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# Static Hysteresis modelling of FeSi NO sheets in rolling and transverse directions

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### Context and objectives

- predict magnetic losses or magnetic weveforms in NO FeSi sheets when excited in both rolling (RD) and transverse direction (TD).
- 2. Need for a vectorial hysteresis model
- 3. Modification of the vector play model [1] improved by [2]

# Original isotropic Model

 $\mathbf{h} = \mathbf{h}_{re} + \mathbf{h}_{ir}$ 

# FeSi 3%wt 0.5 mm thick non oriented material Characterizations have been made by CADEMA group from Torino for the TEAM32 problem [4] Several static loops were measured on Epstein device along different angles with respect to RD

- for different amplitudes.
- Loops measured at RD and TD are used for tests and identification of parameters.
- Loops at intermediate directions are only used for tests.

## 





χ<sup>k</sup>: maximum pining field of the k<sup>th</sup> cell
ω<sub>k</sub>: weight of the k<sup>th</sup> cell





Identification Results the  $(\omega_k, \chi^k)$  sets have been identified following the protocol described in [5].

Table 1:Values of $\omega_k$ and $\chi^k$ sets in RD					
$\omega_k$	0.021	0.237	0.3954	0.1681	0.1773
$\chi^{k}$	0	25.1	51.2	70.4	127.7
$\gamma$	0.965			$\beta$	1.3



Figure 3:Measured and simulated anhysteretic functions in RD and TD



Figure 7:Accuracy versus amplitude of the loops in each direction

#### behavior of the losses vs angle



Figure 8:Measured (left figure) and simulated (right figgure) losses vs  $B_{max}$  for different angles

#### Discussion

- Accuracy in RD is not so good for two reasons:
  - coercivity can not be considered as constant along the  $M_{an(H_{an})}$  curve.



Figure 9:Assumption to respect[1]

• identification of first cells following [5] may be inaccurate. Following [6] can improve accuracy

Figure 1: Example of the two situations of (3)

#### Modifications to include anisotropy

Modifications prosposed in [3] to take into account magnetic anisotropy in FeSi NO sheets.

1. Modifications of the anhysteretic curve (4)

$$\mathbf{M} = M_{an}(||\mathbf{h}_{re}||)G(\gamma)\frac{\mathbf{h}_{re}}{||\mathbf{h}_{re}||}$$
  
with  $\gamma$ , a scalar parameter to identify  
$$G(\gamma)\underline{\mathbf{h}_{re}} = \begin{bmatrix} 1 & 0 \end{bmatrix} \begin{pmatrix} \mathbf{e}_{RD} \end{pmatrix}$$

$$\frac{\mathbf{G}(\gamma)}{||\mathbf{h}_{re}||} = \begin{bmatrix} 0 \ \gamma \end{bmatrix} \left( \mathbf{e}_{TD} \right)$$

2. Modifications of the coercivity (pining field) by making cells ellipsoidal.

 $\chi^k(lpha,eta) = \chi^k_{RD} \left(1 + (eta - 1) \left(1 - lpha^2\right)\right)$  (8) with :

Figure 4:Cumulative distribution of the weights versus pining field in RD and TD and result of eq (8)

#### Example of results

(6)

(7)



in this region as recently shown in [7].

- Proposed modifications are sufficient to qualitatively take into account of the anisotropy
- Losses behaviour vs angle is quatitatively well retrieved. Accuracy of computed losses should be improved.

#### Conclusions and perspectives

- A readily vectorial hysteresis model including anisotropy has been tested.
- Better identification of (ω<sub>k</sub>, χ<sup>k</sup>) or/and improvements of the original model must be made (constant coercivity assumption) for FeSi materials
- More complex modifications can be imagined to improve the accuracy such as

$$\mathbf{\Lambda} = \begin{pmatrix} M_{an_{RD}}(||\mathbf{h}_{re}||) \\ M_{an_{TD}}(||\mathbf{h}_{re}||) \end{pmatrix} \frac{\mathbf{h}_{re}}{||\mathbf{h}_{re}||}$$
(9)

 ${\boldsymbol \bullet}$  inverse the model to have  ${\boldsymbol h}({\boldsymbol b})$ 

• Test this approach with FeSi GO materials

β : a scalar parameter to determine
χ<sup>k</sup><sub>RD</sub> : pining field of the k<sup>th</sup> cell in RD.
α : cosine of the angle between h – h<sup>k</sup><sub>re0</sub> and e<sub>RD</sub>



Figure 2:Illustration of ellispoidal spheres

Figure 5:Comparison of measured and simulated loops at 1.1 T for different angles



Figure 6:Measured (left) and simulated (right) loops at 1.1 T for different angles

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