

## Analysis of the retention of tetracyclines on reversed-phase columns: Chemometrics, design of experiments and quantitative structure-property relationship (QSPR) study for interpretation and optimization

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1 Analysis of the retention of tetracyclines on reversed-phase columns: Chemometrics, design of

2 experiments and quantitative structure-property relationship (QSPR) study for interpretation

- 3 and optimization.
- 4

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#### 14 Abstract

15 In this study, design of experiments was applied for the analysis of 6 reversed phase U-HPLC

16 columns used for the separation of four tetracyclines (TCs): tetracycline, doxycycline,

17 chlortetracycline and oxytetracycline in different elution conditions. In a first part, a fractional

18 factorial design  $(2^{4-1})$  was used to study the influence of four chromatographic parameters: column

19 temperature, pH, flow rate and composition of the mobile phase (i.e. nature of the solvent used as

20 the organic modifier), on the quality of the separation, which was evaluated in terms of peak width

21 and resolution between two pairs of TCs. This experimental design revealed that the nature of the

solvent: acetonitrile (ACN) or methanol (MeOH), and the mobile phase flow rate were the two

23 main factors actually having the most influence on the quality of the separation. Moreover, these

24 two factors presented an antagonistic influence according to the response considered: peak width

25 or peak resolution. In order to understand this behavior, a Doehlert design was performed in the

- 26 second part. It consisted in modeling the evolution of responses as a function of the two main
- 27 factors: nature of the composition of the mobile phase (mix of ACN and MeOH, from 100 % ACN

28	to 100 % MeOH) and mobile phase flow rate (from 0.3 to 0.8 mL.min <sup>-1</sup> ). For all the reversed
29	phase columns studied, an inversion of the elution order of TCs and an increase of the retention
30	factors was observed according to the composition of the organic mixture at the end of the
31	gradient. To understand the modification of the interactions implied in the various retention modes
32	related to the selectivity of the organic solvents used, a quantitative structure-property relationship
33	(QSPR) study was achieved. In this final study, the molecular descriptors of each TCs were
34	connected to its retention factor.
35	
36	Keywords
37	• Tetracyclines
38	Antibiotics
39	• U-HPLC
40	• Design of experiments
41	• Quality by design
42	• Quantitative structure-property relationship
43	
44	Highlights
45	• Design of experiments was applied for the screening of 6 RP U-HPLC columns
46	• Interpretation of the separation of tetracycline, doxycycline, chlortetracycline, oxytetracycline.
47	• The robustness area is located in different specific areas
48	• The optimal conditions differ greatly for the columns tested.
49	• A QSPR study showed deep modification of the retention mechanisms.
50	
51	Introduction
52	The use of veterinary antibiotics to treat diseases, to protect animals from infections or to improve

53 feed efficiency is constantly increasing. Aquaculture is also involved, with its heavy use of

54	prophylactic antibiotics in the aquatic environment: rivers, lakes and oceans [1]. All these treatments
55	result in large amounts of antibiotics being released into various ecosystems [2]. The most used of the
56	broad class of antibiotics are tetracyclines (TCs), followed by $\beta$ -lactamines, sulfonamides,
57	lincosamides, diaminopyrimidines and macrolides [3]. Since the late 1990s, the intense use and misuse
58	of antibiotics has received particular attention due to correlations with the numbers of resistant
59	pathogenic and commensal bacteria worldwide [4]. Studies of these effects on ecosystems and the
60	potential risks of these compounds for human health have involved the development of extraction [5]
61	and separation methods [6] for the identification and quantification of TCs. Because of the high
62	polarity, water solubility and non-volatility of many antibiotics, liquid chromatography, with diode-
63	array (DAD) [7], mass spectrometry (MS) or tandem MS [8] detection, is widely used for their
64	separation and quantification in complex matrices, such as surface water or wastewater [9]. In
65	particular, TCs have been separated on a variety of HPLC Reversed-phase (RP) columns with isocratic
66	or gradient elution. C18, C8, or phenyl selectivity has been used [10-12] with a great variety of
67	aqueous mobile phases using methanol (MeOH) or acetonitrile (ACN) as organic modifier and buffers
68	or acids such as oxalic acid, formic acid, oxalate buffers and citrate buffers. One of the problems
69	encountered with the separation of TCs is the interaction of these molecules with the residual silanols
70	of the stationary phases, leading to marked peak tailing. Zhu et al. [13] proposed the addition of EDTA
71	or oxalic acid to the mobile phase to limit this effect but the use of these agents decreases the
72	sensitivity of MS detection. Cinquina et al. [14] used a ternary mixture of oxalic acid in water (60%),
73	MeOH (25%) and ACN (15%). Skraskova et al. [15] showed the influence of different column
74	chemistries on the separation of TCs and used ACN or MeOH in optimized gradients. Nevertheless, it
75	is commonly accepted that some chromatographic conditions have antagonistic effects on
76	chromatographic quality. For example, conditions that lead to the narrowest peaks are sometimes very
77	different from those that improve the resolution. From this observation, the choice of mean conditions
78	with a mixture of organic solvents at the end of the gradient of elution are often used, without
79	optimization of the quality of separation. Consequently, it seems interesting to study the different
80	factors influencing the quality of TCs separation using chemometric tools and to connect these factors
81	with molecular interactions between the analytes, the stationary phase and the elution solvents.

82 Various chemometric methods are already being developed and applied in order to study and optimize 83 the selectivity of the separation of antibiotics by liquid chromatography [10]. Design of experiments, 84 DoE, is one such mathematical tool, which uses a multivariate approach for an exhaustive study of the 85 factors influencing a phenomenon and / or the determination of predictive models. In the field of 86 chromatographic methods, parameters influencing the quality of the separation are all closely linked 87 [16], making these tools particularly effective. Numerous authors have shown the interest of this type 88 of strategy for the analysis of pharmaceutical compounds using liquid chromatography [17–20]. 89 Moreover, thanks to the determination of predictive models, DoE appears to be a very suitable strategy 90 for performing desirability analysis [21] or predicting robustness areas (RAs) and thus finding the

analytic optimum [22]. RAs are defined as "the multidimensional combination and interaction of input

92 variables (e.g. material attributes) and process parameters that have been demonstrated to provide

assurance of quality" [23]. They can therefore be considered as theoretical zones in which variations

94 of the parameters of the analysis do not significantly alter separation quality.

95 In this context, the aim of the present work was to study and analyze the retention of four TCs:

96 tetracycline (TC), doxycycline (DXC), chlortetracycline (CTC) and oxytetracycline (OTC) on six

97 reversed phase U-HPLC columns by means of a methodological approach based on DoE and QSPR

study. The chemical structures of the four TCs are given in Figure 1.

99 Two column technologies were evaluated: (i) the Core-Shell Technology, with three columns:

100 ACQUITY CORTECS C18, 2.7  $\mu$ m (Waters), KINETEX C18, 1.7  $\mu$ m (Phenomenex) and

101 NUCLEOSHELL RP18, 2.7 µm (Machery-Nagel) and (ii), for fully porous packings, different particle

102 technologies and surface charges were evaluated with ACQUITY UPLC CSH C18, 1.7  $\mu$ m (Waters),

103 ACQUITY UPLC HSS T3, 1.8  $\mu m$  (Waters), and ACQUITY UPLC BEH Shield RP18, 1.7  $\mu m,$ 

104 (Waters). We analyzed the influence of: the selectivity of two organic solvents (ACN, MeOH) in

105 gradient mode, the mobile phase flow rate, the mobile phase pH, and the temperature of the column,

106 by means of experimental design.

107 First of all, preliminary experiments were used to find the most selective of the six columns. Then, for 108 each column chosen, the chromatographic conditions were analyzed in two stages. Firstly, a Fractional 109 Factorial Matrix was used to screen the four chosen analytical parameters: mobile phase composition, 110 gradient time, mobile phase pH, and column temperature, and determine the influence of each of them 111 on: peak width at 5% of the height of each TCs (W<sub>i</sub>), and resolution of critical pairs (Rs). Secondly, 112 the two most effective factors were studied more precisely thanks to a Doehlert Design (DD). The use 113 of this kind of DoE led to the determination of models predicting W<sub>i</sub> and Rs at any point of the 114 experimental field. From these data, a robustness area was defined for each column and optimized 115 chromatographic conditions were highlighted and tested. Finally, in order to understand the molecular 116 mechanisms involved in the retention behavior of these TCs, a quantitative structure-property 117 relationship (QSPR) study was carried out by using artificial neural networks (ANN). This QSPR 118 study allowed a molecular-level analysis of the interactions related to the retention of TCs on the 119 various stationary phases, according to the selectivity of the organic solvent used (ACN and MeOH) 120 and the proportion of each one. This QSPR study enabled the modified order of elution of TCs to be 121 analyzed according to the gradient conditions.

- 122 Materials and methods
- 123 Chemicals

Tetracycline hydrochloride, oxytetracycline, doxycycline and chlortetracycline were purchased from Sigma-Aldrich Co. (St. Quentin Fallavier, France). ACN and MeOH of HPLC grade and formic acid were also obtained from Sigma-Aldrich. All aqueous solutions were prepared using water purified with a milli-Q purification system (Millipore, St. Quentin Yvelines, France). The pH of the 0.1% (v:v) (pH = 2.2) or 0.01% (v:v) (pH = 3.3) aqueous solution of formic acid was measured with a pH-meter (Sartorius, Palaiseau, France).

130 U-HPLC equipment and separation conditions

- 131 U-HPLC analyses were performed using an Acquity<sup>®</sup> H-Class UPLC system composed of a
- 132 quaternary solvent manager, a sample FTN manager and a PDA detector ( $\lambda$ =254 nm) (Waters
- 133 Corporation, Milford, MA, USA). Analyses were monitored by Empower 3 software (Waters Co.).
- 134 Eluents were filtered with 47 mm, 0.45µm nylon membrane discs (Waters Co.).
- 135 The samples  $(10^{-3} \text{ mol.L}^{-1})$  were prepared in pure water and stored at 4°C, in the dark. Each TCs was
- 136 injected (2 µL) separately, as well as in the mixture, for LC analysis and precise determination of the
- 137 chromatographic parameters. For these analyses, a gradient mode was programmed with all initial
- 138 conditions  $t_0$ : 100% aqueous solution of formic acid (pH 2.2 or 3.2) and all final conditions  $t_{end}$ : 100%
- 139 organic solvent (MeOH or ACN), with a run time of 3 minutes, a column temperature of 40 °C when
- 140 using MeOH or 30 °C with ACN as the organic solvent, and a flow rate of 0.6 mL.min<sup>-1</sup>.
- 141 These conditions were applied to 6 reversed phase columns: ACQUITY UPLC BEH Shield RP18, 1.7
- 142 μm, 2.1 x 50 mm (Waters); ACQUITY CORTECS C18, 2.7 μm, 2.1 x 100 mm (Waters); ACQUITY
- 143 UPLC CSH C18, 1.7 μm, 2.1 x 50 mm (Waters); ACQUITY UPLC HSS T3, 1.8 μm, 2.1 x 50 mm;
- 144 KINETEX C18, 1.7 μm, 3 x 50 mm (Phenomenex, Torrance, CA, USA); NUCLEOSHELL RP18, 2.7
- 145 µm, 2 x 100 mm (Macherey-Nagel GmbH, Düren, Germany).

#### 146 Optimized separation conditions

- 147 The separations were carried out on the H-Class UPLC system described previously, on two reversed
- 148 phase columns: ACQUITY CORTECS C18, 2.7 µm, 2.1 x 100 mm (Waters) and ACQUITY CSH
- 149 C18, 1.7  $\mu$ m, 2.1 x 50 mm (Waters). Each TCs (10<sup>-3</sup> mol.L<sup>-1</sup>) was injected (2  $\mu$ L) separately as well as
- 150 in the mixture, for LC analysis, in gradient mode with all initial conditions (% vol.) t<sub>0</sub>: 100% aqueous
- solution of formic acid (pH 2.2) and final conditions: UPLC a t<sub>3min</sub>:25% MeOH, 75% ACN, flow 0.6
- 152 mL.min<sup>-1</sup>; UPLC b t<sub>3min</sub>:88% MeOH, 12% ACN, flow 0.65 mL.min<sup>-1</sup>; UPLC c t<sub>3min</sub>:5% MeOH, 95%
- 153 ACN, flow 0.5 mL.min<sup>-1</sup>. UPLC a was applied with the ACQUITY CORTECS C18 column, and
- 154 UPLC b and UPLC c were applied with the CSH C18 column. For all conditions, the run time was 3
- 155 minutes and the column temperature was 40 °C.

#### 156 Design of Experiments (DoE)

157 Selection of responses and experimental factors

158 The first step of a DoE approach is the selection of the chromatographic parameters to be optimized.

- 159 These parameters are named responses. The present case focused on two responses:
- Peak width at 5% of the height (W<sub>i</sub>) calculated for the TCs injected one by one, expressed in
   seconds
- Resolution (Rs) of the TC pairs: TC and OTC on the one hand, and CTC and DXC on the
   other (eq. 1)

164

$$Rs=2\left(\frac{t_{r(i)}-t_{r(j)}}{W_i+W_j}\right) \qquad eq. 1$$

165

166 with  $t_{r(i)}$  the retention time of the second eluted TCs of the pair and  $t_{r(j)}$  the retention time of the 167 first eluted TCs.

168

The second step consisted in evaluating the experimental parameters likely to significantly affect
responses. These parameters are named factors and noted Ui. In the present study, the selected factors
were:

- 172 .  $U_1$ : Initial mobile phase pH (i.e. formic acid concentration): pH<sub>i</sub> = 2.2, i.e. [HCOOH] = 0.1 % 173 (v:v), or  $pH_i = 3.2$ , [HCOOH] = 0.01 % (v:v) corresponding to low and high pH with values 174 lower than and close to the smallest pKa of the 4 TCs [15]. 175 •  $U_2$ : Type of organic solvent used as modifier in the gradient of elution: pure acetonitrile 176 (ACN), pure methanol (MeOH) or different mixes of the two. These solvents were selected for 177 their differences of polarity, selectivity, and hydrogen bond acidity or basicity, according to 178 the Snyder and Rutan classifications [24]. U<sub>3</sub>: Mobile phase flow rate: from  $Q = 0.3 \text{ mL.min}^{-1}$  to  $Q = 0.8 \text{ mL.min}^{-1}$ , corresponding to a 179 •
- 180 low and high linear velocity for all the column geometries tested.

181	٠	U <sub>4</sub> : Column temperature: $T = 30$ °C or $T = 40$ °C corresponding to a low and high value acting
182		on the viscosity of the mobile phase [25].

183

- 185 The most influential factors among the four mentioned above were selected by using a factorial
- 186 fractional design. This well-known design was chosen to investigate the effect of each factor, and also
- 187 had the advantage of highlighting the possible interactions between factors.
- 188 DoE construction
- 189 <u>Factorial fractional design (FFD)</u>
- 190 An FFD determines the most influential factors, that is to say, factors that have the highest effect on
- 191 the selected response.
- 192 The domains of  $pH_i(U_1)$ ; Solvent type  $(U_2)$ ; flow rate  $(U_3)$  and temperature  $(U_4)$  were 3.2-2.2;
- 193 Acetonitrile (ACN)-Methanol (MeOH); 0.3-0.8 mL.min<sup>-1</sup>; 30-40 °C, respectively.
- 194 The relation between the selected response Y and the coded variables X<sub>i</sub> that are related to the natural
- 195 variables U<sub>i</sub> was expressed as eq. 2:

$$Y = b_0 + \sum_{i=1}^4 b_i X_i + \sum_{i=1}^3 \sum_{\substack{j=2\\i < j}}^4 b_{ij} X_i X_j + \sum_{i=1}^2 \sum_{\substack{j=2\\i < j < k}}^3 \sum_{k=3}^4 b_{ijk} X_i X_j X_k + b_{ijkl} X_1 X_2 X_3 X_4$$
eq. 2

where  $b_i$  represents the estimation of the main effect of factor *i*,  $b_{ij}$  the estimation of the effect of the first order interaction between factor *i* and factor *j*, and  $b_{ijk}$ ,  $b_{ijkl}$  and  $b_{ijklm}$  the estimation of the effect of the interactions of order two, three and four respectively. The aim is to calculate these effects in order to evaluate the influence of each parameter on the response.

Based on this modeled equation, an experimental matrix consisting of 16 different experiments could be generated. However, to reduce the number of experiments required, it was decided to fractionalize the experimental matrix, i.e. to perform only 8 of the 16 experiments. In such cases, it is assumed that some interactions are negligible and consequently can be confounded with significant factors or interactions, resulting in a reduction of the number of experiments required. By this operation, the

205	results obtained are	combinations of	f significant	and negligible effects.	These combinations are named
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206 aliases, noted l<sub>i</sub>. By analyzing the significance of each alias, it is possible to get back to the

- 207 significance of main effects and first order interaction effects.
- 208 Here, it was unlikely that there would be an interaction between the initial pH (represented by X<sub>1</sub>), the
- 209 composition (represented by  $X_2$ ) and the flow rate (represented by  $X_3$ ) of the mobile phase.
- 210 Consequently, the interaction  $X_1X_2X_3$  could be considered negligible and confounded with another
- factor or interaction. In our case, it was assumed that:  $X_4 = X_1X_2X_3$ . From this equation, the defining
- 212 relation could be identified as: I = 1234.

213

214 The defining relation was then used:

- To develop the complete alias structure (Table 1).
- To design the experimental matrix (Table 2)
- 217
- 218 Additional runs (1<sup>a</sup> to 1<sup>e</sup>) were carried out to validate the statistical significance of the results through
- 219 an Analysis of Variance model (ANOVA).
- 220 Table 1: Structure of aliases (FFD)

l <sub>0</sub>	$= b_0 + b_{1234}$	$l_4 = b_4 + b_{123}$
11	$= b_1 + b_{234}$	$l_5 = b_{12} + b_{34}$
$l_2$	$= \mathbf{b}_2 + \mathbf{b}_{134}$	$l_6 = b_{13} + b_{24}$
$l_3$	$= \mathbf{b_3} + \mathbf{b_{124}}$	$l_7 = b_{23} + b_{14}$

	Experimenta	l plan		
Dun	$\overline{U_1}$	U <sub>2</sub>	U <sub>3</sub>	$U_4$
Kull	$pH_i$	Solvent	Flow rate	Temperature
			mL.min <sup>-1</sup>	°C
1 <sup>a</sup>	3.2 (-1)	ACN (-1)	0.3 (-1)	30 (-1)
$1^{b}$	3.2 (-1)	ACN (-1)	0.3 (-1)	30 (-1)
$1^{c}$	3.2 (-1)	ACN (-1)	0.3 (-1)	30 (-1)
$1^d$	3.2 (-1)	ACN (-1)	0.3 (-1)	30 (-1)
1 <sup>e</sup>	3.2 (-1)	ACN (-1)	0.3 (-1)	30 (-1)
2	2.2 (+1)	ACN (-1)	0.3 (-1)	40 (+1)
3	3.2 (-1)	MeOH (+1)	0.3 (-1)	40 (+1)
4	2.2 (+1)	MeOH (+1)	0.3 (-1)	30 (-1)
5	3.2 (-1)	ACN (-1)	0.8 (+1)	40 (+1)
6	2.2 (+1)	ACN (-1)	0.8 (+1)	30 (-1)
7	3.2 (-1)	MeOH (+1)	0.8 (+1)	30 (-1)
8	2.2 (+1)	MeOH (+1)	0.8 (+1)	40 (+1)

222 gradient, flow rate of the mobile phase, column temperature and effect matrix (FFD)

Table 2: Experimental matrix with the pH of the aqueous solution (pH<sub>i</sub>), organic solvent used in the

223

221

#### 224 Doehlert design (DD)

A DD was performed to model the evolution of peak widths and peak resolutions as a function of the organic solvent in the gradient of elution (named  $U_1$  here) and the mobile phase flow rate (named  $U_2$ here ). The aim of this experimental design was to create a surface of response in order to capture the possible nonlinear effects and curvatures in the domain and consequently forecast the response at any point of the domain.

230 The postulated model is the quadratic equation given by eq. 4:

$$Y = b_0 + b_1 X_1 + b_2 X_2 + b_{11} X_1 X_1 + b_{22} X_2 X_2 + b_{12} X_1 X_2$$
eq. 4

231 where Y represents the selected response,  $X_1$  and  $X_2$  the coded forms of the factors  $U_1$  and  $U_2$ 

- 232 respectively, b1 and b2 the estimation of the main effect of factors 1 and 2 respectively, b12 the
- 233 estimation of the effect of the first order interaction between factor  $U_1$  and factor  $U_2$ ,  $b_{11}$  and  $b_{22}$  the
- 234 estimation of the quadratic effect of the factors  $U_1$  and  $U_2$  respectively.

235 
$$X_1 = (U_1 - U_1^0) / \Delta U_1$$
;  $X_2 = (U_2 - U_2^0) / \Delta U_2$ , where the value at the center of the experimental domain

- was 50% for  $U_1^{\ 0}$  and 0.55 mL.min<sup>-1</sup> for  $U_2^{\ 0}$ , and the variation steps  $\Delta U_1$  and  $\Delta U_2$  were 25% and 236
- 237 0.25 mL.min<sup>-1</sup>, respectively. It should be noted that the solvent composition is expressed in terms of
- 238 %MeOH at the end of the gradient of elution (for example, 25%MeOH means that the solvent
- 239 composition is MeOH 25% and ACN 75%).
- 240 The experimental matrix is given in Table 3. Three additional runs were performed to validate the
- 241 statistical significance of the results through an Analysis of Variance (ANOVA). For these
- 242 experiments, pH<sub>i</sub> was fixed at 3.2 and the column temperature at 40 °C.

Table 3: Experimental matrix with the organic mixture composition at the end of the gradient

\_\_\_\_\_

-----

245 (%MeOH), flow rate and effect matrix (DD). The mixture is composed of %MeOH and 100 - %

	Experimental plan							
Run	$\overline{U_1}$	$U_2$						
Itun	% MeOH	Flow rate						
		mL.min <sup>-1</sup>						
1	100 (+1)	0.55 (0)						
2	0(-1)	0.55 (0)						
3	75 (+0.5)	0.799 (+0.87)						
4 <sup>a</sup>	25 (-0.5)	0.301 (-0.87)						
4 <sup>b</sup>	25 (-0.5)	0.301 (-0.87)						
4 <sup>c</sup>	25 (-0.5)	0.301 (-0.87)						
5	75 (+0.5)	0.301 (-0.87)						
6	25 (-0.5)	0.799 (+0.87)						
7	50 (0)	0.55 (0)						

246 MeOH for the ACN proportion.

247

#### 248 DoE analysis

Experimental results obtained from the different designs were analyzed by the statistical graphic
software NemrodW® [26], which was used for the estimation of regression coefficients, statistical
tests, and graphical analysis. The statistical significance was calculated using a classical Analysis of
Variance (ANOVA) model.

253 QSPR study

254 The concept of QSPR studies was proposed in the work of Hammett, Taft, Hanch, Fujita, Free and

255 Wilson [27–30]. ANNs are widely used for variable selection and model construction in QSAR or

QSPR studies [31]. The multilayer feed forward ANNs associated with a back propagation learning
algorithm, proposed by Rumelhart et al. in 1986 [32], were used in this study, with independent input
and output layers [33].

259 The 3D structures of the TCs were optimized using semi-empirical AM1 quantum mechanical 260 calculations of the MOPAC application, in Chem 3D Pro version 14.0 software (CambridgeSoft). An 261 RMS gradient of 0.100 was used to minimize energy for all compounds. The optimized structures 262 were used to calculate 2D and 3D molecular descriptors in the Chem 3D Pro 14.0 and Chem 3D Ultra 263 9.0 software (CambridgeSoft). Four classes of descriptors were calculated: thermodynamic (boiling 264 point, Bp; critical pressure, Cp; critical temperature, Ct; critical volume, Cv; Gibbs free energy, G; 265 heat of formation, H; Henry's law constant, Hc; ideal gas thermal capacity, Ctc; octanol-water 266 partition coefficient, log P; molar refractivity, MR; melting point, Mp; freezing point, Fp; vapor 267 pressure, Vp; water solubility, log S), topological (Balaban index, J; cluster count, CC; molecular 268 topological index, MTI; Wiener index, W), steric (ovality, O; Connolly accessible area, CAA), and 269 electrostatic (dipole moment,  $\mu$ ; dipole length, dl; total valence connectivity, Tvc; total connectivity 270 Tcn). An ANN was created using the Stuttgart Neural Network Simulator version 4.2 (University Of 271 Stuttgart, Germany) with a sigmoid activation function and a back-propagation learning algorithm. 272 This ANN was structured with an input layer connected to each molecular descriptor and an output 273 layer linked to the retention factor (k) of each TCs.

274

#### 275 Results and discussion

276 U-HPLC separation of TCs on the 6 RP columns

277 The typical chromatograms obtained with the 6 RP columns are given in Figure S1 and the retention

278 parameters calculated are given in Table S1.

279 For all the chromatographic conditions, the four TCs were separated into two groups: OTC and TC in

a first group of peaks, followed by CTC and DXC. (Figure S1). Retention times were always increased

by using MeOH as the organic solvent in the gradient of elution and the fastest separation was carried
out in 1.58 min with an ACQUITY UPLC CSH C18 column using ACN as the organic solvent in the
gradient of elution (Figure S1). In contrast, the results show that the peak width of all the TCs
decreased when ACN was used. In fact, the lowest values of W<sub>i</sub> were obtained with MeOH on the
ACQUITY UPLC BEH Shield RP18, ACQUITY CORTECS C18 and ACQUITY UPLC CSH C18
columns (Table S1). The tailing factor values were close to 1 for the ACQUITY CORTECS C18 and
the ACQUITY UPLC BEH Shield RP18 columns for both ACN and MeOH.

288

289 The use of a linear gradient varying from 100% aqueous solution at initial conditions to 100% MeOH 290 or ACN after 3 minutes allowed us to identify the column that satisfied the selected criteria of 291 effectiveness with the smallest peak widths, the shortest retention time and a symmetry of peak close 292 to 1. The polarity and similar chemical structures of TCs led to very different chromatographic 293 developments, including simple linear gradients from 100% aqueous to 100% organic with MeOH and 294 ACN [34]. On the basis of these criteria, we chose a fully porous column: ACQUITY UPLC CSH 295 C18, which gave the lowest W<sub>i</sub> with ACN, and a Core-Shell column: ACQUITY CORTECS C18, 296 which gave a small value for W<sub>i</sub> and a tailing factor close to 1 for ACN and MeOH. These two 297 columns were used in a DoE optimization in order to identify the ideal conditions of retention for 298 these TCs. The analysis of the retention parameters showed great variability of W<sub>i</sub> and Rs for the two 299 selected columns, according to whether ACN or MeOH was used (Table S1). For tf, the variation was 300 not representative when the values obtained with ACN or MeOH were compared for the two selected 301 columns (Table S1). In the DoE phase, the selected criteria were thus  $W_i$  and Rs. 302 For all the columns tested, the order of elution was identical when ACN was used as the organic 303 solvent in the gradient of elution (OTC, TC, CTC then DXC) whereas this order was modified for all 304 the tested columns when MeOH was used (TC eluted before OTC) (Figure S1). A study of the 305 chromatograms showed that this peak inversion was accompanied by an increase in retention times for 306 all the TCs and all the columns tested (Figure S1).

#### 307 Fractional factorial design

308 First, a factorial fractional design was performed to highlight the chromatographic factors that had the 309 most influence, for the two columns selected (ACQUITY CORTECS C18 and ACQUITY UPLC CSH 310 C18), that is to say, the factors that had the greatest effect on the selected responses. Responses were 311 peak widths (W<sub>TC</sub>, W<sub>OTC</sub>, W<sub>CTC</sub>, W<sub>DXC</sub>) and peak resolutions (Rs<sub>TC/OTC</sub>, Rs<sub>CTC/DXC</sub>). The choice of these 312 two complementary chromatographic parameters allowed the width of each chromatographic peak to 313 be optimized, firstly by considering the effect of the analytical conditions over this width. The 314 resolution calculation improved the separation analysis of the four peaks. The chosen factors and their 315 values are detailed in part 2.4.1. In each case, the two levels had to be sufficiently different to induce 316 response variations. 317 The experiments described in the experimental matrix (Table 2) were performed with the two

318 columns. The chromatographic results: peak widths and resolutions, are given in the complementary

data for each column (Table S1). Aliases  $l_1$ ,  $l_2$ ,  $l_3$ ,  $l_4$ ,  $l_5$   $l_6$  and  $l_7$ , were calculated by least squares linear

320 regressions of the experimental results, together with the margin of error (by means of a Student test),

321 by the NemrodW software, for the 6 responses of each column.

322 For all the responses studied, according to the structure of the aliases (Table 1), and considering that

323 interactions between three or more factors were irrelevant, (i) aliases  $l_1$ ,  $l_2$ ,  $l_3$ ,  $l_4$  were almost equal to

324 the corresponding factor effect, respectively  $b_1$ ,  $b_2$ ,  $b_3$ ,  $b_4$ , and (ii)  $l_5 l_6$  and  $l_7$  represented combinations

325 of interaction effects, respectively  $b_{12} + b_{34}$ ,  $b_{13} + b_{24}$ ,  $b_{23} + b_{14}$ . For all TCs, the initial pH of the

326 mobile phase, the solvent type in the gradient of elution and the mobile phase flow rate had significant

327 effects on peak width. The values of aliases  $l_2$  and  $l_3$  were the highest, showing clearly that the two

328 most influential factors were the solvent nature and the mobile phase flow rate.

329 The study of the interaction effects contained in the  $l_6$  and  $l_7$  aliases revealed that interactions between

330 the initial pH of the mobile phase and the solvent type in the gradient of elution  $(b_{12})$ , and between the

331 mobile phase flow rate and temperature (b<sub>34</sub>) did not have significance influence. In contrast,

interactions between initial pH and flow rate (b<sub>13</sub>), solvent type and temperature (b<sub>24</sub>), solvent type and

flow rate (b<sub>23</sub>) and initial pH and temperature (b<sub>14</sub>) seemed to have significant influence on the TCs

- 334 peak widths. Nevertheless, as the temperature did not have significant influence, it can reasonably be
- 335 considered that interactions including this factor were not significant. Thus, interactions  $b_{24}$  and  $b_{14}$
- 336 can be judged non-significant. The other two interactions  $b_{13}$  and  $b_{23}$  need to be studied more precisely
- through their interaction diagrams (Figure 2).
- 338 Each diagram represents the four different combinations of the two factors tested in the experimental
- 339 plan (i.e. for the  $X_1X_3$  diagram:  $X_1 = +1$  and  $X_3 = +1$ ,  $X_1 = +1$  and  $X_3 = -1$ ,  $X_1 = -1$  and  $X_3 = +1$  and  $X_1 = -1$
- 340 = -1 and  $X_3 = -1$ ) and the average of the experimental responses obtained for each combination. From
- 341 these diagrams, it is possible to find the combination that gives the best condition relative to the
- 342 chosen response. In the case of the response W<sub>DXC</sub>, peak width has to be as small as possible, (red
- 343 circle in Figure 2). Consequently, the best conditions for  $W_{DXC}$  are:  $X_1 = +1$ ,  $X_2 = -1$  and  $X_3 = +1$ , i.e.
- 344 pHi = 2.2, solvent = ACN and Q =  $0.8 \text{ mL.min}^{-1}$ .
- 345 Eventually, from the analysis of the Pareto graph and the interaction diagrams it is possible to
- 346 conclude that (i) the two most influential factors are the type of solvent and the mobile phase flow rate
- 347 and (ii) the best conditions to obtain the smallest DXC peak width are:
- Organic solvent in the gradient of elution : pure ACN
- Mobile phase flow rate:  $Q = 0.8 \text{ mL.min}^{-1}$
- Initial mobile phase pH: pHi = 2.2 (i.e. [HCOOH] = 0.1 % (v:v))
- Column temperature: N.S.

The same analysis was repeated for the other responses and for the two columns. It should be noted that the peak width needs to be as low as possible and the resolution between two peaks as close to two as possible. The best conditions obtained in each case are summarized in Table 4 for the two columns.

	Resul	ts										
	ACQUITY UPLC CSH C18 column						ACQUITY CORTECS C18 column					
Factors	Peak	width			Peak re	solution	Peak	width			Peak re	esolution
	W <sub>TC</sub>	W <sub>DXC</sub>	W <sub>CTC</sub>	W <sub>OTC</sub>	Rs	Rs	W <sub>TC</sub>	W <sub>DXC</sub>	W <sub>CTC</sub>	W <sub>OTC</sub>	Rs	Rs
					TC/OTC	CTC/DXC					TC/OTC	CTC/DXC
$pH_i$	2.2	2.2	2.2	2.2	N.S.	2.2	2.2	2.2	2.2	2.2	2.2	2.2
Solvent	ACN	ACN	ACN	ACN	MeOH	МеОН	ACN	ACN	ACN	ACN	MeOH	МеОН
Flow rate	0.8	0.8	0.8	0.8	0.8	0.3	0.8	0.8	0.8	0.8	0.3	0.3
Temperature	N.S.	N.S.	N.S.	N.S.	40	30	N.S.	N.S.	N.S.	N.S.	40	30

# Table 4: Results from analysis of Student test and interaction diagrams for the 6 responses and the twodifferent columns

#### 359

360 From these results, it is possible to conclude, firstly, that the most influential factors were the type of 361 solvent in the gradient of elution and the mobile phase flow rate for the two columns and the six 362 different responses. In the same way, all the responses were enhanced when the mobile phase had a pH 363 = 2.2. It appears that the effect of the temperature on  $W_i$  was not significant, in the selected range, for 364 either of the columns. For Rs, the temperature had a different effect according to the peak pairs 365 TC/OTC and CTC/DXC. The effect was greater with the flow rate of 0.8 mL/min and with MeOH 366 used as the organic solvent in the gradient (Table 4). The temperature applied for the optimized 367 conditions will be 40 °C to take account of the viscosity of MeOH used as organic solvent. The 368 conditions required to optimize the peak widths were the same for the four TCs and for both columns: 369 a mobile phase consisting of acetonitrile as solvent in the gradient of elution with a pH of 2.2, and a flow rate of 0.8 mL.min<sup>-1</sup>. However, the conditions to obtain the best resolution of peaks presented 370

371 some differences from one column to the other and from one critical pair to the other. Globally, the 372 resolution of the two pairs was enhanced when the mobile phase was MeOH with a pH of 2.2, and a 373 flow rate of 0.3 mL.min<sup>-1</sup>.

These observations revealed that the two main factors, the type of solvent in the gradient of elution and the mobile phase flow rate, had opposite influences according to the response considered: peak width or peak resolution. In order to understand this behavior and find optimal conditions whatever the response, a Doehlert design was performed, modeling the evolution of the six responses as a function of the two main factors.

379

#### 380 Doehlert design

The Doehlert design was performed to model the evolution of peak widths and peak resolutions as a function of organic solvent composition at the end of the gradient of elution, and the mobile phase flow rate. It should be noted that the organic solvent was a mix of ACN and MeOH. It is expressed as %MeOH. For example 25%MeOH means that the solvent composition was MeOH 25% and ACN 75%.

386 Experiments described in the experimental matrix (Table 3) were performed with the two columns 387 (ACQUITY CORTECS C18 and ACQUITY UPLC CSH C18). Model coefficients b<sub>1</sub>, b<sub>2</sub>, b<sub>11</sub>, b<sub>22</sub>, and 388 b<sub>12</sub> were calculated by the NemrodW software and validated through ANOVA tests for the six 389 responses and the two columns. Finally, model equations were expressed in the form of surface 390 responses where the evolution of one response was plotted as a function of the two selected factors. 391 Figure S2 shows the isoresponse curves for  $W_{TC}$  (Figure S2a<sub>1</sub>),  $W_{OTC}$  (Figure S2b<sub>1</sub>),  $W_{CTC}$  (Figure 392 S2c<sub>1</sub>), W<sub>DXC</sub> (Figure S2d<sub>1</sub>), Rs<sub>TC/OTC</sub> (Figure S2e<sub>1</sub>) and Rs<sub>CTC/DXC</sub> (Figure S2f<sub>1</sub>) on the ACQUITY 393 CORTECS C18 column, depending on the organic solvent composition and the mobile phase flow 394 rate. In order to find the optimized conditions, an area of interest was chosen for each response. This 395 area fitted the smallest peak widths and the highest peak resolution. Consequently, only peak widths

smaller than 1.5 (Figure S2a<sub>2</sub>, Figure S2b<sub>2</sub>, Figure S2c<sub>2</sub> and Figure S2d<sub>2</sub>) and resolutions higher than 2
(Figure S2e<sub>2</sub> and Figure S2f<sub>2</sub>) were considered.

398 In order to define the robustness area for the ACQUITY CORTECS C18 column, all areas of interest

399 were superimposed in the same graph, resulting in Figure 3. The same analysis is shown for the

400 ACQUITY UPLC CSH C18 column in Figure 4. In these graphs, the experimental area studied by the

401 Doelhert design is represented by a red circle.

402 The hatched area is the overlap of the robustness areas of all responses, it indicates the best operating

403 conditions for the separation of these four TCs in U-HPLC using a given column. Thus, the best

404 separation conditions are obtained, for the ACQUITY CORTECS C18 column, with a mobile phase

405 mainly composed of ACN at the end of the gradient of elution and a flow rate of around 0.6 mL.min<sup>-1</sup>,

406 whereas, for the ACQUITY UPLC CSH C18 column, the mobile phase at the end of the gradient

407 needs to be either pure MeOH with a flow rate higher than 0.65 mL.min<sup>-1</sup> or pure ACN with a flow

408 rate around 0.5 to 0.6 mL.min<sup>-1</sup>.

409 Optimized separation of the TCs

410 From these results, the optimized conditions were defined for the 2 columns. For the ACQUITY

411 CORTECS C18 column, the robustness area shows only one optimized zone, close to 25% MeOH,

412 75% ACN at the end of the gradient of elution. For the ACQUITY UPLC CSH C18 column, two

413 conditions can be applied, with either 88 % MeOH, 12 % ACN or 5 % MeOH, 95% ACN at the end of

the gradient of elution. These three conditions were applied to the separation of the four TCs, as three

415 test points. The chromatograms obtained with the two columns are given in Figure 5 and the

416 calculated retention parameters in Table 5.

417 Table 5 : Retention parameters calculated from U-HPLC optimized chromatograms of TCs solutions:

418 tetracycline (TC), oxytetracycline (OTC), chlortetracycline (CTC) and doxycycline (DXC) obtained

419 on ACQUITY CORTECS C18, 2.7 μm, 2.1 x 100 mm column, with 0.6 mL.min-1, 25% MeOH, 75%

420 ACN at the end of the gradient (a1), and ACQUITY UPLC CSH C18, 1.7 μm, 2.1 x 50 mm with 0.5

421 mL.min-1, 5% MeOH, 95% ACN at the end of the gradient (a2) or with 0.65 mL.min-1, 88%

- 422 MeOH,12% ACN at the end of the gradient (a3) as the organic solvent in gradient mode. tr: retention
- 423 time, k': retention factor,  $W_i$ : peak width at 5%, tf: tailing factor, Rs: resolution.

Compou	ind tr (min)	k'	W <sub>i</sub> (x10 <sup>-2</sup> min.)	tf	Rs
OTC	1.59	3.0	2.05	1.20	2.06
TC	1.67	3.2	2.03	1.28	3.80
CTC	1.79	3.5	2.20	0.95	
DXC	1.86	3.7	2.06	0.77	2.95

Organic Solvent (end of gradient): 25% MeOH, 75% ACN, Column: ACQUITY CORTECS C18, chromatogram a1, Figure 5.

Organic Solvent (end of gradient): 5% MeOH, 95% ACN, Column: CSH C18, chromatogram a2, Figure 5.

Compound	tr (min)	k'	$W_i(x10^{-2} min.)$	tf	Rs
OTC	1.40	3.87	2.01	1.07	
					2.08
TC	1.44	4.00	1.82	1.10	
	1 50		• • • •	0.50	
CTC	1.60	4.57	2,01	0.62	0.54
DUG	1.55	4.51	1.04	0.61	2.54
DXC	1.65	4./1	1.84	0.61	

Organic Solvent (end of gradient): 88% MeOH, 12% ACN, Column: CSH C18, chromatogram a3, Figure 5.

Compound	tr (min)	k'	$W_i(x10^{-2} min.)$	tf	Rs
TC	1.36	5.41	2.04	0.87	
					2.33
OTC	1.41	5.20	1.97	1.02	
CTC	1.63	6.41	2.75	0.62	
					6.22
DXC	1.80	7.21	2.87	0.60	

425 Two DoE tools were used to determine optimized conditions for the separation of TCs on two RP18 426 columns. For the three test points, the objective was achieved for the 4 TCs. The choice of a simple pH 427 modifier (0.1% formic acid in water) and one or two organic solvents at the end of the gradient, 428 revealed one or more robustness zones for the two selected columns. The resolution Rs>2 was 429 obtained with a separation of less than two minutes for the four analytes. The peak widths were also 430 optimized. The lowest values ( $\approx 2x10^{-2}$  min) were obtained with the ACQUITY CORTECS C18 431 column and the gradient conditions UPLC a (25% MeOH, 75% ACN, end of gradient) and for the 432 ACQUITY CSH C18 column with the gradient conditions UPLC c (5% MeOH, 95% ACN, end of 433 gradient). For all the optimized conditions, tf factors were not controlled and varied from 0.60 to 1.28 434 (Table 5).

435 The chromatogram for the optimized conditions with 88% MeOH, 12% ACN at the end of gradient, 436 used with the ACQUITY CSH C18 column, showed a modified order of elution for the TCs (Figure 5, 437 a3). This inversion in elution order of TCs was also observed in the screening phase of the six reversed 438 phase columns, when MeOH was used as the organic solvent to replace ACN (Figure S1). With a 439 majority of ACN at the end of the gradient, the order of the first pair of TCs was OTC-TC (Figure 5, 440 a2). In majority presence of MeOH at the end of the gradient, this order changed to TC-OTC (Figure 441 5, a3). For the ACQUITY CORTECS C18 column, the mixture used at the end of the gradient, 75% 442 ACN, 25% MeOH, showed the OTC-TC order of elution (Figure 5, a1). To study these retention 443 mechanisms and this selectivity related to the solvent used in the end of gradient, we undertook a 444 QSPR study with ANNs, in order to connect the molecular descriptors of each TC to its retention 445 factor, k'. The weights with absolute value >1 of nodes linked to molecular descriptors of the TCs are 446 given in Figure 6. It appears that, in the presence of ACN-rich mixture (75% ACN; 25% MeOH or 447 95% ACN; 5% MeOH), only two molecular descriptors have a significant weight: log P, linked to 448 hydrophobicity; and total valence connectivity (Tvc), related to the steric structure of the molecule. 449 With ACN-rich mixture, k' is not directly linked to the calculated log P for all TCs and the elution 450 order is: OTC, log P: -4.53; TC, log P: -3.76; CTC, log P: -3.24; DXC, log P: -3.41. DXC with a lower 451 log P is eluted after CTC. The steric parameter Tvc shows an important influence in the elution of

452 CTC/DXC, and shows less influence in the elution of OTC/TC. Koopmans et al. [35] showed the

453 importance of calculated log P in the analysis of the retention of polyaromatics using ACN as organic

454 modifier. In their study, the parameter of connectivity chosen (Tcn) did not bring extra information. In

455 the case of TCs, calculated log P does not predict or explain the order of elution of the compounds.

456 For this, it is necessary to add a steric parameter Tvc or Tcn.

457 With MeOH-rich mixture, log P is the descriptor of strongest weight (5.64) and 10 other molecular 458 descriptors are linked to the retention factor of the TCs (Figure 6). Four descriptors have very 459 significant weights >3: log P, Balaban and Tcn; two topological parameters; and a thermodynamic 460 descriptor, critical pressure. With a MeOH-rich mixture, the influence of the steric parameters is very 461 marked for the elution of OTC/TC. The QSPR study showed that the retention of the four TCs was 462 controlled by log P and one steric parameter when ACN was mainly used on all the stationary phases 463 retained in our work. In this case, the retention factors, k', were smaller and lay between 3 and 4.71 464 under the optimized conditions (Table 5, a1, a2). In presence of a majority of MeOH, the retention was 465 controlled by 10 molecular descriptors, including log P, 2 steric descriptors and 1 thermodynamic 466 descriptor for the four having very strong influence (Figure 6). The mechanisms of retention were then 467 significantly modified, with an increase of k' for the four TCs (range 5.41-7.21, Table 5, a3). This 468 diversity of molecular interactions was also connected with an inversion of the OTC/TC elution order 469 (Figure 5, a3) and no modification of the elution order for CTC/DXC. The stationary phases using 470 charged surface hybrid (CSH) technology showed optimized separation with Rs >2 in 2 different 471 elution systems: using 95% ACN and 5% MeOH or 88% MeOH and 12% ACN at the end of the 472 gradient. With CSH columns, the silica particles are covered with positive charges, allowing an 473 electrostatic repulsion of TCs from free silanols, which are separated by hydrophobic and steric 474 interactions (Figure 6). This type of column was used by K. Skraskova et al. for the separation of TCs 475 in surface water [15]. The authors used ACN or MeOH alone to optimize the retentions, without 476 evaluating the optimization of MeOH/ACN mixtures. A low flow of 0.2 mL/min. was applied by Jia et 477 al. for the separation of TCs on a BEH C18 U-HPLC column by using ACN as organic solvent in a 478 gradient mode [36]. MeOH was used in gradient mode for the separation of TCs on a Luna C18

479 column [37]. In a recent review of analytical methods used for the separation of TCs, Kim et al. have 480 shown that ACN used in gradient mode with aqueous formic acid is the preferred mobile phase [38]. 481 However, the influence of each of the organic solvents, ACN and MeOH or mixture, is not analyzed 482 on the separation performances. In this study, we show that it is necessary to carry out 7 experiments 483 (Table 3) to identify the flow and the proportion of ACN/MeOH mixture at the end of gradient to 484 obtain a Rs>2 for the 4 TCs on a U-HPLC RP18 column. It is the chemistry of the stationary phase 485 that determines the optimal proportions of the organic solvent of the gradient mobile phase. For the 486 ACQUITY CORTECS C18 column, the mixture at the end of the gradient must contain less than 30% 487 of MeOH and between 90% and 70% of ACN (Figure 3). For the CSH C18 column, 2 different areas 488 allowing optimized separation are identified: one containing 100% ACN or a mixture of more than 489 90% of ACN with less than 10% of MeOH at the end of the gradient, and the other containing between 490 88% and 95% of MeOH and less than 5% of ACN at the end of the gradient. It is important to note 491 that, when using MeOH as organic solvent, it is necessary to mix it with between 2% and 5% of ACN 492 to optimize the resolution of the 4 TCs (Figure 4). The QSRR study shows that the mechanisms of 493 retention are equivalent on both ACQUITY CORTECS C18 and ACQUITY CSH C18 columns and 494 implies hydrophobic and steric interactions (Figure 6, a1, a2) when ACN is used as the predominant 495 organic solvent at the end of the gradient. The selectivity, solvent strength, acidity or basicity of ACN 496 and MeOH used as the mobile phase was studied and modeled by Snyder [39] and Glaich [40]. For the 497 4 TCs, the QSRR study did not show any influence of a molecular parameter linked to proton 498 exchange, or electronic or polar structure of the analytes (Figure 6). The elution order of the 4 TCs 499 was not directly correlated to log P. The mechanism of retention involved hydrophobic and steric 500 interactions as shown in Figure 6. By molecular simulation, Rafferty et al. [41] showed that 501 ACN/water mixture could interact with the alkyl chains of the column at different levels. ACN largely 502 penetrates the alkyl chains, close to the silica substrate. The result is an increase in the alkyl chain 503 order with the use of ACN. With the use of MeOH, the structure of the alkyl chains is more flexible, in 504 connection with an increased weight of the steric parameters, controlling the retention of the TCs in 505 association with hydrophobic interactions.

#### 506 Conclusion.

507 This study has shown that the robustness area of some particular columns, such as the ACOUITY 508 UPLC CSH C18, is located in different specific areas corresponding to the use of pure organic 509 modifier or a mixture, depending on the chemistry and type of reversed phase column. These optimal 510 conditions are very different from those more currently used in the literature since most of those 511 studies are performed with average conditions, without robustness optimization. In the case presented 512 here, the antagonistic effects of the retention parameter quality are avoided. Moreover, the optimal 513 areas highlighted in this study are very thin and thus could not be found without the methodology used 514 here, and particularly without the use of a Doelhert network. With this optimization methodology, four 515 Tcs could be separated in less than 2 min. with a resolution Rs>2. Simultaneously with the 516 optimization step, it was possible to study the mechanisms of retention at the molecular level. The 517 QSPR study showed the deep modification of the mechanisms involved with the use of ACN or 518 MeOH as the organic modifier. The increase in the factors of retention, k', observed with the use of 519 MeOH is connected with the number and the diversity of the molecular descriptors involved in the 520 chromatographic retention. The mechanism of retention involves hydrophobic and steric interactions 521 and is not directly correlated with oil/water partitioning (log P).

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R1 R2 OH OH			OH	H <sub>2</sub>
TCs	$R_1$	$R_2$	R <sub>3</sub>	$R_4$
Tetracycline (TC)	Н	ОН	CH <sub>3</sub>	Н
Doxycycline (DXC)	Н	Н	CH <sub>3</sub>	ОН
Chlortetracycline (CTC)	C1	ОН	CH <sub>3</sub>	Н
Oxytetracycline (OTC)	Н	ОН	CH <sub>3</sub>	ОН

Figure 1: Molecular structures of the TCs analyzed by RP U-HPLC



Figure 2: Interaction diagrams  $X_1X_3$  and  $X_2X_3$ , for the  $W_{\text{DTC}}$  response on the CORTECS C18 column



Figure 3: CORTECS C18 column: Overlap of areas of interest showing  $Rs_{TC/OTC}$ ,  $Rs_{CTC/DXC}$ ,  $W_{TC}$ ,  $W_{OTC}$ ,  $W_{CTC}$ , and  $W_{DXC}$  in relation with the flow rate and organic mixture composition (%MeOH and %ACN) at the end of the gradient. The typical point C<sub>1</sub> corresponds to a gradient: t0: 100% aqueous solution of formic acid (pH 2.2) and final conditions:  $t_{3min}$ :25% MeOH, 75% ACN, flow 0.6 mL.min<sup>-1</sup>. W: peak width at 5%, Rs: resolution.



Figure 4: ACQUITY UPLC CSH C18 column: Overlap of areas of interest showing  $R_{S_{TC/OTC}}$ ,  $R_{S_{CTC/DXC}}$ ,  $W_{TC}$ ,  $W_{OTC}$ ,  $W_{CTC}$ , and  $W_{DXC}$  in relation with the flow rate and organic mixture composition (%MeOH and %ACN) at the end of the gradient. The typical points correspond to a gradient: t0: 100% aqueous solution of formic acid (pH 2.2) and final conditions for C<sub>2</sub>:  $t_{3min}$ :5% MeOH, 95% ACN, flow 0.5 mL.min<sup>-1</sup>, and for C<sub>3</sub>:  $t_{3min}$ :88% MeOH, 12% ACN, flow 0.65 mL.min<sup>-1</sup>.W: peak width at 5%, Rs: resolution.



Figure 5: Optimized U-HPLC chromatograms of TC solutions: tetracycline (T), oxytetracycline (O), chlortetracycline (C) and doxycycline (D) obtained on CORTECS C18, 2.7 μm, 2.1 x 100 mm column, with flow rate 0.6 mL.min<sup>-1</sup>, pH t<sub>0</sub>=2.2, 25% MeOH, 75% ACN at the end of the gradient (a1), and ACQUITY UPLC CSH C18, 1.7 μm, 2.1 x 50 mm with flow rate 0.5 mL.min<sup>-1</sup>, 5% MeOH, 95% ACN at the end of the gradient (a2) or with flow rate 0.65 mL.min<sup>-1</sup>, 88% MeOH, 12% ACN at the end of the gradient (a3) as the organic solvent in gradient mode



Figure 6: Weight (absolute value) of the key molecular parameters connecting the structures of TCs to their retention factor (k') for the CORTECS column with 25% MeOH, 75% ACN end of gradient (a1), CSH C18 column with 95% ACN, 5% MeOH end of gradient (a2) and 88% MeOH, 12% ACN end of gradient (a3)

