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Aminolysis of cyclic-carbonate vegetable oils as a non-isocyanate route for the synthesis of polyurethane: a kinetic and thermal study

*Wander Y. Pérez-Sena^{1,2}, Xiaoshuang Cai¹, Nasreddine Kebir³, Lamiae Vernières-Hassimi¹,
Christophe Serra⁴, Tapio Salmi², Sébastien Leveneur^{1,2*}*

¹*Normandie Université LSPC-Laboratoire de Sécurité des Procédés Chimiques, EA4704, INSA/Université Rouen, BP08, Avenue de l'Université, 76801 Saint-Etienne-du-Rouvray, France; E-mail: sebastien.leveneur@insa-rouen.fr*

²*Laboratory of Industrial Chemistry and Reaction Engineering, Johan Gadolin Process Chemistry Centre, Åbo Akademi University, Biskopsgatan 8, FI-20500 Åbo/Turku, Finland.*

³*Normandie Université, INSA de Rouen, PBS UMR 6270 FR 3038 CNRS, INSA de Rouen, 685 Avenue de l'Université, 76801 Saint Etienne du Rouvray, France.*

⁴*Université de Strasbourg, CNRS, ICS UPR 22, 23 rue du Loess, BP84047, 67034 Strasbourg Cedex 2, France*

ABSTRACT

Production of polyurethane is increasing since the recent years. Nevertheless, this production uses hazardous chemicals, which is isocyanate. Academy has put a lot of effort to develop some non-isocyanate polyurethane routes. One of the most promising is the aminolysis of cyclic-carbonate by diamine. To industrialize this way of production, kinetic and thermodynamic data are needed. The first steps were to optimize the production of methyl oleate, epoxidized methyl oleate and carbonated methyl oleate. Then, a kinetic model was built for a model reaction which is the aminolysis of carbonated methyl oleate by n-butylamine by taking into account the side reaction of amidation. The model fits correctly the experimental data. A Tian-Calvet calorimeter was used to determine the different reaction enthalpies. It was found that the reactions of aminolysis and amidation were few exothermic.

Keywords: Polyurethane; Vegetable Oils; Kinetic Model; Calorimetry

1. Introduction

In the last years, the production of polyurethane has significantly increased. The global production of this polymer was close to 20 Mt in 2014 making it among the 6 polymers the most produced [1]. This is due to the versatile properties of polyurethanes (PUs). Indeed, the application of these polyurethane materials can be found in different fields such as ship industry, health sector, automotive or bedding [2,3].

Production of PUs is commonly done by the reaction of polyols with di-isocyanates. Polyols can be produced from renewable feedstock like vegetable oils or their derivatives [4-6]. On the contrary, diisocyanate reactant is a petroleum -derived product from the reaction of an amine on phosgene, which is unstable and toxic [7]. Academic community has extensively studied the non-isocyanate route for the production of PUs and the cyclic-carbonate/amine route is more and more interesting for industry [8]. One of the most developed pathways is the reaction between a five-membered bicyclocarbonate and a diamine [7, 9-17].

Synthesis of five-membered cyclic-carbonates can be done by several routes: reaction between CO₂ and 1,2-diols [18] or between oxirane group and γ -butyrolactone [19]. The most common way for the production of cyclic-carbonates is the gas-liquid reaction between CO₂ and oxirane groups [20-22].

Different research groups [8, 28-42] have studied the kinetics of aminolysis for cyclic-carbonate compounds. In the review of the non-isocyanate routes for the production of polyurethanes, Maissoneuve et al. [8] have summarized the kinetics of cyclic-carbonate aminolysis described in the following references [28-42]. It appears that the reaction is of second order in aprotic solvent,

and the kinetics depends on the nature of the solvent. It was also pointed out that at higher reaction temperature, i.e., above 100 °C, some side reactions can occur.

One can also cite the references of Levina et al. [41] and Lambeth and Henderson [42]. They have also noticed that the kinetics of reaction was of second order.

Except the work of Maisonneuve et al. [40], no studies were performed by using carbonated triglycerides or by using free fatty acids.

Aminolysis of carbonated vegetable oils for the production of polyurethane requires the knowledge of kinetic and thermodynamic data for an industrial scale-up. To the best of our knowledge, no such data can be found in the literature. The goal of this study is thus to fill this gap by developing a kinetic model for this reaction system. Aminolysis of carbonated methyl oleate by n-butylamine was chosen as a model system.

Fig. S1 shows the evolution of the viscosity with temperature for the different species, i.e., urethane, ester, epoxidized and carbonated. One can notice that the viscosity of oleic acid (OA) is higher than methyl oleate (MO). The viscosity increases using the epoxidized or carbonated forms. Thus, to avoid any mixing problem due to viscosity, oleic acid was esterified.

The first steps were to optimize the production of methyl oleate, epoxidized methyl oleate, and carbonated methyl oleate (Fig. 1). In the second part, a kinetic model was built by taking into account the amidation reaction, which is a side reaction.

HERE Fig. 1. Synthesis of methyl oleate based urethane.

2. Experimental section

2.1 Materials

The following chemicals were used: oleic acid (purity ≥ 82 wt%), methanol (purity ≥ 99 wt%), formic acid (purity > 98 wt%) and hydrogen peroxide (purity ≥ 33 wt%) were purchased from VWR Chemicals. Sulfuric acid (purity ≥ 95 wt%) was obtained from AppliChem. Magnesium sulfate (purity ≥ 99.5 wt%) was obtained from Sigma Aldrich. Tetrabutylammonium bromide (TBABr) and n-butyl amine (purity ≥ 99.5 wt%) were supplied by Alfa Aesar.

2.2 Analytical methods

A gas chromatography (Bruker SCION 436-GC) equipped with a split injector and an elastic quartz capillary column (ZB-5, Phenomenex, 30 m \times 0.32 mm i.d., 0.25 μ m film thickness) was applied to determine the conversion of oleic acid to methyl oleate in the esterification step (Fig. S2).

The yield of epoxide group during the epoxidation reaction was determined by the method of Jay [43], where oil samples were dissolved in a solution of 10 mL of tetra-n-ethylammonium bromide (20 wt% in acetic acid) and 10 mL of chloroform, then titrated with a TIM-840 automatic titrator (Radiometer Analytical, France) using a 0.1 N perchloric acid solution in acetic acid.

Otherwise, the conversion of unsaturated group was determined through titration of the iodine value using the method of Hanus [44]. Unsaturated group reacts with iodine monobromide forming halogenated single bonds. Then, a potassium iodine solution was added causing the reaction of the remaining unreacted iodine in sample, which forms molecular iodine. Molecular iodine present in sample can be titrated using a standard solution of sodium thiosulfate (0.1 N) and ferroin indicator [45].

¹H-NMR spectra were recorded on a Bruker 300 Fourier transform spectrometer at 300 MHz in CDCl₃ solutions using tetramethylsilane (TMS) as internal standard.

IR spectra were recorded on a FTIR (Perkin-Elmer Spectrum 2000 FTIR), equipped with a diamond ATR device (Attenuated Total Reflection). Spectra were obtained from 10 scans in the (4000 to 500) cm⁻¹ range. The enthalpies of reaction were measured using a Tian–Calvet heat flow calorimeter C80 (Setaram, France).

Viscosity measurement was performed with the aid of a Höppler viscometer (Fungilab S/A, Barcelona, Spain).

It was found that there is a linear relationship between the concentrations of ester and carbonated groups and their corresponding intensity signals from FTIR-analyses (eqs (1-2)).

$$[Carbonated] = A_{Carb} \cdot Abs_{1802cm^{-1}} + B_{Carb} \quad (1)$$

$$[Ester] = A_{Ester} \cdot Abs_{1738cm^{-1}} + B_{Ester} \quad (2)$$

where, *[Carbonated]* and *[Ester]* stand for the concentration of carbonated group and ester group. A_i and B_i are characteristic constants of the FTIR equipment; *Abs* is the intensity of the signal at the corresponding wavelength. Figs. S3 and S4 show the linear correlation between the concentrations of ester and carbonated groups.

2.3 Production of intermediates

2.3.1 Oleic acid esterification

The reaction was carried out in a 500 mL reactor equipped with a mechanical stirrer and reflux condenser. Oleic acid (OA), methanol and sulfuric acid were mixed at a constant temperature of 64 °C with the following molar percentage: 19.2 %, 79.8 % and 1.0 %, respectively [46]. The reaction took 3 h. Next, the mixture was washed five times with preheated distilled water. Then, the organic phase left in the reactor was evaporated using an IKA RV10 control vacuum rotary evaporator (VWR, Darmstadt, Germany) at 70 °C and dried over anhydrous magnesium sulfate. The final products were analyzed by FITR, GC (Fig. S2) and ¹H-NMR analysis.

2.3.2 Epoxidation of methyl oleate

The preparation of epoxidized methyl oleate (EMO) from methyl oleate (MO) was carried out in a 500 mL glass-jacketed reactor equipped with a mechanical stirrer and reflux condenser. The epoxidation was conducted in semi-batch mode, methyl oleate and formic acid were mixed at 40 °C, then hydrogen peroxide was added with a volumetric flow rate of 7.3 mL.min⁻¹ for 1 h. The methyl oleate:formic acid:hydrogen peroxide molar ratio was 1:2:13. The reaction was performed for 4 h. The organic layer (containing the epoxide groups) was separated and washed with water to remove residual H₂O₂ and acids, followed by evaporation and dried over anhydrous magnesium sulfate [46]. Fig. 2 illustrates a simplified scheme of the reactor setup.

HERE Fig. 2. Simplified reactor scheme for the epoxidation.

2.3.3 Carbonation of epoxidized methyl oleate

The carbonated methyl oleate (CMO) was prepared in a 300 mL autoclave equipped with a mechanical stirrer under pressure of carbon dioxide, TBABr was used as catalyst. Fig. 3 shows a simplified scheme of the reactor setup. Based on recent investigations [23, 25, 27, 47-49], the optimum process conditions for carbonation reaction were 130 °C, 30 bar of CO₂ pressure with a catalyst loading of 7 mol%. After eight hours of reaction, the conversion of epoxide group was 99 %. The resulting CMO was diluted in ethyl acetate, and washed four times with distilled water in order to remove TBABr catalyst, the product was dried with a rotary evaporator at 70 °C, and then anhydrous magnesium sulfate was used to dry traces of water before the aminolysis [50].

HERE Fig. 3. Simplified reactor scheme for the carbonation.

2.4 Aminolysis reaction

Aminolysis was carried out under semi-batch mode in a 300 mL reactor equipped with a mechanical stirrer and a reflux condenser by reacting carbonated methyl oleate (CMO) and *n*-butyl amine (nBA) to produce urethanized methyl oleate (UMO). The latter reactant was added dropwise to avoid rapid temperature increase. The reactor setup is similar to the one shown in Fig. 2. The influences of temperature and feed flow rate were studied. The concentrations of urethane and ester groups were estimated by FTIR analysis. Indeed, there is a side reaction, which is the amidation of the ester groups [8, 51-52]. The products were also characterized by titration and ¹H-NMR analysis.

The experimental matrix used for the parameter estimation is displayed in Table 1. The term Q_{feed} stands for the volumetric flow rate of *n*-butylamine.

HERE Table 1. Experimental matrix.

2.5 Calorimetry

Reaction enthalpies were measured in a Tian-Calvet calorimeter (C80 Setaram) under isothermal mode. It is a twin calorimeter with a measured and reference cells in reversal mode. Fig. 4 shows a schematic view of the setup inside the calorimeter. Approximately 1 gram of sample was inserted in both the reference and measuring cells. Once the temperature and the flow heat rate in the cells were stable, the reaction was started. The heat flow released during the reaction course is due to the chemical reaction. More information about this system can be found in the references of our group [53-55].

To determine the reaction enthalpies of aminolysis and amidation, two experiments were performed.

In the first experiment, the measurement cell was filled with CMO in one compartment and with n-butylamine in the other one, and the reference cell was filled with CMO in one compartment and with ethyl acetate in the other one (Fig. 4a). Ethyl acetate was chosen because it does not react with CMO and has similar specific heat capacity, as is the case with n-butylamine. Since there are no reactions in the reference cell, the total energy released by the system was the one for aminolysis and amidation reactions.

In the second experiment, the measurement cell was filled with CMO in one compartment and with n-butylamine in the other one, and the reference cell was filled with methyl oleate (MO) in one compartment and with n-butylamine in the other one (Fig. 4b). In the reference cell, amidation reaction also occurred, thus, the total energy released by the system was the one for aminolysis reaction.

HERE Fig. 4. Reversal mixing cells of C80 calorimeter.

3. Results and discussion

3.1 Product characterization

3.1.1 Oleic acid esterification

Since the esterification is a reversible reaction [56], a large molar excess of methanol was used to favor the ester formation. The maximum yield obtained was 93 % confirmed by GC analysis. Fig. 5 shows the FTIR spectra of oleic acid (OA) and methyl oleate (MO). The absorption band of ester group is at 1738 cm^{-1} , which confirms the production of methyl oleate during the reaction. Otherwise, the band at 1710 cm^{-1} corresponds to carbonyl of residual acid groups. $^1\text{H-NMR}$ spectra (Fig. 6) also confirm the quantitative conversion of oleic acid to methyl oleate from the emergence of the corresponding signal of methyl ester group at 3.66 ppm as well as from the displacement of the signal of methylene group in alpha position to acid group from 2.34 ppm to 2.29 ppm.

HERE Fig. 5. FTIR-spectra for OA, MO, EMO, CMO and UMO.

3.1.2 Epoxidation of methyl oleate

The concentration of epoxide groups was followed by titration using a 0.1 mol.L⁻¹ perchloride acid solution. The maximum concentration was reached after 4 h, with an epoxy yield of 91 % and a conversion of 98 % for double bonds. To minimize the side reaction of ring-opening, the most appropriate time was 4 h. The FTIR spectra of epoxidized methyl oleate (Fig. 5) shows the appearance of bands between 815 - 950 cm⁻¹, which are related to stretching vibration of epoxide groups. Compared to methyl oleate, the disappearance of the band in the range of 3000 – 3050 cm⁻¹ showed that the unsaturated groups were consumed [57]. Furthermore, ¹H-NMR revealed that the signal at 5.34 ppm arising from carbon-carbon double bonds has disappeared (Fig. 6). Epoxide formation was confirmed by the appearance of a signal at 2.90 ppm [46].

HERE Fig. 6. ¹H-NMR for OA, MO, EMO, CMO and UMO.

3.1.3 Carbonation of Epoxidized methyl oleate

As illustrated in Fig. 7, CMO was prepared by converting the epoxide group of EMO with carbon dioxide in the presence of TBABr as catalyst. The oxirane ring of methyl oleate was attacked by the bromide of the catalyst leading to ring opening, followed by the nucleophilic attack of the alkoxide. Then, the five-membered carbonate was produced by the ring closure reaction of the resulting carboxylate [50, 58-60].

HERE Fig. 7. Conversion of epoxidized methyl oleate to carbonated methyl oleate.

The optimum conditions (load of catalyst, pressure, temperature) for the carbonation reaction have been studied before, concluding that a catalyst loading higher than 7 mol% barely increases the conversion rate [46]. During the investigation made by Ait Aissa et al. [26], a thermal stability analysis of the catalyst was carried out, and it was found that temperature higher than 130 °C can cause a decomposition of TBABr, and subsequently the diminution of selectivity due to the formation of undesired secondary products. In this sense, the conditions for the carbonation of epoxidized methyl oleate were carefully optimized, with a temperature of 130 °C and a fixed pressure of 30 bar. A reaction time of 8 hours was selected, resulting in a 99 % conversion of epoxide groups.

The FTIR spectrum of CMO (Fig. 5) shows a strong band at 1800 cm^{-1} corresponding to the carbonate group. This band has a similar height with the one of ester group at 1738 cm^{-1} , which denotes similar concentration according to the literature [48], and that the yield of carbonated group is high. The absence of absorption bands of epoxide group between 815-950 cm^{-1} confirms the fact that the conversion of epoxide group to carbonated groups is high. $^1\text{H-NMR}$ spectra showed signals between 4.40-4.95 ppm assigned to carbonated groups [43].

3.1.4 Aminolysis reaction of carbonated methyl oleate

Fig. 1 shows the reaction of carbonated methyl oleate with n-butylamine. In this reaction system, two reactions occur: aminolysis, and amidation as a side reaction. The products were analyzed by FTIR and $^1\text{H-NMR}$ analysis. Fig. 5 shows the decrement of signal at 1802 cm^{-1} corresponding to some unreacted carbonated groups. It was also noticeable new absorption bands at 1720 cm^{-1} and 1647 cm^{-1} , which are typical for urethane and amide groups [19]. The conversion of carbonated groups was also confirmed through $^1\text{H-NMR}$ (Fig. 6) through the disappearance of the cyclic-carbonate signals at 4.22 ppm and 4.61 ppm. In the range of 4.8 -5.2 ppm, the broad signal is assigned to protons of NH and those in alpha position to the oxygen of the urethane function. Protons in alpha to the nitrogen of this function arised at 3.16 ppm. The signal at 3.55 ppm is ascribed to protons in alpha position to hydroxyl groups. These correlations are in quite consistency with those of Tryznowski et al. [61] and Meng et al. [62].

3.2 Calorimetry results

The evolution of the heat-flow rate as function of time is depicted in Fig. 8a. It stands for the overall energy released due to urethane formation and to amide formation at 60 °C. Fig. 8b shows the heat released only during the formation of urethanes at 60 °C.

HERE Fig. 8.a Heat profiles for CMO and n-butylamine system at 60 °C. b. Heat profile for the production of urethanes at 60 °C.

By integrating the curves in Fig. 8a, the overall enthalpy of the reactional system (amidation + aminolysis) was found to be -23.90 kJ per mole of carbonated group. Then, the corresponding integration of heat-flow rate shown in Fig. 8b provides the enthalpy due to the formation of urethanes, which was found to be -18.92 kJ.mol⁻¹. Thus, the enthalpy of amidation is -5.02 kJ.mol⁻¹. These reaction enthalpies indicate that these reactions are not very exothermic.

3.3 Kinetic model

In order to monitor the evolution of the reaction system in a quantitative way, samples were analyzed by FTIR spectroscopy during the reaction (Eqs (1-2)). These experimental data were used to estimate the kinetic constants of the production of urethane and amide groups.

Kinetics

Aminolysis reaction was considered as an elementary reaction. Amidation is a reversible reaction. Thus, their kinetic rate equations were expressed as

$$R_{Aminol} = k_{Aminol} \times [Carbonated][nBA] \quad (3)$$

$$R_{Amid} = k_{Amid} \times \left([Ester][nBA] - \frac{[Amide][MeOH]}{K_c} \right) \quad (4)$$

where, R_{Aminol} and R_{Amid} represent the reaction rate of aminolysis and amidation reaction, k_{Aminol} and k_{Amid} stand for the kinetic constants of aminolysis and amidation reaction and $[Carbonated]$, $[Ester]$, $[nBA]$, and $[Amide]$ are the concentrations of carbonated group, ester group, n-butyl amine, and amide group, respectively. K_c is the equilibrium constant for the amidation reaction.

The evolution of K_c can be expressed by a van't Hoff's law:

$$K_c(T_R) = K_c(T_{Ref}) \times \exp\left(\frac{-\Delta H_{R,Amid}}{R} \times \left(\frac{1}{T_R} - \frac{1}{T_{Ref}}\right)\right) \quad (5)$$

where, T_R and T_{Ref} represent the reaction temperature and reference temperature and R is the universal gas constant and $\Delta H_{R,Amid}$ is the enthalpy of the amidation reaction, which was found to be $-5.02 \text{ kJ}\cdot\text{mol}^{-1}$ from the calorimetry experiment. The equilibrium constants K_c was estimated at a reference temperature of $70 \text{ }^\circ\text{C}$.

Mass Balance

A simplified scheme of the aminolysis is shown in Fig. 9.

HERE Fig. 9. Aminolysis of carbonated methyl oleate.

The volumetric flow rate was constant during the addition time, thus, one gets

$$\frac{dV_r}{dt} = Q_{feed} \text{ for } t < t_{add} \text{ and } \frac{dV_r}{dt} = 0 \text{ L} \cdot \text{s}^{-1} \text{ for } t > t_{add} \quad (6)$$

where, Q_{feed} is the volumetric flow rate, t_{add} is the addition time and V_r is the volume of the reaction.

Ordinary differential equation 6 was used to simulate the evolution of the reactor volume.

Mass balance for all compounds in the reaction system can be expressed as:

$$\frac{d[Carbonated]}{dt} = -R_{Aminol} - [Carbonated] \times \frac{Q_{feed}}{V_r} \quad (7)$$

$$\frac{d[nBA]}{dt} = -(R_{Aminol} + R_{Amid}) + ([nBA]_{feed} - [nBA]) \times \frac{Q_{feed}}{V_r} \quad (8)$$

$$\frac{d[UMO]}{dt} = R_{Aminol} - [UMO] \times \frac{Q_{feed}}{V_r} \quad (9)$$

$$\frac{d[Ester]}{dt} = -R_{Amid} - [Ester] \times \frac{Q_{feed}}{V_r} \quad (10)$$

$$\frac{d[Amide]}{dt} = R_{Amid} - [Amide] \times \frac{Q_{feed}}{V_r} \quad (11)$$

$$\frac{d[MeOH]}{dt} = R_{Amid} - [MeOH] \times \frac{Q_{feed}}{V_r} \quad (12)$$

where, $[UMO]$ and $[MeOH]$ are the concentration of urethanized methyl oleate and methanol, respectively.

Parameter estimation

For the estimation of the kinetic constants, the software MODEST was used [63]. The ordinary differential equations ODEs (6-12) were solved out by the ODESSA algorithm based on backward difference methods.

Concentrations of ester and carbonated groups were used as observables. The objective function θ was minimized by the Simplex and Levenberg-Marquardt algorithms.

$$\theta = \sum(C_i - \hat{C}_i) \quad (14)$$

where, C_i is the experimental concentration and \hat{C}_i is the concentration simulated by the model.

To define the reliability of the model to the experimental data, the following coefficient of explanation was defined as

$$R^2 = 1 - \frac{\sum(C_i - \bar{C}_i)^2}{\sum(C_i - \hat{C}_i)^2} \quad (15)$$

where, \bar{C}_i is the average value of the experimental concentration. The coefficient of explanation was higher than 90 %, which means that the model is correct.

To minimize the dependency between the activation energy and the pre-exponential factor, rate constants were expressed by using a modified Arrhenius equation.

$$k_i(T_R) = k_i(T_{Ref}) \times \exp\left(\frac{-E_{a_i}}{R} \left(\frac{1}{T_R} - \frac{1}{T_{Ref}}\right)\right) \quad (16)$$

where, k_i is reaction rate constant, E_a is the activation energy, T_R represents the reaction temperature and reference temperature, R is the universal gas constant and T_{Ref} was fixed to 66.85 °C in our study.

Table 2 presents the values of the estimated parameters with associated standard deviations. The standard errors were estimated within 95 % of the confidence interval. One can notice that the standard deviations are low for the kinetic constants. For the equilibrium constant K_C for the amidation reaction at 70 °C, the standard deviation is of 78 % due to the complexity to estimate such thermodynamic parameters. Nevertheless, this deviation is still acceptable.

HERE Table 2. Kinetic constants estimated at 66.85 °C and statistical data.

The results of the kinetic modeling are presented in Figs. 10a-10f. One can notice that the model fits correctly the experimental concentration of carbonated and ester groups. For the sake of information, the simulated concentrations of amide and urethane were also plotted. Figs. 11a-11b shows the contour plot for the estimated kinetic and activation energy constants for both reactions. It is clear that the minimum of the objective function was reached.

HERE Fig. 10a. Fit of the model for the aminolysis of CMO at 40 °C and 4 mL.min⁻¹.

HERE Fig. 10b. Fit of the model for the aminolysis of CMO at 60 °C and 1 mL.min⁻¹.

HERE Fig. 10c. Fit of the model for the aminolysis of CMO at 70 °C and 1 mL.min⁻¹.

HERE Fig. 10d. Fit of the model for the aminolysis of CMO at 50 °C and 2 mL.min⁻¹.

HERE Fig. 10e. Fit of the model for the aminolysis of CMO at 50 °C and 4 mL.min⁻¹.

HERE Fig. 10f. Fit of the model for the aminolysis of CMO at 50 °C and 3 mL.min⁻¹.

HERE Fig. 11a. Contour plot of kinetic parameters for the aminolysis.

HERE Fig. 11b. Contour plot of kinetic parameters for the side reaction of amidation.

4. Conclusion

The use of cyclic-carbonate such as carbonated vegetable oils and amine represents a greener and safer way for the production of non-isocyanate polyurethane. Several articles have discussed about this way of production but few of them have proposed a kinetic model. The goal of this article was to build a kinetic model for a model reaction: aminolysis of carbonated methyl oleate with n-butylamine.

In the first part of this study, the esterification and epoxidation steps were optimized to have the maximum yield in ester and epoxide groups. In the second part, several experiments of aminolysis were performed under isothermal mode in a semi-batch reactor. A Tian-Calvet calorimeter was used to determine the enthalpies of amidation and aminolysis reactions. It was found that these reactions are not very exothermic, i.e., $\Delta H_{R,Amid} = -5.02 \text{ kJ. mol}^{-1}$ and $\Delta H_{R,Aminol} = -18.92 \text{ kJ. mol}^{-1}$.

A kinetic model was built by taking into account the aminolysis reaction and the side reaction of amidation. A non-linear regression method was used to estimate the kinetic constants for these two reactions by using the experimental concentrations of ester and carbonated groups as observable. The model fits quite well with the experimental concentrations.

In order to shift to industrial application, aminolysis of carbonated vegetable oils with diamines should be the continuation of this study.

Notation

<i>Amide</i>	amide groups
<i>Carbonated</i>	carbonated groups
<i>Carb</i>	carbonation reaction
<i>Ester</i>	ester group
E_a	activation energy [kJ.mol ⁻¹]
FTIR	fourier transform infrared spectroscopy
¹ H-NMR	proton nuclear magnetic resonance
ΔH_R	reaction enthalpy [kJ.mol ⁻¹]
k_i	reaction rate constant or kinetic constant [L.mol ⁻¹ .s ⁻¹]
K_c	equilibrium constant
<i>MeOH</i>	methanol
Q_{feed}	volumetric flow rate [L.s ⁻¹]
R_i	reaction rate [mol.L ⁻¹ .s ⁻¹]
R	universal gas constant
r	reaction rate for a reactant or product [mol.L ⁻¹ .s ⁻¹]
T	temperature [K]
t_{add}	addition time [s]
V_r	volume of reaction [L]
C_i	experimental concentration [mol.L ⁻¹]
\hat{C}_i	simulated concentration [mol.L ⁻¹]

Subscripts and superscripts

0	initial
<i>add</i>	addition
<i>Amid</i>	amidation
<i>Aminol</i>	aminolysis
<i>feed</i>	feed
<i>i</i>	component i
<i>r</i>	reactor

Abbreviations

<i>CMO</i>	carbonated methyl oleate
<i>EMO</i>	epoxidized methyl oleate
<i>MO</i>	methyl oleate
<i>UMO</i>	urethanized methyl oleate
<i>nBA</i>	n-butylamine
<i>OA</i>	oleic acid
<i>TBABr</i>	tetra-n-butylammonium bromide
<i>MeOH</i>	methanol

Tables

Table 1. Experimental matrix.

Table 2. Kinetic constants estimated at 66.85 °C and statistical data.

Figures

Fig. 1. Synthesis of methyl oleate based urethane.

Fig. 2. Simplified reactor scheme for the epoxidation.

Fig. 3. Simplified reactor scheme for the carbonation.

Fig. 4. Reversal mixing cells of C80 calorimeter.

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Fig. 6. ¹H-NMR for OA, MO, EMO, CMO and UMO.

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Fig. 11a. Contour plot of kinetic parameters for the aminolysis.

Fig. 11b. Contour plot of kinetic parameters for the side reaction of amidation.

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