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Static Hysteresis modelling of FeSi NO sheets in rolling and transverse directions

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Context and objectives

- 1. predict magnetic losses or magnetic weveforms in NO FeSi sheets when excited in both rolling (RD) and transverse direction (TD).
- 2. Need for a vectorial hysteresis model
- 3. Modification of the vector play model [1] improved by [2]

Original isotropic Model

$$\mathbf{h} = \mathbf{h}_{re} + \mathbf{h}_{ir} \tag{1}$$

$$\mathbf{h}_{re} = \sum_{k=1}^{N} \omega_k \mathbf{h}_{re}^k \qquad (2)$$

$$\mathbf{h}_{re}^k = \begin{cases} \mathbf{h}_{re0}^k & \text{if } ||\mathbf{h} - \mathbf{h}_{re0}^k|| < \chi^k \\ \mathbf{h} - \chi^k \cdot \frac{\mathbf{h} - \mathbf{h}_{re0}^k}{||\mathbf{h} - \mathbf{h}_{re0}^k||} & \text{otherwise} \end{cases}$$

$$(3)$$

$$\mathbf{M} = M_{an}(||\mathbf{h}_{re}||) \cdot \frac{\mathbf{h}_{re}}{||\mathbf{h}_{re}||}$$

$$\mathbf{b} = \mu_0(\mathbf{M} + \mathbf{h})$$
(5)

$$\mathbf{b} = \mu_0(\mathbf{M} + \mathbf{h}) \tag{5}$$

- χ^k : maximum pining field of the k^{th} cell
- ω_k : weight of the k^{th} cell

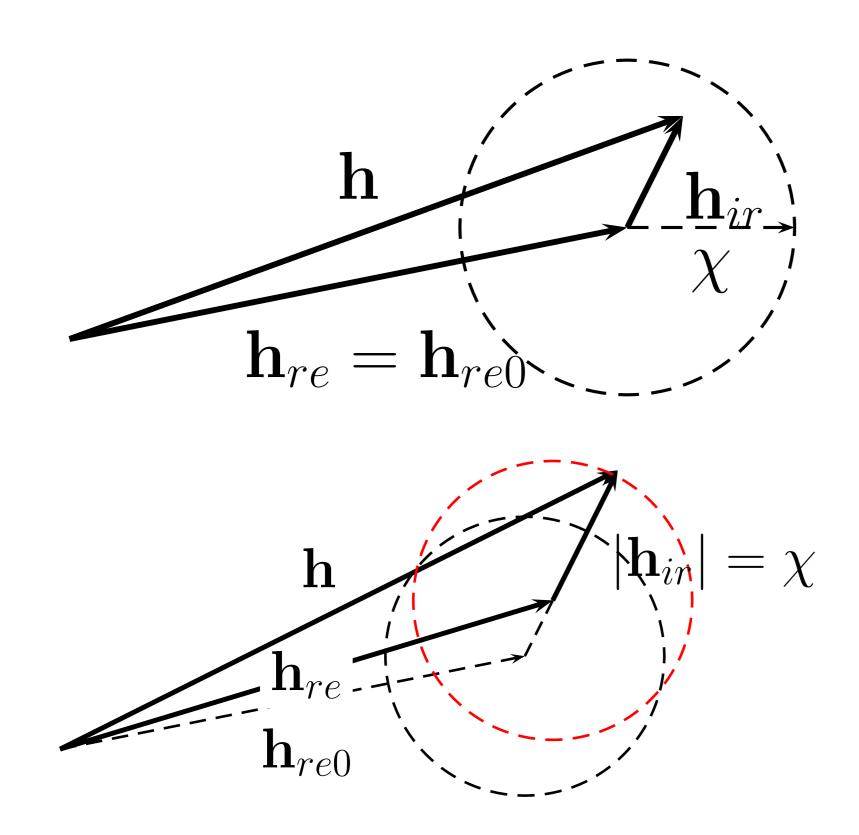


Figure 1:Example of the two situations of (3)

Modifications to include anisotropy

Modifications prosposed in [3] to take into account magnetic anisotropy in FeSi NO sheets.

1. Modifications of the anhysteretic curve (4)

$$\mathbf{M} = M_{an}(||\mathbf{h}_{re}||)G(\gamma)\frac{\mathbf{h}_{re}}{||\mathbf{h}_{re}||}$$
(6)

with γ , a scalar parameter to identify

$$G(\gamma) \frac{\mathbf{h}_{re}}{||\mathbf{h}_{re}||} = \begin{bmatrix} 1 & 0 \\ 0 & \gamma \end{bmatrix} \begin{pmatrix} \mathbf{e}_{RD} \\ \mathbf{e}_{TD} \end{pmatrix}$$
(7)

2. Modifications of the coercivity (pining field) by making cells ellipsoidal.

$$\chi^k(\alpha,\beta) = \chi^k_{RD} \left(1 + (\beta-1)\left(1-\alpha^2\right)\right) \tag{8}$$
 with :

- ullet β : a scalar parameter to determine
- χ_{RD}^{k} : pining field of the kth cell in RD.
- α : cosine of the angle between $\mathbf{h} \mathbf{h}_{re0}^k$ and \mathbf{e}_{RD}

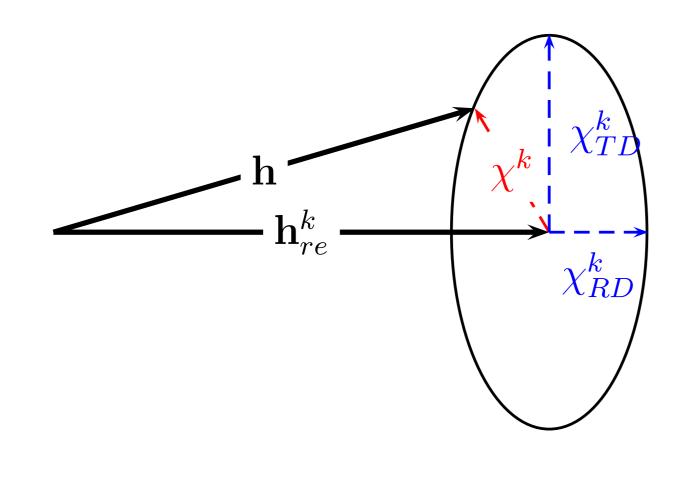


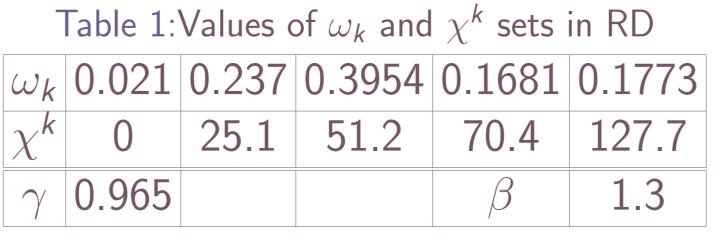
Figure 2: Illustration of ellispoidal spheres

Tested material and methods

- FeSi 3%wt 0.5 mm thick non oriented material
- Characterizations have been made by CADEMA group from Torino for the TEAM32 problem [4]
- Several static loops were measured on Epstein device along different angles with respect to RD for different amplitudes.
- Loops measured at RD and TD are used for tests and identification of parameters.
- Loops at intermediate directions are only used for tests.

Identification Results

the (ω_k, χ^k) sets have been identified following the protocol described in [5].



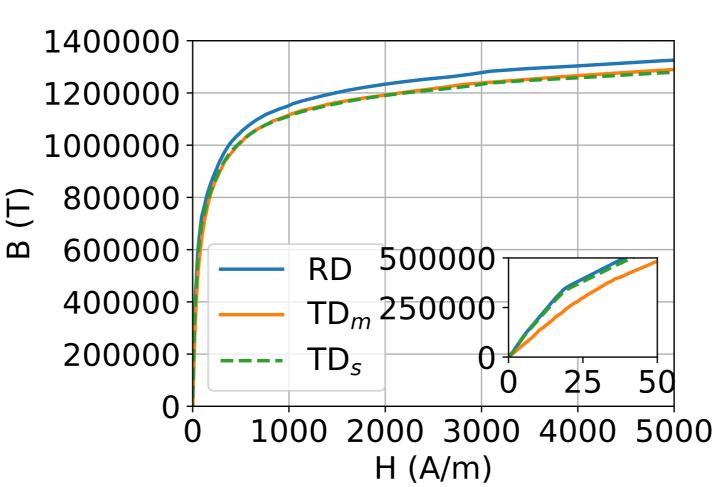


Figure 3: Measured and simulated anhysteretic functions in RD and TD

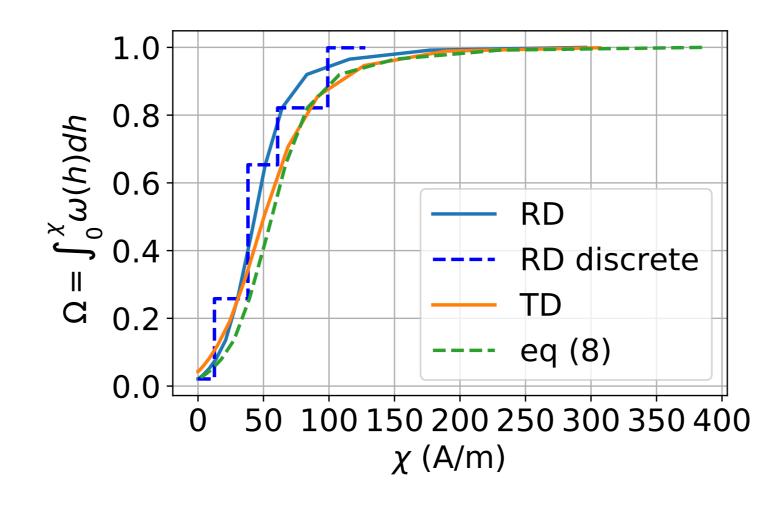


Figure 4: Cumulative distribution of the weights versus pining field in RD and TD and result of eq (8)

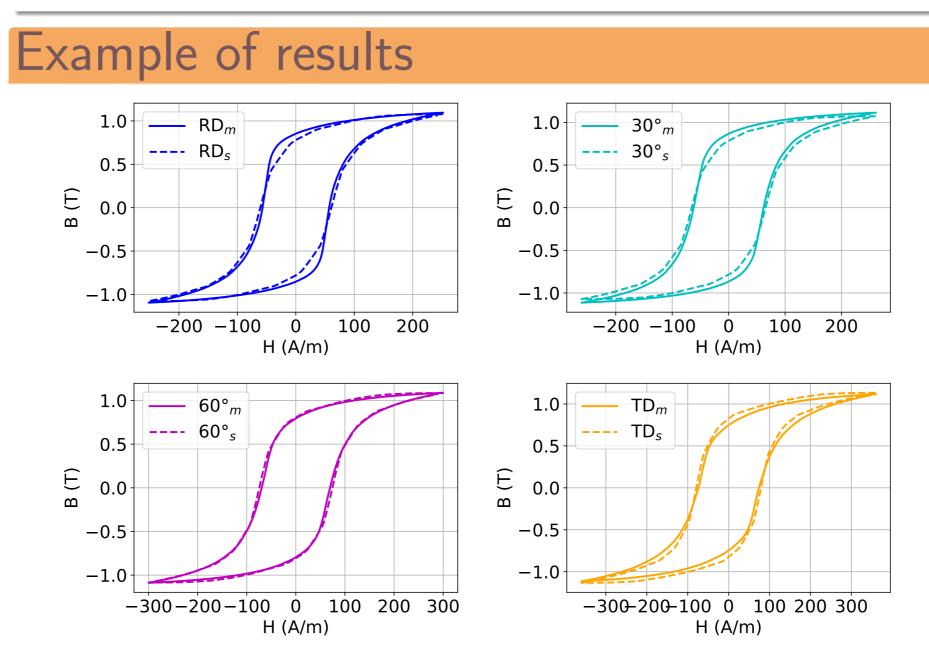


Figure 5: Comparison of measured and simulated loops at 1.1 for different angles

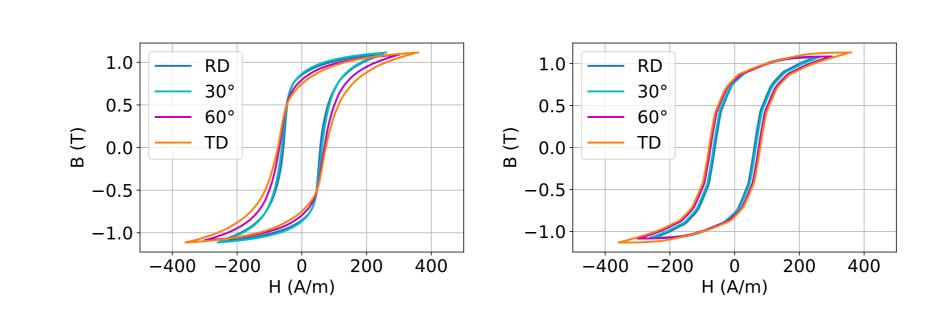


Figure 6: Measured (left) and simulated (right) loops at 1.1 T for different angles

Accuracy analysis of the loops

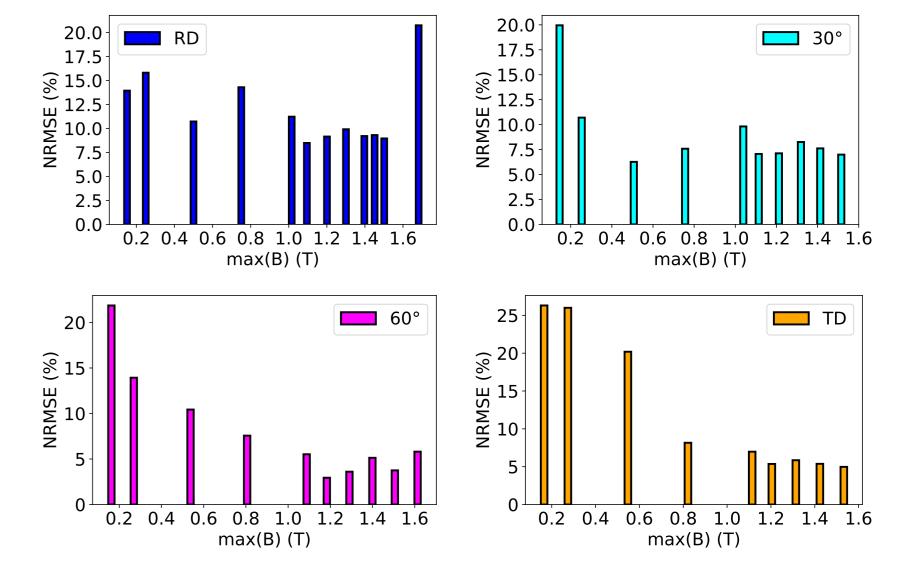


Figure 7: Accuracy versus amplitude of the loops in each direction

behavior of the losses vs angle

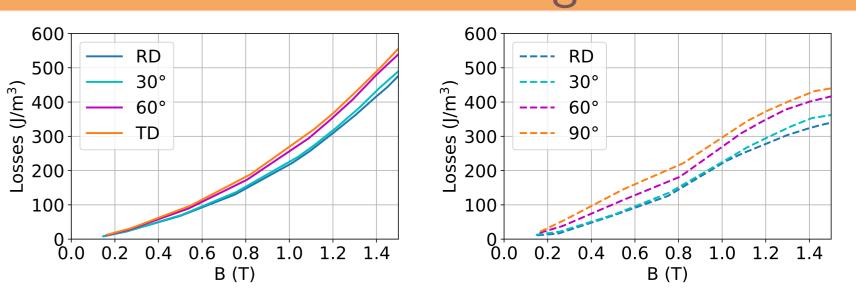


Figure 8: Measured (left figure) and simulated (right figgure) losses vs B_{max} for different angles

Discussion

Accuracy in RD is not so good for two reasons:

 coercivity can not be considered as constant along the $M_{an(H_{an})}$ curve.

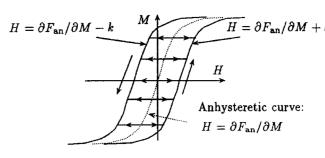


Figure 9:Assumption to respect[1]

- identification of first cells following [5] may be inaccurate. Following [6] can improve accuracy in this region as recently shown in [7].
- Proposed modifications are sufficient to qualitatively take into account of the anisotropy
- Losses behaviour vs angle is quatitatively well retrieved. Accuracy of computed losses should be improved.

Conclusions and perspectives

- A readily vectorial hysteresis model including anisotropy has been tested.
- Better identification of (ω_k, χ^k) or/and improvements of the original model must be made (constant coercivity assumption) for FeSi materials
- More complex modifications can be imagined to improve the accuracy such as

$$\mathbf{M} = \begin{pmatrix} M_{an_{RD}}(||\mathbf{h}_{re}||) \\ M_{an_{TD}}(||\mathbf{h}_{re}||) \end{pmatrix} \frac{\mathbf{h}_{re}}{||\mathbf{h}_{re}||}$$
(9)

- inverse the model to have **h(b)**
- Test this approach with FeSi GO materials

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