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INTELLIGENT MODELING OF WOVEN MATERIALS

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ABSTRACT

This paper shows the particular application of the general approach "Intelligent Optimal Design" to the design of a woven composite material used o make radomes and for which the mechanical and electromagnetical properties have to satisfy special properties. Although the design of such a material needs the control of almost 50 design parameters, with a very limited number of examples of materials in the data base, but with a special description of each material, it is possible to extract the rules necessary to predict the behaviour of any new material with a rather good accuracy and thereafter, to reach the optimal design (minimum cost) associated to any new requirements.

INTRODUCTION

Due to the economical and safety considerations, the engineers are forced to find the optimal design of their structures when multiphysical aspects have to be considered. Although they have sophisticated experimental set-ups, beautiful theories/models and powerful numerical tools, usually, they can not afford to realize several tests or simulations to extract the "best" case and they have to face still several lockings in their industrial world:

• no satisfactory constitutive modeling of materials, no real control of the accuracy of the numerical simulations, no real definition of the initial state and/or the effective loading of the structure

• no insurance to have noted and measured the main signals during the tests or the returns of experiments, usually, no perfect repetability of the tests

• the results predicted by the theories/models are often very far from the experimental ones.

These problems have no a complete solution as the experts do not understand them in their whole. "Copyright © 2000 by the American Institute of Aeronautics and Astronautics, Inc. All rights reserved" Moreover, the available data are often not statistically representative (limited number), fuzzy, qualitative and missing in part.

To overcross these lockings, the actual best knowledge of the researchers/experts have to be intelligently mixed with the results of experiments or real returns.

That it is why, a new approach "the intelligent optimal design of materials and structures" was elaborated, see full details in the book J. Zarka et al (2000). In this approach it is needed:

i) to build a DATA BASE of examples i.e. to obtain some experimental, real or simulated results where the EXPERTS indicate all variables or descriptors which may take a part. This is, at first, done with some PRIMITIVE descriptors \boldsymbol{x} , which are often in a different number and different types for each example. Then, the data are transformed with the introduction of some INTELLIGENT descriptors XX, with the actual knowledge whole thanks to (but usually insufficient) beautiful theories and models. These descriptors may be number, boolean, strings, names of files which give access to data bases, or treatments of curves, signals and images. Now, for all examples, their number and their type are always the same which is the only one way to allow the fusion of data. The results or conclusions may be classes (good, not good, ...) or numbers.

ii) to generate the RULES with any Automatic Learning Tool (based on logical rules, statistics, machine learning, numerical learning, fuzzy logic, neural networks...). Each conclusion is explained as function or set of rules of some among the input intelligent descriptors with a known reliability or accuracy.

iii) to optimize at two levels (Inverse Problems):

• considering the intelligent descriptors as independent; it is possible to get the OPTIMAL SOLUTION satisfying the special required properties and allowing the DISCOVERY OF NEW MECHANISMS,

• considering the intelligent descriptors linked to primitive descriptors for a special family; it is possible to obtain the optimal solution which is technologically possible.

So, not only a Practical Optimal Solution is obtained but also the Experts may learn the missing parts, may build models or theories based only on the retained intelligent descriptors and guided by the shapes of the rules or relationships.

Composites are more and more often used in the mechanical engineering, the civil engineering, the automotive, the aeronautical and the naval industries. It is necessary to reduce their acquisition cost while improving the life cycle and safety of the structures.

Many general contributions have been made to understand the physics and to develop models for the mechanical, electromagnetical global properties of aggregates during the modeling which is called homogenization. Simplified models, simple bounds of the properties or and even sophisticated theories ... were produced.

In the case of the woven composites, idealized geometry and even numerical finite element methods due to the complex geometry, were also done. The simulated results are sometimes near from the real experimental ones, but very often they do not give sufficient elements to be used into the real design.

This design implies a multiphysics problem: how to design the optimal woven composite (i.e. to give the composition and the process) for any special application when, only a few tests are available (due to the cost in money and time) and when the simulated predictions are not reliable.

Textile composite materials are woven fabrics with more efficient properties than layered composites. The description of the process is rather difficult: fibers are used to make bundles which are then intertwined according several types.

Here, we consider only a special hybrid woven composite where in one bundle one or two fibers are used and where one or two bundles are used for the warp and the fill in one layer. The geometrical description for the layer was given by the University of Technology of Compiègne. All the fabrics are made with 16 identical layers.

BUILDING THE DATA BASE

Eleven different fibers are available. Each fiber is fully characterized from a data base of materials. Only one resin is used and characterized.

	L										
	COOL ST.								10.300.000 N	2202	(799) (799)
E_trac_F	73	55	86 ¹	85	72	14	2.48	3.5	104.3	100	
Polsson F	0.17	0.2	0.2	0.2	0.2	0.4	0.2	0.2	0.2	0.2	0.
Permittivity_F	6.13	4	61	3.9	3.78	3	2.08	3.1	3.3	2.2	3.
Spec Mass F	1 2.59	2.14	2.53	1.8	2.2	1.38	2.1	1.3	1.41	0.97	1.2
Spec_Price_F	50	450	175	250	900	35	600	1000	900	750	1000
	RESIN		I	i	ľ	! [1	1	
E_trac_R	3.52		1	1	- 1	1			1	I	
Poisson_R	0.3		1		1	1		1	1	1	
eps R	2.6		1	1		1	i	l l	1)	
tg_perte_R	4		1	1	1	1	·		1	1	
Spe Mass R	1.05		1	1	1	1	1		1	1	
Spe Price R	786		1		1	1			1	1	

Figure 1: Data for the basic elements



Figure 2: Position of the bundles in the fabric



Figure 3: Definition of microscopic parameters **PRIMITIVE DESCRIPTION**

The composite materials are all equilibrated fabrics with a constant step of 2: i.e. the two bundles in the warp and the fill are the same. Usually, the fabric is characterized by the macroscopic parameters:

• Porosity (x%) (rather difficult to control !)

• Nature of fibers (Glass, Peek..among the selected eleven fibers)

• Total_weight of fibers per unit surface in one layer (zzz gr)

Hybridation_massic_ratio for the two
bundles

$$Tx \ 1 = \frac{mass \ (fiber \ 1)}{mass \ (fiber \ 1) + mass \ (fiber \ 2)}$$

$$Tx 2 = \frac{\text{mass (fiber 2)}}{\text{mass (fiber 1) + mass (fiber 2)}}$$

Thickness of the fabric

• Nature of the resin (here only one). For this special problem, there are 49 active design parameters (twice {22 for each fiber: 0 or 1 selected or not, the concentration, with the number of fibers in the bundle}) + 5 for the process.

NUMB_FIBERS	PEI	PEHT	Vectran HS	PEEK	PTFE	Polyetter	Silica	Glass S2	Glass_R	Gines_0	Giass E
	0	े ¹ 1	· 0	0	σ	0	0	0	0	e	0
	84.25	80,46	75.93	79.00	75.02	80.08	76.66	73.74	75.95	85.05	77.93
						BUNDLE 2	TERS FOR I	ACTIVE PARAMI			
NUNB FISERS	PEI	PEHT	Vectran HS	PEEK	PTFE	Palyester	Silice	Gians S2	Glass_R	Glass_D	Glass E
		i de la c		0	0	0	0		0	.0	.0
	84.25	80.46	75.03	79.00	75.02	80.08	76.66	73.74	75.95	.05.95	77,63
				ic	THE FABR	METERS FOR	CTIVE PARA				
						10	orosity	P			
						180	rammage	G			
						65	ybridB1	9			
						35	ibrid92	Ĥ			
							distant and	*			

Figure 4: Primitive active design parameters **A Design of Experiments (DOE) is impossible**. Indeed, only sixteen woven composite materials were ordered. At the AIA/CP, they were, then, mechanically characterized according the classical normalized tests: the resistance and the elastic modulus in tension, as in compression, flexion, and

shearing, are defined and measured. The fabrics were also electromagnetically

characterized: the dielectric constant and the loss tangent are measured.

At last, at UTC, some microscopic parameters were measured by cutting the fabric:

- A_{v1}: width of the first bundle
- A'_{v2} : width of the second bundle
- H.: height of one wave of fibers

• HH: height of one layer (the thickness of the fabric is here 16 x HH).

rel_CVR	Hybridation %	Total_wei_fibers	T VF %	I MR %	porosity	Ayt	Ay2	нн	HT	
2628	100% Silice (SiC2)	270.00	46.30	35.60	000	0.59	0.59	029	0.27	
2529	100%/Glass_E	290.00	54.80	25.40	1.06	1.90	1.90	031	031	
2397	100%Gloss_D	260.00	47.60	34.80	000	0,96	096	0.26	026	
2407	52% Stice#48% Polyester	160.00	51.70	33.80	5.88	0,58	0.80	0.18	81.0	
2414	54.5% Gloss_E /46.5% Polyester	253,00	48.00	36,70	5.69	0.58	0.53	0.28	0.25	
2412	51,5% Glass_D/48,5% Polyester	273,00	\$1.10	3400	1.96	0,57	0.56	028	027	
2408	64% Silicay36% PEHT	254.00	49.30	40.70	13.38	0.63	0.55	0.33	0.30	
2418	75.2% Gass_\$2/248 PEI	246.00	5430	35.80	256	0.62	0.71	0.29	0.29	
2419	45% Gloss_S2/55PEHT	262.00	48.90	43.50	3.02	0,63	061	0.38	0.33	
2420	100% Vectron	270.00	47.00	43.80	6.55	092	0.92	0.41	037	
2475	71,8% Sillog/28.2% PEI	265.00	49,10	3620	7.89	0.62	0,70	0.29	027	
2470	73.4% Goss_E/30.6% PEEK	260.00	48.30	3490	6,62	0.74	0.59	026	024	
2471	59% Gloss_D/31% PEEK	260,00	50,90	3610	6.80	0.62	0.55	026	0.24	
2474	59.7% Silice/40.3% PTFE	253,00	54.60	28,60	9,63	1.00	0.95	0.25	0,25	
2478	60% Sillow 25% PTFE/15% PEEK	267,00	45.30	38.30	0.00	0.63	066	026	023	
2484	65% Glass_D/10,5% Vector v24.5% PEHT	259,00	48.60	41.10	7.14	078	0.55	0,34	0,31	
			1							

TVF=Volumetibas

TMR =Resincontent in% waight

sigma_t Ec ref CVR Et sigma_c Ef sigma_f \$13 eps tg_loss 347.00 1940 2628 15.40 102.00 15.60 169.00 18.70 2.89 0.003 2529 24.70 443.00 23.40 186.00 21.10 293.00 27.60 4.39 0.011 2397 11.50 245.50 15.50 118.20 12.50 223.20 18.10 3.20 0.006 2407 13.40 324.70 16.50 82.20 11.10 162.30 11.20 3.03 0.004 2414 11.00 225.00 13.60 143.00 15.00 3.62 0.010 81.00 11.50 90.90 12.40 2412 9.90 196.00 13.80 157.00 14.90 3.22 0.005 2408 12.30 47.00 11.50 8.00 342.00 13.90 88.80 2.64 0.002 2418 10.60 283.00 13.30 83.00 12.00 150.00 16.90 3.16 0.012 2419 0 00 351.00 13.00 63.50 14.40 123.00 13.50 2.94 0.015 2420 11.80 417.00 12.50 46.00 14.10 156.00 10.70 2.85 0.003 2475 13.20 90.00 13.50 139.00 16.40 2.94 0.003 342.00 16.80 2470 15.20 260.00 15.20 88.00 13.80 149.00 17.00 3.82 0.009 2471 10.00 162.00 10.00 84.00 9.30 133.00 14.30 3.10 0.007 9.80 2.82 83.00 12.80 2474 14.30 325.00 15.10 158.00 0.005 2478 12.30 303.00 14.00 68.00 14.50 127.00 13.20 2.76 0.006 2483 15.00 305.00 14.80 63.00 13.00 128.00 13.20 3.33 0.010 2484 13.20 218.00 13.20 59.00 13.20 119.00 12.70 2.84 0.004

Figure 5: Experimental data on the woven fabrics

INTELLIGENT DESCRIPTION

It is impossible with the classical mathematical tools of data analysis to represent these results. There is no enough tests. We need to be able to make the fusion of the different fibers in the bundles and of the different fabric parameters. For that, we use the actual knowledges.

• For one bundle i.e. one dimensional composite, analytical approximated models for the elastic and electromagnetic properties are available.

This is also the case for layer with straight bundles.
As a rough approximation, at first, it was assumed that the woven fabric is assimilated to a layered material with the warp in one layer and the yarn in the other layer with a 90 ° angle.

• Then, quasi-analytical models and finite element based models were also built. (the calculations of the elastic properties were made in one internal report of UTC based on the Ishikawa and Chou's works.

• For the electromagnetic properties, we use for one fiber, the Bruggeman's model and for two different fibers, the Kingery's model.

Even if these simulated results are not very well representative of the experimental values on the fabrics, they allow to make the fusion and to help the learnings.

The set of the values predicted by these models are here our intelligent descriptors.

Successively, for each case or material, described by its active design parameters or primitive descriptors, we have analytically, the mass and the price of the fabric, and the bundles properties. We compute these intelligent descriptors based on the models for layered composites and woven composites.

AUTOMATIC LEARNINGS

Once the data base of examples has been created within its intelligent description, it is possible to learn the various conclusions as functions of these intelligent descriptors. More than that, we were able to learn the intelligent descriptors directly from the primitive descriptors as functions of functions. For this special problem, we used general regression net or polynomial net in NeuroShell from Wards systems. They are both based on numerical learnings.

Then, after all these learnings, we are able to compute the other intelligent descriptors:

· for the process

 A_{y_1} first bundle , A_{y_2} second bundle H, wave of fibers, HH one layer.



MASS and PRICE OF THE WOVE From exact analytical entrovisions	N COMPOSITE MATER	UAI.		
Viot	4000.00	Vfib+Vre4	3924.00 Vrea	2425,63
M6b1	3146.58	Vfibl	781.11 Mres	2546,91
M6b2	1640.34	Viib2	1024.15	
Mass_comp	569349	Price comp	3889.82	

Figure 7: Evaluations for microstructure and price • for the layers with straight bundles

EXM1, EYM1, NUXYM1, NUYXM1, GXYM1 EXM2, EYM2, NUXYM2, NUYXM2, GXYM2 for the fabric

Eps_th, simulated permittivity

Exy_th, Poisson_th and Gxy_th simulated elastic coefficients.

We build these descriptors for all the 16 examples.

		SIMULATE	DELAST	PROPERT	Es	[
FOR LAYE	R WITH STR	AIGHT BUNI	DLE 1		FÖR FAVER	พกษราสัง	NGHT BUNDLE ?	<u>(</u>
EXM1	4.1516175	۱ 			 	EXM2	7.44831496	
EYM1	4.13247603					EYM2	4.39191131	
NUXYM1	0.22352363			 			0 24199844	
NUYXMI	0.22249305					NUYXM2	0.14269478	
GXYM1	1.84063346,			<u> </u>		GXYM2	1.96926104	
SIMULATED	electroma	ANETIC PRO	PERTIES FOF	THE FABRIC				
Volbund 1	1024.15284		1		F	1		
Volbund2	885.35213			1	I.	1		
Eps fib1	2.08			1	ł.	1		
Eps_fib2	208			+-	[1		
Eps th	2.84912875	L		+				

Figure 8: Evaluations for straight bundle layers

SIMULATED	MECHAN	CALF	ROPERTIE	S FO	R THE WOVE	NCOMPOSITE MATE	RIAL
Mass_resin	2546.91	Min	1296.00	Max	4710.00		1
Porosity	0.02	Min	0.00	Max	0.13	1	1
al	0.80	Min	0.50	Max	2.00	-	1
a2	0.65	Min	0.50	Max	2.00		
НТ	0.21	Min	0.17	Max	0.50	Exy_th	13.39
нн	0.25	Min	0.18	Max	0.41		
EXMI	4.15	Min	39.69	Max	78.95	Gxy_th	3,88
EYMi	4.13	Min	15.94	Max	24.79		
NUXYMI	0.22	Min	0.21	Max	0.22	Poisson_th	0.19
NUYXMI	0.22	Min	0.06	Max	0.10		
GXYMI	1.84	Min	6.38	Max	10.11		
EXM2	7.45	Min	2.75	Max	78.95		
EYM2	4.39	Min	2.71	Max	24.79		
NUXYM2	0.24	Min	0.21	Max	0.30		1
NUYXM2	0.14	Min	0.06	Max	0.25	1	1

Figure 9: First evaluations for the woven fabric

Then, we can after all these learnings, give the

prediction for the real measured experimental conclusions or values of the fabric: Ft, Fsigmat, Fc, Fsigmac, Ff, Fsigmaf, FS13, Eps and t Tg-loss.

FINAL PREDIC	TIONS								- 1			
Mass_resin	2546.91	Min	1000.00	Max	4710.00				1			
Porosity	0.02	Min	0.00	Max	0.13							
al	0.80	Min	0.50	Max	2.00							
a2	0.65	Min	0.50	Max	2.00							
нн	0.25	Min	0.17	Max	0.50	-						
нт	0.21	Min	0.18	Max	0.41							
EXMI	4.15	Min	39.69	Max	78.95							
EYM1	4.13	Min	15.94	Max	24.79							
NUXYMI	0.22	Min	0.21	Max	0.22							
NUYXMI	0.22	Min	0.06	Max	0.10							
GXYM1	1.84	Min	6.38	Max	10.11							
EXM2	7.45	Min	2.75	Max	78.95							
EYM2	4.39	Min	2.71	Max	24.79							
NUXYM2	0.24	Min	0.21	Max	0.30				'			
NUYXM2	0.14	Min	0.06	Max	0.25							
GXYM2	1.97	Min	1.1.1	Max	10.11							
Exy_th	13.39	Min	10.90	Max	28.32							
Gxy_th	3.88	Min	3.15	Max	6.96							
Poisson_th	0.19	Min	0.13	Max	0.21							
eps_th	2.85	Min	2.68	Max	4.29		_					
PREDICTEDE	FORROTH	NET	COROPERTIE	S FOR THE	WOVENC	OMPOSITE	МА	TERIA	J .	<i>4</i> •	9 165)	en.
eps	1.88	1	tR_loss	0.01		1						
PREDICTED M	 ECHANICAL	 _PROI	i Perties for	i The Wov	EN COMPO	SITE MATI	 ERL/	NL.				
FL	73.73		Fc	1.41		Ff			0.01			
Fsigmat	1765.37		Fsigmac	205.70		Fsigmaf	10	1147	5.51			
FS13	41.49		ļ .				Τ					

Figure 10: Final predictions for the woven fabric

OPTIMAL DESIGN OF THE WOVEN FABRIC

Indeed, this approach allows to go much further and to answer to the real problem: we have to design the fabric such that its mechanical end electromagnetic properties satisfy some requirements.

We may assume that, for economical reasons, this fabric must be obtained at the lowest price but any other objective function may be taken. This optimization problem is very difficult as, here also, there is no convexity of the functions, moreover, even if we have a reasonable representation of the functions this is not the case of their gradient. Only particular algorithms may be used. However, as all our functions are represented analytically (polynomial functions), and do not imply any new finite element analysis or test, the time to evaluate them is very short even within the program EXCEL. We use the add-on Genehunter of Wards Systems to have the total integration of this Optimal Design of the Woven Fabric.

It is elementary to introduce any new constraint on the design variables or on the conclusions or between the conclusions by referencing the particular cells.



JEOR - Jed a

Figure 11: Intelligent optimal design tool Acknowledgments

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