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### ACS APPLIED ELECTRONIC MATERIALS

## <sup>1</sup> Huge Reduction of the Wake-Up Effect in Ferroelectric HZO Thin <sup>2</sup> Films

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8 Supporting Information

9 **ABSTRACT:** The wake-up effect is a major issue for ferroelectric  $HfO_2$ -based 10 memory devices. Here, two TiN/HZO/TiN structures deposited by magnetron 11 sputtering on silicon are compared. The maximum remanant polarization is 12 higher than 21  $\mu$ C/cm<sup>2</sup> for both samples, but a strong difference is observed in

13 the electrical behavior. For the mesa sample, the difference between the

maximum and initial remanent polarization is only 3  $\mu$ C/cm<sup>2</sup>, whereas it is

around 14  $\mu$ C/cm<sup>2</sup> in the non-mesa case. We discuss the root causes of these

16 behaviors in light of GIXRD results.



Letter

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17 **KEYWORDS:** HfO<sub>2</sub>, ZrO<sub>2</sub>, HZO, ferroelectricity, wake-up effect, FRAM

 $\neg$  he discovery of ferroelectric Si-doped HfO<sub>2</sub><sup>1</sup> has paved 18 L the way to a wide variety of research interests and 19 20 technical developments. The growing number of papers 21 dealing with  $HfO_2$ -based materials<sup>2</sup> is a relevant indicator of 22 the growing interest for this subject. Undeniably, many 23 applications could benefit from ferroelectric HfO2-based 24 materials such as ferroelectric random access memory 25 (FRAM), a ferroelectric field effect transistor (FeFET), a 26 negative capacitance field effect transistor (NCFET), a 27 ferroelectric tunnel junction (FTJ), synaptic devices, pyro-28 electric energy harvesters, piezoelectric devices, and so on. 29 However, major issues are still hindering the appearance of  $_{30}$  ferroelectric HfO<sub>2</sub>-based materials on the market. These issues 31 are mainly related to the well-known wake-up effect, imprint, 32 fatigue, and endurance. Recent studies on the subject point out 33 crystallographic phase change and oxygen vacancy diffusion 34 during cycling as the root causes of the issues cited above.

Of all the numerous dopants that have been tested in 36 ferroelectric  $HfO_2$ -based materials, the most addressed is 37 probably  $Zr^{4+}$ , because both  $HfO_2$  and  $ZrO_2$  are already used 38 in the CMOS<sup>3</sup> and DRAM<sup>4</sup> industries. Moreover,  $Zr^{4+}$  allows 39 the lowest annealing temperature of all dopants, making it 40 compatible with the silicon semiconductor industry.

<sup>41</sup> Compared to the hundreds of articles dealing with (Hf, <sup>42</sup> Zr)O<sub>2</sub> solid solutions (HZO) deposited by ALD, sputtering <sup>43</sup> has rarely been used.<sup>5–14</sup> However, the deposition of materials <sup>44</sup> by sputtering shows many benefits compared to ALD:

- (ii) Sputtering can prevent carbon contamination that 46 cannot be avoided with ALD precursors. 47
- (iii) The deposition can be performed at room temperature. 48
- (iv) In principle, sputtering can be carried out in one run in 49 the same sputtering chamber. 50
- (v) Sputtering is a low-cost reproducible process. 51

Consequently, HZO development could be greatly 52 enhanced by using sputtering. 53

Moreover, most of the articles dealing with HZO sputtering 54 use cosputtering.<sup>7–9,11,13,14</sup> Cosputtering enables more paramst eters to be tuned, particularly the Zr doping.<sup>11</sup> However, for 56 industrial manufacturing, single target sputtering appears to be 57 simpler and less expensive. 58

In this work, two different structures were realized by 59 magnetron sputtering with a single target. Their performances 60 are among the best in sputtering, but their behaviors are 61 completely different. Particularly, the mesa structure presents a 62 significantly reduced wake-up effect. We discuss the origins of 63 these differences and the consequences for electrical measure- 64 ment methods used to characterize ferroelectric  $HfO_2$ -based 65 materials.

The structure shown in Figure 1a is called NM-sample for 67 fl "non-mesa" structure and the structure shown in Figure 1b is 68 called M-sample for "mesa" structure. 69

45 (i) Sputtering can be much faster than ALD deposition.

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Figure 1. Scheme of (a) the NM-sample and (b) M-sample.

Si substrates were cleaned with ultrasonication in acetone r1 and ethanol for 1 min. Substrates are Si-doped and (100)r2 oriented. The native oxide layer of each substrate is removed r3 by a buffer oxide etch (BOE) process. For both processes, a 50 r4 nm-thick bottom electrode (BE) is deposited in the conditions r5 detailed in Table 1. This layer blankets the entire Si substrate.

Table 1. Film Growth Conditions for TiN and HZO

t1

	sputtering	
target-substrate distance	8 cm	
base pressure	$<5 \times 1^{-7}$ mbar	
deposited elements	TiN	(Hf, Zr)O <sub>2</sub>
substrate	Si	Si/TiN
target	Ti	$ZrO_2/HfO_2$ (50/50)
target RF power	300 W	100 W
holder DC bias voltage	60 V	none
gas	Ar = 50  sccm	Ar = 50  sccm
	$N_2 = 3 \text{ sccm}$	
working pressure	$5 \times 10^{-3}$ mbar	$5 \times 10^{-2}$ mbar
deposition speed	5.2 nm/min	5 nm/min
rapid thermal annealing (RTA) conditions		
temperature	450 °C	
atmosphere	$N_2$	
duration	30 s	

76 Then, an HZO layer covering the whole TiN layer is
77 deposited. The HZO thickness is measured by X-ray
78 reflectivity (XRR). HZO layers are 12.3 nm-thick and 11.0
79 nm-thick for the M-sample and the NM-sample, respectively.
80 For the NM-sample, UV photolithography is carried out.
81 Then, a 50 nm-thick TiN TE followed by a 100 nm Pt top
82 electrode for mechanical and electrical contact are deposited. A
83 lift-off step is then performed. Finally, the NM-sample is
84 annealed by RTA under the conditions described in Table 1. It
85 means that, for the NM-sample, HZO is only partially covered
86 during the RTA crystallization process.

For the M-sample, the HZO layer is blanketed with a 50 nm-88 thick TiN layer. Then, UV photolithography and lift-off are 89 carried out to define the electrodes with the deposition of a 90 100 nm-thick Pt layer followed by a 50 nm-thick Cr layer. Cr is 91 used as a hard mask for etching. The M-sample is annealed by RTA in the conditions described in Table 1. Finally, the  $_{92}$  sample is etched by RIE at 300 W (RF) for 20 min with SF<sub>6</sub> as  $_{93}$  a reactive gas. The final structure is presented in Figure 1b. For  $_{94}$  this structure, HZO is fully covered with TiN TE during the  $_{95}$  annealing step.

GIXRD is performed on a four-circle Smartlab Rigaku 97 diffractometer using a 9 kW copper rotating anode. 98

Electrical characterization is carried out on 20  $\mu$ m diameter 99 capacitors using a probe station and a setup composed of an 100 arbitrary waveform generator (Nippon Factory WF1966), a 101 transimpedance current amplifier (Keithley 428), and a 12 bit 102 Digital Storage Oscilloscope (Nicolet Integra 40). 103

Endurance tests were performed with bipolar square pulses 104 (commonly called set/reset sequence) until breakdown. The 105 set/reset sequence is achieved in two different configurations: 106 2.5 kHz/3.5 V and 1.0 MHz/3.0 V. The first sequence allows 107 the stress to be maximized without breakdown. The second 108 set/reset sequence is used in order to be as close as possible to 109 the microelectronic standard, and it is therefore used as a 110 reference.

*P*–*E* curves are obtained using the PUND technique. This <sup>112</sup> consists of applying a negative set pulse followed by two <sup>113</sup> positive pulses (P and U) and then two negative pulses (N and <sup>114</sup> D). The PUND maximum amplitude voltage equals that of the <sup>115</sup> set/reset sequence. PUND pulses are triangular pulses with a <sup>116</sup> rise/fall time of 100  $\mu$ s, corresponding to 2.5 kHz <sup>117</sup> ( $=\frac{1}{4 \times 100} \mu s^{-1}$ ).

 $_{4 \times 100}$  First, the change of the sum of the absolute values of the  $_{118}$ 

positive remanent polarization and the negative remanent 119 polarization  $|P_{r+}| + |P_{r-}|$  during cycling is studied. Figure 2 120 f2 shows the results for the two different set/reset sequences 121 described in the experimental section. 122

At 1.0 MHz and 3.0 V (Figure 2a),  $|P_{r+}| + |P_{r-}|$  for the NM- 123 sample starts at around 5  $\mu$ C/cm<sup>2</sup>. This value increases until 124 10<sup>5</sup> cycles, where it reaches around 29  $\mu$ C/cm<sup>2</sup>. Then, it 125 decreases until breakdown. Such an effect is not observable for 126 the M-sample. Indeed,  $|P_{r+}| + |P_{r-}|$  starts at 25  $\mu$ C/cm<sup>2</sup> (instead 127 of 5  $\mu$ C/cm<sup>2</sup> for the NM-sample) and reaches a maximum of 128 32.8  $\mu$ C/cm<sup>2</sup> at 2 × 10<sup>3</sup> cycles. So, the wake-up effect can be 129 considered negligible in these conditions. Subsequently, fatigue 130



**Figure 2.** Change of  $|P_{r+}| + |P_{r-}|$  versus the number of cycles with the stress conditions (a) 1.0 MHz and 3.0 V and (b) 2.5 kHz and 3.5 V for the NM-sample (black curve) and M-sample (red curve).



Figure 3. Polarization versus applied electrical field for (a) the NM-sample at  $10^5$  cycles and (b) the M-sample at  $2 \times 10^3$  cycles under the stress conditions: 2.5 kHz and 3.5 V.

<sup>131</sup> begins and breakdown occurs after  $5 \times 10^5$  cycles. In <sup>132</sup> comparison, the NM-sample breaks down after  $1 \times 10^7$  cycles. <sup>133</sup> More severe stress conditions were also applied (Figure 2b). <sup>134</sup> The same tendencies are observed: here, the wake-up effect is <sup>135</sup> also significantly reduced on the M-sample compared to that <sup>136</sup> on the NM-sample, but it is detrimental for the endurance of <sup>137</sup> the M-sample. In fact, the breakdown occurs at a lower number <sup>138</sup> of cycles for the M-sample compared to for the NM-sample.

For both samples,  $|P_{r+}| + |P_{r-}|$  values are much higher at 2.5 140 kHz/3.5 V and the breakdown occurs earlier. These results are 141 consistent with previous observations.<sup>15–17</sup>

For both stress conditions, the  $P_r$  of the NM-sample 142 increases until it exceeds the  $P_r$  of the M-sample for a given 143 number of cycles, because fatigue occurs earlier for the M-144 sample. As a consequence, at 1.0 MHz/3.0 V (Figure 3a), 145 between the first cycle and the breakdown, the M-sample has a 146 147 higher maximum  $P_r = 16.4 \ \mu C/cm^2$  than the NM-sample, whereas at 2.5 kHz/3.5 V (Figure 2b), the M-sample has a 148 higher maximum  $P_r = 21.7 \ \mu C/cm^2$ . This is due to the 149 150 reduced wake-up effect. In fact, with the M-sample, the 151 maximum remanent polarization is always reached very rapidly, 152 whereas with the NM-sample, the higher the stress conditions, 153 the faster you can reach the maximum remanent polarization. Moreover, for the NM-sample, fatigue is always reached at 154 around  $10^6$  cycles, which means that under a low-stress 155 sequence, fatigue is reached on the NM-sample before crossing 156 the curve of the M-sample. It follows that the M-sample has a 157 higher remanent polarization under low-stress conditions, 158 whereas the NM-sample has a higher maximum remanent 159 polarization under high-stress conditions. Therefore, the 160 maximum  $P_r$  seems to be more dependent on the stress 161 conditions than on the structures themselves, which could have 162 important consequences on industrial applications. 163

The M-sample has a reduced wake-up effect, but it also 164 shows a sign of fatigue before the NM-sample. It is possible 165 that the M-sample is already in an awake state, which leads to 166 the absence of wake-up and an earlier fatigue and breakdown 167 compared to the NM-sample. 168

For the M-sample, the maximum  $P_r$  minus the initial  $P_r$  is 169 around 3–4  $\mu$ C/cm<sup>2</sup> in both conditions. In comparison, the 170 difference is between 12 and 16  $\mu$ C/cm<sup>2</sup> for the NM-sample. 171 There is 1 order of magnitude between both increases of  $P_r$  172 during the wake-up. 173

In high-stress conditions, there is no double peak for the M- 174 sample, and in low-stress conditions, the double peak 175 disappears at the second measurement cycle. For the NM- 176



Figure 4. GIXRD measurements comparing the NM-sample (black curve) and the M-sample (red curve) (a) before RTA and (b) after RTA. M stands for monoclinic, O stands for orthorhombic, and T stands for tetragonal phases.

177 sample, a double peak is clearly observable during the first 178 measurement cycle, and a small peak (coming from the double 179 peak) is observable until  $10^3$  cycles for high-stress conditions 180 and until 5 ×  $10^4$  cycles for low-stress conditions (see the 181 Supporting Information for more details).

Finally, at 10 cycles, an inflection point can be seen. It is caused by the measurements realized due to the PUND technique, which also wakes the sample. The PUND measurement is negligible after 20 cycles, as compared to the set/reset cycles.

187 It is to be noted that these results have been reproduced on 188 many electrodes.

To assess the quality of our films, Figure 3 shows the 190 polarization versus the electrical field when  $P_r$  has reached its 191 maximum value. PUND and PN curves are represented. The 192 value of  $P_r$  is higher in PN curves, because PN includes the 193 leakage current.  $P_r$  values of the PN measurements have not 194 been discussed in this report, because they can include 195 extrinsic effects. Leakage is very well-compensated, because the 196 PN curves show open cycles, whereas PUND does not. Also, 197 the P-E curves by PUND show very pinched cycles, which 198 means that the samples are very well-saturated.

Then, grazing incidence X-ray diffraction is carried out to 199 200 enlighten the electrical characterizations. Figure 4 shows GIXRD results before (Figure 4a) and after (Figure 4b) 201 annealing of the NM-sample and the M-sample. ICDD card 202 nos. 00-038-1420 and 00-004-0802 were respectively used for 203 204 TiN and Pt. For the HZO m-phase, ICDD card no. 04-002-5428 was used. The peak at around 30.5° for the o/t-phase 205 came from the work of Lee et al.,<sup>8</sup> and we knew from the first 206 paper on ferroelectricity in hafnium oxide by Böscke et al.<sup>1</sup> that 207 208 a peak at around 25° can be mistaken with the peak coming 209 from the m-phase at this angle. In Figure 4a, the M-sample 210 presents a TiN(111) peak, which is not visible in the NM-211 sample. This is probably caused by the different structures of 212 the TiN TE in each sample. Comparing the NM-sample and 213 the M-sample in Figure 4b, it is clear that the polycrystalline 214 nature of the samples is completely different. The NM-sample 215 shows clear monoclinic phases (m-phases), whereas no 216 monoclinic peak can be seen in the M-sample. On the M-

sample, only the o(111) peak can be seen. Other peaks come 217 from the electrodes. 218

At the microcrystalline scale, the orthorhombic phase (o- 219 phase) is recognized as the origin of ferroelectricity. m-Phases 220 are assumed to be parasitic phases for ferroelectricity. Two 221 hypotheses are generally considered as the causes of the wake- 222 up effect according to Fengler et al:<sup>18</sup> crystallographic phase 223 change contributions and oxygen vacancy diffusion. Grimley et 224 al.<sup>19</sup> have observed a phase transition from the m- to the o- 225 phase using scanning transmission electron microscopy 226 (STEM) and impedance spectroscopy. Therefore, tremendous 227 reduction in the amount of m-phase in the M-sample could 228 have led to a drastic decrease in the wake-up effect. Moreover, 229 the presence of many monoclinic orientations coexisting with 230 the o-phase on the NM-sample could also play a key role in the 231 oxygen vacancy redistribution, because the number of 232 interfaces between crystallites has increased on the NM- 233 sample. In fact, the crystalline structure influences the 234 redistribution of charged defects, the mobility of these charges, 235 charge trapping, and charge screening. For that reason, it can 236 be concluded that the microcrystalline structure seems to be 237 the main parameter influencing the two different electrical 238 behaviors observed in this Letter. 239

One could argue that the different crystalline structures are 240 due to the TiN TE difference between the two samples. In fact, 241 in the case of the M-sample, TiN is blanketed over the entire 242 HZO layer, whereas in the case of the NM-sample, it covers 243 only the areas under the top electrodes. This implies a 244 completely different stress state between the two samples. As a 245 consequence, in the case of the M-sample, it turns the o-phase 246 into the lowest energy phase. It has actually been demonstrated 247 that TiN TE acts as a tensile stressor on the HZO film during 248 the annealing process.<sup>20–24</sup> The stress inhibits the formation of 249 the monoclinic phase during HZO crystallization, forming an 250 orthorhombic phase that generates a large ferroelectric 251 polarization, even at low process temperatures. 252

Finally, Chernikova et al.<sup>25</sup> compare the  $P_r$  performances of 253 an HZO layer and a La-doped HZO layer called "HZLO". The 254 HZO layer has a very low wake-up effect but also a very low 255 endurance, whereas HZLO has a very high endurance with a 256

257 very high wake-up effect. The exact same phenomenon is 258 observed here when measuring the NM-sample and the M-259 sample. Consequently, the root causes of the huge reduction of 260 the wake-up effect and the decreasing of cycles before 261 breakdown in both articles could be assumed to be the 262 same. However, they observed that "the HZLO film showed a 263 slightly larger grain size compared to the HZO film". 264 Consequently, according the authors of the article, "the bulk 265 free energy difference between the FE o-phase and non-FE m-266 phase decreased after La doping." Unfortunately, this cannot 267 explain what is happening in our work, because the observation 268 of clear monoclinic peaks in the GIXRD pattern of the NM-269 sample Figure 4b suggests that the free energy difference 270 decreases. Manufacturing both structures with HZLO instead of HZO may help to shed light on this mystery. 271

<sup>272</sup> This Letter reports the fabrication of two samples deposited <sup>273</sup> by magnetron sputtering with excellent performances, quite <sup>274</sup> similar to samples deposited by ALD.<sup>25</sup>  $P_r$  values are among <sup>275</sup> the highest for samples deposited by sputtering.

276 Although the M-sample and the NM-sample show very 277 similar maximum  $P_r$  values, both samples demonstrate 278 completely different electrical behavior. During cycling, the 279 increase of the  $P_r$  value for the NM-sample is more than an 280 order of magnitude higher than that of the M-sample. It is 281 accompanied by a decrease of the endurance, which is 2 orders 282 of magnitude higher for the NM-sample than for the M-283 sample.

As the electrical behaviors are not the same, for low-stress conditions, the M-sample has a higher maximum  $P_r$  value during cycling, whereas for high-stress conditions, the NMsample has a higher  $P_r$  value during cycling. As a matter of fact, thas been proven that maximum  $P_r$  values are more sensitive stress conditions than the to structures themselves.

The origins of the different electrical behaviors come from the microcrystalline structures of the two samples, according to GIXRD results. The crystallization takes place during the annealing step. During annealing, the M-sample is built with a TiN TE fully covering the HZO layer, whereas the TiN only partially covers the HZO layer in the case of the NM-sample. It induces different stress states, which lead to two different microcrystalline patterning. The M-sample shows no monose clinic peak, whereas the NM-sample shows many monoclinic orientations. This explains the huge reduction of the wake-up and effect.

#### 301 ASSOCIATED CONTENT

#### 302 Supporting Information

303 The Supporting Information is available free of charge on the 304 ACS Publications website at DOI: 10.1021/acsaelm.9b00367.

Chronograms for the M-sample and NM-sample describing the presence, the absence, and the mergers of the double peak obtained due to the PUND measurements (PDF)

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314 Notes

315 The authors declare no competing financial interest.

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