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# 17.2% efficiency $\text{CuIn}_{1-x}\text{Ga}_x\text{Se}_2$ thin-film based mini-module thanks to alternative architecture yielding 81% fill factor

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**Abstract.** An alternative to conventional  $\text{Cu(In,Ga)Se}_2$  module structure is proposed and experimentally investigated. This alternative module structure, which consists in applying metallic buses to connect monolithically adjacent cells in series, is likely to offer the opportunity of minimizing both optical and electrical losses observed in conventional module structure compared to small area cells. The fabrication process of such alternative modules is presented. The performances achieved are discussed in comparison with a standard small-area-cell elaborated simultaneously. Despite slightly lower output voltage per cell, the alternative module structure demonstrates an efficiency of 17.2% (with 81% fill factor), against 16.4% (with 75% fill factor) for the standard cell. This promising result opens new routes to decrease the gap observed between small-area-cells and industrial modules.

**Keywords:** CIGSe / thin-film solar cells / alternative module structure

## 1 Introduction

Photovoltaic technology based on chalcopyrite  $\text{Cu(In,Ga)(S,Se)}_2$  (CIGSe) polycrystalline thin films has recently achieved the outstanding efficiency level of 22.9% at the laboratory scale [1]. Nevertheless, there still exists a large gap between the performance of these small-area-cells and industrial modules. This gap originates, to a large extent, from the conventionally used monolithic cell interconnection. Indeed, the industrial module structure implies three patterns (labeled P1, P2 and P3) for series connections [2]. Even when optimal, this conventional structure unavoidably leads to the losses listed below:

- the active area is decreased because of the interconnection inactive zone (at least 10% of the total area);
- the sheet resistance of the window layer, generally made of  $\text{ZnO:Al}$  (AZO), has to be lowered down to about 5–10  $\Omega/\text{sq}$  to prevent increased series resistance. Increasing AZO thickness or free-carrier concentration induces additional photon absorption thus optical losses;
- the expected ohmic contact between the window layer and the  $\text{Mo/MoSe}_2$  is generally associated with increased series resistance.

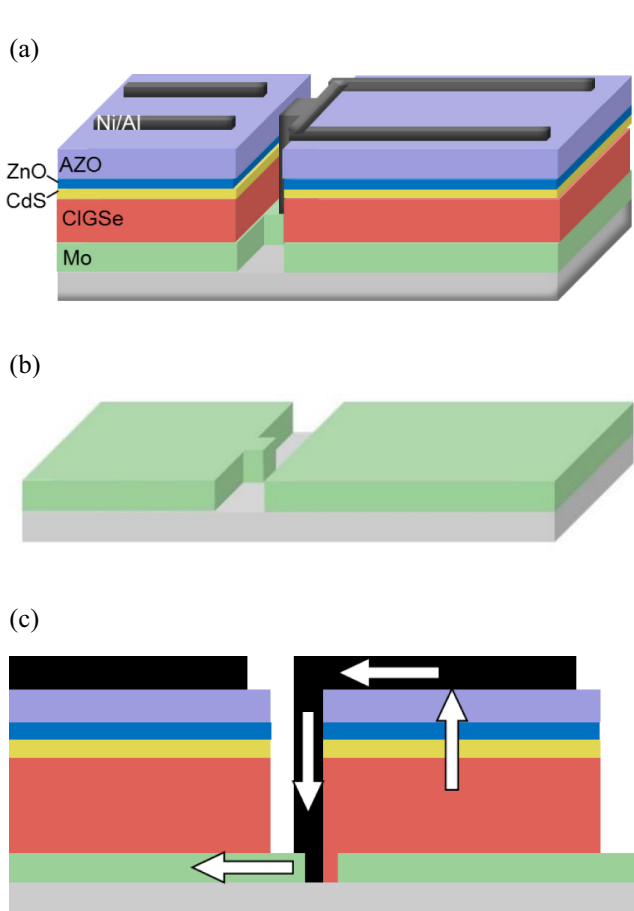
In order to overcome these limitations, we investigated an alternative module structure, already proposed by the University of Uppsala two decades ago [3,4] and starts being industrially implemented by Solibro [5]. This modified structure relies on the use of metallic grids to monolithically connect adjacent cells.

In the present study, we show that such an approach indeed allows solving, at the laboratory scale, most of the limitations mentioned above.

## 2 Description of the alternative structure

As illustrated in Figure 1, the basic concept of the alternative module structure consists of using metallic buses to ensure the electrical connection between the Mo-rear contact of a cell N to the  $\text{ZnO:Al}$  topping electrode of the adjacent cell. This approach allows keeping the  $\text{ZnO:Al}$  window layer as thin and resistive as for small-scale cells design. Moreover, the electrical contact between the Mo and the metallic bus is expected to be stable and weakly resistive. Finally, this structure requires a single mechanical patterning, performed after the device stack is completed, and before metallic buses are deposited. In the present study, we used electron gun evaporated  $\text{Ni/Al/Ni}$  buses, as for the small area cells. The Mo-back contact has been patterned using photolithography as described in the following section. The resulting etched

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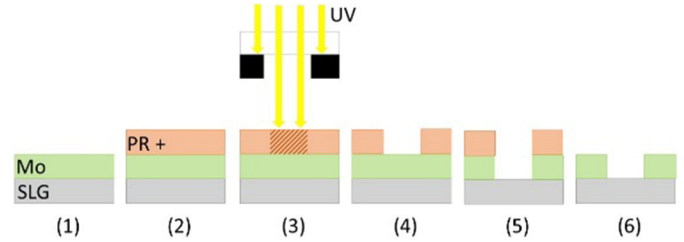
**Fig. 1.** Schematic representations (not to scale) of the alternative module with 3D view (a, b) and cross section (c). The top image shows the different layers: the metallic front contact (in black), the window ZnO/ZnO:Al (AZO) bilayer (in purple and blue), the CdS buffer layer (in yellow), the CIGSe absorber material (in red) and the Mo-back contact (in green). In addition, Figure 1b shows the patterned molybdenum layer. Figure 1c presents interconnection layout between two adjacent cells, the electrons flow is illustrated by white arrows.

line width is about  $150\ \mu\text{m}$  and complete in depth. A  $2\ \mu\text{m}$ -thick co-evaporated polycrystalline CIGSe thin film easily fills in the entire etched area.

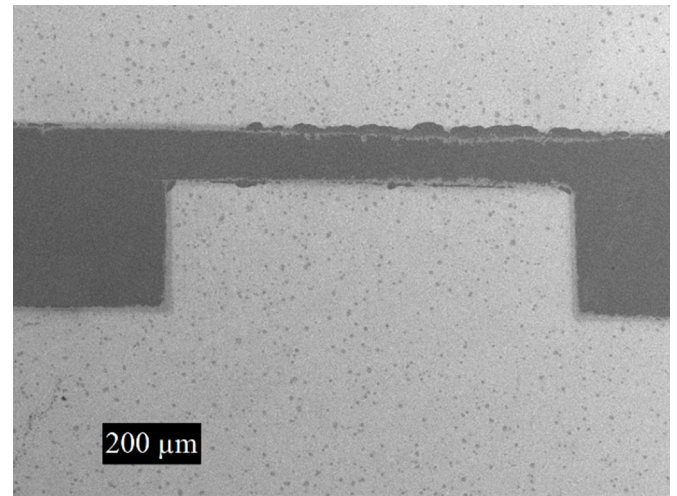
### 3 Mo rear-contact patterning

As illustrated in Figure 1, the fabrication of the alternative module structure firstly requires a specific patterning of the Mo layer. Photolithography was used to etch the back contact according to the required crenellated design. The different steps of this process are qualitatively illustrated in Figure 2 and the great lines of the experimental details are shortly described in the following.

Firstly, about  $4\ \mu\text{m}$  of positive photoresist is applied by spin-coating onto the Mo layer, and baked for 3 minutes. The UV-light exposure through the photomask and the development durations were empirically adjusted. The concentra-



**Fig. 2.** Illustration of the photolithography process. Glass/molybdenum substrates (1) are spin-coated with a positive photoresist (2). The resulting stack is exposed to UV light, throughout a laboratory-designed photomask (3). The soluble photoresist is washed away during the development (4). The unprotected molybdenum is etched with  $\text{K}_3[\text{Fe}(\text{CN})_6]$  solution (5). The unsoluble photoresist is finally removed in acetone (6).



**Fig. 3.** Scanning electron microscopy image (top-view) of a patterned molybdenum-coated substrate.

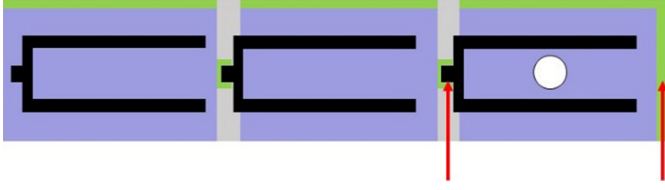
tion and pH of the etching solution ( $\text{K}_3[\text{Fe}(\text{CN})_6]$ ) were also optimized in order to achieve sharp, well-defined Mo-edges, as shown by the SEM image presented in Figure 3.

One should notice that, as already mentioned, the approach followed here aimed at using the same shadow mask for the metallic buses as that used for the grids of small size solar cells; therefore, the etched line width (about  $150\ \mu\text{m}$ ) shown in Figure 3 is far from the technological capabilities of the lithography actually employed in the field of silicon based microelectronics.

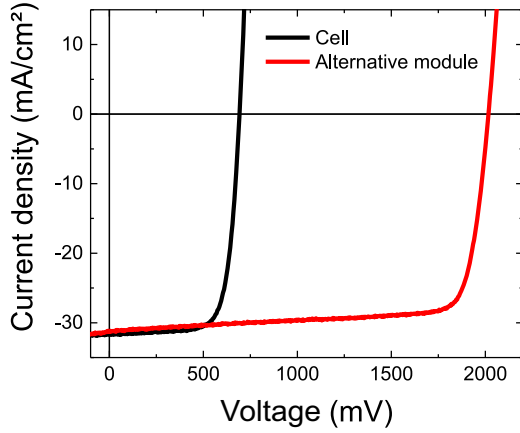
As a result, the series connection of adjacent cells is ensured by the metallic bus, contacting the Mo of the N-1 cell side and the AZO of the N cell side. For these first investigations, the alternative modules consisted of three connected cells (see Fig. 4).

### 4 Fabrication of devices

Both small size cells and alternative modules were fabricated on 1 mm-thick soda lime glass (SLG) coated with 400 nm-thick DC-sputtered Mo-layer. Independently



**Fig. 4.** Schematic of a typical 3-cell module. It shows Mo (green), AZO (purple), metallic grids (black). The red arrows define the front and back contacts for both  $J(V)$  and EQE individual measurements. The white filled circle illustrates the illuminated area for EQE measurement.



**Fig. 5.**  $J(V)$  characteristics measured under standard testing conditions, and adjusted to the  $J_{sc}$  deduced from the EQE measurement (active area). The cell and the alternative module (3-cell) were fabricated simultaneously.

of the targeted application (small size cell or module), CIGSe layers were co-evaporated following the conventional 3-stage process [6]. The mean gallium to group III (GGI) and copper to group III (CGI) ratios, determined by electron dispersive X-ray spectroscopy, are 0.3 and 0.9, respectively. After the CIGSe absorber layer is completed, a KF-post-deposition treatment was applied. A chemical bath deposited CdS layer was employed as n-type junction partner. The window layer consisted of conventional RF-sputtered ZnO/ZnO:Al bilayer; one should notice that the thickness and sheet resistance of the window is the same for cells and modules. For both targeted applications, Ni/Al/Ni grids were evaporated throughout a shadow mask. The resulting shadowing is expected being about 2% of  $0.5 \text{ cm}^2$  cell area. No antireflection coating was applied to the devices.

To summarize, all of the fabrications steps were exactly the same for both types of devices (cells and modules); the only additional process steps for modules are the patterning of the Mo rear contact and mechanical P3 prior to metal grids deposition.

The performance of the resulting  $0.5 \text{ cm}^2$  cells and alternative modules (3 interconnected cells) were investigated from  $J(V)$  measurements (@  $25^\circ\text{C}$ ) under AM1.5G spectrum. A laboratory-made external quantum efficiency (EQE) setup was used to compare the performance of cells

**Table 1.** Photovoltaic parameters of two representative devices fabricated simultaneously.

	Cell	Alternative module
$V_{OC}$ /cell (mV)	702.0	684.0
$J_{SC}$ ( $\text{mA}/\text{cm}^2$ )	31.3*	31.2*
$FF$ (%)	75	81
Efficiency (%)	16.4	17.2
$J_0$ ( $\text{A}/\text{cm}^2$ )	$1.4\text{E}-8$	$8.3\text{E}-13$
$n$	1.85	1.07
$R_S$ ( $\Omega.\text{cm}^2$ )	0.33	0.08
$R_{SH}$ ( $\Omega.\text{cm}^2$ )	453	316
$V_{MP}$ (mV)	570	1795
$J_{MP}$ ( $\text{mA}/\text{cm}^2$ )	28.7	27.9
$P_{max}$ (mW)	8.2	25.1

\* Active area  $J_{sc}$  calculated from EQE.

and modules. Indeed, an additional interest of the alternative module architecture proposed is that each interconnected cell can be characterized individually by  $J(V)$  and EQE as illustrated in Figure 4. For individual cell  $J(V)$  measurement, only the investigated cell is illuminated and contacts are probed as for a small size cell. For the measurement of individual cell EQE, the incident photons are brought to the active area of the cell thanks to an optical fiber, as illustrated in Figure 4.

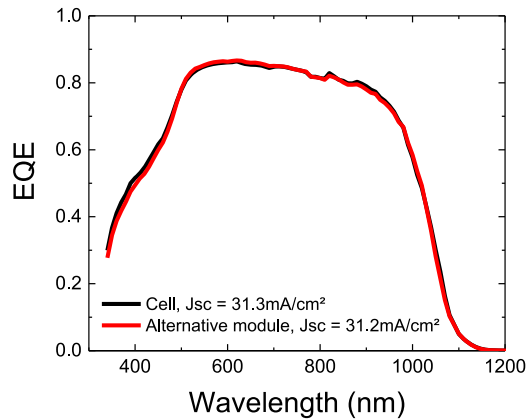
## 5 Results

Figure 5 plots representative  $J(V)$  curves of a cell ( $0.5 \text{ cm}^2$ ) and an alternative module (3 cells connected in series), fabricated simultaneously. The corresponding photovoltaic parameters are detailed in Table 1.

The most impressive photovoltaic parameter achieved by the alternative structure is undoubtedly the fill factor, which reached 81%. This high value results from very low series resistance ( $0.08 \Omega.\text{cm}^2$ ), which supports the relevance of applying metallic buses to interconnect adjacent cells.

As shown in Figure 6, both the EQE of the small size cell and of a representative cell in module are very similar, both showing about  $31.3 \text{ mA}/\text{cm}^2$ .

In addition, those EQE suggest the absorbers have the same absorption threshold, hence similar optical band gap. This is important to mention because the output voltage of the module is 2.05 V (corresponding to 684 mV/cell), whereas that of the solar cell is 702 mV. One should notice that the  $V_{oc}$  of the cells constituting the modules were also measured to be  $685 \pm 5 \text{ mV}$ , therefore also lower than that of the small size cell. Those  $\sim 20 \text{ mV}/\text{cell}$  difference are still not fully understood and deserves caution. According to the representative results presented in Table 1, the extracted saturation current ( $J_0$ ) is four decades lower for modules compared to cells. This suggests the effective holes concentration in CIGSe is higher for modules than for cells [7]. One could incriminate the CIGSe that grows directly onto soda-lime glass (where



**Fig. 6.** EQE of cell and alternative module based on CIGSe (without anti-reflective coating).

the Mo has been etched) since this location undergoes a different substrate surface temperature and much higher sodium availability. Consequently, the structural, chemical and electrical properties of the polycrystalline layer synthesized directly on the bare SLG are probably very different to those of layers grown on SLG/Mo [8]. This hypothesis should assuredly be further explored in order to determine the origins of the lowered  $V_{OC}$  per cell within the module.

## 6 Summary

In the present study, we described alternative module architecture leading to high efficiency CIGSe photovoltaic devices. Thanks to the use of metallic buses connecting adjacent cells, it appears possible to overcome most of the limitations inherent to the conventional CIGSe module structure. As first attempt, we have fabricated a 3-cell module demonstrating a photovoltaic conversion efficiency of 17.2% (in-house measurement, active area), which overperforms the small size cell fabricated simultaneously. This result is very promising because there still exist many rooms for improvement. Beside this outstanding performance, the alternative architecture proposed offers many perspectives to better understand the operation of CIGSe

module since the design used allows characterizing each individual cell within a module.

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## Author contribution statement

Lionel Assmann was in charge of back and top contacts deposition. Stephane Ginestar co-developed the process to pattern molybdenum back contacts. Justine Lorthioir organized the work through active layers deposition, co-developed patternings and wrote a largest part of the article. Ludovic Arzel co-supervised the work and made the simulations. Nicolas Barreau co-supervised the work and contributed to the final version of the paper.

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