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1 WIDE BAND GAP KESTERITE ABSORBERS FOR THIN FILM SOLAR CELLS:  
2 POTENTIAL AND CHALLENGES FOR THEIR DEPLOYMENT IN TANDEM DEVICES

3  
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## 1 BROADER CONTEXT

2 The power conversion efficiency of the dominant single junction photovoltaic technology is  
3 approaching its theoretical limit. Further progress, with higher efficiencies and lower cost,  
4 requires improving current technologies in new ways, whilst using cheap, abundant materials.  
5 An approach to increase the efficiency is the construction of double junction solar cells  
6 combining a top and bottom cell in a tandem device. If an established technology – such as  
7 crystalline silicon – is used for the bottom cell, a relatively wide band gap material is needed  
8 for the top cell. An ideal top cell would be low-cost and be made of abundant, non-toxic  
9 materials. Typical top cell candidates that have been presented have some significant  
10 drawbacks: Perovskite top cells, for example, contain toxic elements and have well-known  
11 stability issues. III-V top cells are well studied for concentrators, but are too costly for tandem  
12 applications. In this contribution, we report on our detailed fundamental analysis of a new  
13 candidate absorber material, namely high band gap kesterite films. The Sn in the standard  
14  $\text{Cu}_2\text{ZnSn}(\text{S,Se})_4$  kesterite structure is replaced by Ge (or Si), increasing the band gap to a level  
15 where it is of interest in tandem configurations. This study describes the potential and the  
16 challenges that are involved with the use of wide band gap kesterite absorbers in future  
17 tandem devices.

18

## 19 ABSTRACT

20 This work reports on developments in the field of wide band gap  $\text{Cu}_2\text{ZnXY}_4$  (with X = Sn, Si  
21 or Ge, and Y = S, Se) kesterite thin film solar cells. An overview on recent developments and  
22 the current understanding of wide band gap kesterite absorber layers, alternative buffer layers,  
23 and suitable transparent back contacts is presented.  $\text{Cu}_2\text{ZnGe}(\text{S,Se})_4$  absorbers with absorber  
24 band gaps up to 1.7 eV have been successfully developed and integrated into solar cells.  
25 Combining a CdS buffer layer prepared by an optimized chemical bath deposition process  
26 with a 1.36 eV band gap absorber resulted in a record  $\text{Cu}_2\text{ZnGeSe}_4$  cell efficiency of 7.6 %,  
27 while the highest open-circuit voltage of 730 mV could be obtained for a 1.54 eV band gap  
28 absorber and a Zn(O,S) buffer layer. Employing  $\text{InZnO}_x$  or  $\text{TiO}_2$  protective top layers on  
29  $\text{SnO}_2:\text{In}$  transparent back contacts yields 85-90 % of the solar cell performance of reference  
30 cells (with Mo back contact). These advances show the potential as well as the challenges of  
31 wide band gap kesterites for future applications in high-efficiency and low-cost tandem  
32 photovoltaic devices.

33

## 34 KEYWORDS

35 Thin-film solar cells, wide band gap, kesterite, germanium, semi-transparent

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## I. INTRODUCTION

World-record single-junction solar cell efficiencies of monocrystalline silicon-wafer (Si) and thin-film (TF) solar cells are 26.7 % and 22.9 % [1,2], respectively, thus approaching their theoretical (Shockley-Queisser) limit of 30 % under standard illumination conditions [3]. One approach to increase the efficiency of solar cells above this limit is the construction of tandem devices. A tandem device consists of two solar cells: a wide band gap ( $E_G$ ) solar cell (in which the photovoltaically active absorber material has an optical band gap of 1.5-2.0 eV) harvests the high-energy photons and a small band gap solar cell (in which the absorber has a band gap of 1.0-1.5 eV) harvests the low-energy photons. This approach can lead to theoretical efficiencies of up to 44 % under 1-sun illumination [4].

With a band gap of 1.1 eV [4], Si-wafer-based devices are the ideal bottom cell candidate, but many prominent top cell candidates have issues related to abundance, toxicity, stability, or cost [5]. Therefore, we consider kesterite-based devices as potential top cells for tandem device applications, because  $\text{Cu}_2\text{ZnSn}(\text{S,Se})_4$ -type kesterite solar cells are stable, made out of abundant and non-toxic components, and already achieve relatively high performance [1]. Depending on the  $[\text{S}]/([\text{S}]+[\text{Se}])$  composition, the band gap of the kesterite absorber can be tuned between 1.0 and 1.5 eV [6]. Highest efficiencies for  $\text{Cu}_2\text{ZnSn}(\text{S,Se})_4$ -based devices are achieved when absorbers with band gaps between 1.1 and 1.2 eV are employed [7], which is too low for efficient (top) tandem solar cell applications. However, (partially) replacing tin atoms with silicon or germanium atoms has the potential to result in kesterite absorbers with band gaps even above 1.5 eV [8,9]. This work aims to give an overview on the recent development and current understanding of (i) these wide band gap kesterite absorber layers, (ii) alternative (non-toxic) buffer layer candidate materials, and (iii) suitable transparent back contacts (TBCs) allowing tandem configuration. A summary of recently published results is complemented with new experimental findings and a theoretical study of the efficiency potential of devices based on wide band gap kesterite absorbers. Thus, the paper aims at covering all aspects of deploying kesterite wide-band gap absorbers as top cells in tandem solar cell applications in order to identify inherent bottlenecks that may limit device performance and present generally valid optimization approaches and first results to lay the foundation and pave the way for future more detailed studies that undeniably have to follow.

## 2. EXPERIMENTAL, RESULTS, AND DISCUSSION

### 2.1. ABSORBER LAYER

First, we give an overview of the absorber layer formation, in which two main approaches are applied, i.e. sequential evaporation (Section 2.1.1) and solution-based deposition (Section

1 2.1.2). The first approach (respective samples are henceforth called → EVAP-sample) is more  
2 convenient to study different metal components and is, therefore, used to investigate the  
3 replacement of Sn atoms with Si or Ge in EVAP-Cu<sub>2</sub>ZnSn(S,Se)<sub>4</sub> absorber layers; while in the  
4 second approach (→ SOL-sample), the focus is on the replacement of Sn with Ge and the  
5 optimization of the involved wet chemistry. Note that there will inherently be variations in  
6 properties of the kesterite absorbers deposited by the different methods (i.e., using sequential  
7 evaporation or solution-based deposition), however the findings that are presented in the  
8 manuscript – while not exactly transferrable – mainly relate to universally relevant conditions  
9 that will arise in cell production regardless of the absorber deposition method.

#### 10 2.1.1. EVAPORATION-BASED PROCESS

11 The polycrystalline absorber layers are fabricated using a two-step vacuum-based approach;  
12 see Figure S1. Soda lime glass (SLG) substrates of 1.3 mm thickness are used, on which a 150-  
13 nm-thick Si(O,N) diffusion barrier is first deposited, followed by a 400-nm-thick Mo layer.  
14 The thin Si(O,N) diffusion barrier is deposited in order to avoid the diffusion of elements  
15 from the glass substrate into the absorber. Early tests have shown that the evaporated  
16 absorber quality is better if this diffusion barrier is added. On top of this substrate, a multilayer  
17 of different metals is deposited using a Pfeiffer PLS 500 evaporation system. For accurate layer  
18 thickness control, a quartz microcrystal balance is used. This metal multilayer is then annealed  
19 in an Annealsys As-One 150 rapid thermal annealing system that is equipped with a 10 % H<sub>2</sub>Se  
20 (diluted in N<sub>2</sub>) gas line and a 100 % H<sub>2</sub>S gas line. This way, the layers are selenized or sulfurized  
21 under a continuous flow of H<sub>2</sub>Se or H<sub>2</sub>S. During this selenization/sulfurization step, a  
22 polycrystalline layer is formed with typical grain sizes in the order of 0.5 to 1 μm.

#### 23 2.1.1.1. Si-BASED COMPOUNDS

24 We have used metal layer stacks, including Si, to explore the possibility of fabricating EVAP-  
25 Cu<sub>2</sub>ZnSiSe<sub>4</sub>, -Cu<sub>2</sub>Zn(Si,Sn)Se<sub>4</sub>, -Cu<sub>2</sub>SiSe<sub>3</sub>, -Cu<sub>2</sub>SiS<sub>3</sub>, -Cu<sub>8</sub>SiSe<sub>6</sub>, and -Cu<sub>8</sub>SiS<sub>6</sub> layers [10].  
26 Unfortunately, the Si appears to be largely unreactive at processing temperatures below  
27 600 °C, which is the maximum temperature allowed for SLG substrates. Only EVAP-Cu<sub>8</sub>SiSe<sub>6</sub>  
28 and EVAP-Cu<sub>8</sub>SiS<sub>6</sub> could be produced in a reliable way, without significant presence of  
29 secondary phases, leading to polycrystalline absorber layers with high-intensity  
30 photoluminescence (PL) peaks at energies of 1.35 (for EVAP-Cu<sub>8</sub>SiSe<sub>6</sub>) and 1.84 eV (EVAP-  
31 Cu<sub>8</sub>SiS<sub>6</sub>) [11]. However, no functioning solar cells could be fabricated with these absorber  
32 layers, as the doping seemed to be too high (in the order of 10<sup>18</sup> cm<sup>-3</sup> or higher), and the  
33 minority carrier lifetime seemed to be lower than 0.2 ns, leading to functioning diodes but no  
34 photocurrent. One observation that could also explain the absence of any photoactivity is the  
35 formation of SiO<sub>2</sub> during absorber processing. Figure 1 shows hard x-ray photoelectron  
36 spectroscopy (HAXPES) survey spectra of an EVAP-Cu<sub>8</sub>SiS<sub>6</sub> sample before (black) and after  
37 (red) sulfurization treatment. Upon sulfurization, the O and Na (most likely diffused from the

1 SLG substrate) contents increase. The inset shows the region of the Si 2s and S 2p core level  
2 lines compared to reference positions of silicon compounds [12]. The Si 2s line of the  
3 sulfurized layer stack shifts to higher binding energies compared to the Si 2s peak before  
4 sulfurization. The comparison with the reference positions indicates the conversion of Si-Si  
5 into Si-S<sub>2</sub> and/or Si-O<sub>2</sub> bonds. The fact that the S 2p line can only be clearly observed on a  
6 magnified (x 25) scale together with the high O 1s intensity for the sample after sulfurization,  
7 however, suggests that the surface region of the sulfurized sample has mainly a SiO<sub>2</sub> character,  
8 which would prevent efficient charge carrier transport.

### 9 2.1.1.2. Ge-BASED COMPOUNDS

10 For the fabrication of polycrystalline EVAP-Cu<sub>2</sub>ZnGeSe<sub>4</sub> layers, we have used 180 nm of Ge,  
11 125 nm of Zn and 170 nm of Cu as starting layers [13]. These layer thicknesses were chosen  
12 in order to end up with a Zn-rich and Cu-poor composition of the absorber layer, with  
13 Cu/(Zn+Ge) = 0.9 and Zn/Ge = 1.05. This metal stack was then selenized for 15 minutes in a  
14 continuous flow of H<sub>2</sub>Se at a temperature of 460 °C. The resulting absorber layer is  
15 polycrystalline with a typical grain size in the order of 500 nm. Figure S2 shows a cross-section  
16 scanning electron microscopy (SEM) image of a finished solar cell stack, exemplifying the grain  
17 morphology of the absorber as well as the other layers of the solar cell stack. A Bragg  
18 Brentano X-ray diffraction (XRD) measurement of a finished absorber layer on a Mo back  
19 contact clearly shows the Cu<sub>2</sub>ZnGeSe<sub>4</sub> peaks with a small contribution of a ZnSe secondary  
20 phase, as a small shoulder of the main Cu<sub>2</sub>ZnGeSe<sub>4</sub> peaks at angles around 27.3 and 45.3  
21 degrees, shown in Figure 2. Due to the Zn-rich nature of the absorber layer, the presence of  
22 ZnSe secondary phase has to be expected. Cu<sub>2-x</sub>Se and GeSe<sub>2</sub> secondary phases cannot be  
23 identified within the accuracy of the XRD measurements. Also note that the peaks of the  
24 ternary phase Cu<sub>2</sub>GeSe<sub>3</sub> overlap with the main peaks of the Cu<sub>2</sub>ZnGeSe<sub>4</sub> phase completely,  
25 making it impossible to distinguish these phases by XRD. To visualize the secondary phases,  
26 cross-section energy dispersive X-ray spectroscopy (EDX) elemental maps of the absorber  
27 were acquired in scanning transmission electron microscopy (STEM) mode, shown in Figure  
28 3. The observed regions of elemental inhomogeneities are attributed to ZnSe – which seems  
29 to be present in large amounts at the top surface of the absorber – and Cu<sub>2</sub>GeSe<sub>3</sub> / Cu<sub>2-x</sub>Se  
30 phases – which are present more at the grain boundaries and at the backside Mo interface.  
31 Some of the absorbers were lift-off in order to record Raman spectra near the EVAP-  
32 Cu<sub>2</sub>ZnGeSe<sub>4</sub>/Mo interface. Both sides (front absorber and at the back side, i.e. near the back  
33 contact) were analyzed. At the front Cu<sub>2</sub>ZnGeSe<sub>4</sub> side (as published in [29]), only Cu<sub>2</sub>ZnGeSe<sub>4</sub>  
34 is clearly detected, but presence of Cu<sub>2</sub>GeSe<sub>3</sub> and Cu<sub>2-x</sub>Se cannot be excluded as their Raman  
35 peaks overlap with Cu<sub>2</sub>ZnGeSe<sub>4</sub>. At the back side only 2H-MoSe<sub>2</sub> related peaks are observed.  
36 Time and energy resolved photoluminescence measurements (not shown) reveal a PL peak  
37 at an energy of about 1.36 eV, with a decay time in the order of 2 ns. The band gap of this

1 absorber is thus too small to be employed as a top cell of tandem devices. However, due to  
2 the high throughput of the evaporation process route/equipment, a large number of respective  
3 EVAP-Cu<sub>2</sub>ZnGeSe<sub>4</sub> samples are available and were thus (for practical reasons and to allow for  
4 good statistics) chosen for most of our optimization efforts with respect to the absorber  
5 surface treatment (see Section 2.2.1), the buffer layer (see Section 2.2.2), and the TBC (see  
6 Section 2.4).

### 7 2.1.2. Ge-BASED COMPOUNDS BY SOLUTION-BASED PROCESS

8 The SOL-Cu<sub>2</sub>ZnGe(S,Se)<sub>4</sub> absorbers were deposited in a two-step process as schematically  
9 drawn in Figure S3. A metal salt solution was deposited onto a Mo-coated SLG substrate by  
10 doctor-blade coating with subsequent drying on a hot plate. Different solvents, metal salts  
11 and chalcogen sources have been evaluated in a previous manuscript [14]. Here, the chemical  
12 composition of the absorbers is Cu/(Zn+Ge)=0.7 and Zn/Ge=1.0 which is slightly more Cu-  
13 poor than the EVAP-Cu<sub>2</sub>ZnGeSe<sub>4</sub> layers. The chemical and electronic structure of respective  
14 SOL-Cu<sub>2</sub>ZnGe(S,Se)<sub>4</sub> absorbers and, in particular, the impact of the absorber formation by  
15 annealing in Se-atmosphere has been monitored by lab-based soft x-ray photoelectron  
16 spectroscopy (XPS) and synchrotron-based HAXPES. The XPS measurements were  
17 performed in the off-synchrotron analysis chamber at EMIL in ultra-high vacuum (base  
18 pressure < 5×10<sup>-10</sup> mbar) employing a non-monochromatized Mg K<sub>α</sub> (1253.56 eV) x-ray tube  
19 (PREVAC RS40BI) as excitation source. The photoelectrons were detected by a Scienta  
20 Omicron Argus CU electron analyzer. HAXPES was measured at beamline BL15XU at SPring-  
21 8 using an excitation energy of 6 keV and a Scienta R4000 electron analyzer (see [15,16] for  
22 more details on the experimental setup; same measurement conditions apply for the data  
23 shown in Figure 1). Figure 4 shows the XPS S 2p/Se 3p (left panel) and HAXPES shallow core  
24 level (right panel) spectra of a SOL-Cu<sub>2</sub>ZnGe(S,Se)<sub>4</sub> sample prepared from a solution of Cu-,  
25 Zn- and Ge-oxides in water and ammonium thioglycolate. Upon selenization, a clear Se 3d  
26 signal in the shallow core level region and the Se 3p core level dominating the S 2p/Se 3p  
27 energy region can be observed. The fit of the spectrum with S 2p and Se 3p doublets (see top  
28 spectrum in Figure 4 – left panel) reveals the presence of at least two Se species, and two S  
29 species – where the secondary (S) peak most likely indicates the presence of S-O<sub>x</sub> and Se-O<sub>x</sub>  
30 (with x ≥ 3). The presence of Se-O<sub>x</sub> is also indicated by the high-binding energy shoulder of  
31 the Se 3d line in the shallow core level region (and depicted in the right panel of Figure 4).  
32 Quantifying the fit results yields a (surface) [S]/([S]+[Se])-ratio of approximately 0.1,  
33 significantly lower than the bulk composition of 0.3 [14]. The chemical environment of S in  
34 the absorber precursor layer (i.e., before selenization) is also rather complex – as indicated  
35 by the broad S 2p spectrum with a low binding energy shoulder (in the bottom spectrum in  
36 Figure 4 – left panel), which significantly deviates from the expected spectral shape of a S 2p  
37 doublet (see blue fit component on the top spectrum). The shallow core level photoemission

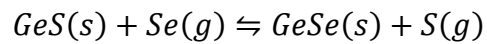


1 lines additionally reveal that the selenization process impacts the Zn/Cu ratio (the Cu 3p line  
2 intensity is significantly increased) and the chemical bonding environment of Ge (see inset of  
3 Figure 4 – right panel). Presumably, oxidized Ge is converted to form Ge-Se bonds upon  
4 selenization. Finally, the location of the valence band maximum at 0.2 ( $\pm 0.1$ ) eV (below the  
5 Fermi level), indicated by the arrow in Figure 4 (right panel), is in agreement with a p-type  
6 doped material, which can generally be observed for these kinds of absorbers.

7 To fabricate solar cells, CdS buffer layers are deposited by chemical-bath deposition (CBD)  
8 followed by a sputtered ZnO and ZnO:Al layer. Although the band alignment of  
9  $\text{Cu}_2\text{ZnGe}(\text{S,Se})_4$  with CdS is believed to be non-ideal, in a direct comparison with potential  
10 alternative buffer layer candidate materials a CdS buffer was found to result in the highest  
11 efficiencies [17]. The morphology of a SOL- $\text{Cu}_2\text{ZnGe}(\text{S,Se})_4$  absorber with CdS buffer can be  
12 seen in the cross-section transmission electron microscopy (TEM) image displayed in Figure  
13 S4(a). It shows two distinct layers within the SOL- $\text{Cu}_2\text{ZnGe}(\text{S,Se})_4$ : larger grains on top and  
14 smaller grains at the bottom. Note that the CdS layer on top of the absorber is only 50 nm  
15 thick and therefore hard to identify in this image. All elements are for the most part  
16 homogeneously distributed within the absorber layer; therefore, only the distribution of Zn  
17 signal is shown in Figure S4(b), where some brighter spots in the large-grain layer can be seen,  
18 which we interpret as indication for the presence of a  $\text{Zn}(\text{S,Se})_2$  secondary phase. Additionally,  
19 the signal of carbon residues that arise from thiourea is displayed in Figure S4(c). Here carbon  
20 is only present in the small-grain layer, whereas the large-grain layer is mostly carbon-free.  
21 With a higher magnification (not shown), an amorphous layer covering the  $\text{Cu}_2\text{ZnGe}(\text{S,Se})_4$   
22 particles can be seen. The distribution of Cd [Figure S4(d)] shows that, in contrast to other  
23 investigations of kesterite absorbers with a CBD-processed CdS buffer [18], no major  
24 diffusion of Cd into the absorber layer can be detected.

25 Our standard solution-based deposition approach results in SOL- $\text{Cu}_2\text{ZnGe}(\text{S,Se})_4$  absorber  
26 material with a band gap of around 1.5 eV [14]. For application in tandem solar cells, a slightly  
27 higher absorber band gap would be advantageous. One possible means to increase the band  
28 gap would be a partial or complete cation substitution, e.g., Si for Ge [9], Ag for Cu [19], or  
29 Ba for Zn [20]. However, a more complicated phase diagram is expected when using  
30 additional elements, and so we focus on increasing the band gap by tuning the anion  
31 composition (i.e., the  $[\text{S}]/([\text{S}]+[\text{Se}])$ -ratio), a well-established method for  $\text{Cu}_2\text{ZnSn}(\text{S,Se})_4$   
32 absorbers. In general, the anion composition can be controlled (i) in the metal salt solution  
33 and/or (ii) during the annealing process. It is used in slight excess to ensure that enough S is  
34 present to form the kesterite phase during the drying step on a hot plate. If one would like  
35 to lower the band gap of the SOL- $\text{Cu}_2\text{ZnGe}(\text{S,Se})_4$  absorber, thiourea could partly or  
36 completely be replaced by selenourea to decrease the  $[\text{S}]/([\text{S}]+[\text{Se}])$ -ratio or fabricate S-free  
37 SOL- $\text{Cu}_2\text{ZnGeSe}_4$  absorbers. However, further increasing the amount of thiourea would only

1 lead to excess chalcogen that cannot be incorporated into the kesterite lattice (and also more  
2 residual carbon and nitrogen) and does, therefore, not lead to an increase of the  
3  $[S]/([S]+[Se])$ -ratio and thus absorber band gap. Therefore, we focus on increasing the  
4  $[S]/([S]+[Se])$ -ratio during the annealing step, following approach (ii). The most obvious  
5 procedure would be to anneal the sample in the simultaneous presence of Se and S. However,  
6 the boiling point of S is 445°C [21], considerably lower than the annealing temperature of  
7 550°C, and thereby does not allow a constant S supply during the annealing. Therefore, GeS  
8 is used as an additional sulfur source [22], which is expected to release S into the gas phase  
9 via the following reaction:



11 To allow for fine-tuning of the absorber band gap, the amount of GeS was varied between 0  
12 and 100 mg. As a result, S is incorporated into the kesterite lattice, as can be seen from the  
13 shift of the 112-reflection in the XRD patterns displayed in Figure 5. Using Vegard's law the  
14  $[S]/([S]+[Se])$ -ratio can be estimated based on this data, revealing that it varies in a range  
15 between 0.27 and 0.50 [22]. However, the peak shape of the 112-reflections slightly changes  
16 with the amount of GeS. Starting from 40 mg (resulting in an absorber with a band gap of 1.67  
17 eV [22]), a shoulder at higher diffraction angles is visible, indicating the coexistence of an  
18 orthorhombic phase that is known to occur for high  $[S]/([S]+[Se])$ -ratios in  $Cu_2ZnGe(S,Se)_4$   
19 absorbers [23].

20 To evaluate the influence on the solar cell performance, the current density-voltage [i.e.,  $J(V)$ ]  
21 characteristics of the best solar cells from SOL- $Cu_2ZnGe(S,Se)_4$  absorbers with external  
22 quantum efficiency (EQE)-derived band gaps of 1.5, 1.6 and 1.7 eV (corresponding to  
23  $[S]/([S]+[Se])$ -ratios of 0.27, 0.39, and 0.50, respectively) are compared in Figure 6; the  
24 corresponding cell parameters are listed in Table 1. As expected, the short-circuit current  
25 density ( $J_{sc}$ ) decreases with increasing absorber band gap. The open circuit voltage ( $V_{oc}$ )  
26 increases considerably from 617 to 683 mV when the absorber band gap is increased from  
27 1.5 to 1.6 eV, but decreases for the 1.7 eV absorber. The fill factor (FF) shows a slight decrease  
28 with absorber band gap, and efficiency reducing from 6.0 to 2.7 %. The loss in  $V_{oc}$  for devices  
29 based on absorbers with a band gap larger than 1.6 eV represents the most crucial loss in this  
30 sample series, which might be linked to the above-mentioned coexistence of a kesterite and  
31 an orthorhombic phase. However, the band alignment between absorber and buffer layer  
32 might also become severely performance limiting, especially for solar cells based on 1.7 eV  
33 band gap  $Cu_2ZnGe(S,Se)_4$  absorbers. To make these absorbers viable for application as top  
34 cells for tandem configurations, significant efficiency enhancements are required (see  
35 discussion below). In order to achieve this improvement of wide band gap kesterite solar cell  
36 efficiencies, an optimization of all layers in the TF layer stack, especially the buffer/absorber  
37 interface, has to be performed (see Section 2.2).

## 2.2. SURFACE TREATMENT AND BUFFER LAYER OPTIMIZATION

For the absorber layers discussed in Section 2.1, two paths toward optimization of performance were pursued: (i) selective etching of the ZnSe secondary phases (mentioned in Section 2.1.1.2) was successfully carried out and the impact on the final solar cell properties was determined (as discussed in Section 2.2.1). (ii) The CdS buffer layer deposition was optimized, and the employment of alternative buffer layers evaluated (as discussed in Section 2.2.2). Due to its better availability this work – unless stated otherwise – was done on evaporated EVAP-Cu<sub>2</sub>ZnGeSe<sub>4</sub> absorbers.

### 2.2.1. ABSORBER SURFACE TREATMENT

Various absorber characterizations techniques reveal the presence of ZnSe at the surface of EVAP-Cu<sub>2</sub>ZnGeSe<sub>4</sub> kesterites prepared by the two-step process of evaporating metal layers in vacuum with subsequent selenization of the layer stack (detailed in Section 2.1.1.2). The presence of secondary phases at the absorber/buffer interface is usually reported to have a deleterious effect on the efficiency of the resulting solar cells [24]. To prevent this, a (selective) chemical etching process for ZnSe is included as part of the standard procedure to prepare efficient solar cells. To find the proper etching procedure, we identified two previously reported etching strategies: (i) acidic etching with hot HCl, and (ii) an oxidation route at room temperature with KMnO<sub>4</sub> in a sulfuric acid medium [25]. Raman spectroscopy with an excitation wavelength of 458 nm allows detection of even small traces of ZnSe due to the resonant measurement conditions (i.e., excitation energy is close to the band gap of ZnSe,  $\approx 2.7$  eV) [26], hence, (resonant) Raman spectroscopy was used as the main characterization tool to aid in determining the optimal experimental etching conditions (temperature, concentration, duration) that result in a ZnSe-free EVAP-Cu<sub>2</sub>ZnGeSe<sub>4</sub> surface. For approach (i), this means etching with a 12 wt% HCl solution, see Figure 7. For approach (ii), a 2-minute etch at room temperature in an aqueous solution of 1 mol/L KMnO<sub>4</sub> in 1 mol/L H<sub>2</sub>SO<sub>4</sub> is sufficient to effectively remove ZnSe. Ultimately, the HCl etching was chosen as the standard etching procedure based on practical arguments (parameter control, processing, and solution stability). The optimized HCl etching conditions used in standard solar cell manufacturing have been determined to be: 15 min etching in a 12 wt% HCl solution at a temperature of 80 °C.

Solar cells were prepared based on EVAP-Cu<sub>2</sub>ZnGeSe<sub>4</sub> absorbers (from the same batch) grown on Mo coated Si(O,N)/SLG, followed by CBD of CdS buffer layer, sputtering of an i-ZnO/ZnO:Al window bi-layer and finalized by e-beam deposition of Ni/Al/Ni grids for the front contact. Two absorbers served as references (i.e., not etched) and three were HCl treated at 60, 70, and 80 °C. Resonant Raman spectra confirm that only the untreated

1 references contain ZnSe at the surface. The effect of this etching procedure on  $V_{OC}$ , FF, and  
2 EQE are presented in Figures 8 and 9. The  $V_{OC}$  of the cells prepared with untreated references  
3 are in the range of 500-550 mV, which corresponds to 45-50 % of the maximum achievable  
4  $V_{OC}$  ( $V_{OC,max}$ ) for such an absorber band gap (i.e., PL peak at 1.36 eV). In comparison, high-  
5 efficiency  $Cu_2ZnSn(S,Se)_4$  solar cells typically achieve 55-60% of  $V_{OC,max}$  [27]. The lower  $V_{OC}$   
6 observed here with Ge-kesterite solar cells is suspected to partially originate from a non-ideal  
7 buffer/absorber interface (allowing for charge carrier recombination). The presence of ZnSe  
8 on the surface of the absorber (or at the buffer/absorber interface) may explain the losses.  
9 This explanation is supported by the fact that  $V_{OC}$  is significantly improved for solar cells for  
10 which the EVAP- $Cu_2ZnGeSe_4$  absorber underwent prior HCl etching (resulting in a ZnSe free  
11 absorber surface), reaching around 55 % of  $V_{OC,max}$ . Despite this significant  $V_{OC}$  improvement,  
12 solar cells prepared with HCl-treated absorbers result in lower efficiencies due to a dramatic  
13 FF loss and an EQE drop at longer wavelength (usually ascribed to a reduced collection length).

14 To determine the origin of the FF and collection length losses after HCl etching, surface  
15 characterization by HAXPES has been performed at the HiKE endstation [15] equipped with  
16 a Scienta R4000 electron analyzer and located at the BESSY II KMC-I beamline [16] at HZB,  
17 using an excitation energy of 2.1 keV. The HAXPES survey spectra of an as-deposited (i.e.,  
18 not etched; black spectrum) and a HCl etched EVAP- $Cu_2ZnGeSe_4$  sample (red spectrum) are  
19 shown in Figure 10. All  $Cu_2ZnGeSe_4$ -related photoemission and Auger lines can be observed,  
20 as expected. In addition, signals related to oxygen (O 1s), carbon (C 1s), and for the as-  
21 deposited EVAP- $Cu_2ZnGeSe_4$  also cadmium (Cd 3d) can be observed. The presence of oxygen  
22 and carbon can be attributed to a surface contamination layer formed due to the (short) air  
23 exposure of the samples. The significant increase of the C 1s line upon HCl etching is most  
24 likely related to additional contamination during the etching procedure. The presence of  
25 cadmium on the as-deposited sample is ascribed to cross contamination from CdS/EVAP-  
26  $Cu_2ZnGeSe_4$  samples that have been transported in the same sample box. Due to these varied  
27 and significant states of surface contamination, we deliberately refrain from attempting to  
28 quantify the HAXPES data but rather discuss them qualitatively. The HAXPES survey spectrum  
29 of the as-deposited EVAP- $Cu_2ZnGeSe_4$  sample is dominated by Zn and Se signals. Upon HCl  
30 etching, the Zn- and Se-related signals are significantly reduced, and the Cu/Zn ratio is  
31 enhanced, in good agreement with the Raman results discussed above, i.e. the presence of a  
32 ZnSe (surface) phase before etching and its removal upon HCl-treatment. The inset of Figure  
33 10 shows the related detail spectra of the Se  $3d_{3/2}$  and  $3d_{5/2}$  spin-orbit split doublet, having a  
34 separation between 0.8 and 0.9 eV. The spectral shape of the Se 3d line significantly changes  
35 upon HCl etching. For the HCl-etched EVAP- $Cu_2ZnGeSe_4$  sample, the peak shape is  
36 attributed to the presence of (at least) two species. The main species (indicated with "M" in  
37 the inset; also dominating the spectrum of the as-deposited EVAP- $Cu_2ZnGeSe_4$  sample) is  
38 ascribed to a selenide, i.e., to selenium in a  $Cu_2ZnGeSe_4$  and/or ZnSe environment – based

1 on the comparison of the Se 3d data with Ref. [12]. Based on this data it is not possible to  
2 unambiguously differentiate between ZnSe and  $\text{Cu}_2\text{ZnGeSe}_4$ . The low-intensity secondary  
3 species (indicated with “S” in the inset) that is responsible for the additional high-binding  
4 energy spectral intensity can most likely be explained by oxidized selenium ( $\text{SeO}_x$ ,  $x \geq 3$ ).  
5 However, note that due to the large spread of binding energy values found in published  
6 references [12], the presence of a germanium selenide binary phase (with Ge being in an  
7 oxidation state  $> 2+$ ) and/or formation of Se-C bonds (in-line with the increased C signal) can  
8 also not be ruled out as an explanation for the high-binding energy Se 3d contribution.  
9 Whether and how this second Se species affects the chemical environment of additional  
10  $\text{Cu}_2\text{ZnGeSe}_4$  elements and/or the electronic structure of the absorber and how this is related  
11 to the observed solar cell characteristics is the topic of ongoing research. Work on the device  
12 level is in progress with the goal of developing a wet-chemical treatment to remove the HCl-  
13 etch induced formation of the second Se species in order to recover the FF and collection  
14 length, while keeping the  $V_{\text{OC}}$  gain resulting from HCl etching.

### 15 2.2.2. BUFFER LAYER DEVELOPMENT

16 The most widely used buffer layer for Cu chalcogenide thin film solar cells is CdS prepared  
17 by CBD. This preparation process results in a highly defect-rich material, also containing  
18 oxygen (OH) and carbon impurities [28]. Some of the properties of CBD-grown CdS (e.g.  
19 composition, defect nature, structure) depend on the experimental deposition parameters  
20 (concentration of the precursors, temperature of the chemical bath, etc.). Consequently, the  
21 CBD-CdS recipe needs to be adjusted for each absorber material for optimal solar cell  
22 performance. Hence, we empirically tuned the experimental parameters of the CdS  
23 deposition on the evaporated EVAP- $\text{Cu}_2\text{ZnGeSe}_4$  absorbers. We observe a  $V_{\text{OC}}$  increase with  
24 increasing deposition duration, accompanied with a decrease of FF and  $J_{\text{SC}}$  after a critical  
25 duration. More details about the buffer layer optimization, which resulted in a new record  
26 efficiency of 7.6 % for  $\text{Cu}_2\text{ZnGeSe}_4$  based solar cells, can be found in Ref. [29].

27 Although it is the most-used buffer material for kesterite solar cells, CdS has a quite low  
28 optical band gap energy (2.4 eV) and high absorption coefficient for a material that would  
29 ideally be transparent. Consequently, there is a loss in current due to absorption of solar  
30 radiation in the CdS is in the range of 1-2 mA/cm<sup>2</sup>. In case of a potential kesterite/Si tandem  
31 configuration, this loss would manifest in a 4 to 14 % relative decrease of the theoretically  
32 achievable  $J_{\text{SC}}$  [3]. Moreover, another important prerequisite to reach high efficiency is an ideal  
33 buffer/absorber interface that allows for lossless charge carrier transport without barriers for  
34 charge carriers and preventing high-rate charge carrier recombination routes. In order to  
35 systematically optimize the buffer/kesterite interface, we prepared solar cells based on wet-  
36 chemical deposited (see Section 2.1.2) 1.5 (+/- 0.05) eV band gap SOL- $\text{Cu}_2\text{ZnGe}(\text{S},\text{Se})_4$   
37 absorbers (prepared according to the solution approach discussed in detail in Section 2.1.2)

1 and different buffer layer materials. The five different buffer materials used were: sputtered  
2 (“rf”)  $\text{Zn}(\text{O}_{0.6}\text{S}_{0.4})$ , CBD- $\text{Zn}(\text{O},\text{S})$ , CBD- $\text{CdS}$ , atomic layer chemical vapor deposited (ALCVD)  
3  $\text{In}_2\text{S}_3$ , and co-evaporated (“co-evap.”)  $\text{CdIn}_2\text{S}_4$ . A detailed discussion can be found in Ref. [17],  
4 briefly: Compared to the  $\text{CdS}$  reference,  $\text{In}_2\text{S}_3$  and  $\text{Zn}(\text{O}_{0.6}\text{S}_{0.4})$  buffers have a higher  
5 transmission, i.e., less absorption in the buffer layer (in the 350-500 nm wavelength range), as  
6 shown in Figure II. Solar cells with  $\text{Zn}(\text{O}_{0.6}\text{S}_{0.4})$  buffers also yield higher  $V_{\text{OC}}$  values. For these  
7 devices, a higher activation energy of the dominant recombination process was also derived  
8 (compared to the  $\text{CdS}$  reference) [17], strongly suggesting a more preferable electronic  
9 structure of the buffer/SOL- $\text{Cu}_2\text{ZnGe}(\text{S},\text{Se})_4$  interface. The sputtered- $\text{Zn}(\text{O}_{0.6}\text{S}_{0.4})$  buffered  
10 solar cells, however, achieve a lower overall efficiency, mainly due to reduced FF and  $J_{\text{SC}}$ , as  
11 presented in Table S1 [17]. We speculate that those losses originate from the nature of the  
12 deposition method, as all vacuum deposited buffer layers suffer from similar  $J_{\text{SC}}$  and FF losses,  
13 compared to solution-prepared  $\text{CdS}$ . For that reason, we also investigated wet-chemically  
14 deposited  $\text{Zn}(\text{O},\text{S})$  buffers. With CBD- $\text{Zn}(\text{O},\text{S})$  buffers, SOL- $\text{Cu}_2\text{ZnGe}(\text{S},\text{Se})_4$  based solar cells  
15 achieve similar FF and  $J_{\text{SC}}$  values as the  $\text{CdS}$  reference, but lower  $V_{\text{OC}}$  values. A tentative  
16 explanation for this observation is the different composition of CBD- $\text{Zn}(\text{O},\text{S})$  and sputtered-  
17  $\text{Zn}(\text{O}_{0.6}\text{S}_{0.4})$  buffers: certainly the O/S ratio, which determines the optical band gap of the  
18  $\text{Zn}(\text{O},\text{S})$  material, can be different and the CBD- $\text{Zn}(\text{O},\text{S})$  buffer may also contain oxide,  
19 hydroxide (OH), and/or carbon impurities, which can also have an impact on the  
20 optoelectronic properties. Additional work is in progress to optimize the CBD- $\text{Zn}(\text{O},\text{S})$  buffer  
21 aiming at combining the good  $J_{\text{SC}}$  and FF values with the high  $V_{\text{OC}}$  that is obtained when  
22 sputtered- $\text{Zn}(\text{O}_{0.6}\text{S}_{0.4})$  is used as a buffer.

23

### 24 2.3.DEVICE SIMULATIONS

25 Numerical simulations were carried out using the SCAPS software [30] to determine the best  
26 device design for  $\text{Cu}_2\text{ZnGe}(\text{S},\text{Se})_4$ -based top cells in a tandem configuration, with a focus on  
27 suggesting suitable TBCs. The parameters used in the simulations are listed in Table S2  
28 [31,32]. Most of the parameters related to the absorber material, such as thickness, doping  
29 concentration, band gap, and absorption coefficient, were extracted from (our own) electrical  
30 and optical measurements. Parameters related to  $\text{MoSe}_2$  and  $\text{MoO}_3$  were taken from  
31 literature, and those related to  $\text{CdS}$  and  $\text{ZnO:Al}$  layers are already available in the SCAPS  
32 software. Two configurations were tested in the simulations:  $\text{Cu}_2\text{ZnGe}(\text{S},\text{Se})_4$  substrate or  
33 superstrate solar cells, as shown in Figure S5. In the standard configuration [substrate, Figure  
34 S5(a)], a thin layer of  $\text{MoSe}_2$  was inserted in the model between the  $\text{Cu}_2\text{ZnGe}(\text{S},\text{Se})_4$  absorber  
35 layer and the Mo contact. The presence of  $\text{MoSe}_2$  layer at the absorber/Mo interface was  
36 previously reported for  $\text{Cu}(\text{In},\text{Ga})\text{Se}_2$  [33] and  $\text{Cu}_2\text{ZnSnSe}_4$  [34] TF solar cells. It was shown  
37 to be beneficial for TF solar cells performance if its thickness is controlled to avoid detrimental

1 effects on series resistance. The improvement of the solar cell performance is mainly due to  
2 a reduction of the barrier height and better charge carrier collection at the interface between  
3 the absorber and the Mo contact if MoSe<sub>2</sub> is present. For tandem cells, the Mo back contact  
4 needs to be replaced by a TBC, see Figure S5(b). However, most of the transparent  
5 conductive oxides (TCOs) used in solar cells have a low work function (4.7-4.9 eV [35]) and  
6 thus – if Anderson’s rule holds true for these complex heterojunctions – may not result in a  
7 preferable energy level alignment with the Cu<sub>2</sub>ZnGe(S,Se)<sub>4</sub> absorber layer when used as back  
8 contact. In this case, the use of an intermediate layer, such as a thin MoSe<sub>2</sub> or MoO<sub>3</sub>, can  
9 mitigate this issue. MoO<sub>x</sub> was successfully used in superstrate configuration as an interfacial  
10 layer between a transparent SnO<sub>2</sub>:In (ITO) back contact and Cu(In,Ga)Se<sub>2</sub> absorbers [36] and  
11 was shown to also be a good interfacial layer for the Cu<sub>2</sub>ZnSnSe<sub>4</sub> based solar cells (applied  
12 either as a layer between the absorber and the Mo contact to improve the back contact  
13 properties or as a primary back contact) [37-38].

14 Figure S6 shows the J(V) curves calculated for different device configurations. The solar cell  
15 parameters are given in Table 2. For the Cu<sub>2</sub>ZnGe(S,Se)<sub>4</sub> substrate configuration (a), the  
16 calculated J(V) curve is based on series resistance and shunt resistance values of 4.7 and  
17 365 Ωcm<sup>2</sup>, respectively. These resistances have been extracted from the J(V) curve of one of  
18 the most efficient EVAP-Cu<sub>2</sub>ZnGeSe<sub>4</sub> substrate solar cells (5.4 % power conversion efficiency).  
19 In the configurations (b)-(d), the J(V) curves were calculated after the (simulated) optimization  
20 of the absorber doping concentration (10<sup>16</sup> cm<sup>-3</sup>) and of the values for series and shunt  
21 resistance (R<sub>s</sub> ≤ 0.5 Ωcm<sup>2</sup>; R<sub>sh</sub> ≥ 800 Ωcm<sup>2</sup>). In case of a superstrate with TBC [configuration  
22 (c)], the low solar cell performance is due to a strong reduction of the V<sub>OC</sub> caused by the low  
23 work function of ZnO:Al (AZO). The best configuration for superstrate solar cell was  
24 obtained by considering a thin “buffer layer” of MoO<sub>3</sub> between the absorber and a TCO back  
25 contact (d). It should be noticed that an ITO back contact acts also as a Na barrier. If  
26 insufficient Na content limits the device performance, however, Na needs to be deliberately  
27 added in a controlled way, e.g. by means of post-deposition treatment [39].

## 29 2.4. TRANSPARENT BACK CONTACTS

30 TBCs for potential use in the wide band gap Cu<sub>2</sub>ZnGe(S,Se)<sub>4</sub> kesterite top cell of a four  
31 terminal photovoltaic tandem cell with a c-Si bottom cell have been studied. In addition to  
32 the electronic structure considerations in the previous section, the back contact must be  
33 transparent for photons with an energy below the band gap of the absorber layer and stable  
34 under its processing conditions. Independent of the processing route [evaporation-based (see  
35 Section 2.1.1) or solution-based (see Section 2.1.2.)], the kesterite absorber is formed by high-  
36 temperature annealing of the precursor layer stack in H<sub>2</sub>Se and/or H<sub>2</sub>S atmosphere. It is  
37 expected that this selenization/sulfurization will be the most critical processing step that the

1 TBC has to withstand.  $\text{H}_2\text{Se}$  is a more powerful reducing agent than is  $\text{H}_2\text{S}$  [40], and so we  
2 focus on the impact of annealing in  $\text{H}_2\text{Se}$  atmosphere on the optoelectronic and chemical  
3 properties of the TBCs in the following. The most widely used TCOs: ITO, AZO, and  $\text{SnO}_2:\text{F}$   
4 (FTO) – were selected for exposure tests [41,42]. It is assumed that the S-containing  
5 atmosphere during annealing required to achieve the  $[\text{S}]/([\text{S}]+[\text{Se}])$  composition necessary for  
6 the desired higher absorber band gap will have similar effects.

7 In order to simulate the impact of  $\text{H}_2\text{Se}$  exposure during a  $\text{Cu}_2\text{ZnGe}(\text{S},\text{Se})_4$  deposition process,  
8 the optical and chemical properties of the selected TCOs have been tested before and after  
9 exposure to a 20 sccm  $\text{H}_2\text{Se}$  flow for 15 min at various treatment temperatures (400 and  
10 450 °C). A first screening showed that ITO had the highest likelihood for yielding working  
11 devices but would require a protective top layer (to make it more stable during absorber  
12 processing). Furthermore, our SCAPS simulations (see Section 2.3) of  $\text{Cu}_2\text{ZnSn}(\text{S},\text{Se})_4$  devices  
13 had shown that employing ITO instead of Mo (which is the standard back contact for single-  
14 junction devices) would result in an efficiency drop of 60 rel.% (see Table 2). The same  
15 simulations showed that this deterioration may be fully prevented by using an additional  $\text{MoO}_3$   
16 interlayer between ITO and absorber resulting even in an efficiency gain of 80 rel.% (see Table  
17 2). Hence, thin sputtered  $\text{MoO}_3$  layers applied on top of a 135-nm-thick sputtered ITO before  
18 absorber deposition – as protection layer and for improved energy level alignment – were  
19 first explored. However,  $\text{MoO}_3$  is significantly reduced upon  $\text{H}_2\text{Se}$  exposure; in Section 2.4.1,  
20 we explore alternative protective layers.

#### 21 2.4.1. PROTECTIVE TOP LAYERS

22 In this section, the effectiveness of  $\text{Al}_2\text{O}_3$ ,  $\text{InZnO}_x$  (IZO), and  $\text{TiO}_2$  as protection of ITO during  
23 selenization/sulfurization is explored. The study is conducted by means of  $\text{H}_2\text{Se}$  exposure tests  
24 at 400°C and 450°C (i.e., annealing temperatures relevant for absorber formation), as well as  
25 by experiments on the device level. The top layers were deposited by means of atmospheric  
26 pressure spatial atomic layer deposition (S-ALD, plasma enhanced for IZO) [43].

##### 27 2.4.1.1. LAYER PROPERTIES

28  $\text{Al}_2\text{O}_3$  is known to be an excellent passivation and barrier (i.e., protective layer) material of  
29 high chemical stability; it is however electrically insulating. IZO and  $\text{TiO}_2$  are candidates for  
30 forming more conductive protective layers. In order to determine the minimum thickness for  
31 being a sufficient protective top layer and to test if such a thickness would yield a working  
32 device, a set of  $\text{Al}_2\text{O}_3$  (1-30 nm), IZO (1-120 nm), and  $\text{TiO}_2$  (2-60 nm) layers of different  
33 thicknesses were deposited by means of S-ALD on ITO coated SLG substrates. The  
34 absorption spectra (derived from reflectance and transmittance) shown in Figure 12 suggest  
35 that the decrease of ITO transmittance (i.e., increase of absorption) induced by  $\text{H}_2\text{Se}$  exposure  
36 could (to some degree) be prevented with a  $> 2$  nm  $\text{Al}_2\text{O}_3$  (not shown),  $> 30$  nm IZO, or  $>$



1 60 nm TiO<sub>2</sub> top layer. However, the TiO<sub>2</sub> layers are less effective at temperatures of 450°C  
2 and higher [see Figure 12(c)]. After H<sub>2</sub>Se exposure at 450°C, the average absorption for an  
3 135-nm-thick ITO layer with a 30-nm-thick IZO and 60-nm-thick TiO<sub>2</sub> protective layer is 8  
4 and 18 %, respectively, in the near infra-red regime (between 750 nm and 1100 nm).

5 HAXPES was used for chemical structure analysis of the IZO/ITO back contact configuration  
6 and its changes upon H<sub>2</sub>Se exposure in order to probe the deterioration of ITO and the  
7 protection mechanism of IZO. Note that same measurement conditions apply as for the  
8 HAXPES data shown in Figures 1 and 4. The Sn 3d XPS spectra of a bare ITO sample and ITO  
9 samples with either a 10 or a 30 nm protective IZO top layer before and after H<sub>2</sub>Se treatment  
10 at 450 °C are shown in Figure 13. Before the H<sub>2</sub>Se treatment, for the bare ITO and 10 nm  
11 IZO/ITO sample, Sn resides in a chemical environment best described by a combination of  
12 ITO, SnO, and SnO<sub>2</sub>. However, note that asymmetric core level lines are generally found for  
13 (highly conductive) ITO and are generally attributed to final-state effects [44]. No Sn signal is  
14 observed for the 30 nm IZO/ITO sample, due to insufficient probing depth and complete  
15 coverage of the ITO by the IZO. (The inelastic mean free path of the Sn 3d photoelectrons  
16 excited with 6 keV photons in In<sub>2</sub>O<sub>3</sub> is around 7 nm [45]). After H<sub>2</sub>Se treatment, the spectral  
17 intensity of the Sn 3d line is significantly redistributed, indicating that the chemical  
18 environment of Sn has changed; SnSe and/or SnSeO<sub>x</sub> are likely present. Furthermore, the Sn  
19 3d intensity increases after the H<sub>2</sub>Se treatment for the 10 nm IZO/ITO sample, suggesting  
20 either that Sn diffuses into the IZO layer and/or the degree of ITO coverage decreases. If the  
21 protective layer does not completely cover the ITO, it will not prevent the chemical reaction  
22 between ITO and H<sub>2</sub>Se, the evidence of which is the formation of Sn-Se bonds. Additional  
23 HAXPES data suggest a significant chemical interaction between IZO and H<sub>2</sub>Se, implying that  
24 IZO acts as a sacrificial agent to protect ITO from H<sub>2</sub>Se. Note that additional measurements  
25 on TiO<sub>2</sub>/ITO test structures (not shown) reveal a different protection mechanism: TiO<sub>2</sub> is  
26 largely unaffected by H<sub>2</sub>Se annealing.

#### 27 2.4.1.2. SOLAR CELL DEVICES

28 EVAP-Cu<sub>2</sub>ZnGeSe<sub>4</sub>-based devices were manufactured on sputtered ITO/SLG substrates with  
29 S-ALD deposited Al<sub>2</sub>O<sub>3</sub>, IZO, and TiO<sub>2</sub> protective layers. As references, similarly prepared  
30 devices with a standard Mo back contact on a Si(O,N)/SLG substrate were also fabricated and  
31 tested. A CBD-CdS buffer and a sputtered i-ZnO/AZO bi-layer emitter was used as the front  
32 window. The (5×5 cm<sup>2</sup>) EVAP-Cu<sub>2</sub>ZnGeSe<sub>4</sub> cell stack samples were finished by applying a  
33 Ni/Ag grid for local J(V) measurements. Table 3 depicts measured J(V) parameters of the  
34 champion cells. As stated earlier, an Al<sub>2</sub>O<sub>3</sub> thickness above 2 nm is needed for an effective  
35 H<sub>2</sub>Se protection of ITO. However, the 3 nm thick Al<sub>2</sub>O<sub>3</sub> layer used here already reduces the  
36 cell performance dramatically due to its insufficient conductivity. This issue could be  
37 overcome by using a perforated Al<sub>2</sub>O<sub>3</sub> layer, which (through the formed point contacts) allows

1 sufficient charge carrier transport while also acting as a passivation and barrier layer. Devices  
2 with an ITO back contact with or without either a 30 nm  $\text{TiO}_2$  or IZO protective top layer  
3 function better, yielding efficiencies of about 85-90 % of that of reference cells with a Mo back  
4 electrode. The lower efficiencies likely result from a higher sheet resistance of the back  
5 contact and a presumably less ideal energy level alignment at the absorber/back contact  
6 interface compared to the Mo back electrode. The combination of ITO back electrode with  
7  $\text{TiO}_2$  protection layer results in a higher  $V_{\text{OC}}$  than an ITO back electrode with or without IZO  
8 protection layer, but not in a higher  $J_{\text{SC}}$  value – finding an explanation for this observation is a  
9 subject of ongoing discussion.

10 Figure 14 depicts the absorption (derived from reflectance and transmittance) for a complete  
11 EVAP- $\text{Cu}_2\text{ZnGeSe}_4$  solar cell layer stack on a 60 nm  $\text{TiO}_2$  protected ITO back electrode. The  
12 absorption of the complete cell stack for energies directly below  $E_{\text{G}}$  ( $\text{Cu}_2\text{ZnGeSe}_4$ ) is 65 % for  
13 60 nm  $\text{TiO}_2$ /ITO and 55 % for 30 nm IZO/ITO (not shown) back contacts. These values are  
14 higher than the sum computed from the absorption of the individual layers (i.e., back contact  
15 after  $\text{H}_2\text{Se}$  exposure, absorber, and front window), as illustrated in Figure 14 for the 60 nm  
16  $\text{TiO}_2$ /ITO back contact. This may be due to slightly varying absorber layer deposition and/or  
17 selenization process conditions, annealing-induced formation of species at the absorber  
18 (precursor)/TBC interface, or internal reflections and higher absorption of the front window  
19 when deposited on the actual (rough) absorber layer. In order to reduce the optical losses in  
20 a complete device, more analysis of the composition and morphology of the layers and their  
21 interfaces in the cell stack will be needed. To reduce near-infrared absorption due to free  
22 charge carriers in both the highly-doped back and front contact, more effort is required to  
23 develop transparent materials with high mobilities and reasonable charge carrier densities.

24

### 25 3. OUTLOOK

26 The bottom cell in a tandem configuration will only receive the illumination transmitted  
27 through the top cell, and so a good transmission at  $h\nu <$  than the top cell absorber band gap  
28 is crucial for the top cell structure to successfully be employed in tandem configurations, as  
29 discussed in the previous section. A thin top cell combined with a TBC is generally used to  
30 assure this. To investigate the effect of the top cell transparency on the performance of the  
31 bottom cell (c-Si), we calculated the efficiency of the bottom cell as a function of the light  
32 transmitted through the top cell, as shown in Figure 15. The bottom cell is modeled as a 25  
33 % efficient silicon cell with rear locally diffused contacts (PERL technology [46]) and  
34 Lambertian light trapping [47-48]. For the tandem cell, a four-terminal mechanically stacked  
35 configuration is considered. In Figure 15, the efficiency of the c-Si bottom cell under the  
36 absorbing 1.5 eV band gap  $\text{Cu}_2\text{ZnGe}(\text{S,Se})_4$ -based cell is shown as a function of top cell

1 transmission. Furthermore, the total efficiency of the tandem configuration assuming a top  
2 cell efficiency of 8, 15, and 22 % is shown. In the case of a  $\text{Cu}_2\text{ZnGe}(\text{S,Se})_4$  (1.5 eV)-based top  
3 cell of 8 % efficiency (i.e., a performance level similar to the one reached as a result of joint  
4 research efforts of this consortium, see Section 2.2.2), a transparency higher than 80 % is  
5 required to achieve a total tandem device efficiency that is higher than the efficiency of the c-  
6 Si bottom cell alone (25 %, horizontal dashed line in Fig. 21). In case the efficiency of the top  
7 cell can be increased to 15 % (a performance level that seems feasible based on our device  
8 simulation in Section 2.3, see Table 2), a transparency above 50 % is sufficient for viable  
9 tandem application. Finally, for a 22 % efficient top cell (a performance level that has been  
10 shown for other polycrystalline chalcogenide-based absorbers [2]) respective tandem devices  
11 would reach efficiencies > 25% with even more relaxed top cell transparency requirements.

12 A maximal transparency of approximately 40 % for a real-world  $\text{Cu}_2\text{ZnGe}(\text{S,Se})_4$ /TBC layer  
13 stack was shown in this contribution (see Fig. 20 and discussion in Section 2.4.1.2); there is a  
14 realistic potential to increase this to 60 % if chemical reactions at the interfaces and/or internal  
15 reflections can be minimized. Hence, wide band gap kesterites might very well represent a  
16 material class that may be used as absorber in tandem device top cells if further significant  
17 advancements in cell performance (8 → 15%) and transmission (40 → 60%) are achieved.  
18 Based on the progress presented in this paper (compare status 2015 and 2018 indicated as  
19 ❶ and ❷ in Figure 15), it indeed seems feasible to reach the realistic performance scenario  
20 (❸ in Figure 15) if optimization efforts continue.

21

## 22 4. CONCLUSIONS

23 Absorbers in which Sn had been substituted by Si did not result in functioning solar cells; most  
24 likely due to too high doping (in the order of  $10^{18} \text{ cm}^{-3}$ ) and/or the formation of  $\text{SiO}_2$  at the  
25 absorber surface. However,  $\text{Cu}_2\text{ZnGe}(\text{S,Se})_4$  absorbers with band gaps above 1.5 eV have  
26 been successfully developed and integrated into solar cells. Typically, ZnSe is present in large  
27 amounts on the top surface of these absorbers; it is shown here that this impurity can be  
28 selectively removed with chemical etching: (i) with 12 wt% HCl at a temperature of 60-85 °C,  
29 and (ii) in 1M  $\text{KMnO}_4$  / 1M  $\text{H}_2\text{SO}_4$  aqueous solution. The standard CBD-CdS has been  
30 optimized, resulting in a record efficiency of 7.6 % for EVAP- $\text{Cu}_2\text{ZnGeSe}_4$  based solar cells  
31 (with Mo back contact).  $\text{In}_2\text{S}_3$ ,  $\text{Zn}(\text{O,S})$ , and  $\text{CdIn}_2\text{S}_4$  alternative buffer layers were also tested,  
32 where the highest  $V_{\text{OC}}$  and presumably the best electronic buffer/absorber interface structure  
33 could be obtained with sputtered  $\text{Zn}(\text{O,S})$ .

34 The solar cell performance of substrate/superstrate  $\text{Cu}_2\text{ZnGe}(\text{S,Se})_4$  solar cells with TBC for  
35 tandem application was simulated using SCAPS to evaluate various configurations and identify  
36 performance-limiting factors. It was found that when low work function, TCO-based, TBCs

1 (like ITO) are used, an “interlayer” is required to reduce the blocking barrier at the  
2 absorber/TCO interface, ideally achieving an Ohmic contact. The device simulation suggests  
3  $\text{MoO}_x$  as an ideal interlayer candidate material for  $\text{Cu}_2\text{ZnGe}(\text{S,Se})_4$  superstrate cells for  
4 tandem applications.  $\text{MoO}_x$  is, however, unstable under real-world absorber processing  
5 conditions; the use of an alternative, stable material causes the majority of respective  
6 (transparent) cells to be still limited by a low  $V_{\text{OC}}$ .

7 ITO was shown to be a well-performing candidate for a TBC, but it requires a protective top  
8 layer (i.e.,  $\text{Al}_2\text{O}_3$ , IZO, or  $\text{TiO}_2$ ) if it is to remain transparent after exposure to the Se (and/or  
9 S) atmosphere needed for the absorber deposition process. ITO back contacts with a  
10 protective layer of 30-nm-thick IZO or 60-nm-thick  $\text{TiO}_2$  have an average absorption of 8 and  
11 18 %, respectively, in the near infra-red regime. The efficiency of solar cells using an ITO with  
12 IZO or  $\text{TiO}_2$  protective layers achieves 85-90 % of the performance of reference cells with  
13 Mo back contact (at a maximal transparency of 40 %).

14 In summary,  $\text{Cu}_2\text{ZnGe}(\text{S,Se})_4$  absorbers with potential for future application as top cell in  
15 tandem configurations have been developed. Different optimization routes mostly addressing  
16 the buffer/absorber interface have been suggested and proven to be effective to advance  
17 device performance. In order to make wide band gap kesterites a prime candidate absorber  
18 material for the top cell in tandem devices, similar approaches are crucially needed extending  
19 the efforts to all aspects of the complete cell stack, tackling interface *and* bulk properties in  
20 order to improve cell efficiency and transmission. In order to accomplish this challenge, it is  
21 proposed to focus future research on increasing the solar cell performance before addressing  
22 the transparency of these solar cell devices.

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9

10

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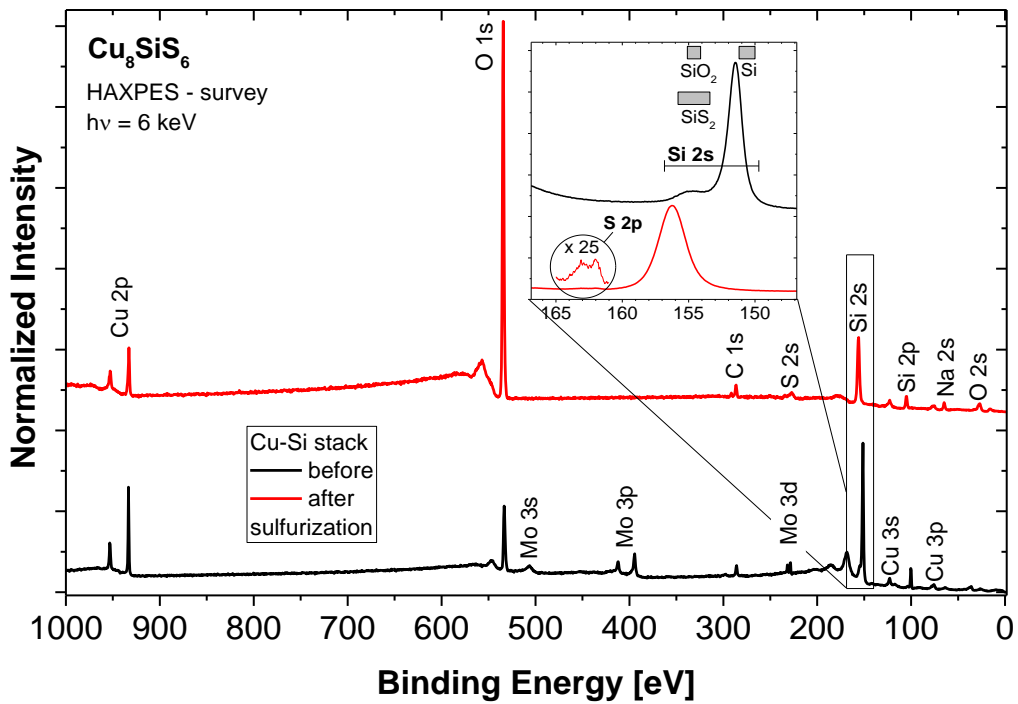
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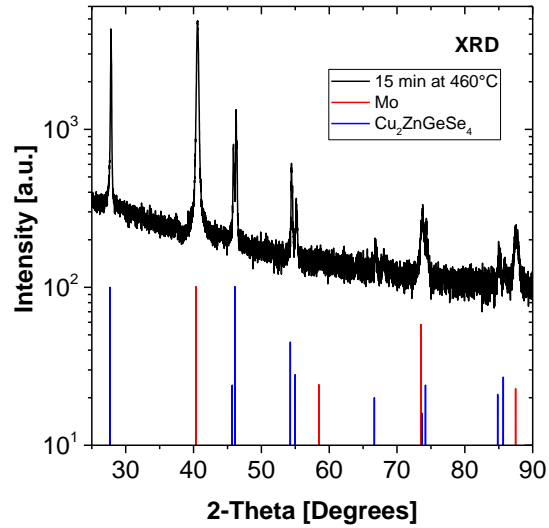
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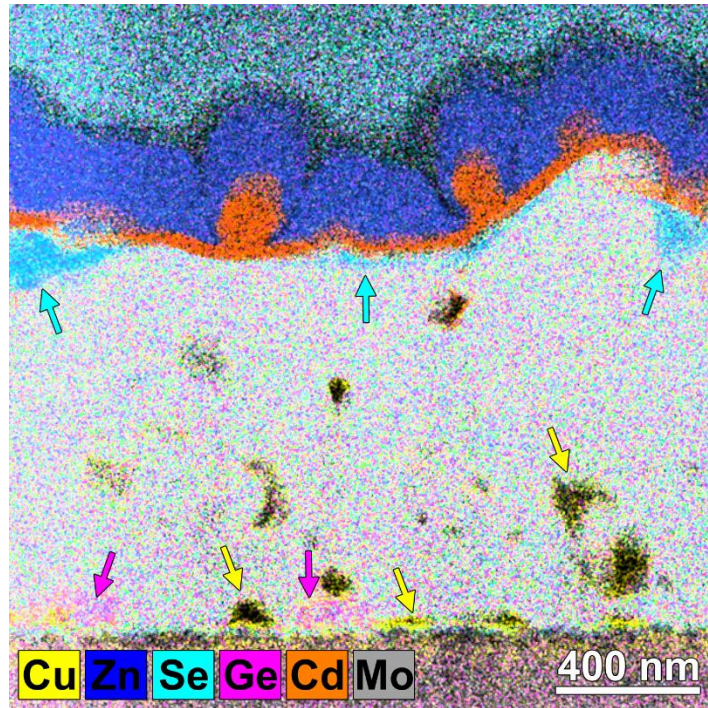


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 2 Figure 1: Hard x-ray photoelectron survey spectra of an EVAP-Cu<sub>8</sub>SiS<sub>6</sub> sample before (black)  
 3 and after (red) sulfurization treatment (spectra are offset for clarity). Due to the  
 4 sulfurization, the oxygen and sodium (most likely diffused from the soda-lime glass  
 5 substrate) contents increase. The inset shows the region of the Si 2s and S 2p core level  
 6 lines compared to reference positions [12] of silicon compounds (note that the order of  
 7 appearance is different compared to the survey spectra for better visibility). The S 2p line  
 8 can only be clearly observed on a magnified (x 25) scale.  
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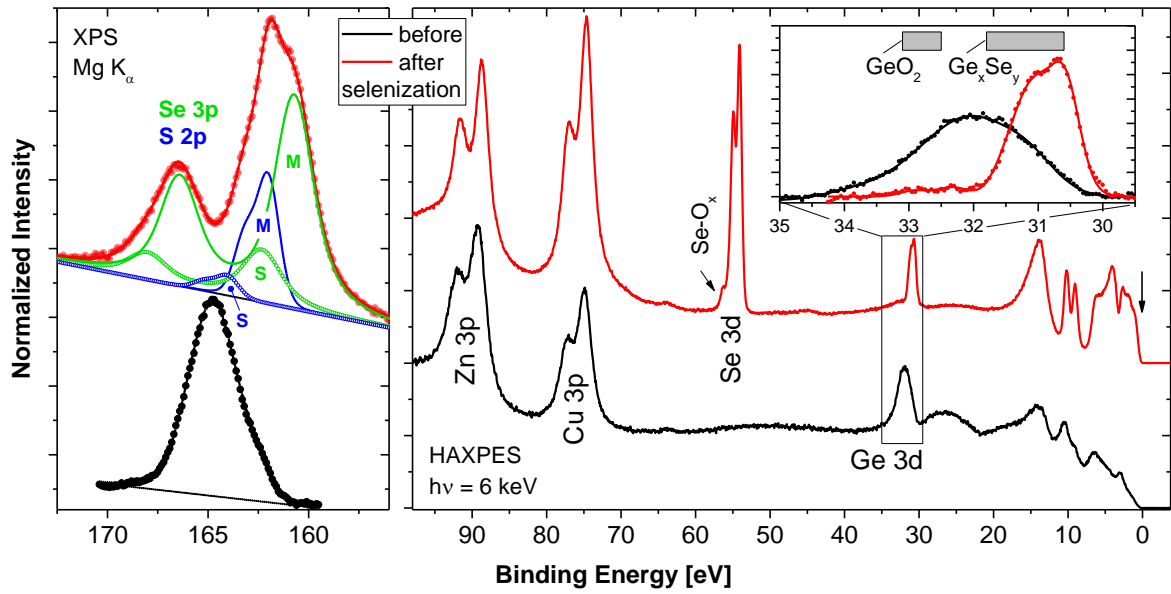
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Figure 2: X-ray diffraction pattern of the EVAP-Cu<sub>2</sub>ZnGeSe<sub>4</sub> absorber layer fabricated by selenizing the precursor stack for 15 min at 460°C on a Mo back contact together with reference positions for Cu<sub>2</sub>ZnGeSe<sub>4</sub> and Mo (PDF card 00-052-0867).



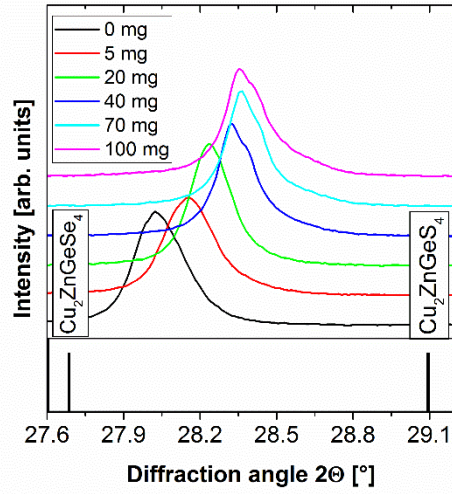
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Figure 3: Cross-section STEM-EDX elemental map of a complete EVAP-Cu<sub>2</sub>ZnGeSe<sub>4</sub> solar cell sample with CdS buffer layer and ZnO window, showing in some regions inhomogeneous elemental distributions, most likely caused by secondary phases. Regions attributed to ZnSe- (blue arrows), Cu<sub>2</sub>GeSe<sub>3</sub>- (pink arrows), and Cu<sub>2-x</sub>Se-like (yellow arrows) phases are indicated. See also [13].



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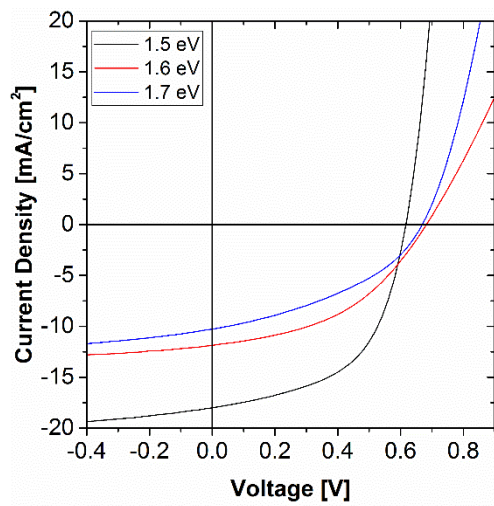
Figure 4: XPS (left panel) and HAXPES (right panel) S 2p/Se 3p and shallow core level spectra, respectively, of a SOL-Cu<sub>2</sub>ZnGe(S,Se)<sub>4</sub> absorber before (black) and after (red) Se-annealing induced absorber formation (spectra are offset for clarity). For the S 2p / Se 3p spectrum of the sample after selenization the respective fits of the S 2p (blue) and Se 3p (green) doublets are also shown. (M – main species, S – secondary species). The inset in the right panel shows the region of the Ge 3d shallow core level compared to reference positions for germanium compounds [12].



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2 Figure 5: 112-reflection of XRD patterns from SOL-Cu<sub>2</sub>ZnGe(S,Se)<sub>4</sub> absorbers processed in  
3 the presence of different amounts of GeS (0-100 mg).

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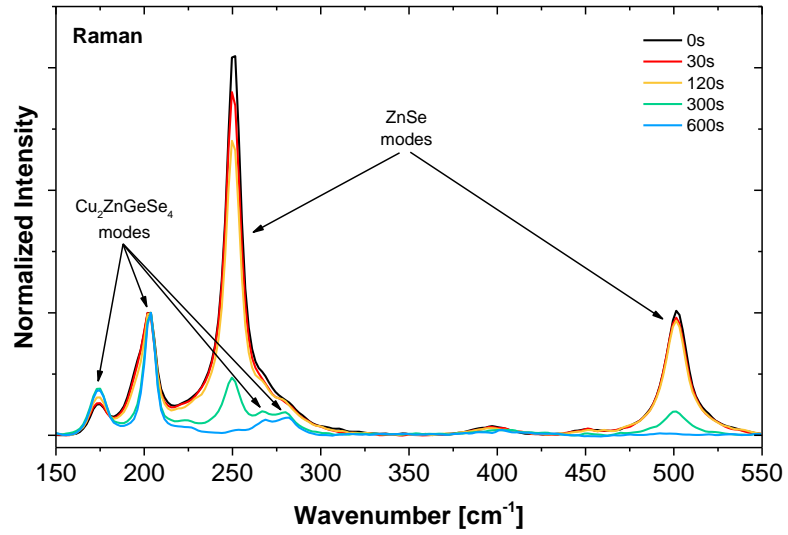
Figure 6:  $J(V)$ -characteristics of the best solar cells that were prepared from SOL- $\text{Cu}_2\text{ZnGe}(\text{S},\text{Se})_4$  absorbers with band gaps of 1.5, 1.6, and 1.7 eV, respectively, as determined from EQE. The corresponding  $[\text{S}]/([\text{S}]+[\text{Se}])$ -ratios are 0.27, 0.39, and 0.50.

$E_G$ (eV)	1.5	1.6	1.7
Eff. (%)	6.0	3.6	2.7
$V_{OC}$ (mV)	617	683	669
$J_{SC}$ (mA/cm <sup>2</sup> )	18.0	11.9	10.3
FF (%)	54.1	44.1	39.7

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2 Table I: Solar cell parameters of solar cells with SOL-Cu<sub>2</sub>ZnGe(S,Se)<sub>4</sub> absorbers with band  
3 gaps of 1.5, 1.6, and 1.7 eV, respectively.

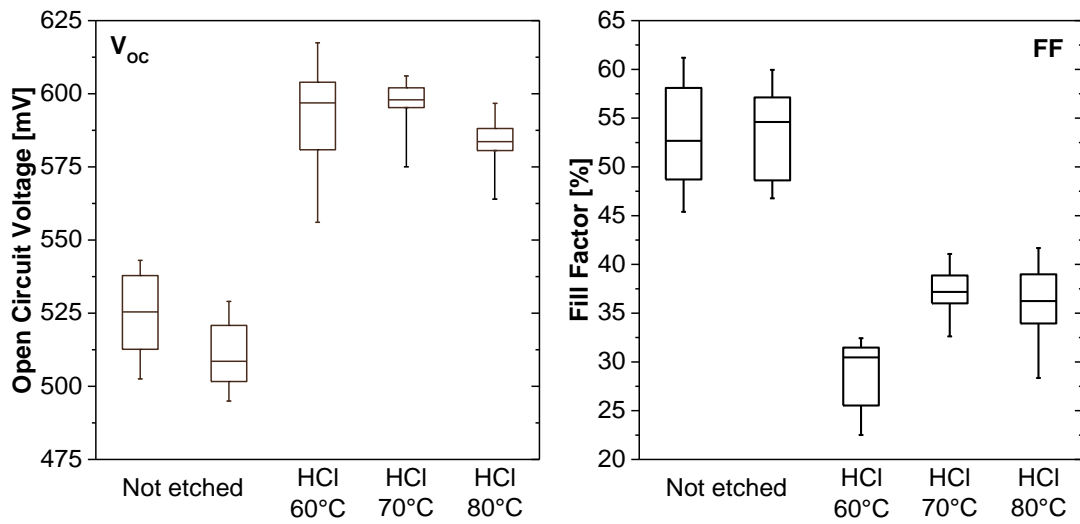
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Figure 7: Raman spectra recorded with an excitation wavelength of 458 nm of EVAP-Cu<sub>2</sub>ZnGeSe<sub>4</sub> samples that underwent HCl etching (T = 75°C, 12 wt% HCl) for different durations (from 0 to 600 s). Intensities are normalized to the most intense Cu<sub>2</sub>ZnGeSe<sub>4</sub> peak (≈ 204 cm<sup>-1</sup>).

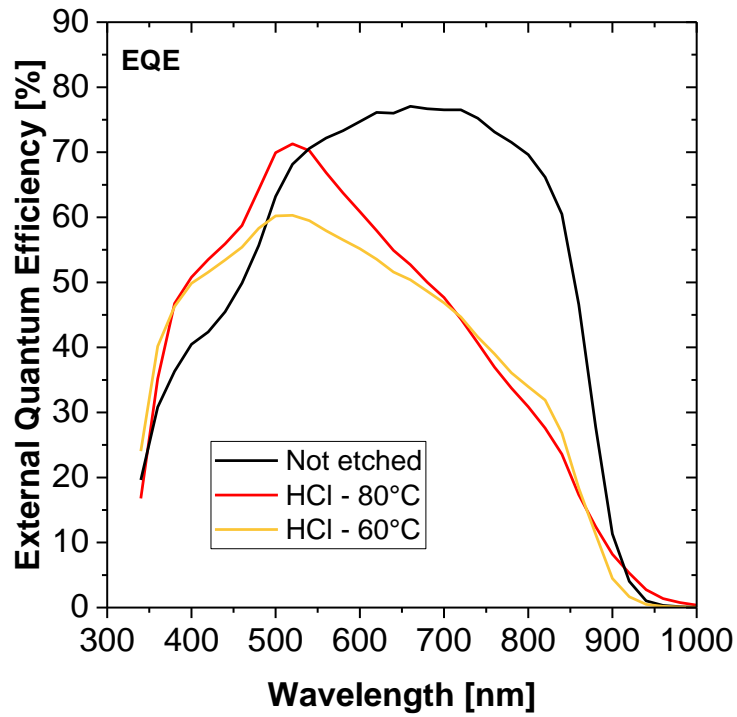




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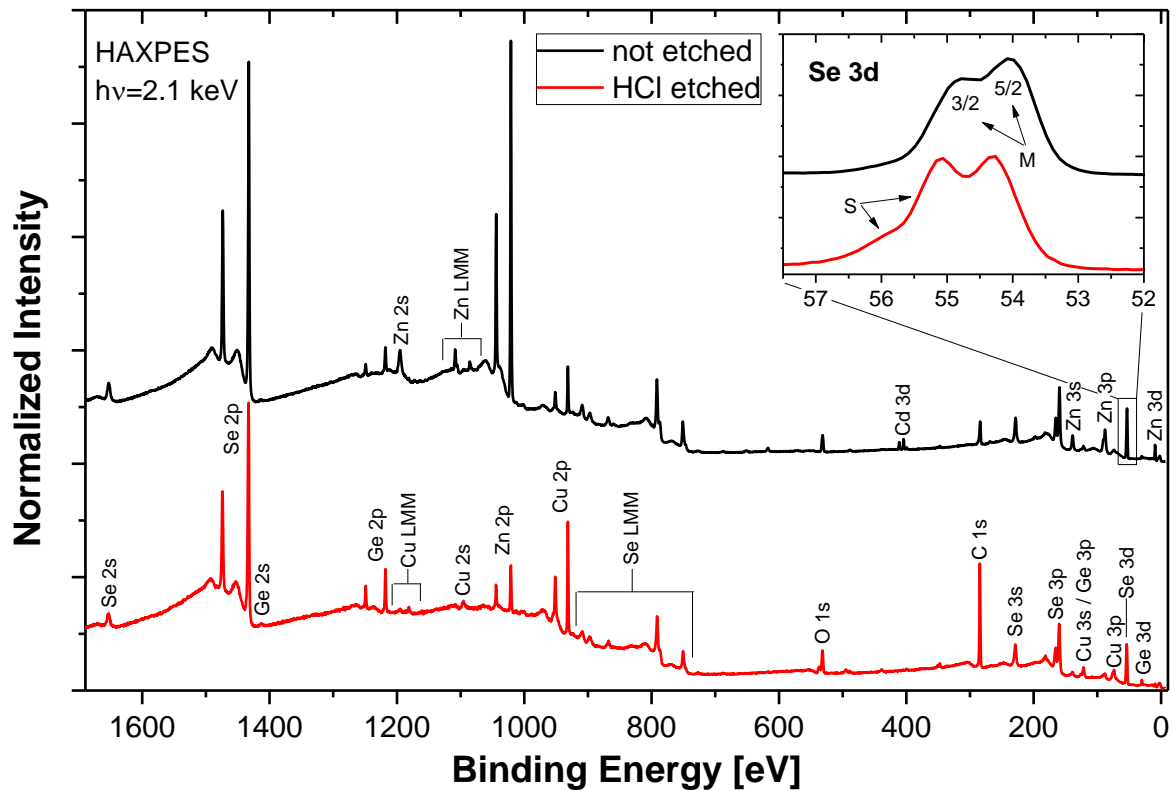
2 Figure 8:  $V_{oc}$  and FF mean values of EVAP- $Cu_2ZnGeSe_4$  based solar cells prepared using not-  
 3 etched absorbers and absorbers HCl etched (using a 12 wt% HCl solution) at different  
 4 temperatures (60 min at 60°C, 40 min at 70°C, 15 min at 80°C; 8-12 cells per sample, solar  
 5 cell area  $\approx 0.5 \text{ cm}^2$ ).

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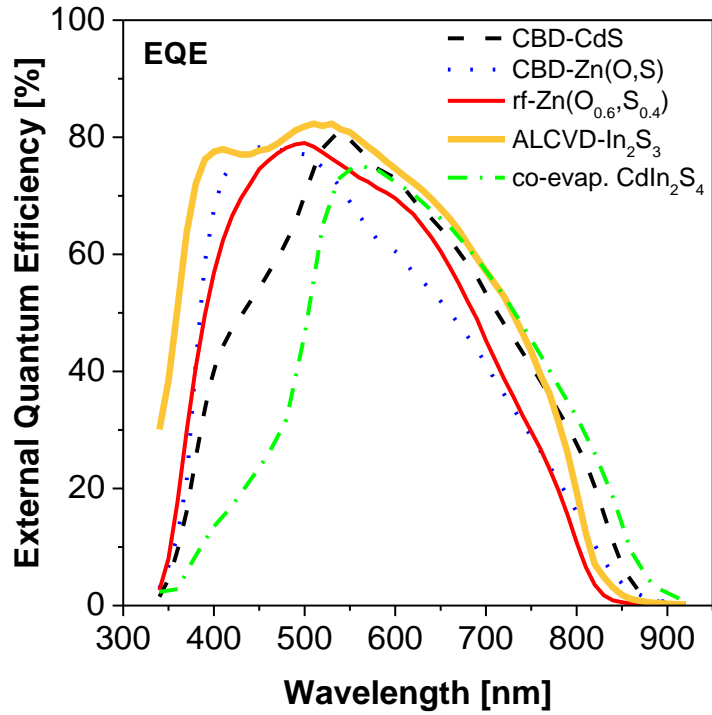
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Figure 9: Representative EQE spectra of EVAP-Cu<sub>2</sub>ZnGeSe<sub>4</sub> solar cells based on not-etched absorbers and absorbers HCl etched (using a 12 wt% HCl solution) at different temperatures (60 min at 60°C, 15 min at 80°C).



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 2 Figure 10: HAXPES survey spectra of an as-deposited / not etched (black spectrum) and  
 3 HCl etched (red spectrum) EVAP- $\text{Cu}_2\text{ZnGeSe}_4$  absorber. Spectra are offset for clarity and  
 4 all prominent lines are labelled. Inset: Detail spectra of the related Se 3d energy region, with  
 5 the 3/2 and 5/2 spin-orbit split doublet indicated. Further, the approximate positions of the  
 6 Se  $3d_{3/2}$  and  $3d_{5/2}$  lines of the main (“M”) and secondary (“S”) selenium species are depicted.

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Figure 11: Representative EQE spectra of solar cells with SOL-Cu<sub>2</sub>ZnGe(S,Se)<sub>4</sub> absorber and different buffer layers: sputtered (rf) Zn(O<sub>0.6</sub>S<sub>0.4</sub>), CBD-Zn(O,S), CBD-CdS, atomic layer chemical vapor deposited (ALCVD) In<sub>2</sub>S<sub>3</sub>, and co-evaporated (“co-evap.”) CdIn<sub>2</sub>S<sub>4</sub>.

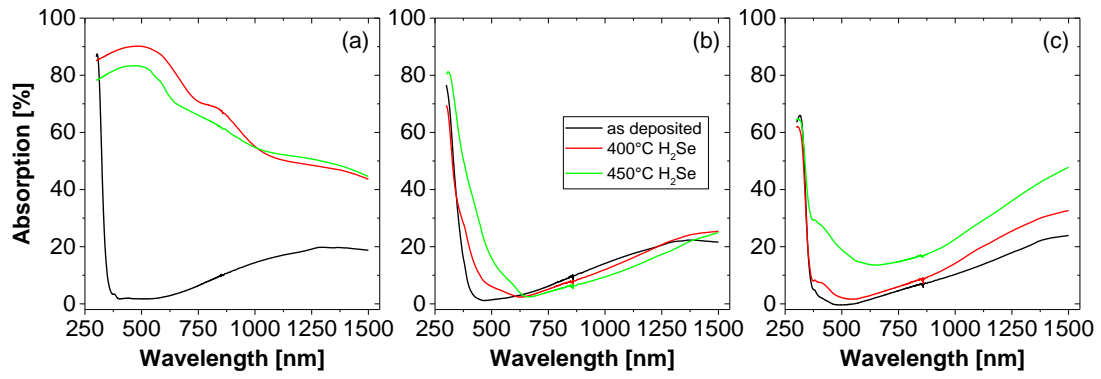
	Cell configurations			
Solar cell parameters	(a)	(b)	(c)	(d)
Back contact	MoSe <sub>2</sub> /Mo	MoSe <sub>2</sub> /Mo <sup>(○)</sup>	TCO <sup>(○)</sup>	MoO <sub>3</sub> /TCO <sup>(○)</sup>
V <sub>OC</sub> (mV)	553	572	287	1000
J <sub>SC</sub> (mA/cm <sup>2</sup> )	19.70	20.00	17.60	22.00
FF (%)	56.30	71.00	65.54	67.90
Eff. (%)	6.22	8.14	3.31	15.00

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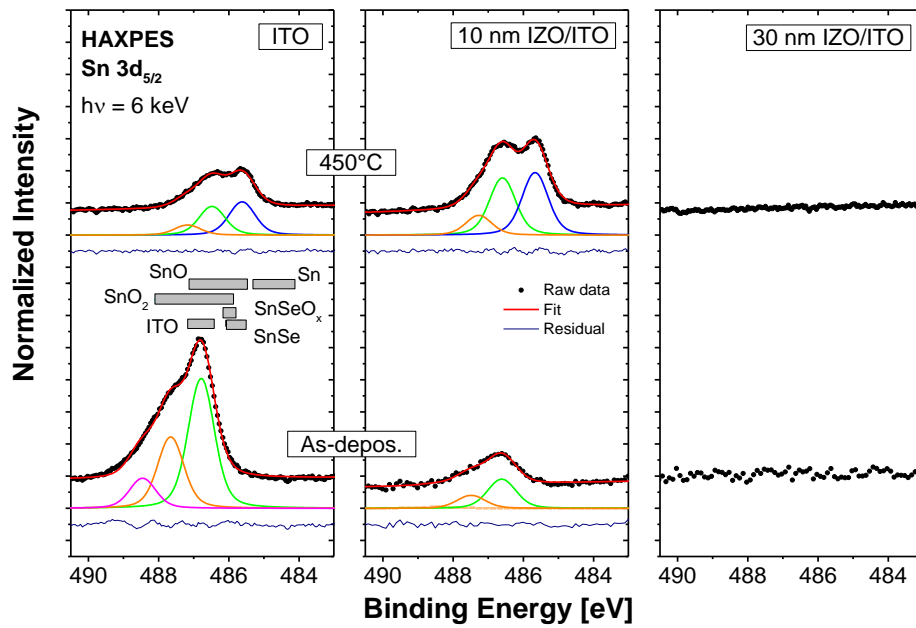
2 Table 2: Solar cell parameters calculated for the different configurations as derived from the  
3 J(V) data shown in Figure S6. <sup>(○)</sup> Results from device simulation employing optimized  
4 parameters (see Table S2).

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 2 Figure 12: Absorption of ITO without (a) and with a 30 nm IZO (b), and with a 60 nm TiO<sub>2</sub>  
 3 (c) protective top layer before (i.e., as-deposited) and after H<sub>2</sub>Se exposure at 400 and  
 4 450°C.



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Figure 13: Sn  $3d_{5/2}$  HAXPES spectra of the ITO, 10 nm, and 30 nm IZO/ITO samples before (“As-depos.”) and after  $H_2Se$  treatment at 450 °C. The curve fit was done by using one linear background and three Voigt profiles. The grey boxes indicate the Sn  $3d_{5/2}$  energetic position for reference compounds [12].

Back contact	Protective top layer	Eff. <sub>max</sub> (%)	J <sub>sc</sub> (mA/cm <sup>2</sup> )	V <sub>oc</sub> (mV)	FF (%)
ITO	None	3.6	19.9	487	37.6
ITO	IZO (30 nm)	4.0	27.1	471	31.2
ITO	Al <sub>2</sub> O <sub>3</sub> (3.5 nm)	0.8	9.3	364	23.9
ITO	TiO <sub>2</sub> (30 nm)	4.3	17.3	600	41.3
SiON/Mo	None	4.7	18.6	600	42.3

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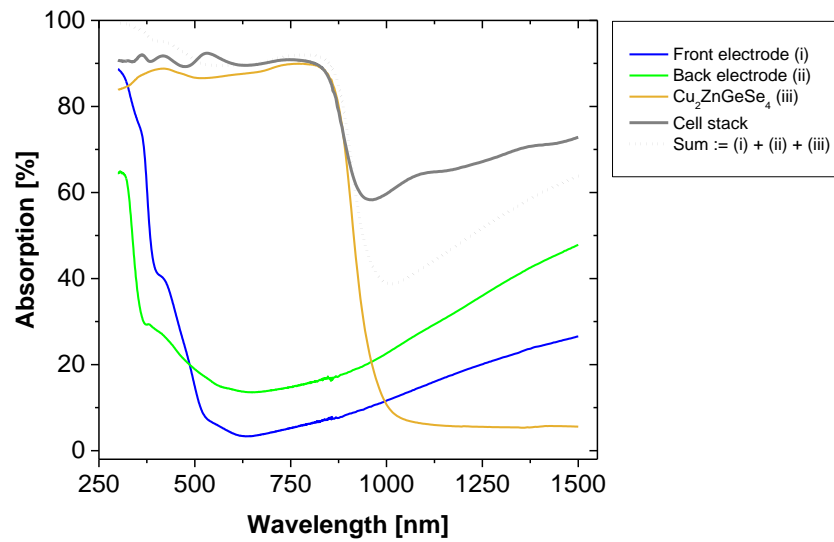
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Table 3: Overview of the J(V) parameters of the manufactured EVAP-Cu<sub>2</sub>ZnGeSe<sub>4</sub> devices (best cells).

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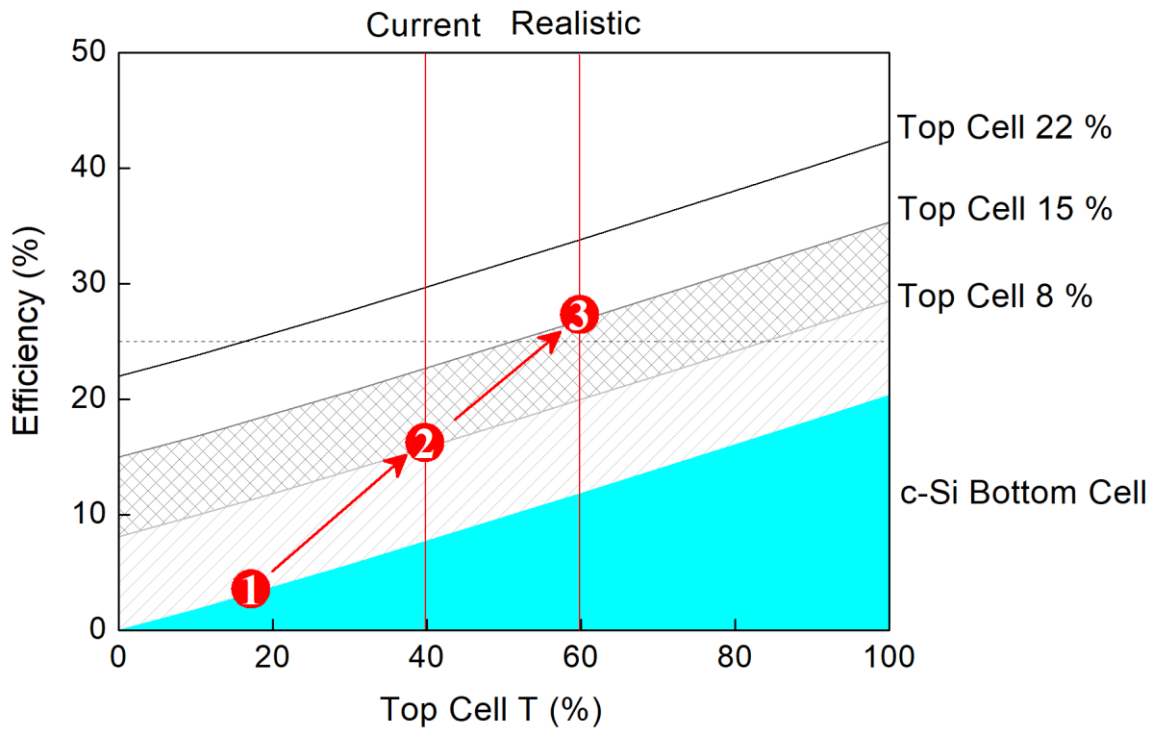
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Figure 14: Absorption spectra of the (complete) front electrode/EVAP-Cu<sub>2</sub>ZnGeSe<sub>4</sub>/60 nm TiO<sub>2</sub>/ITO cell stack and of the individual stack components: (i) ZnO:Al front electrode, (ii) 60 nm TiO<sub>2</sub>/ITO back electrode after H<sub>2</sub>Se exposure at 450°C, (iii) EVAP-Cu<sub>2</sub>ZnGeSe<sub>4</sub> absorber (as-deposited on quartz glass substrate) compared to their spectral sum := (i) + (ii) + (iii).



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2 Figure 15: The efficiency of a four-terminal mechanically stacked geometry c-Si bottom+top  
 3 cell as function of the light transmitted through the top cell ( $T$  for  $\lambda \geq hc/E_{g_{top}}$ ). As top cell,  
 4 8 and 15 % CZGSe and 22 % CIGS cells are used. The horizontal dashed line indicates the  
 5 efficiency of the c-Si bottom cell alone and serves as a performance reference. ❶ and ❷  
 6 indicate the performance situation in 2015 ( $\eta \approx 3\%$  and  $T \approx 17\%$ , calculated for measured  
 7 transparency of CZGSe on TBC (ITO/TiO<sub>2</sub>)) and 2018 (as reported in this publication:  $\eta \approx$   
 8  $8\%$  and  $T \approx 40\%$ ). ❸ indicates a realistic performance scenario for which  $\eta$  and  $T$  have to  
 9 be increased to 15 % and 60 %, respectively.

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1 **SUPPLEMENTARY MATERIAL FOR**

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3 **WIDE BAND GAP KESTERITE ABSORBERS FOR THIN FILM SOLAR CELLS:**  
4 **POTENTIAL AND CHALLENGES FOR THEIR DEPLOYMENT IN TANDEM DEVICES**

5  
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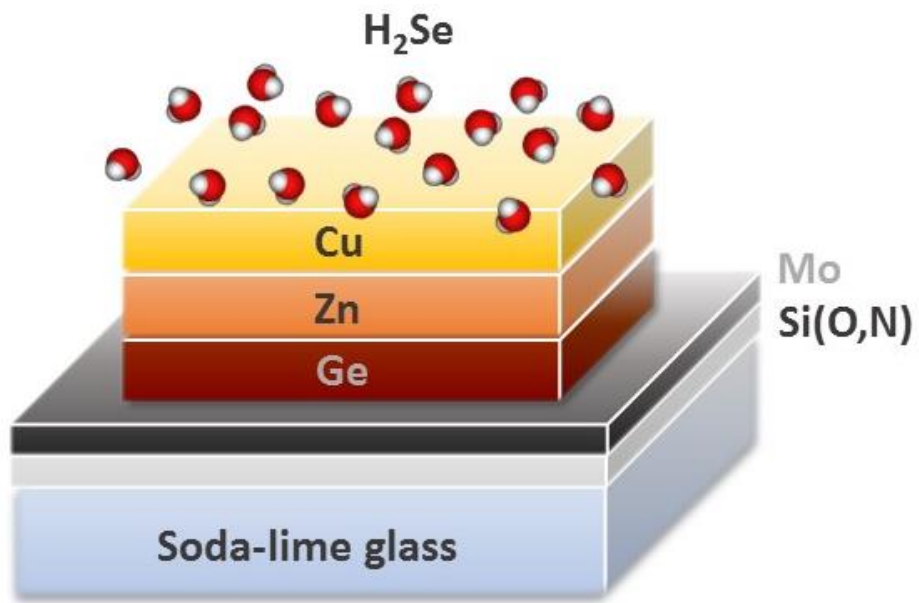
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Figure S1: Schematic representation of the two-step selenization process used for EVAP-Cu<sub>2</sub>ZnGeSe<sub>4</sub> absorber fabrication.

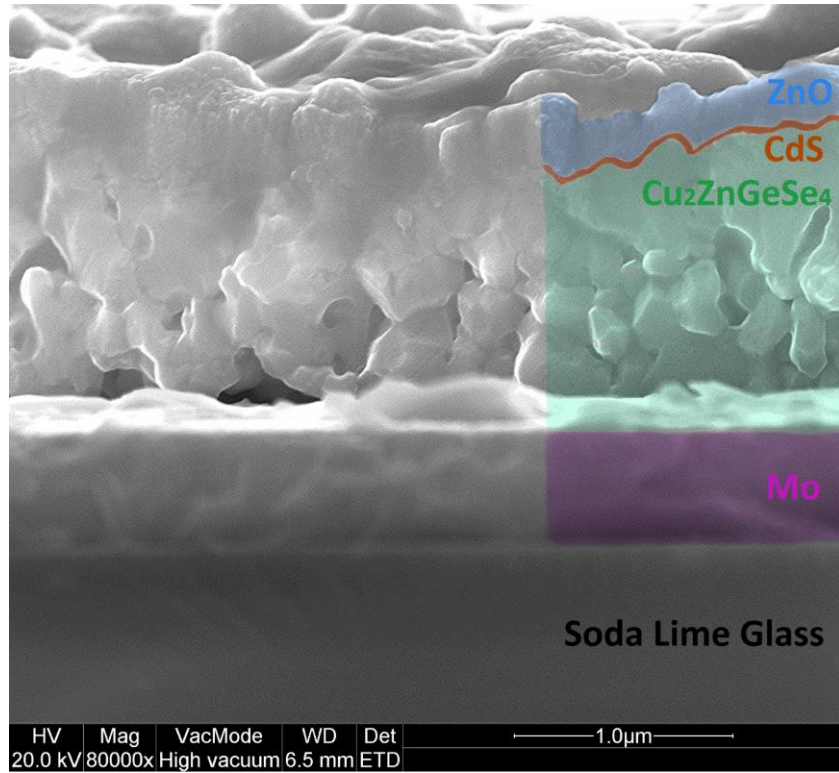
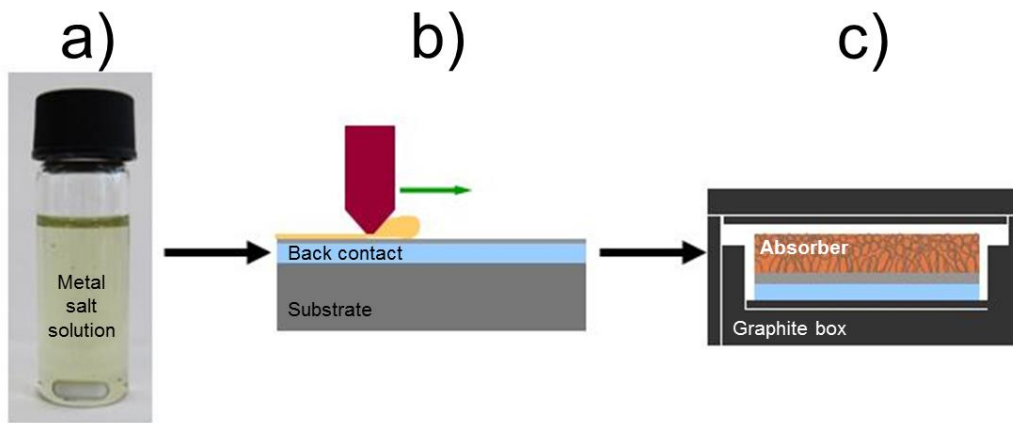


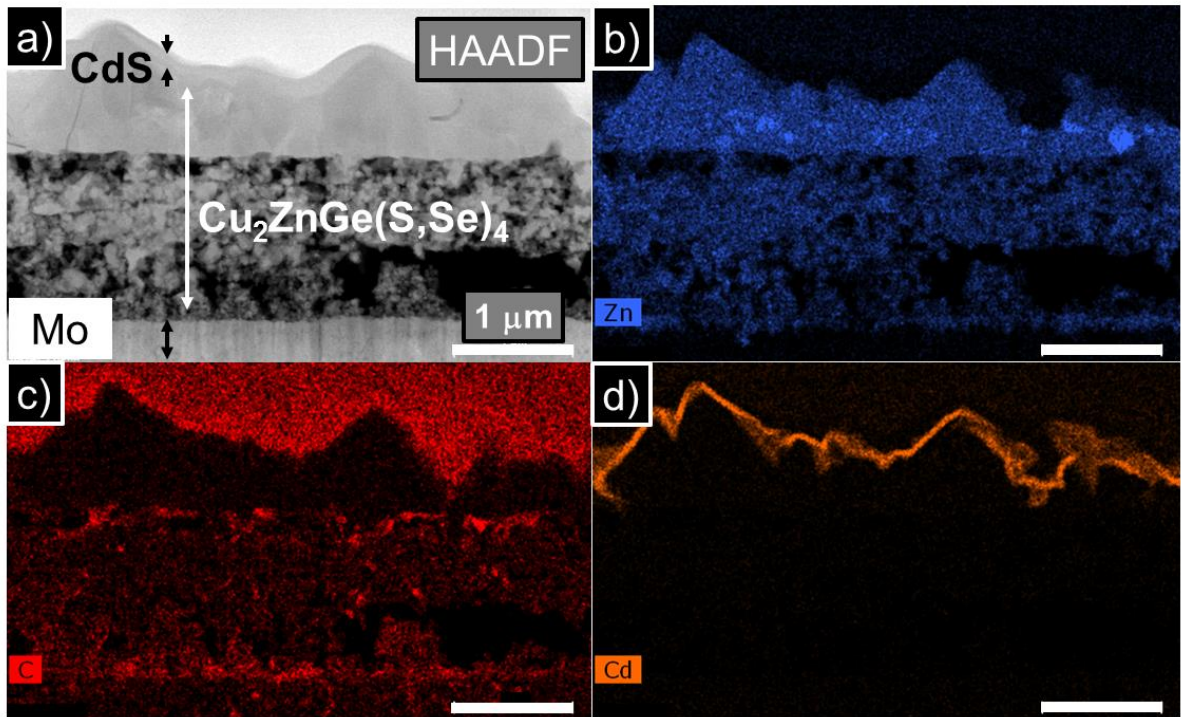
Figure S2: Cross-section scanning electron microscopy image of a finished EVAP-  
 $\text{Cu}_2\text{ZnGeSe}_4$  solar cell sample, showing the grain morphology of the absorber and contact  
layer.



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2 Figure S3: Schematic illustration of the solution process of preparing a SOL-Cu<sub>2</sub>ZnGe(S,Se)<sub>4</sub>  
3 absorber: a) metal salt solution, b) doctor blade coating, c) annealing in Se atmosphere.

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Figure S4: Cross-section high angle annular dark field (HAADF) STEM image of a SOL- $\text{Cu}_2\text{ZnGe}(\text{S,Se})_4$ -based solar cell with CdS buffer and ZnO window (a), and the elemental maps of Zn (b), C (c) and Cd (d).



Buffer layer	V <sub>OC</sub> (mV)	FF (%)	J <sub>sc</sub> (mA/cm <sup>2</sup> )	E <sub>G</sub> (eV)	Eff. (%)
CBD CdS <sup>[17]</sup>	617	54.1	18.0	1.47	6.0
CBD Zn(O,S)	512	51.2	17.7	1.51	4.6
rf-Zn(O <sub>0.6</sub> S <sub>0.4</sub> ) <sup>[17]</sup>	730	48.3	13.0	1.54	4.6
ALCVD In <sub>2</sub> S <sub>3</sub> <sup>[17]</sup>	469	48.2	14.9	1.49-1.54	3.4
Co-evap. CdIn <sub>2</sub> S <sub>4</sub> <sup>[17]</sup>	354	49.6	14.7	1.44	2.6

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2 Table S1: Electrical parameters for the most efficient buffer/SOL-Cu<sub>2</sub>ZnGe(S,Se)<sub>4</sub> solar cells.

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Parameter	ZnO:Al	CdS	Cu <sub>2</sub> ZnGe(S,Se) <sub>4</sub>	MoSe <sub>2</sub> <sup>[31]</sup>	MoO <sub>3</sub> <sup>[32]</sup>
d (μm)	0.120	0.050	1-2	0.04-0.10	0.04
E <sub>G</sub> (eV)	3.3	2.4	1.47-1.5	1.1	2.85
χ (eV)	4.4	4.2	4.54	4.14	2.6
μ <sub>n</sub> (cm <sup>2</sup> /V.s)	100	100	10	100	100
μ <sub>p</sub> (cm <sup>2</sup> /V.s)	25	25	2	25	20
N <sub>d</sub> (cm <sup>-3</sup> )	10 <sup>18</sup>	3×10 <sup>17</sup>	-	-	-
N <sub>A</sub> (cm <sup>-3</sup> )	-	-	2×10 <sup>15</sup> / 10 <sup>16</sup> <sup>(○)</sup>	10 <sup>16</sup>	10 <sup>18</sup>
R <sub>s</sub> (Ω.cm <sup>-1</sup> )	4.7 / 0.5 <sup>(○)</sup>				
R <sub>sh</sub> (Ω.cm <sup>-1</sup> )	365 / 800 <sup>(○)</sup>				

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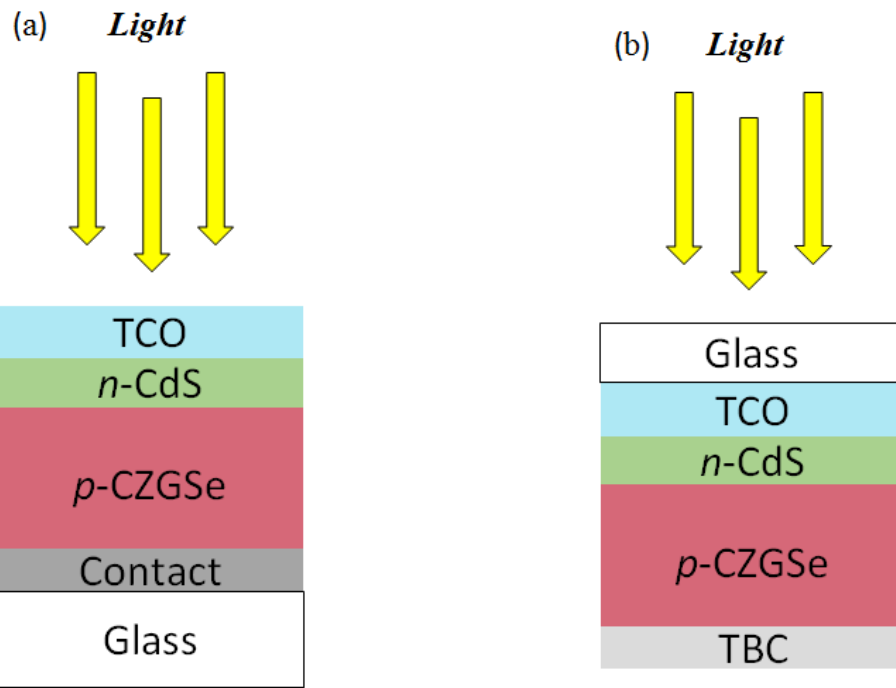
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Table S2: Parameters used in the simulations at standard solar cell test conditions.

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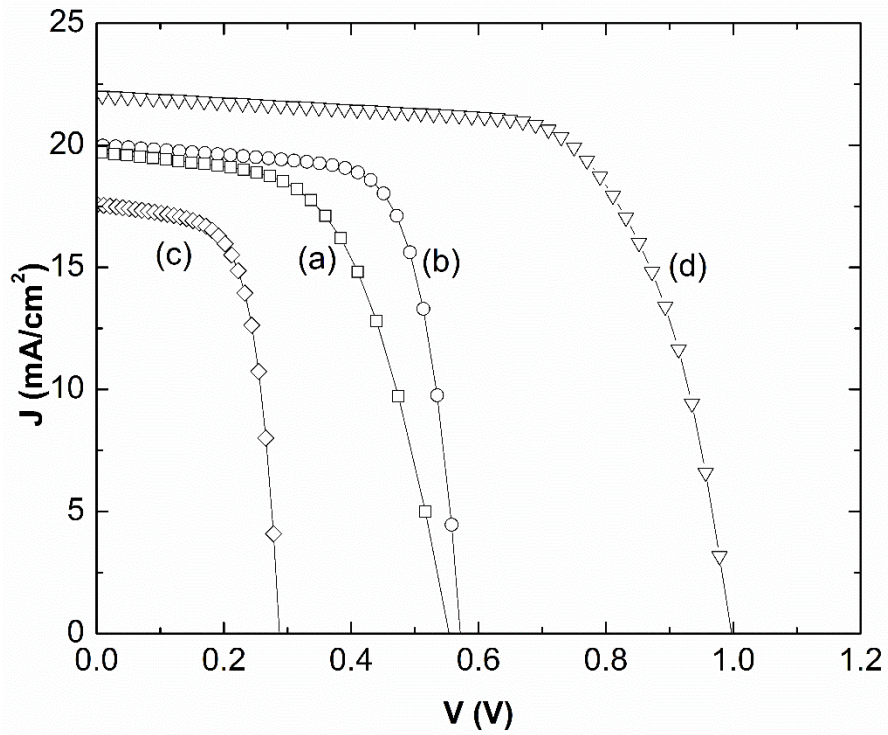
<sup>(○)</sup> Optimized parameters.

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Figure S5: Schematic of the two different configurations considered in the device simulations: (a) substrate and (b) superstrate.



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2 Figure S6: Calculated  $J(V)$  curves for different substrate/superstrate configurations: (a)

3 substrate =  $\text{Cu}_2\text{ZnGe}(\text{S},\text{Se})_4/\text{MoSe}_2/\text{Mo}/\text{glass}$ , (b) same configuration as (a) but using

4 optimized device simulation parameters (see Table S2), (c) superstrate =

5  $\text{Cu}_2\text{ZnGe}(\text{S},\text{Se})_4/\text{TCO}$ , and (d) superstrate =  $\text{Cu}_2\text{ZnGe}(\text{S},\text{Se})_4/\text{MoO}_3/\text{TCO}$ . For

6 configurations (c) and (d) also optimized parameters were used in the device simulation.

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