_o=3)
- 641

642 Figures



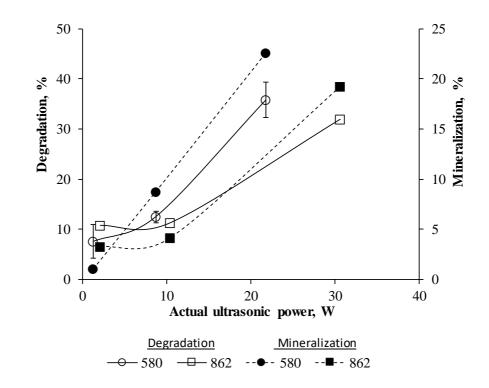
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644 Fig 1.



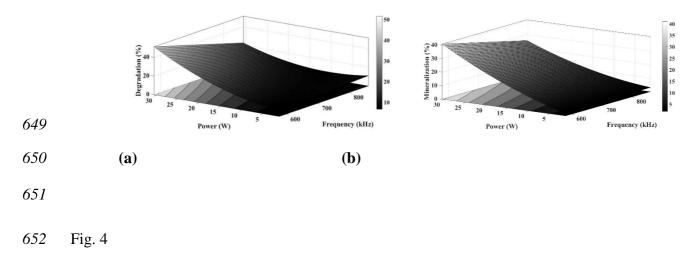
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646 Fig 2.

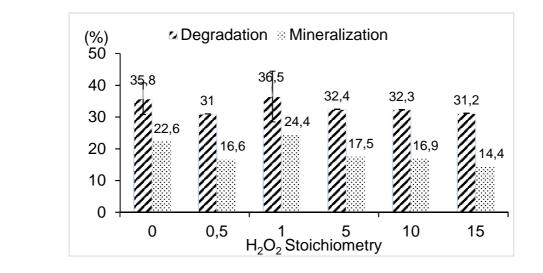


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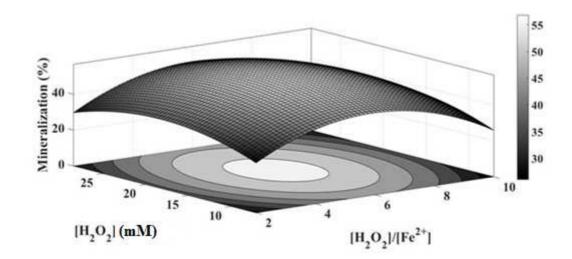
648 Fig. 3.



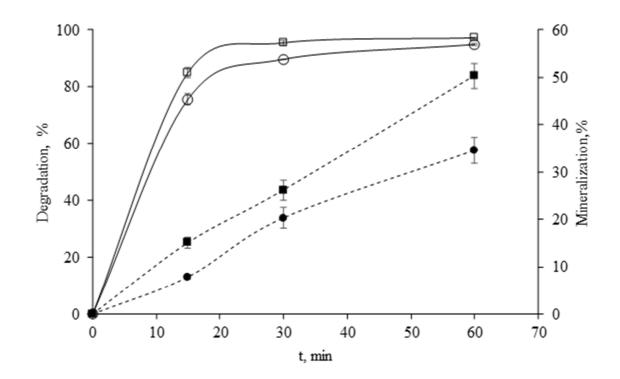




655 Fig 5.



657 Fig 6.



658

659 Fig 7.

661 Tables

No.	Frequency (kHz)	Actual
1	580	Min (1,35)
2	862	Min (2,07)
3	580	Med (8,74)
4	862	Med (10,37)
5	580	Max (21,77)
6	862	Max (30,57)
7	862	Max (30,57)

Table 1. Experimental design 2*3 for the evaluation of ultrasonic frequency and power

Table 2. Degradation pseudo first-order rate constant for three different ultrasonic power at

665 frequency 580-862 kHz ([CIP]_o: 100 mg L^{-1} , T: 30 °C, pH_o=3)

	Frequency (kHz)	$P_{min}(W)$ (value)	P _{med} (W) (value)	P _{max} (W) (value)
	580	0.0039 (1.35)	0.0045 (8.74)	0.0066 (21.77)
	862	0.0032 (2.07)	0.0040 (10.37)	0.0045 (30.57)
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Table 3. Effect of Fe^{2+}/H_2O_2 on CIP sonochemical degradation (t=15 min) and mineralization

677 (t=60 min), (F=580 kHz, P = 30.6 W, [CIP]₀= 100 mg L⁻¹, T = 30°C, pHo= 3). *Fenton

678 reaction without ultrasound

Row				
	c(H2O2)	c(H2O2)/c(Fe ²⁺)	Degradation (%), 15	Mineralization (%), 60
	mM		min	min
1	0	-	9.3	17.4
2	14.2	-	9.5	24.4
3	7.1	10	92.3	31.0
4	7.1	6	99.0	36.9
5	7.1	2	93.4	31.6
6	14.2	10	89.7	31.5
7	14.2	6	98.4±1.4	62.0±2.3
			96.4*	30.3*
8	14.2	2	92.4	34.5
9	28.4	10	95.9	28.5
10	28.4	6	99.8	50.4
11	28.4	2	98.5	28.5

Table 4. Physico-chemical characteristics of WW matrix before and after treatment by sono-*Fenton process ([CIP]₀: 100 mg L⁻¹, T: 30 °C, pH₀=3)*

Parameter	Unit	WW-01 ^a	WW-02 ^a	After son	o-Fenton ^b
Temperature	°C	26	26	30	30
pН	-	6.7	3	3	3
H_2O_2	mM	-	-	14.2	31.8
H_2O_2/Fe^{2+}	-	-	-	6	6
BOD ₅	$mg \ O_2 \ L^{\text{-1}}$	66 ± 1	76 ± 5	72 ± 3	65 ± 4
COD	$mg \ O_2 \ L^{\text{-}1}$	203 ± 43	368 ± 18	230 ± 21	180 ± 14
TOC	mg C L ⁻¹	74 ± 3	131 ± 1	85 ± 4	66 ± 4
SS	mL L ⁻¹	2.5 ± 0.1	2.3 ± 0.2	0	0
Conductivity	μS cm ⁻¹	1213	n.a.	n.a.	n.a.
Floating matter	-	present	present	non	non
BOD ₅ /COD	-	0.33	0.21	0.31	0.36
BOD ₅ removal	%	-	-	4.8*	14.2*
COD removal	%	-	-	37.4*	51.1*
TOC removal	%	-	-	34.6*	50.3*

^aAverage of three sampling results; ^bAverage of two experiments; n.a: non available;

*Referred to WW-02

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685 Supporting informat

Table 1S. Regression and variance analysis for equation 4 (Degradation as function of

688 ultrasonic frequency and power).

		Regression analys	sis		
Parameter	Estimate	Error	t-statistic	p-value	
Constant	-6.032	4.82043	-1.251	0.429	
F	0.021	0.007	3.08	0.2	
F * P	-0.004	0.0005	-6.864	0.092	
Р	2.612	0.327	7.989	0.079	
P * P	0.039	0.009	4.284	0.146	
		Analysis of varianc	e		
Source	Sum of squares	Mean square	F-ratio	p-value	
Model	744.985	186.246	93.91	0.076	
Residual	1.98333	1.98333			
Total correlation	746.969				
R-squared = 99.73 q	%	Standard error of	estimation = 1.408		
Mean absolute error	r = 0.515				

Table 2S. Regression and variance analysis for equation 5 (Mineralization as function of

ultrasonic frequency and power).

Parameter	Estimate	Error	t-statistic	p-valu
Constant	-3.249	4.91	-0.662	0.628
F	0.007	0.007	1.0	0.5
F * P	-0.002	0.0005	-4.137	0.151
Р	1.949	0.333	5.852	0.108
P * P	0.017	0.009	1.831	0.318
		Analysis of varianc	e	
Source	Sum of squares	Mean square	F-ratio	p-valu
Model	402.0	100.5	48.85	0.010
Residual	2.06	2.06		
Total correlation	404.06			
R-squared = 99.49	%	Standard error of	estimation = 1.434	
Mean absolute error	r = 0.524			

703 hydrogen peroxide concentration and H_2O_2/Fe^{2+} concentration ratio for sono-Fenton reaction).

		egression analysis		
Parameter	Estimate	Error	t-statistic	p-value
Constant	-13.2	20.8	-0.63	0.571
H ₂ O ₂	3.12	2.19	1.42	0.25
H_2O_2/Fe^{+2}	13.86	4.61	3.01	0.057
$H_2O_2 * H_2O_2$	-0.09	0.06	-1.49	0.233
$H_2O_2 * H_2O_2/Fe^{+2}$	0.007	0.09	0.07	0.946
$H_2O_2/Fe^{+2*}H_2O_2/Fe^{+2}$	-1.18	0.35	-3.31	0.045
		Analysis of variance		
Source	Sum of squares	Mean square	F-ratio	p-value
Model	856.2	171.2	12.65	0.102
Residual	194.1	64.7		
Total correlation	1050.3			
R-squared = 81.52 %	uared = 81.52 % Standard error of estimation = 8.14			
Mean absolute error = 3	3.92			