

# **Asynchronous Switched Observers Design for Switched Takagi-Sugeno Systems Subject to Output Disturbances**

Djamel E.C. Belkhiat, Dalel Jabri, Kevin Guelton, Noureddine Manamanni,

Issam Chekakta

### **To cite this version:**

Djamel E.C. Belkhiat, Dalel Jabri, Kevin Guelton, Noureddine Manamanni, Issam Chekakta. Asynchronous Switched Observers Design for Switched Takagi-Sugeno Systems Subject to Output Disturbances. IFAC Conference on Intelligent Control and Automation Sciences (ICONS), 2019, Belfast, United Kingdom. pp.49-54, 10.1016/j.ifacol.2019.09.117. hal-02343262

## **HAL Id: hal-02343262 <https://hal.science/hal-02343262v1>**

Submitted on 12 Jul 2024

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**Intelligent Control Available online at www.sciencedirect.com** 



IFAC PapersOnLine 52-11 (2019) 49–54



#### Asynchronous Switched Observers Design ynchronous Switched Observers Desi r Switched Takagi-Sugeno Systel Asynchronous Switched Observers Design ynchronous Switched Observers Desi<br>for Switched Takagi-Sugeno Systems Subject to Output Disturbances Djamel E.C. Belkhiat ∗ Dalel Jabri ∗ Kevin Guelton ∗∗ for Switched Takagi-Sugeno Systems for Switched Takagi-Sugeno Systems Subject to Output Disturbances Subject to Output Disturbances

Djamel E.C. Belkhiat ∗ Dalel Jabri ∗ Kevin Guelton ∗∗ Djamel E.C. Belkhiat \* Dalel Jabri \* Kevin Guelton \*\* Noureddine Manamanni ∗∗ Issam Chekakta ∗ Noureddine Manamanni ∗∗ Issam Chekakta ∗ Djamel E.C. Belkhiat ∗ Dalel Jabri ∗ Kevin Guelton ∗∗ ∗∗ ∗ Djamel E.C. Belkhiat ∗ Dalel Jabri ∗ Kevin Guelton ∗∗ Noureddine Manamanni ∗∗ Issam Chekakta ∗

∗ DAC HR Laboratory, Ferhat Abbas University Setif 1, Setif, Algeria ∗ DAC HR Laboratory, Ferhat Abbas University Setif 1, Setif, Algeria ∗ DAC HR Laboratory, Ferhat Abbas University Setif 1, Setif, Algeria (e-mails: {djamel.belkhiat,dalel.jabri,issam.chekakta} @univ-setif.dz)<br>\*\* CReSTIC EA3804, Université de Reims Champagne-Ardenne,<br>Campus Moulin de la Housse RP1039, 51687 Reims Ceder ? Franc CRESITO EASOLA, Universite de Reims Champagne-Ardenne,<br>Campus Moulin de la Housse BP1039, 51687 Reims Cedex 2, France (e-mails: {kevin.guelton,noureddine.manamanni}@univ-reims.fr)  $(e-mails: \{djameel. \text{jabri}, \text{rindel.} \text{jabri}, \text{rindel.} \text{jabri}, \text{rindel.} \}$  (which set the  $\{djameel. \text{jabri}, \text{rindel.} \text{jabri}, \text{rind$ (e-mails: {kevin.guelton,noureddine.manamanni}@univ-reims.fr) (e-mails: {kevin.guelton, noureddine.manamanni} @univ-reims.fr)  $\int^*$ \* CReSTIC EA3804, Université de Reims Champagne-Ardenne, $\int^*$ Campus Moulin de la Housse BP1039, 51687 Reims Cedex 2. Franc (e-mails:  $k$ evin.guelton, noured in  $\mathcal{L}$ 

of switched continuous-time Takagi-Sugeno (TS) systems subject to output disturbances. The of switched continuous-time Takagi-Sugeno (TS) systems subject to output disturbances. The considered switched TS observer is proposed for the continuous-state estimation when the active switched modes of the system are unknown or not precisely known. The design conditions, obtained modes of the system are unknown of not precisely known. The design conditions, obtained via switched Lyapunov-like function candidates, are expressed as Linear Matrix Inequality (LMI) and satisfy  $H_{\infty}$  disturbance attenuation performances. The effectiveness of Inequality (LMI) and satisfy  $H_{\infty}$  disturbance attenuation performances. The effectiveness of the proposed approach is illustrated through the simulation of an academic example. the proposed approach is illustrated through the simulation of an academic example. **Abstract:** This paper deals with the design of asynchronous switched observers for a class Abstract. This paper deals with the design of asynchronous switched observers for a class<br>of switched continuous-time Takagi-Sugeno (TS) systems subject to output disturbances. The<br>considered switched TS observer is propos the proposed approach is illustrated through the simulation of an academic example. obtained via switched Lyapunov-like function candidates, are expressed as Linear Matrix Inequality (LMI) and satisfy  $H_{\infty}$  disturbance attenuation performances. The effectiveness of

© 2019, IFAC (International Federation of Automatic Control) Hosting by Elsevier Ltd. All rights reserved. Switched Takagi-Sugeno systems, Asynchronous systems, Asynchronous systems, Asynchronous switched observer design, LMIS. the proposed approximation of an accept through the simulation of an accept through the simulation of an accept through the example. The example of a satisfy the effective attenuation performance at the effectiveness of  $\odot$  2019, IFAC (International Federation of Automatic Control) Hosting by Elsevier Ltd. All right

Keywords: Switched Takagi-Sugeno systems, Asynchronous switched observer design, LMIs. Keywords: Switched Takagi-Sugeno systems, Asynchronous switched observer design, LMIs.

### 1. INTRODUCTION 1. INTRODUCTION 1. INTRODUCTION

The use of new technological devices, for instance real-The use of new technological devices, for instance real-The use of new technological devices, for instance realtime embedded control plants, makes switched systems suitable and realistic to model several physical systems involving both continuous and discrete dynamic behavior formal board continuous and discrete dynamic behaviors. In this context, fruitful theoretical results have been proposed for the state estimation of switched systems, see e.g. (Alessandri and Coletta, 2001; Hamdi et al., 2009; Jabri et al., 2012; Belkhiat et al., 2011). These approaches can be classified into two categories: In one hand, some authors assume that the active switched mode is known at any time and, consequently, the observer switches synat any time and, consequently, the observer switches syn-Coletta, 2001; Belkhiat et al., 2015; Ethabet et al., 2018). In the other hand, when the systems' active mode is in the other hand, when the systems active mode is in practice, the observer's switching laws cannot precisely In practice, the observer s switching haws call to precisely hatch the system's ones, teading to asynchronous switches 2017; Xiang et al., 2012). The observer design conditions 2017; Xiang et al., 2012). The observer design conditions<br>for switched systems are often obtained via the direct<br>Lyapunov methodology. In this framework, pioneer works<br>considered common quadratic Lyapunov functions, see e. Lyapunov methodology. In this framework, pioneer works for switched systems are often obtained via the direct for switched systems are often obtained via the direct for switched systems are often obtained via the direct considered common quadratic Lyapunov functions, see e.g. Lyapunov methodology. In this framework, pioneer works Lyapunov methodology. In this framework, pioneer works Lyapunov methodology. In this framework, pioneer works (Alessandri and Coletta, 2001). Although the convergence of the estimation error is guaranteed regardless of the sysor the estimation error is guaranteed regardless of the sys-<br>tems and observers' switches, these common quadratic approaches remain very conservative. Therefore, some results have considered switched quadratic Lyapunov functions to relax the design conditions and expand them to a larger class of switched systems (Belkhiat et al., 2015; Xiang relax the design conditions and expand them to a larger et al., 2012). et al., 2012). class of switched systems (Belkhiat et al., 2015; Xiang class of switched systems (Belkhiat et al., 2015; Xiang class of switched systems (Belkhiat et al., 2015; Xiang relax the design conditions and expand them to a larger relax the design conditions and expand them to a larger et al., 2012). et al., 2012). class of switched systems (Belkhiat et al., 2015; Xiang class of switched systems (Belkhiat et al., 2015; Xiang for switched systems are often obtained via the direct

Furthermore, Takagi-Sugeno (TS) fuzzy systems are nowa-Furthermore, Takagi-Sugeno (TS) fuzzy systems are nowa-Furthermore, Takagi-Sugeno (TS) fuzzy systems are nowa-Turntermore, Takagi-Sugeno (TS) fuzzy systems are nowa-<br>days extensively used for the modeling and control design days extensively used for the modeling and control design Furthermore, Takagi-Sugeno (TS) fuzzy systems are nowa-<br>days extensively used for the modeling and control design et al., 2012).<br>Furthermore days extensively used for the modeling and control design of switched systems exhibiting nonlinear dynamics, see e.g. of switched systems exhibiting nonlinear dynamics, see e.g. of switched systems exhibiting nonlinear dynamics, see e.g. of switched systems exhibiting hominear dynamics, see e.g.<br>(Jabri et al., 2011, 2012, 2018b, a; Cherifi et al., 2019). However, although several progress have been made in some fields of switched TS systems as the stability and stabilization issues, there is still space for improvements on state estimation and switched TS observers design. To this ends, Lendek et al. (2012) have proposed a nonquadratic Lyapunov function-based approach to design switched TS observers for a class of periodic discrete-time TS models. Then relaxed conditions, considering the  $\alpha$ also models. Then relaxed conditions, considering the dihave been proposed (Lendek et al., 2014). Recently, to estimate the state vector of discrete-time TS fuzzy switched system under synchronous switching, Liu et al. (2018) have proposed a synthesis approach to perform a design nave proposed a synthesis approach to perform a design<br>of switched Luenberger-type observers. Several sufficient system under synchronous switching, Liu et al. (2018)<br>have proposed a synthesis approach to perform a design<br>of switched Luenberger-type observers. Several sufficient<br>conditions were established by constructing multiple Ly punov functions and common Lyapunov functions. In the punov functions and common Lyapunov functions. In the continuous time framework, a design method for observerbased output feedback control for a class of switched fuzzy based output feedback control for a class of switched fuzzy<br>systems with time-varying delay is proposed in (Zhang<br>at al. 2018). Moreover, the estimation of the lateral value et al., 2018). Moreover, the estimation of the lateral velocity et al., 2016). Moreover, the estimation of the fateral velocity and yaw rate using switched Takagi-Sugeno fuzzy interval observers have been developed in (Ifqir et al., 2017). In the latter mentioned study, the active mode is assumed. to be available at any time, which allows to automatically to be available at any time, which allows to automatically<br>select the appropriate candidate observer. The main results have been expressed in terms of sufficient LMI-based conditions through the use of a switched fuzzy Lyapunov function. Note that most of the available studies in the such that the constant in the available statutes in the<br>switched TS framework consider that the observer and the<br>switch and the constant of the state of the state of system to be estimated share the same switched sets and that both switch at the same instants. This is obviously a drawback for two reasons: 1) the observer state doesn't that both switch at the same instants. This is obviously a drawback for two reasons: 1) the observer state doesn't drawback for two reasons: 1) the observer state doesn't drawback for two reasons: 1) the observer state doesn't that both switch at the same instants. This is obviously a  $d$  drawback for two reasons: 1) the observer state doesn't

match the system's state (especially during transients) leading to different switching instants even if the same switched sets are considered, 2) in practical applications, measuring both the switching instant and modes from the plant remains a tricky challenge to implement such observers. To circumvent these drawback, the goal of this paper is to design asynchronous observers for continuoustime switched TS systems subject to output disturbances (i.e. additive sensor fault) with  $H_{\infty}$  performance specifications and under arbitrary switching sets and sequences. Indeed, to the best of the authors' knowledge, this hasn't been explored so far, which motivates this study.

In what follows, new LMI-based conditions for the design of asynchronous switched TS observers for a class of switched TS fuzzy systems subject to external bounded output disturbances, under arbitrary switching sets and sequences, is presented. In this study, we assume that the exact switching sequence is unknown (or not precisely known) but only the set of all the admissible switches is known. The proposed approach ensures that, without external disturbances, the estimation error asymptotically converges to zero regardless the switches of the system and the observer. In addition, it ensures the robustness of the observer against output disturbances.

The paper is organized as follows. Section II presents the considered class of switched TS fuzzy systems as well as the problem statement. Section III details the proposed LMI-based conditions for the design of the proposed robust switched observer. Finally, an academic example is considered in section IV to illustrate the effectiveness of the proposed approach.

#### 2. PRELIMINARIES AND PROBLEM STATEMENT

Let us consider the class of nonlinear switched systems represented by switched TS models given as follows:

$$
\begin{cases}\n\dot{x}(t) = \sum_{j=1}^{m} \sum_{i_j=1}^{r_j} \sigma_j(t) h_{i_j}(z_j(t)) \left( A_{i_j} x(t) + B_{i_j} u(t) \right) \\
y(t) = Cx(t) + Ww(t)\n\end{cases}
$$
\n(1)

where  $x(t) \in \mathbb{R}^{\eta}$ ,  $y(t) \in \mathbb{R}^{\rho}$ ,  $u(t) \in \mathbb{R}^{\nu}$ ,  $w(t) \in$  $\mathbb{R}^v$  represent respectively the state, the measurement (output), the input vectors and a  $L_2$ -norm bounded output disturbance vector.  $m$  is the number of switching modes.  $r_j$  is the number of fuzzy rules associated to the  $j^{th}$ mode. For  $j = 1, ..., m, i_j = 1, ..., r_j, A_{i_j} \in \Re^{\eta \times \eta}$ ,  $B_{i_j} \in \Re^{\eta \times v}$ ,  $C \in \Re^{\rho \times \eta}$  and  $W \in \Re^{\rho \times v}$  are constant matrices describing the local dynamics of each polytops.  $z_j(t)$  are vectors of premise variables and  $h_{i_j}(z_j(t)) \geq$ 0 are membership functions satisfying the convex sum proprieties  $\sum_{i=1}^{r_j} h_{i_j}(z_j(t)) = 1$ . The piecewise continuous functions  $\sigma_j(t) \in \{0,1\}$  represent the system's switching laws defined such that the active system in the  $l^{th}$  mode leads to:

$$
\begin{cases}\n\sigma_j(t) = 1 & \text{if } j = l \\
\sigma_j(t) = 0 & \text{if } j \neq l\n\end{cases}
$$
\n(2)

Note that, in this paper the switching functions  $\sigma_j(t)$  of switched TS models (1) are supposed to be unavailable from measurements but occur at defined switching sets  $S_{j,j^+}$  where j and  $j^+$  denote respectively the active modes before and after switching. Without loss of generality, these switching sets are described in this paper by linear hyper-planes such that:

$$
S_{j,j^{+}} = \{ x \in \Re^{\eta} | s_{j,j^{+}} x = 0 \}, \quad (j, j^{+}) \in I_{s} \tag{3}
$$

where  $s_{j,j+}$  are constant scalars (possibly unknown),  $I_s$ denotes the set of admissible switches, which are assumed known in this study, i.e.  $(j, j^+) \in I_s$  if a switch from mode  $i$  to  $i^+$  is possible.

Remark 1. This work is not concerned with unmeasured premise variables, see e.g. (Ichalal et al., 2018) and references therein for studies dealing with that topic (without considering switched systems). Thus, in this paper, the premise variables  $z_i(t)$  are assumed to be known and depend only on the measured output, i.e.  $z_i(t) \equiv y(t)$ .

Our goal is to design the following robust switched fuzzy observer, dedicated to estimate the continuous state  $x(t)$ of (1).

$$
\begin{cases}\n\dot{\hat{x}}(t) = \sum_{\hat{j}=1}^{m} \sum_{i_{\hat{j}}=1}^{r_{\hat{j}}} \hat{\sigma}_{\hat{j}}(t) h_{i_{\hat{j}}}(y(t)) \left( A_{i_{\hat{j}}}\hat{x}(t) + B_{i_{\hat{j}}}u(t) + K_{i_{\hat{j}}}(y(t) - \hat{y}(t)) \right) \\
\hat{y}(t) = C\hat{x}(t)\n\end{cases}
$$
\n(4)

where  $\hat{x}(t) \in \Re^{\eta}$ ,  $\hat{y}(t) \in \Re^{\rho}$  represent respectively the estimated state and output vectors.  $\hat{j} = 1, ..., m$  are the observer's switched modes having each  $r_{\hat{i}} \equiv r_j$  fuzzy rules, i.e.  $i_{\hat{j}} = 1, ..., r_{\hat{j}}$ .  $K_{i_{\hat{j}}}$  are the observer gain matrix to be synthesized. The piecewise continuous function  $\hat{\sigma}_{\hat{i}}(t) \in$  ${0, 1}$  is the observer's switching law, whose switches can occur according to the observer's own switching sets  $\bar{S}_{\hat{i},\hat{j}+}$ , i.e. possibly mismatching the switching sets of the system (3), and given as follows:

$$
\bar{S}_{\hat{j},\hat{j}^{+}} = \{\hat{x} \in \Re^{\eta} | \bar{s}_{\hat{j},\hat{j}^{+}}\hat{x} = 0\}, \quad \left(\hat{j},\hat{j}^{+}\right) \in I_{s} \quad (5)
$$

where  $\bar{s}_{\hat{i},\hat{j}+}$  are constant scalars.

Notations. In the sequel, to lighten the mathematical expression, the premise entries  $z_j$  will be omitted when there is no ambiguities and the following notations will be employed for fuzzy matrices:

$$
M_{h_{\sigma}} = \sum_{j=1}^{m} \sum_{i=1}^{r_j} \sigma_j(t) h_{i_j}(y(t)) M_{i_j}
$$
 (6)

and:

$$
N_{h_{\hat{\sigma}}} = \sum_{\hat{j}=1}^{m} \sum_{i_{\hat{j}}=1}^{r_{\hat{j}}} \hat{\sigma}_{\hat{j}}(t) h_{i_{\hat{j}}}(y(t)) N_{i_{\hat{j}}} \tag{7}
$$

Moreover, the subscript † denotes the Moore-Penrose pseudo-inverse and  $\mathcal{H}_e(M) = M + M^T$ .

Note that the switching sets  $\bar{S}_{\hat{i},\hat{j}+}$  depend on the estimated state  $\hat{x}$  from the observer, whereas the switching sets  $S_{i,j+1}$ depend on the system's state  $x$ . Moreover, as mentioned in the introduction, the synchronous case  $(\sigma(t)=\hat{\sigma}(t))$ is not realistic, especially during transient since  $\hat{x}(t) \neq$  $x(t)$ . Therefore, in the sequel, we will not consider the synchronous case but the more general case where the switched system (1) and the switched observer (4) operate asynchronously in different modes  $(\sigma(t) \neq \hat{\sigma}(t))$  and with

possibly mismatching switching sets  $(\bar{S}_{\hat{j},\hat{j}^+} \not\equiv S_{j,j^+})$ . In this asynchronous case, the dynamics of the estimation error  $e = x(t) - \hat{x}(t)$  can be expressed as:

$$
\dot{e}(t) = (A_{h_{\sigma}} - K_{h_{\hat{\sigma}}}C) e(t) + (A_{h_{\sigma}} - A_{h_{\hat{\sigma}}}) x(t) + (B_{h_{\sigma}} - B_{h_{\hat{\sigma}}}) u(t) - K_{h_{\hat{\sigma}}} W w(t)
$$
 (8)

Moreover, let us notice that the dynamics of the estimation error  $(8)$  depends on the state vector  $x(t)$ , the input vector  $u(t)$  and also on the disturbance vector  $w(t)$ . Thus, the following statements are defined as the observer design requirements:

- With zero disturbance input condition  $(w(t) = 0)$ , the estimation error  $e(t)$  asymptotically converges to zero.
- For all non zero  $w(t) \in L_2[0,\infty)$ , the following  $H_{\infty}$ criterion is considered:

$$
\int_{0}^{\infty} e^{T}(t) e(t) dt \leq \gamma^{2} \int_{0}^{\infty} w^{T}(t) w(t) dt \qquad (9)
$$

where  $\gamma > 0$  is an attenuation level from  $w(t)$  to  $e(t)$ , to be minimized.

To conclude these preliminaries, let us recall the following useful lemma for the proof of the conditions proposed in the next section.

Lemma 2. (S-procedure(Derinkuyu and Pınar, 2015)). Let  $L \subset L^2$  be time invariant subspace and  $\psi_k : L \to$  $R, (k = 0, \ldots M)$ , be continuous time invariant quadratic forms. Suppose that there exist  $f_* \in L$  such that  $\psi_1(f_*)$  $0, ..., \psi_M(f_*) > 0$ , then the following statement are equivalent:

- i.  $\psi_0(f) \leq 0$  for all  $f \in L$  such that  $\psi_1(f)$  $0, ..., \psi_M(f) > 0.$
- ii. There exist  $\tau_1 \geq 0, ..., \tau_M \geq 0$  such that  $\psi_0(f)$  +  $\tau_1 \psi_1(f) + ... + \tau_M \psi_M(f) \leq 0$  for all  $f \in L$ .

### 3. MAIN RESULT

The goal of this section is to provide sufficient LMI-based conditions to design the fuzzy gain matrices  $K_{h_{\hat{\sigma}}}$  of the observer (4) such that the robust  $H_{\infty}$  requirements defined above are satisfied. The main result is summarized by the following theorem.

Theorem 3. Let us consider the switched TS system (1) and the asynchronous switched TS observer (4). For given scalar  $\varepsilon > 0$ , if, for all combinations of  $i = 1, ..., r_j$ ,  $(j, \hat{j}) \in \{1, ..., m\}^2$  and  $(\hat{j}, \hat{j}^+) \in I_s$ , there exist a scalar  $\lambda > 0$  and the matrices  $P_{\hat{j}} = P_{\hat{j}}^T > 0$ ,  $G_{\hat{j}}$ ,  $Y_{i_{\hat{j}}}$  such that the scalar  $\gamma > 0$  is minimized and satisfying the following conditions:

i. The following equality and set of LMIs are satisfied:

$$
P_{\hat{j}+} = P_{\hat{j}} + G_{\hat{j}}^T C + C^T G_{\hat{j}} \qquad (10)
$$

$$
\begin{bmatrix} \Gamma_{i_j i_j} & (*) & (*) & (*) \\ A_{i_j}^T P_{\hat{j}} - A_{i_j}^T P_{\hat{j}} & -\lambda \varepsilon & 0 & 0 \\ B_{i_j}^T P_{\hat{j}} - B_{i_j}^T P_{\hat{j}} & 0 & -\lambda \varepsilon & (*) \\ -Y_{i_j} W & 0 & 0 & -\gamma^2 I \end{bmatrix} < 0 \qquad (11)
$$
with  $\Gamma_{i_j i_j} = \mathcal{H}_e \left( P_{\hat{j}} A_{i_j} - Y_{i_j} C \right) + (1 + \lambda) I$ ,

ii.  $\forall \hat{x}$  ∈  $\bar{S}_{\hat{i},\hat{j}+}$ , the state of the switched observer is updated according to:

$$
\hat{x}^{+} = \left(I - R_{\hat{j}}^{-1} \left(CR_{\hat{j}}^{-1}\right)^{\dagger} C\right) \hat{x} + R_{\hat{j}}^{-1} \left(CR_{\hat{j}}^{-1}\right)^{\dagger} y
$$
\n(12)

with:

$$
R_{\hat{j}} = V_{\hat{j}} \sqrt{\Lambda_{\hat{j}}} V_{\hat{j}}^T \tag{13}
$$

and where  $V_{\hat{i}} \in \Re^{\eta \times \eta}$  is composed of the orthonormal eigenvectors of  $P_{\hat{i}}$  and  $\Lambda_{\hat{i}} \in \Re^{\eta \times \eta}$  is the spectral matrix for  $P_{\hat{i}}$ , i.e. a diagonal matrix composed with the eigenvalues of  $P_{\hat{j}}$  and  $\sqrt{\Lambda_{\hat{j}}}$  denotes a diagonal matrix containing the square root of these eigenvalues,

then the observer gains are given by  $K_{i_j} = P_j^{-1} Y_{i_j}$  and the observer's state  $\hat{x}(t)$  converge asymptotically to the system's state  $x(t)$  (without external disturbances), i.e. the estimation error  $e(t) \rightarrow 0$  when  $t \rightarrow +\infty$ , and the  $H_{\infty}$  criterion (9) is satisfied (for external disturbances attenuation).

**Proof.** Let us consider the following multiple Lyapunov function candidate:

$$
v(t) = e^{T}(t) P_{\hat{\sigma}} e(t)
$$
 (14)

where  $P_{\hat{\sigma}} = \sum_{j=1}^{m} \sigma_j(t) P_j$  with  $P_{\hat{j}} = P_{\hat{j}}^T > 0$ . The time derivative of  $(14)$  can be written as:

$$
\dot{v}(t) = 2\left(e^T P_{\hat{\sigma}} \left(A_{h_{\sigma}} - K_{h_{\hat{\sigma}}} C\right) e + e^T P_{\hat{\sigma}} \left(A_{h_{\sigma}} - A_{h_{\hat{\sigma}}}\right) x\right.\left.+ e^T P_{\hat{\sigma}} \left(B_{h_{\sigma}} - B_{h_{\hat{\sigma}}}\right) u - e^T P_{\hat{\sigma}} K_{h_{\hat{\sigma}}} W w\left(t\right)\right)
$$
\n(15)

Moreover, the  $H_{\infty}$  criterion (9) is satisfied if:

$$
\dot{v}(t) + e^{T}(t) e(t) - \gamma^{2} w^{T}(t) w(t) < 0 \qquad (16)
$$
\nwhich can be rewritten as:

$$
\psi(t)^{T} \Omega(t) \psi(t) < 0 \tag{17}
$$

with  $\psi(t) = \begin{bmatrix} e^T & x^T & u^T & w^T \end{bmatrix}$  and:

$$
\Omega(t) = \begin{bmatrix} \mathcal{H}_e \left( P_{\hat{\sigma}} A_{h_{\sigma}} - P_{\hat{\sigma}} K_{h_{\hat{\sigma}}} C \right) + I & (*) & (*) & (*) \\ A_{h_{\sigma}}^T P_{\hat{\sigma}} - A_{h_{\hat{\sigma}}}^T P_{\hat{\sigma}} & 0 & 0 & 0 \\ B_{h_{\sigma}}^T P_{\hat{\sigma}} - B_{h_{\hat{\sigma}}}^T P_{\hat{\sigma}} & 0 & 0 & 0 \\ -P_{\hat{\sigma}} K_{h_{\hat{\sigma}}} W & 0 & 0 & -\gamma^2 I \end{bmatrix}
$$

To deal with the inequality (17), with a scalar  $\varepsilon > 0$ , let us consider the following constraint:

$$
||e||_2^2 - \varepsilon \left( ||x||_2^2 + ||u||_2^2 \right) > 0 \tag{18}
$$

From (18) and applying lemma 1, the inequality (17) is satisfied if there exists a scalar  $\lambda > 0$  such that:

$$
\begin{bmatrix}\n\Gamma(t) & (*) & (*) & (*) \\
A_{h_{\sigma}}^T P_{\hat{\sigma}} - A_{h_{\hat{\sigma}}}^T P_{\hat{\sigma}} & -\lambda \varepsilon & 0 & 0 \\
B_{h_{\sigma}}^T P_{\hat{\sigma}} - B_{h_{\hat{\sigma}}}^T P_{\hat{\sigma}} & 0 & -\lambda \varepsilon & (*) \\
&- P_{\hat{\sigma}} K_{h_{\hat{\sigma}}} W & 0 & 0 & -\gamma^2 I\n\end{bmatrix} < 0\n\tag{19}
$$

where  $\Gamma(t) = \mathcal{H}_e (P_{\hat{\sigma}} A_{h_{\sigma}} - Y_{h_{\hat{\sigma}}} C) + (1 + \lambda) I$ .

With the bijective change of variable  $Y_{h_{\hat{\sigma}}} = P_{\hat{\sigma}} K_{h_{\hat{\sigma}}}$ , the inequality (19) is satisfied if the LMI conditions (11) hold. Now, we have to prove that the Lyapunov Function candidate (14) is decreasing at the observer's switching instants, i.e.:

$$
(x - \hat{x}^+)^T P_{\hat{j}^+} (x - \hat{x}^+) \le (x - \hat{x})^T P_{\hat{j}} (x - \hat{x}) \qquad (20)
$$

where, at switching instants,  $\hat{j}$  and  $\hat{j}^+$  denotes respectively the observer's previous and forthcoming switched modes and  $\hat{x}^+$  the estimated state to be updated, whose value computation will be further detailed.

Following the pioneer work of Petterson (2005), let us first assume that  $\hat{x}^+$  satisfies  $y = C\hat{x}^+$ . In that case we have  $C(x - \hat{x}^+) = y - y = 0$  and, for any matrix M of appropriate dimension, the following equality holds:

$$
\left(x - \hat{x}^+\right)^T \left(M^T C + C^T M\right) \left(x - \hat{x}^+\right) = 0 \tag{21}
$$

Then, assume that there exist the matrices  $G_{\hat{i}}$  such that the equality  $(10)$  is satisfied, according to  $(21)$  the inequality (20) can be rewritten as:

$$
(x - \hat{x}^+)^T P_{\hat{j}} (x - \hat{x}^+) \le (x - \hat{x})^T P_{\hat{j}} (x - \hat{x})
$$
 (22)

Now, we need to determine the updated value of the observer's state  $\hat{x}^+(t) \in \overline{S}_{\hat{i},\hat{j}^+}$  such that the inequality (22) is verified. To this end, let us consider  $R_{\hat{i}} \in \Re^{\eta \times \eta}$ such that  $P_{\hat{j}} = R_{\hat{j}}^T R_{\hat{j}}$ . Note that, according to the spectral theorem (Derinkuyu and Pinar, 2015), the matrices  $R_{\hat{i}}$  can be obtained as given in (13). Thus, the inequality (22) is equivalently satisfied if:

$$
\left\| R_{\hat{j}}\left(x - \hat{x}^{+}\right) \right\| \le \left\| R_{\hat{j}}\left(x - \hat{x}\right) \right\| \tag{23}
$$

To find the updated value  $\hat{x}^+$ , lying on the hyper plane  $y = C\hat{x}^+$ , that minimizes the distance  $\left\| R_{\hat{j}}\left(x - \hat{x}^\dagger\right) \right\|$ , let us consider the following optimization problem:

$$
\min_{\hat{x}^+} \left\| R_{\hat{j}}\left(\hat{x}^+ - \hat{x}\right) \right\|
$$
\nsubject to :  $C\hat{x}^+ = y$  (24)

By denoting  $\alpha_{\hat{j}} = R_{\hat{j}} (\hat{x}^+ - \hat{x})$ , i.e.  $R_{\hat{j}} \hat{x}^+ = \alpha_{\hat{j}} + R_{\hat{j}} \hat{x}$ , the optimization problem (24) can be rewritten as:

$$
\min_{\hat{x}^+} \left\| \alpha_{\hat{j}} \right\|
$$
\nsubject to : 
$$
CR_{\hat{j}}^{-1} \alpha_{\hat{j}} = y - C\hat{x}
$$
\n(25)

which solution, being the minimum length least square solution to  $y - C\hat{x}$ , is:

$$
\alpha_{\hat{j}} = \left(CR_{\hat{j}}^{-1}\right)^{\dagger} \left(y - C\hat{x}\right) \tag{26}
$$

Hence:

$$
R_{\hat{j}}\hat{x}^{+} = R_{\hat{j}}\hat{x} + \left(CR_{\hat{j}}^{-1}\right)^{\dagger} (y - C\hat{x}) \tag{27}
$$

Left multiplying (27) by  $R_{\hat{j}}^{-1}$  yields to (12). This ends the  $\Box$   $\Box$ 

#### 4. NUMERICAL EXAMPLE

The present section is dedicated to illustrate the effectiveness of the proposed switched TS observer design approach. To this end, let us consider the following second order switched TS system with two switched modes and two rules in each of them:

$$
\begin{cases}\n\dot{x}(t) = \sum_{j=1}^{2} \sum_{i=1}^{2} \sigma_j(t) h_{i_j}(z_j(t)) (A_{i_j} x(t) + B_{i_j} u(t)) \\
y(t) = Cx(t) + W\omega(t)\n\end{cases}
$$

(28) with the state vector  $x^T = [x_1 \ x_2]$  and the matrices  $A_{1_1} =$  $\begin{bmatrix} -0.2 & 10 \\ 0 & 0 \end{bmatrix}$  $-2$   $-1$ 1  $, A_{2_1} =$  $\begin{bmatrix} 1.5 & 2 \end{bmatrix}$  $-6$   $-0.5$ 1  $, B_{1_1} =$  $\lceil 1$  $\boldsymbol{0}$ 1 ,  $B_{2_1} =$  $\bar{[}0$ 1 1 in the first mode and  $A_{1_2}$  =  $\begin{bmatrix} -2 & 12 \\ 2 & 12 \end{bmatrix}$  $-2$   $-1$ Ī. ,

 $A_{2_2} = \begin{bmatrix} 1.5 & 2 \\ -2.5 & 1 \end{bmatrix}$  $-2.5$  1.9 1  $, B_{1_2} =$  $\lceil 2$  $\theta$ 1 ,  $B_{2_2} =$  $\lceil 0$ 2 1 in the second one,  $C = [-1, -1.5]$ ,  $W = [0.1, 0.1]$  and the membership functions  $h_{1_1}(y(t)) = 1 - \sin^2(y(t)), h_{1_2}(y(t)) = 1$  $h_{1_1}(y(t)), h_{2_1}(y(t)) = 1 - (\sin(3y(t)))^2$  and  $h_{2_2}(y(t)) =$  $1-h_{2_1}(y(t)).$ 

Solving the LMI-based conditions given in the theorem 3, we obtain the gains  $K_{1_1} = \begin{bmatrix} 53.5 \\ -62 \end{bmatrix}$  $-62.8$ 1 ,  $K_{1_2} = \begin{bmatrix} 31.2 \\ -40 \end{bmatrix}$  $-40.3$ 1 ,  $K_{2_1} = \begin{bmatrix} 20.3 \\ -21 \end{bmatrix}$  $-21.8$ 1 ,  $K_{2_2} = \begin{bmatrix} 17.4 \\ -20 \end{bmatrix}$  $-20.5$ 1 for the switched observer (4) and the Lyapunov matrices  $P_1$  =  $17.9$  15.5 15.5 14.4 1 ,  $P_2 =$  $10.8$  10.1 10.1 14.3 1 , with  $\gamma = 5.5, \, \varepsilon = 20, \, G_1 = [3.6 \, 0.04]$ and  $\lambda = 8.6$ .

In the sequel, we assume that the system (28) switches within the frontier defined by the hyper planes  $S_{1,2} = x_1 +$  $0.25x_2$  and  $S_{2,1} = x_1 + x_2$ . Moreover, the simulation of the switched system (28) is performed with the input signal:

$$
\begin{cases} u(t) = 1 & 0 \le t \le 2s \\ u(t) = 10\sin(\pi t + 2) & 2 < t \le 5s \end{cases}
$$
 (29)

and the output disturbance:

$$
\begin{cases} w(t) = [0 \ 0]^T & 0 \le t \le 2.5s \\ w(t) = [1 \sin(0.8\pi t + 10) \ 0]^T & 2.5 < t \le 4s \\ w(t) = [0 \ 0]^T & 4 < t \le 5s \end{cases}
$$
(30)

Then, two cases are considered in simulation for the switching hyper planes of the designed asynchronous switching TS observer.

Case 1: The designed switched observer  $(4)$  and the switched system (28) share the same switching sets, i.e.  $\overline{S}_{\hat{i},\hat{j}+} = S_{j,j}$ . For simulation purpose, the system and observer initial state vectors have been respectively set as  $x^T(0) = [3 \ 16.5], \hat{x}^T(0) = [-2 \ -10].$  That is to say, the observer and the system have been respectively initialized in their first and second modes.

The simulation results for this case are shown in Fig.1 to Fig.4. Fig. 1 exhibits the phase planes of the observer and the system. Fig. 2 shows the trajectories of both state and estimated vectors. Moreover, Fig. 3 shows the estimation error evolution. In addition, Fig. 4 depicts the evolution of both system's and observer's modes. This simulation illustrates the ability of the designed observer to accurately estimate the system's state when they both share the same switching sets. Moreover, let us highlight that, even if the system and the observer share the same switching sets, they remain asynchronous (i.e.  $\hat{\sigma}(t) \neq \sigma(t)$ ) since they don't cross the hyper-planes' frontiers exactly at the same instants. This is pointed-out in the zooms shown in Fig. 4. However, when the transient is passed, i.e. when the observer's state get close to the system state, this case also allows the estimation of the system's switching instants from the observer ones.

Case  $2$ : This second case is dedicated to show what happens when only poor knowledge regarding to the system's switching law are available. For instance, this is



Fig. 1. System's and observer's phase planes, + denotes the initial conditions and  $\bullet$  the final states (*Case 1*).



Fig. 2. States and estimated states evolution (*Case 1*).



Fig. 3. Evolution of the estimation errors  $(Case 1)$ .



Fig. 4. Evolution of system and observer modes (Case 1).

often the case in practical application when parametric identification of the system's switching law are biased. The only difference with regard to the previous case  $(Case 1)$ is that the observer's switching sets defer from the ones of the switched system  $(\bar{S}_{ij} \neq \bar{S}_{ij})$ . Thus, in this case, to perform the simulation we define the observer's switching sets as  $\bar{S}_{\hat{1},\hat{2}} = 0.97\hat{x}_1 + 0.22\hat{x}_2$  and  $\bar{S}_{\hat{2},\hat{1}} = 0.97\hat{x}_1 + 0.90\hat{x}_2$ .

For this simulation, the same initial states as in Case 1 for both the system and the observer have been considered for comparison purpose. Therefore, with the considered switching sets, the observer and the system are still respectively initialized in their first and second modes.

The simulation results are shown in Fig.5 to Fig.8. In contrast to the first case, Fig.8 shows that the system and the observer switch within different time frames because they do not share the same switch sets. Indeed, in some larger time-intervals, the switched system (1) and the switched observer (4) operate asynchronously in different modes  $(\sigma(t) \neq \hat{\sigma}(t))$ . This is clearly shown in Fig.8 for  $t \in [1.5, 2.6]$  where the system belongs to mode 2 while the observer belongs to mode 1, leading to poorer state estimation (see Fig 7 and 5). Note also that the external output disturbance acts during this interval, which doesn't help the observer to quickly converge. However, after a while (for  $t > 2.7$ ), the observer better catches the system's state as their respective switching frontiers gets closer and, in this case, we can observe that their respective switching laws tend to synchronize (see the zooms in Fig. 8). This illustrates that the state estimation is produced with good accuracy after a finite time interval, asserting the validity of the proposed asynchronous switched TS observer design methodology.



Fig. 5. System's and observer's phase planes, + denotes the initial conditions and  $\bullet$  the final states (*Case 2*).



Fig. 6. States and estimated states evolution (*Case 2*).



Fig. 7. Evolution of estimation error  $(Case 2)$ .



Fig. 8. Evolution of both system's and observer's mode  $(Case 2)$ .

#### 5. CONCLUSION

This work has dealt with the design of a robust observer for a class of switched TS systems subject to external output disturbances. The proposed observer delivers the continuous state estimation under arbitrary switching sequence. Thanks to a candidate multiple switched Lyapunov functional, LMI-based conditions, satisfying  $H_{\infty}$  rejection disturbance performances, for the robust observer design has been obtained. Finally, illustrative examples, showing clearly the efficiency of the designed observer, have been presented. Note that, in this study, it assumed that the premise variables are measurable. Thus, the extension of the proposed design method to the case of unmeasurable premise variables will be the focus of our future work.

#### ACKNOWLEDGEMENTS

The authors would like to thank Mr. Enrico Muth for his interest in this study.

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