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# Protecting Carbon Nanotubes from Oxidation for Selective Carbon Impurity Elimination

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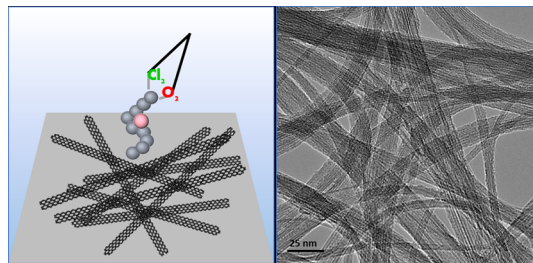
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## Supporting Information

**ABSTRACT:** Purity of carbon nanotubes (CNTs) is essential to avoid a dramatic decrease in their performances. In addition to metallic impurities, carbonaceous impurities have been shown to be responsible for pronounced effects. However, they are highly difficult to be selectively removed from CNT samples because of the similar chemical reactivity of these two kinds of carbon species. The existing purification methods often lead to high CNT consumption (>90 wt %). The proposed method consists of a one-pot gas-phase treatment combining chlorine and oxygen. The CNT powder maintained in a chlorine stream is submitted to oxygen at moderate temperature [350 and 500 °C for single-walled CNTs (SWCNTs) and double-walled CNTs (DWCNTs), respectively], and the thermal treatment is then pursued at 900–1000 °C under chlorine alone. Our work reveals that this approach is able to significantly improve the selectivity of elimination of carbonaceous impurities. Thanks to the proposed purification treatment, only 19 and 11 wt % of carbon species (mainly carbon impurities) are lost for DWCNTs and SWCNTs, respectively. The mechanism proposed involves a protective effect by grafting of chlorine favored to the CNT walls. Because our simple one-pot purification method is also versatile and scalable, it opens new perspectives for CNT applications in high-added value fields.



## 1. INTRODUCTION

Carbon nanomaterials, such as carbon nanotubes (CNTs) and graphene, are exciting materials showing a combination of superior properties: lightness, thermal and electrical conductivity, and optical and mechanical properties.<sup>1</sup> The technology of CNT synthesis, although in a continuous state of improvement, cannot avoid the use of catalysts to increase the conversion rate from carbon precursors to the production of carbon nanomaterials, as this rate is still far below 100%.<sup>2–6</sup> The presence of both metal and carbon impurities has negative effects on the CNT properties.<sup>7,8</sup> It is widely known that magnetic properties of CNTs are dominated by catalyst residues even at low content.<sup>9</sup> Thermal and electrical conductivity and mechanical properties (tensile strength) are dramatically decreased because of carbon impurities in CNT samples.<sup>10</sup> Although it was first attributed to the CNTs themselves, the observed electrocatalytic activity has been shown to be due to metallic catalyst impurities<sup>11,12</sup> or carbonaceous by-products.<sup>13–15</sup> Similar mistrusted effects on electrochemical properties from carbon impurities in graphene samples have been reported by Pumera et al.<sup>16</sup>

The purification of CNTs has been extensively desired, and various methods allow to efficiently remove metallic

contamination.<sup>17,18</sup> Some methods to remove only catalyst residues consist of annealing the CNT powder at a temperature in the 2000–2500 °C range under N<sub>2</sub>, Ar, or vacuum.<sup>19–21</sup> However, even if high-quality CNTs can be prepared from the standard methods, they still fail in selectively removing carbonaceous impurities without excessive loss of CNTs, leading to low sample yield.<sup>22</sup> The main reason explaining this difficulty of eliminating carbon impurities without attacking the CNTs is their too close chemical reactivity.<sup>23,24</sup> Standard approaches use strong acids, which are known to damage the CNTs and lead to weak sample yield; they also create functional groups at the CNT surface and produce large amounts of amorphous carbon debris.<sup>25</sup> These surface groups and debris are prejudicial for further CNT applications, for which surface and interfacial phenomena play the major role.<sup>8,26</sup> Gas-phase routes using air and/or oxygen, hydrogen, carbon dioxide, and ammonia have been also reported as efficient purification methods to selectively remove carbonaceous impurities from CNT samples.<sup>27,28</sup> Thermal air

or oxygen oxidation at moderate temperature was able to selectively attack amorphous carbon or carbonaceous impurities of lower oxidation resistance than CNTs.<sup>29–32</sup> High-temperature heating in hydrogen or in ammonia has been proposed as an effective purification treatment.<sup>33,34</sup> Carbon dioxide was also used as a milder oxidant with successful attack of carbon impurities and less damaging of CNTs.<sup>35,36</sup> For these gas-phase methods, a subsequent treatment usually in a liquid medium, such as nitric or hydrochloric acid, is required to remove the metallic impurities. Interestingly, halogens, such as bromine<sup>37</sup> and chlorine, under various forms (hydrogen chloride,<sup>38</sup> tetrachloromethane,<sup>39</sup> or chlorine<sup>40,41</sup>) are able to effectively remove metallic impurity from CNTs, carbon species (including CNTs and carbonaceous impurities) being untouched. In a previous work,<sup>42</sup> we had shown that the addition of oxygen in chlorine could lead to the removal of carbon impurities from double-walled CNTs (DWCNTs). Unfortunately, the combustion rate at the high temperature used (950 °C) was too rapid and not possible to be controlled to reduce the CNT loss, which was as high as 95%. In spite of the extensive research in the field, efficient elimination of carbonaceous impurities from CNT samples has not been achieved without damaging and consuming the majority of CNTs; the missing key is to reach a high degree of selectivity of carbonaceous impurity attack.

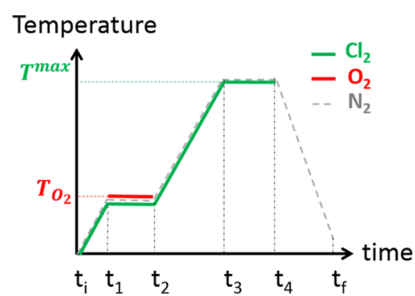
We present here experimental results that evidence a high selectivity in the elimination of carbonaceous impurities with respect to CNTs occurring in particular working conditions. Moreover, in contrast with the few available reported non-damaging methods, our approach allows to prepare purified CNTs while limiting the number of chemical treatments.<sup>43–45</sup> Our entirely gas-phase treatment consists of a concomitant thermal activation of a protection/combustion effect of the carbon species before the spontaneous elimination of the formed metallic chlorides in a one-pot treatment. The favored oxidation of carbonaceous impurities is demonstrated by applying this treatment to both single-walled CNTs (SWCNTs) and DWCNTs. The results show that the combination of chlorine and oxygen at temperatures as low as 350–500 °C can be a powerful asset for an effective carbon impurity elimination with a much higher carbon yield than previously reported 81 wt % instead of 5 wt %.<sup>42</sup> These results have been achieved thanks to a strong protecting effect of CNTs against combustion occurring in a quite low-temperature range (350–500 °C) when oxygen is introduced in chlorine while carbonaceous impurities remain susceptible to be vaporized. The proposed reaction mechanism, unprecedented in the literature, which allows to explain this finding, is based on the identified tunable reactivity between oxygen and chlorine toward carbon species, that is, CNTs and carbon impurities. The method we propose here hence fulfills all of the requirements to purify large volumes of CNTs with high sample yields, which is of great interest for their practical applications.

## 2. MATERIALS AND METHODS

**2.1. CNT Purification.** The DWCNT sample was synthesized by catalytic chemical vapor deposition under optimized operating conditions;<sup>46</sup> the raw DWCNT sample is referred to as rD. The raw HiPco SWCNT samples used for this work were supplied by NanoIntegris Inc. For the purification of the HiPco sample, because of the numerous conditions tested, we had to use several raw batches of

SWCNTs. Each one has been distinguished: rS1-2 is the starting raw SWCNT sample, which has been purified to prepare S1 and S2; rS3-5 corresponds to the raw SWCNTs used to obtain S3, S4, and S5; and rS6 for S6. The experimental conditions used for the purification of both SWCNTs and DWCNTs are given in the [Supporting Information](#), Table S1. Moreover, the treatment of a DWCNT sample was intentionally stopped after the O<sub>2</sub> dwell under Cl<sub>2</sub> at 500 °C; this sample is referred to as mD.

For the purification treatment ([Figure 1](#)), the CNT powder (~150 mg) was placed in a silica boat (length 10 cm) in a



**Figure 1.** Schematic of the applied one-pot purification method displaying the nature of the gas used in each step, and the temperature sequence (dwells and ramps).

tubular oven (diameter 2 cm), which was first flushed by nitrogen (nitrogen being also the carrier gas for the process) to carefully remove air; purified chlorine at around 200 mL/min was incorporated into the set-up while the temperature was increased (10 °C/min). When the temperature reached the chosen value,  $T_{O_2}$  ( $T_{O_2}$  variation range: 250–950 °C), O<sub>2</sub> with a flow rate of 2–4 mL/min was injected for the desired duration ( $t_1$ – $t_2$  in the 20–60 min range). After the Cl<sub>2</sub>/O<sub>2</sub> treatment stage, the sample was heated at  $T_{Cl_2}$  for 1 h under chlorine alone before natural cooling (see also [Table S1](#)).

With the used conditions regarding the O<sub>2</sub> flow rate and duration of its injection, the used O<sub>2</sub> volume is around 200 mL ( $9 \times 10^{-3}$  mol). The amount of carbon for the experiments is at most  $8 \times 10^{-3}$  mol. That means that for every experiment carried out, the amount of oxygen content used is sufficient enough to burn all the unwanted carbon-based species.

**2.2. Characterization Techniques.** Transmission electron microscopy (TEM) observations were performed using a JEM-ARM 200F apparatus at an accelerating voltage of 80 kV. At least 30–40 images taken at different places were analyzed for each sample in order to guarantee a representative description of the samples. Thermogravimetric analysis (TGA) was performed with a Setaram Setsys evolution 1750 by using dry air as the carrier gas and a temperature ramp of 5 °C/min from room temperature to 900 °C. The metal oxide content evaluated by TGA was directly used to calculate the yield of removal of metallic impurity ( $Y_m$ ) after purification; that means that the oxygen part corresponding to the respective stoichiometric amount in the oxidized form of each metal present in the (raw or purified) CNT samples is included in  $Y_m$ .

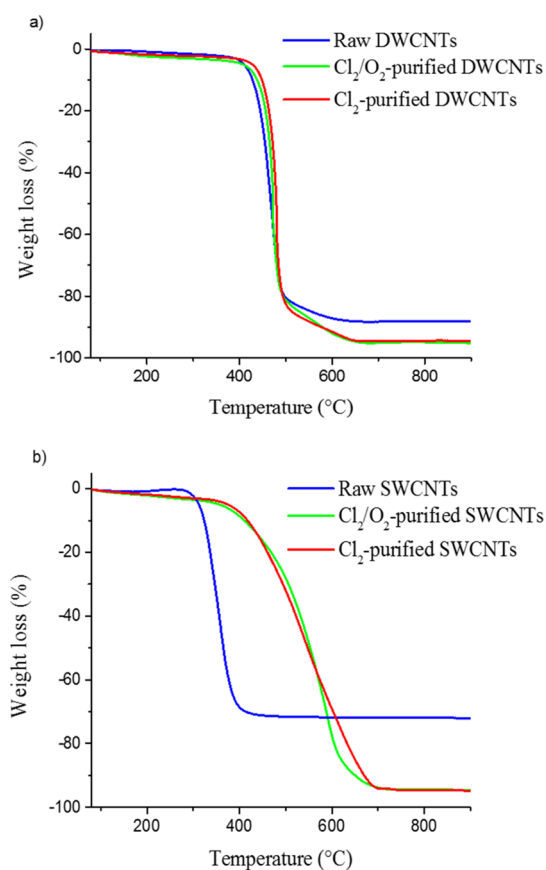
Micro-Raman spectroscopy was carried out with a LabRAM HR 800 micro-Raman spectrometer with two incident wavelengths: 632.8 and 514.5 nm. The incident laser beam, focused on the sample with an  $\times 50$  objective, was reduced with an optic filter to avoid any damage due to overheating during

the spectrum recording. The recorded number of spectra (at least 3) depended on the observed data dispersion. After subtraction of a baseline, the  $I_D/I_G$  intensity ratio was determined by dividing the height of the D band by that of the G band. As only one representative spectrum is shown for each sample, the D/G ratio was close to the average of  $I_D/I_G$  of the sample. The given  $I_D/I_G$  evolutions correspond to the evolution of the average value of the  $I_D/I_G$  ratios obtained for each spectrum for the sample, after the applied chemical treatment. For Auger electron spectroscopy (AES), the CNT powder is fixed with a copper scotch on a molybdenum sample holder. A primary electron energy of 2500 eV is focused on the sample, and a cylindrical detector with a resolution of 1 eV is used for data collection.

X-ray photoelectron spectroscopy (XPS) spectra were collected on a Kratos Axis Ultra (Kratos Analytical, UK) spectrometer equipped with a monochromatic Al  $K\alpha$  source (1486.6 eV). All spectra were recorded at a  $90^\circ$  takeoff angle, with the analyzed area being about  $0.7 \times 0.3$  mm. Survey spectra were acquired with 1.0 eV step and 160 eV analyzer pass energy and the high-resolution regions with 0.1 eV step and 20 eV pass energy (instrumental resolution better than 0.5 eV). Curve fitting was performed using a Gaussian/Lorentzian (70/30) peak shape after Shirley's background subtraction and using the X-vision 2.2.11 software.

### 3. RESULTS AND DISCUSSION

**3.1. Purification Approach, Carbonaceous Impurity Removal, and CNT Quality.** From the synthesis method, catalyst residues remain in the CNT samples, including DWCNTs and SWCNTs. DWCNTs contain cobalt- and molybdenum-based impurities. The latter represent about 10% of the sample weight. The as-produced HiPco SWCNT sample contains iron-based impurities at a non-negligible amount, reaching a third or more of the sample weight. The used DWCNTs have an internal and external average diameter of 1.35 and 2.05 nm, respectively, with a length between 1 and 10  $\mu\text{m}$ . The diameter of the SWCNTs varies from 0.7 to 2 nm, and their length is similar to that of the DWCNTs. Non-nanotube carbon species are also present in both CNT samples, inherent to the chemical vapor deposition (CVD) synthesis. The close reactivity between these carbonaceous impurities and the CNTs is clearly put into evidence from their resistance against oxidation by means of TGA. The combustion of CNT samples commonly appears as one single weight loss, meaning that CNTs and non-nanotube carbon species burn off in the same temperature range, as is the case also for the DWCNTs and SWCNTs used here (cf. Figure 2). The as-produced DWCNT and SWCNT powders were submitted to our one-pot thermal treatment under chlorine (until  $T^{\text{max}}$ ), in which oxygen is introduced at a chosen temperature,  $T_{\text{O}_2}$  ( $T_{\text{O}_2}$  being  $\leq T^{\text{max}}$ ), the carrier gas being nitrogen,  $\text{N}_2$  (Figure 1 and Table 1). With the aim of investigating the mechanisms involved in the  $\text{Cl}_2/\text{O}_2$ -based treatment, we have performed experiments with different approaches: (i)  $\text{O}_2$  was introduced in the reactor at a temperature lower than that used for the final dwell in chlorine ( $T_{\text{O}_2} < T^{\text{max}}$ ) (D1, S1, and S2); (ii)  $\text{O}_2$  was introduced during the  $\text{Cl}_2$  dwell,  $T_{\text{O}_2} = T^{\text{max}}$  (D2, S3, and S4); (iii) treatments under  $\text{Cl}_2$  only (D3 and S5) or  $\text{O}_2$  only (D4 and S6) were also conducted (Table 1 and Supporting Information, Table S1). Among all of the performed treatments, for the sake



**Figure 2.** TGA curves (in dry air, temperature ramp  $5^\circ\text{C}/\text{min}$ ) for the raw and selected CNTs treated with  $\text{Cl}_2$  and  $\text{Cl}_2/\text{O}_2$  (a): raw DWCNT rD (blue);  $\text{Cl}_2$ -purified DWCNT D3 (red);  $\text{Cl}_2/\text{O}_2$ -purified DWCNT D1 (green) and for SWCNTs (b): raw SWCNT (blue) rS1-2;  $\text{Cl}_2$ -purified SWCNT S5 (red);  $\text{Cl}_2/\text{O}_2$ -purified SWCNT S1 (green).

of clarity, we present those showing significant differences in metallic removal and/or carbon impurity elimination, consistency and reproducibility having been carefully tested.

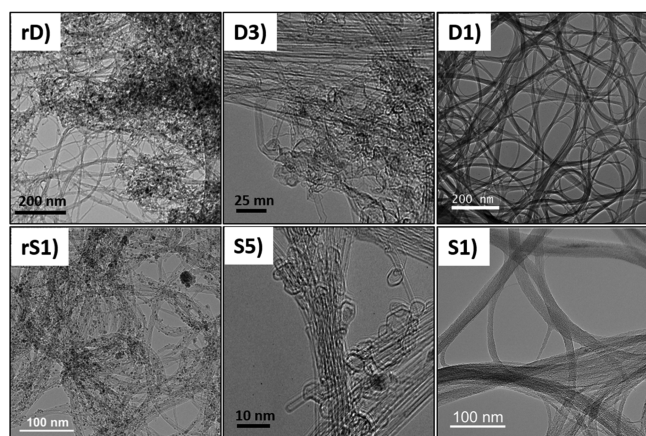
The typical behavior from TGA of the raw and treated CNT samples after treatment with  $\text{Cl}_2$  alone and with a mixture  $\text{Cl}_2/\text{O}_2$  is shown in Figure 2. For the raw DWCNT sample, the shape of the TGA curves and the observed combustion temperatures are quite similar (around  $500^\circ\text{C}$ ) before and after purification (Figure 2a). Raw SWCNTs burn off around  $350^\circ\text{C}$ , and the combustion temperature is upshifted to around  $550^\circ\text{C}$  after purification (Figure 2b). The pronounced upshift ( $\sim +200^\circ\text{C}$ ) of the combustion temperature for SWCNTs may be due to the greater metal content in this sample compared to that in DWCNT; the upshift of the burn-off temperature of CNTs is indeed commonly observed after the elimination of the metallic impurities<sup>47</sup> (Supporting Information, Figure S1).

Figure 3 shows TEM images of the used DWCNT and SWCNT samples before (Figure 3, rD and rS) and after different treatment conditions. Metallic and carbon impurities can be easily noticed in both SWCNT and DWCNT samples on the TEM images of the starting raw samples. As normally observed, these impurities widely cover the CNT interlacing. After heating the powdered CNT sample under chlorine, carbon impurities were still present and could be clearly imaged (Figure 3, D3 and S5). These non-nanotube species

**Table 1. Temperature at Which O<sub>2</sub> Is Introduced in the Purification Reactor, Temperature of Cl<sub>2</sub> Dwell (T<sup>max</sup>), Occurrence of Carbon Impurity Removal, Resulting Oxidized Metallic Impurity Content M<sub>p</sub> in wt % and Their Content n<sub>m</sub> in at. %, Metal Removal Yield Y<sub>m</sub>, and Carbon Consumption after Purification C<sub>c</sub><sup>a</sup>**

sample	O <sub>2</sub> introduction temperature (T <sub>O<sub>2</sub></sub> )/°C	Cl <sub>2</sub> dwell temperature (T <sup>max</sup> )/°C	carbon impurity removal	M <sub>p</sub> (M <sub>r</sub> )/wt %	n <sub>m</sub> /at. %	Y <sub>m</sub> /%	C <sub>c</sub> /%
rD				10.2	1.9		
D1	500	1000	y	4.8	0.9	53	19
D2 <sup>y</sup>	950	950	y	0.01	0.002	99.9	95
D3		1100	n	5.5	1.0	46	21
D4	500		n	72.8	13.5		98
rS1-2				28.0	7.7		
S1	350	900	y	5.4	1.2	81	11
S2	600	900	y	4.8	1.1	83	47
rS3-5				44.5	14.7		
S3	800	800	y	5.0	1.1	88.8	76
S4	900	900	y	3.6	0.8	91.9	91
S5		900	n	5.2	1.2	88.3	3
rS6				33.0	9.6		
S6	350		n	N.A.			

<sup>a</sup>Y<sub>m</sub> and C<sub>c</sub> are defined in the text. <sup>y</sup>From an earlier work.<sup>42</sup>

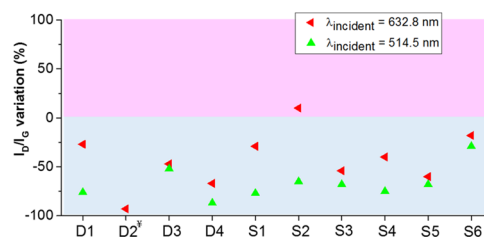


**Figure 3.** Typical TEM bright-field micrographs of the raw and treated DWCNT and SWCNT samples: raw DWCNT (rD), Cl<sub>2</sub>-purified DWCNT (D3), Cl<sub>2</sub>/O<sub>2</sub>-purified DWCNT (D1), raw SWCNT (rS1-2), Cl<sub>2</sub>-purified SWCNT (S5), Cl<sub>2</sub>/O<sub>2</sub>-purified SWCNT (S1).

are present in various shapes, more or less spherical or crooked particles, with a size in the 5–10 nm range or higher. On the nanometer scale, their structure is quite well ordered with graphitic multi-layer walls observable at high magnification (not shown). Quantifying the carbonaceous impurities within a CNT sample is complex.<sup>48–51</sup> Even if they remain very rough, their content can be estimated from TEM,<sup>28</sup> about 10–30% in these samples. As expected and already reported by applying chlorine alone,<sup>40,41</sup> carbon impurities were not eliminated from the CNT samples (D3 and S5). However, they were completely destroyed as oxygen was added to chlorine (Figure 3, D1 and S1). In the Cl<sub>2</sub>/O<sub>2</sub>-treated samples (D1, D2, S1, S2, S3, and S4), CNTs appear very clean, without any other impurity visible on most of the TEM images (Table 1). From time to time, either metallic or carbon impurities could still be observed, but the efficiency of their removal is really obvious. In the presence of chlorine, the carbon impurities could be selectively eliminated from the CNT samples when O<sub>2</sub> was introduced at 500 °C or higher and at 350 °C or higher for DWCNTs and SWCNTs, respectively. Absorbance spectroscopy, performed on S1 (corresponding to the SWCNTs

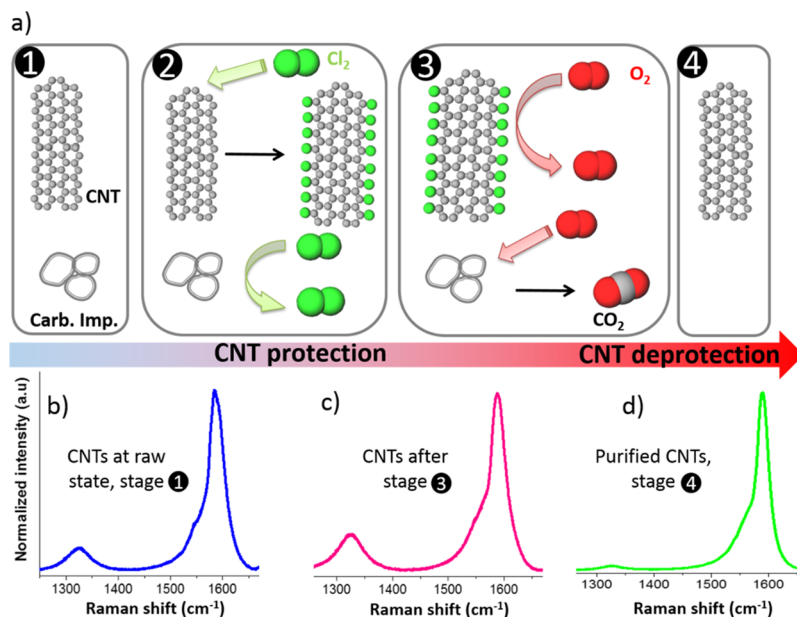
purified by using the optimized conditions), has shown that carbon impurity content was significantly reduced in these purified SWCNTs compared to the raw SWCNTs (cf. Supporting Information, Figure S2). If O<sub>2</sub> is introduced at lower temperature, the amount of carbon impurities with respect to CNTs is similar to what is observed in the respective raw sample. When only oxygen was used (D4 and S6), carbon impurities were not eliminated from the samples (not shown) and combustion of both CNTs and carbon impurities occurred simultaneously, as further discussed from TGA.

Raman spectroscopy is a powerful technique to probe any modification (improvement or damaging) of the CNT structure after a chemical treatment.<sup>52</sup> In a Raman spectrum, the G band (around 1590 cm<sup>-1</sup>) is characteristic of the sp<sup>2</sup> network formed by the double-bonded carbon atoms and the D band (around 1330 cm<sup>-1</sup>) is related to “disorder” or defects when the hybridization of carbon atoms turns to sp<sup>3</sup> through damaging or functionalization. The evolution of the I<sub>D</sub>/I<sub>G</sub> intensity ratio is hence a signature of the structural quality modification of CNTs. Figure 4 gives the variation of the I<sub>D</sub>/I<sub>G</sub> intensity ratio for the studied samples, including Cl<sub>2</sub>, O<sub>2</sub>, and Cl<sub>2</sub>/O<sub>2</sub>-purified CNTs for both DWCNT and SWCNT.



**Figure 4.** Variation of I<sub>D</sub>/I<sub>G</sub> (%) of each treated sample compared to its respective raw CNT sample. <sup>y</sup>From a preceding work (ref 42).

For our treatment conditions, except for S2 with the red incident wavelength (λ = 632.8 nm), for which the temperature (600 °C) for oxygen introduction can be prejudicial to some part of CNTs, I<sub>D</sub>/I<sub>G</sub> was decreased for all the treated samples, meaning that the CNTs were not damaged by any of the applied treatments (Figure 4). The observed decrease in the D band might be due to various



**Figure 5.** (a) Proposed mechanism for the selective removal of carbon impurities. (1)  $t = t_i$ ; (2)  $t \leq t_1$ ; (3)  $t_1 \leq t \leq t_2$ ; (4)  $t = t_f$ ;  $t_x$  is the time sequence as defined in Figure 1. Also, typical Raman spectroscopy spectrum of DWCNTs in the raw state (b), DWCNTs collected just after the  $\text{Cl}_2/\text{O}_2$  step (c), and DWCNTs at the end of the purification procedure (d).  $\lambda_{\text{incident}} = 632.8 \text{ nm}$ .

effects, which can be also combined: (i) curing of CNT defects due to the high temperature used, and (ii) elimination of the most defective CNTs, (iii) removal of amorphous carbon layers deposited on CNTs.<sup>53,54</sup>

**3.2. Impurity Removal Yield, Sample Yield, and Overall Efficiency of the Purification Method.** TGA in air is commonly used to determine oxidized mineral impurity content in CNT samples. With increasing temperature, complete combustion of the carbon species occurs, and the remaining weight corresponds to non-carbon impurities: that is, oxidized metallic impurities. As usually encountered, the oxidized metallic impurities,  $M_r$ , are about 10 wt % ( $\sim 2$  at. %) and 30–45 wt % ( $\sim 7$ –15 at. %) for the used raw DWCNT and SWCNT samples, respectively (Table 1). The atomic content of metal-based impurities,  $n_m$ , was roughly estimated by dividing the metal oxide weight (from TGA) by the molar mass of the corresponding catalyst(s).

Whatever the CNT purification conditions, in the presence of chlorine, the content of the metal residues ( $n_m$ ) falls down to values close to 1 at. % for the two types of samples (Table 1). Removal of metal impurities certainly occurs in the high-temperature range when either  $\text{Cl}_2$  or  $\text{Cl}_2/\text{O}_2$  is used. At these temperatures, metal chlorides are easily formed and their sublimation is favored,<sup>41</sup> leading to their elimination from the CNT samples.

The metal removal yield,  $Y_m$ , is defined as  $Y_m = \frac{M_r - M_p}{M_r}$ , where  $M_r$  and  $M_p$  correspond to the mineral residue content from TGA, that is, the oxidized metallic impurities of the raw and the purified CNT, respectively.  $Y_m$  is relatively good (80–90%), especially for SWCNTs because the raw SWCNT sample contains a large amount of catalyst impurities. That part of remaining metal residues is much more difficult to remove from the samples without destroying the majority of CNTs. It certainly corresponds to the metal nanoparticles already described to be highly protected in the CNT inner channels, their encapsulation occurring during CNT growth by CVD.<sup>5,55–57</sup> For both DWCNT and SWCNT samples, the

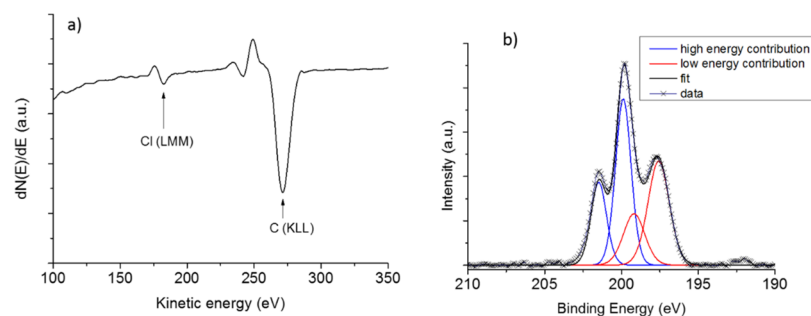
carbon impurities could be efficiently eliminated when  $\text{Cl}_2/\text{O}_2$  was used instead of  $\text{Cl}_2$  alone (Figure 2 and Table 1).

The second relevant parameter to assess a CNT purification process is the carbon consumption ( $C_c$ ) because it eventually allows to appreciate the CNTs lost through the treatment.  $C_c$  corresponds to the carbon loss through purification:

$$C_c = \frac{100 - M_r - (100 - M_p)Y_s}{100 - M_r}, \text{ where } Y_s = \frac{m_p}{m_r} \text{ is the overall sample yield determined from the ratio between the weight of the purified sample } m_p \text{ over the mass of the raw one } m_r.$$

We point out that  $C_c$  includes the consumption of both CNTs and carbon impurities. As expected, increasing  $T_{\text{O}_2}$ , which allows a better catalyst removal, also induces high carbon consumption ( $>50\%$ ) (D2, S4, and S5). Importantly, this consumption is well below 50% for D1 and S1, samples in which metallic and carbon impurities have been removed with good yields for both of them.

In the literature, it is problematic to retrieve the overall sample loss or carbon impurity loss because of the complexity of the applied treatments and the multi-step nature of the methods involved. Regarding DWCNTs, Flahaut et al. have reported an effective elimination of disordered carbon species by air<sup>53</sup> with a sample yield lower than 20%.<sup>31</sup> Selective elimination of carbon impurities from SWCNT samples is found in a few studies. The work by Dementev et al. reported the selective removal of carbon impurities from (arc discharge-produced) SWCNTs by dynamic air oxidation, but metal impurities were not removed.<sup>58</sup> Rosario-Castro et al. used a standard multi-step purification method for purifying HiPco SWCNTs, including a nitric acid treatment followed by wet air oxidation and Soxhlet extraction in HCl, and finally, the sample was annealed at 425 °C.<sup>59</sup> Iron content was reduced by 89%, and carbon loss subsequent to the applied treatments was not determined. Wang et al. applied a wet combined treatment using  $\text{H}_2\text{O}_2$  and HCl. They could decrease the iron content in HiPco SWCNTs by 86% while keeping a carbon yield of 75%, but “little damage” of the CNT sidewalls was reported.<sup>44</sup>



**Figure 6.** Auger (a) and XPS (b) analysis of mD.

Among the purification procedures involved in halogen-based compounds, after the oxidation of iron impurities by oxygen, Xu et al. used a mixture of fluorinated compounds ( $\text{SF}_6$  and  $\text{C}_2\text{H}_2\text{F}_4$ ) to form metal fluorides eliminated by subsequent Soxhlet extraction (multi-step method).<sup>60</sup> The authors reported a SWCNT yield of 68% with “little sidewall damage”. Zimmerman et al. have developed a chlorine-based method consisting of bubbling  $\text{Cl}_2$  in HCl containing SWCNTs, and they lost 96 wt % of the starting HiPco SWCNTs sample.<sup>38</sup> To the best of our knowledge, purification showing a selective elimination of carbon impurities, with low carbon consumption (<50%) and without any CNT damage, has not been reported yet. Remarkably, our results show that the method we propose is able to successfully combine metal elimination and selective attack of carbon impurities among carbon species in a one-pot treatment. The structural quality of the purified CNTs is preserved and even improved without an excessive consumption of the nanotubes.

**3.3. Proposed Mechanism.** We propose a mechanism explaining the combustion selectivity toward the carbonaceous impurities based on the known specific reactivity between halogens and carbon nanomaterials, including CNTs. This mechanism also originates from a deep analysis of the behavior of carbon nanomaterials in an oxidative medium.

The mechanism proposed in Figure 5a is based on several consistent aspects. Figure 5a(1) schematizes the CNTs and the carbonaceous impurities. In this work, from combustion selectivity of the carbon impurities observed with and without chlorine (see, for instance, D1 and D3), it is obvious that chlorine plays the major role in preventing CNT from combustion by oxygen. The reactivity of CNTs with halogens or halogenated compounds has shown remarkable effects in carbon chemistry.<sup>61</sup> For example, regarding fluorine, the easiness<sup>62,63</sup> and reversibility<sup>64,65</sup> of the fluorination of CNTs account for its extensive interest especially because fluorocarbons could be used in a lot of applications. Grafting of chlorine to large  $\text{sp}^2$ -based carbon materials or carbon impurities has been shown to be less favorable than the formation of covalent C–Cl bonds on smaller and high-quality CNTs.<sup>66,67</sup> In our samples, both DWCNTs and SWCNTs have a lower curvature radius (<3 nm) compared to that within the non-nanotube species (>5 nm), as observed by TEM. CNTs with a smaller diameter are thus expected to have a better affinity with chlorine (Figure 5a(2)). Compared to the raw CNTs (Figure 5b), Raman spectroscopy performed on the CNT sample for which the treatment was stopped just after the  $\text{Cl}_2/\text{O}_2$  dwell (mD), on purpose, shows an increase in the D/G ratio compared to the raw CNTs (Figure 5c). The intensity of the D band is decreased at the end of the  $\text{Cl}_2/\text{O}_2$ -process, as shown in Figure 5d and in agreement with Figure 4. We have

not observed any G-band shift probably because of the too small amount of chlorine-containing functional groups present on the CNT walls. Such G-band shift because of doping effect by halogen was reported to be weakly pronounced or not visible after fluorine grafting.<sup>63,68</sup> However, the observed D/G ratio for mD may be attributed to covalent functionalization of the CNT walls by chlorine (cf. also Supporting Information, Figure S3). This hypothesis is also supported by the AES of this CNT sample for which chlorine could be well detected<sup>69</sup> [Figure 6a and Fourier transform infrared (FTIR) results, Supporting Information, Figure S4]. XPS analysis also revealed the presence of chlorine species at the surface of mD (Figure 6b). Two components (each consisting of the 3/2 and 1/2 level with a spin–orbit splitting of 1.6 eV) were required to obtain a satisfactory fit of the Cl 2p core-level spectrum. The low-energy contribution with the  $2\text{p}_{3/2}$  component at ca. 197.5 eV corresponds to more electronegative chlorine atoms probably coming from metal. The high-energy contribution with the  $2\text{p}_{3/2}$  component at ca. 199.9 eV is attributed to chlorine bonded to carbon<sup>70</sup> in agreement with Raman spectroscopy. From XPS, chlorine atomic content was decreased by a factor of almost 2 between mD and D1, being as low as around 0.83 at. % in D1 (Supporting Information, Figure S5).

Even if chlorine is only sparsely attached to the CNTs, its known power as a flame retardant leads to a favored carbon impurity combustion when oxygen is introduced in the reactor. This protective shield against combustion, which has been already suggested without any evidence,<sup>38,42</sup> leads to the combustion of carbonaceous impurities by  $\text{O}_2$  at  $T_{\text{O}_2}$  whereas the CNTs are protected by  $\text{Cl}_2$  (Figure 5a(3)). This protection induces a substantial improvement of removal selectivity between carbonaceous impurities and CNTs close to the combustion temperature (S1, D1). This beneficial effect disappears when  $T_{\text{O}_2}$  is increased, because carbon combustion becomes highly favorable and very fast (S2, S3, and S4). The well-known lability of the C–Cl bond certainly favors the detachment of chlorine from the CNTs by heating (Figure 5a(4),d). On the basis of the proposed mechanism, our method is versatile because purification occurs with optimum efficiency as oxygen is introduced at the combustion temperature of the samples for both DWCNT and SWCNT.

## 4. CONCLUSIONS

This work proposes a solution to the long-standing issue of carbon impurities removal while avoiding excessive attack and consumption of CNTs. The challenge comes from the widely known too close chemical reactivity of carbon impurities and CNTs. This is an important finding because CNT purification



cannot be avoided for a lot of applications and the existing purification methods are time and sample consuming. Our one-pot treatment consists of heating the sample under chlorine up to  $T^{\text{max}}$  (around 1000 °C) and introducing oxygen at a given temperature,  $T_{\text{O}_2} \leq T^{\text{max}}$ . The best treatment is then obtained when  $T_{\text{O}_2}$  corresponds to the combustion temperature range of the CNT sample, as determined by TGA. We have shown that chlorine plays an essential role by combining the removal of metallic impurities and protection of the CNTs from combustion. Moreover, the efficiency of the proposed method has been demonstrated to be due to a substantial increase in the combustion selectivity of the carbonaceous impurities with respect to CNTs. The proposed mechanism appears then to be a powerful tool because it could be easily adapted to other source of carbon nanostructures with other kind of metal impurities (Ni, Al, ...) also. Moreover, the present approach has the enormous advantage to produce, in a one-pot treatment, large volumes of purified CNTs. The developed treatment process hence has a high scale-up potential, and it could open new opportunities for CNT applications.

## ■ ASSOCIATED CONTENT

### 📄 Supporting Information

The Supporting Information is available free of charge on the ACS Publications website at DOI: [10.1021/acs.jpcc.8b12554](https://doi.org/10.1021/acs.jpcc.8b12554).

Experimental conditions for the performed treatments for both DWCNTs and SWCNTs, stability against combustion from TGA under dry air after applying an annealing program under helium, carbon impurity in SWCNT samples investigated by UV–NIR absorbance spectroscopy, chlorine grafting to CNT walls evidenced by RBM analysis from Raman spectroscopy and with FTIR, and XPS wide scans for rD, D1, and mD (PDF)

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### Notes

The authors declare no competing financial interest.

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## Supporting Information

### Protecting Carbon Nanotubes From Oxidation for Selective Carbon Impurity Elimination

N. Berrada, A. Desforges, C. Bellouard, E. Flahaut, J. Gleize, J. Ghanbaja, B. Vigolo

#### 1) Experimental treatment conditions

The treatment conditions used for purifying the DWCNT and SWCNT samples are gathered in Table S1.

**Table S1.** Experimental conditions used for purifying DWCNT and SWCNT samples. The used flow rates are 4 mL/min and 200 mL/min for O<sub>2</sub> and Cl<sub>2</sub>, respectively. <sup>‡</sup> from a preceding work

1

Samples		D1	D2 <sup>‡</sup>	D3	D4	S1	S2	S3	S4	S5	S6
O <sub>2</sub> dwell	Temperature (°C)	500	950	-	500	350	600	800	900	-	350
	Duration (min)	60	60	-	60	60	60	60	20	-	60
Cl <sub>2</sub> dwell	Temperature (°C)	1000	950	1100	-	900	900	800	900	900	-
	Duration (min)	60	120	120	-	60	60	60	20	60	-

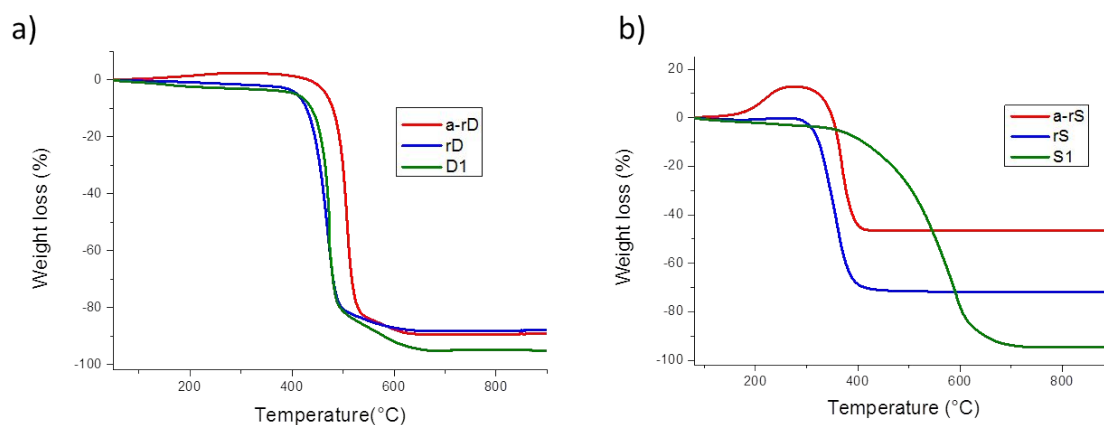
## **2) Stability against combustion highlighted by TGA under dry air**

Both DWCNT and SWCNT samples have been annealed under He ( $O_2 < 0.1$  ppm mole) by following the same heating steps than that used under  $Cl_2/O_2$  for D1 and S1, respectively. The prepared samples are referred to as a-rS and a-rD, respectively. The thermograms (using a Setaram TGA92, temperature ramp  $5^\circ C/min$  under air) were recorded for the two thermally treated samples. The results are shown in Fig. S1.

For the DWCNT samples, we observe a small upshift of the combustion temperature ( $+ 35^\circ C$ ) between the annealed DWCNTs and the raw and the purified samples (rD and D1). The impurity content being quite similar for rD and a-rD, the observed upshift for a-rD treated under inert gas may be due to a healing effect: such effect is obviously not observed for the sample treated under chlorine D1.

For the SWCNT samples, we notice here a high increase (28.0 to 53.6 wt. %) of the remaining mineral impurity content despite the good quality of the inert gas used. The gain in weight starting from  $200^\circ C$ , corresponding to the metal oxidation, is more pronounced after annealing (a-rS). We hypothesize that a carboreduction phenomenon could happen during the annealing process. Indeed, carbon can reduce the metal oxides into metal which is re-oxidized during TGA under air. In that case, carbon is gasified which could explain its relative reduction in weight in the sample. In a-rS, the metal content is higher than that of rS. If we only consider the catalysis effect due to these impurities, the combustion should occur at lower temperature than that of rD. Therefore, the better oxidation stability of a-rS observed after the thermal treatment under He is probably due an annealing effect. For S1, even if such annealing effect cannot be excluded, the much greater combustion temperature observed is probably mainly due to the strong reduction in the metallic impurities.

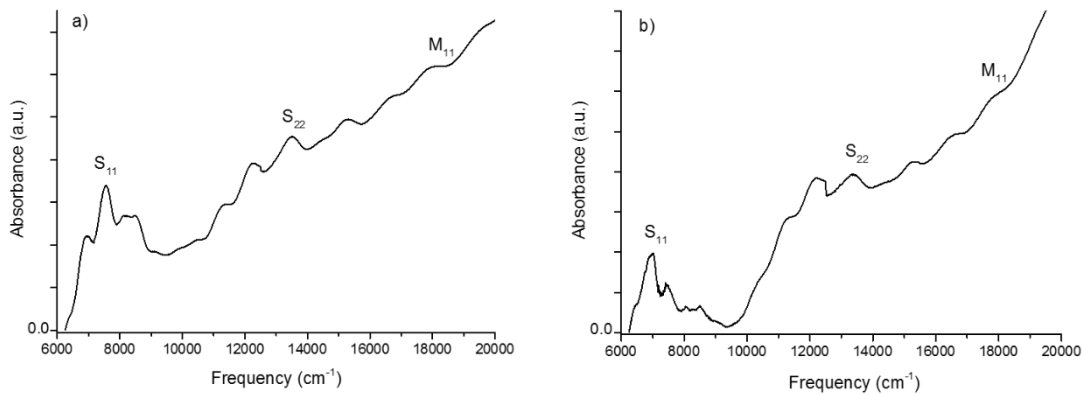
Figure S1 shows the thermograms of the raw, the purified and the thermally treated raw sample for both DWCNTs (Fig. S1a) and SWCNTs (Fig. S1b).



**Fig. S1.** TGA curves (in dry air, temperature ramp 5°C/min) for the (a) DWCNTs and (b) SWCNTs. Respectively, the raw samples rD and rS (blue), the annealed-raw samples a-rD and a-rS (red) and the Cl<sub>2</sub>/O<sub>2</sub> purified samples D1 and S1 (green).

### 3) Carbon impurity investigated by UV-NIR absorbance spectroscopy

Near Infrared (NIR) spectroscopy was carried out by using a Cary 6000i UV-Vis-NIR apparatus from Agilent. The samples were prepared by following the method found in the work reported by Itkis et al.<sup>2</sup> Briefly, 10 mg of the SWCNT powder (rS or S1) was added to 20 mL of N,N-dimethylformamide (DMF). After 10 min of sonication, the solutions were diluted 10 times in order to obtain light grey solutions. Without centrifugation, the supernatant was used for analysis so that the analyzed part was representative of the sample. Figure S2 shows Vis-NIR results for rSWCNT (Fig. S2a) and S1 (Fig. S2b).

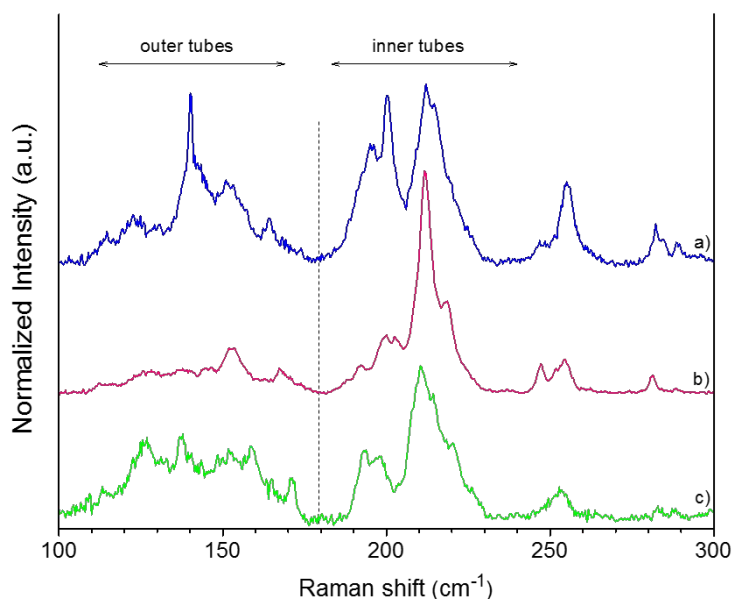


**Fig. S2.** NIR spectra of (a) the raw and (b) the purified SWCNTs by  $\text{Cl}_2/\text{O}_2$  in the optimized conditions (S1).

A semi-quantitative analysis was conducted by using the  $S_{22}$  transition as reported in the work from Itkis *et al.*<sup>2</sup> For our two (rS and S1) samples, after subtracting a baseline, the total area corresponding to the  $S_{22}$  band, the contribution of SWCNTs ( $\pi$ -plasmon) and the carbon impurities, *i.e.* AA(T), and the area of only the  $S_{22}$  feature, *i.e.* AA(S), were calculated between the spectral cutoffs 12500 and 17050  $\text{cm}^{-1}$ . The ratio AA(S)/AA(T) was of 0.0116 and 0.0365 for rS and S1, respectively. Even if an absolute estimation of the purity is difficult to obtain<sup>2</sup>, these results show that the carbon impurity contribution is significantly lower in the purified SWCNTs in agreement with TEM observations.

#### 4) Evidence of chlorine grafting to CNT walls

Figure S3 shows the RBM of the raw DWCNTs (rD) (Fig. S3a), the DWCNTs for which the treatment was stopped just after the  $\text{Cl}_2/\text{O}_2$  dwell at 500°C (mD) (Fig. S3b) and the DWCNTs collected at the end of the  $\text{Cl}_2/\text{O}_2$  purification method (D1) (Fig. S3c).

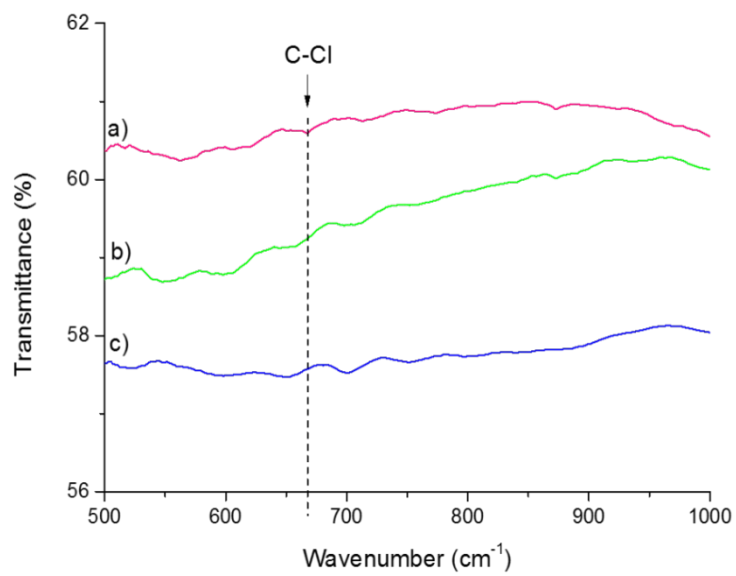


**Fig. S3.** RBMs of (a) rD, (b) mD and (c) D1.  $\lambda_{\text{incident}} = 632.8 \text{ nm}$

Fourier transform infrared (FTIR) experiments were carried out on a spectrometer Agilent 680. The CNT powder was mixed with potassium bromide (KBr) and compacted under pressure to obtain a pellet. Transmission IR spectra were recorded in the 400–4000  $\text{cm}^{-1}$  range. The spectral resolution was 2  $\text{cm}^{-1}$  and 50 scans were co-added for each spectrum.

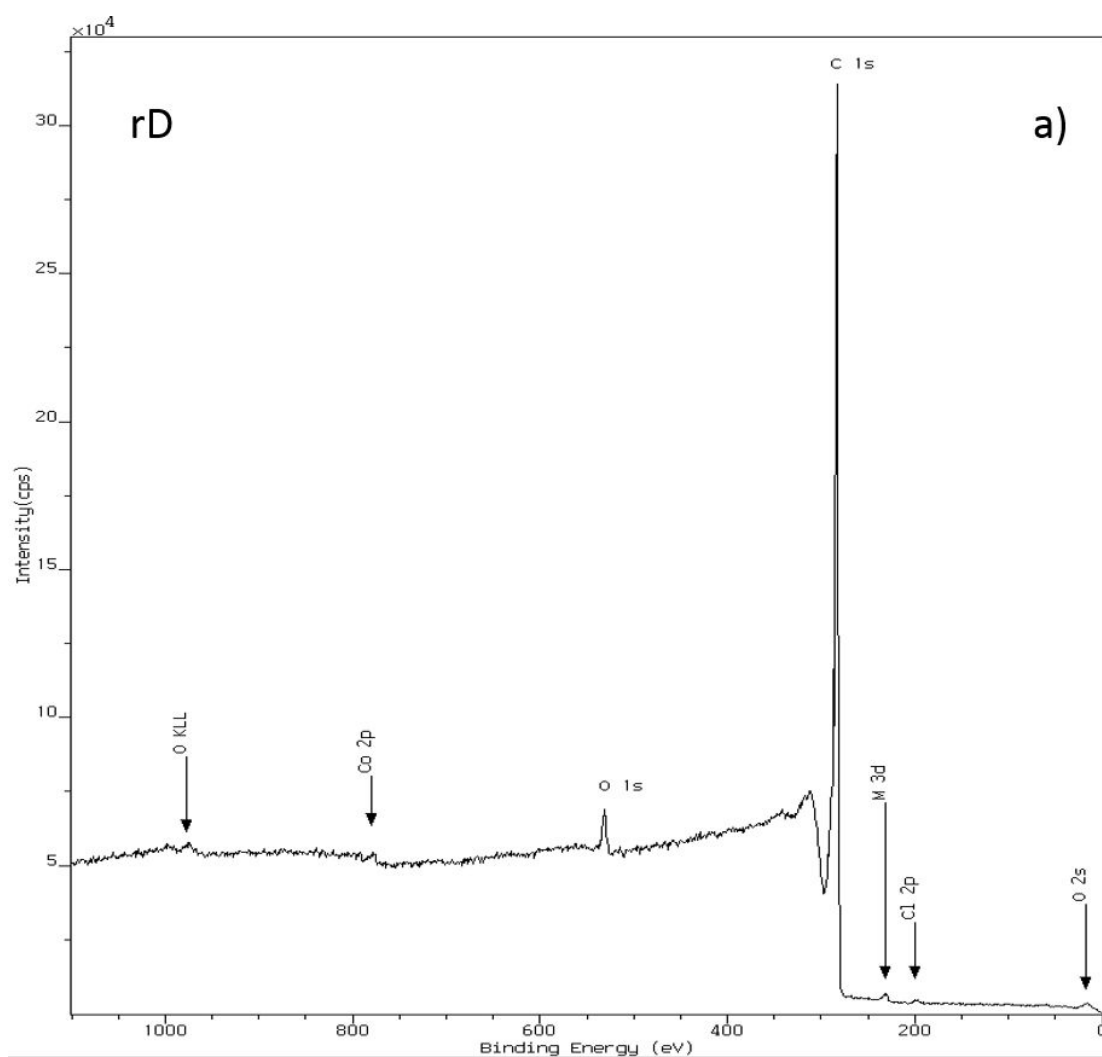
Figure S4 shows IR spectra of the raw DWCNTs (rD) (Fig. S4c), the DWCNTs for which the treatment was stopped just after the  $\text{Cl}_2/\text{O}_2$  dwell at 500°C (mD) (Fig. S4a), and the DWCNTs collected at the end of the  $\text{Cl}_2/\text{O}_2$  purification method (D1) (Fig. S3b). Compared to rD and D1, an additional peak of weak intensity but clearly visible appears at around 667  $\text{cm}^{-1}$ . This feature is assigned to the C-Cl vibrations<sup>3</sup> detected only in mD.



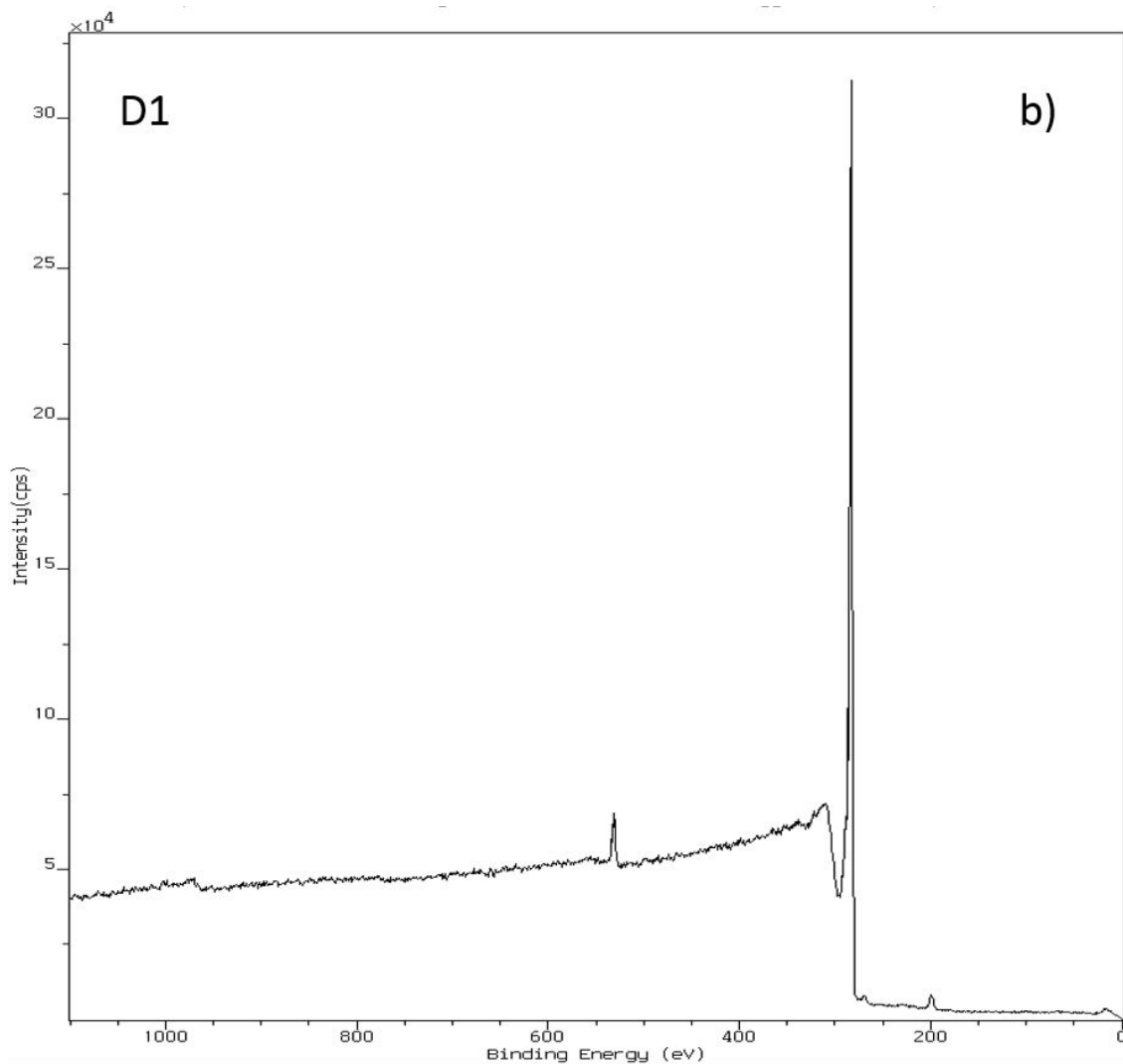


**Fig. S4.** IR spectra of (a) mD, (b) D1 and (c) rD.

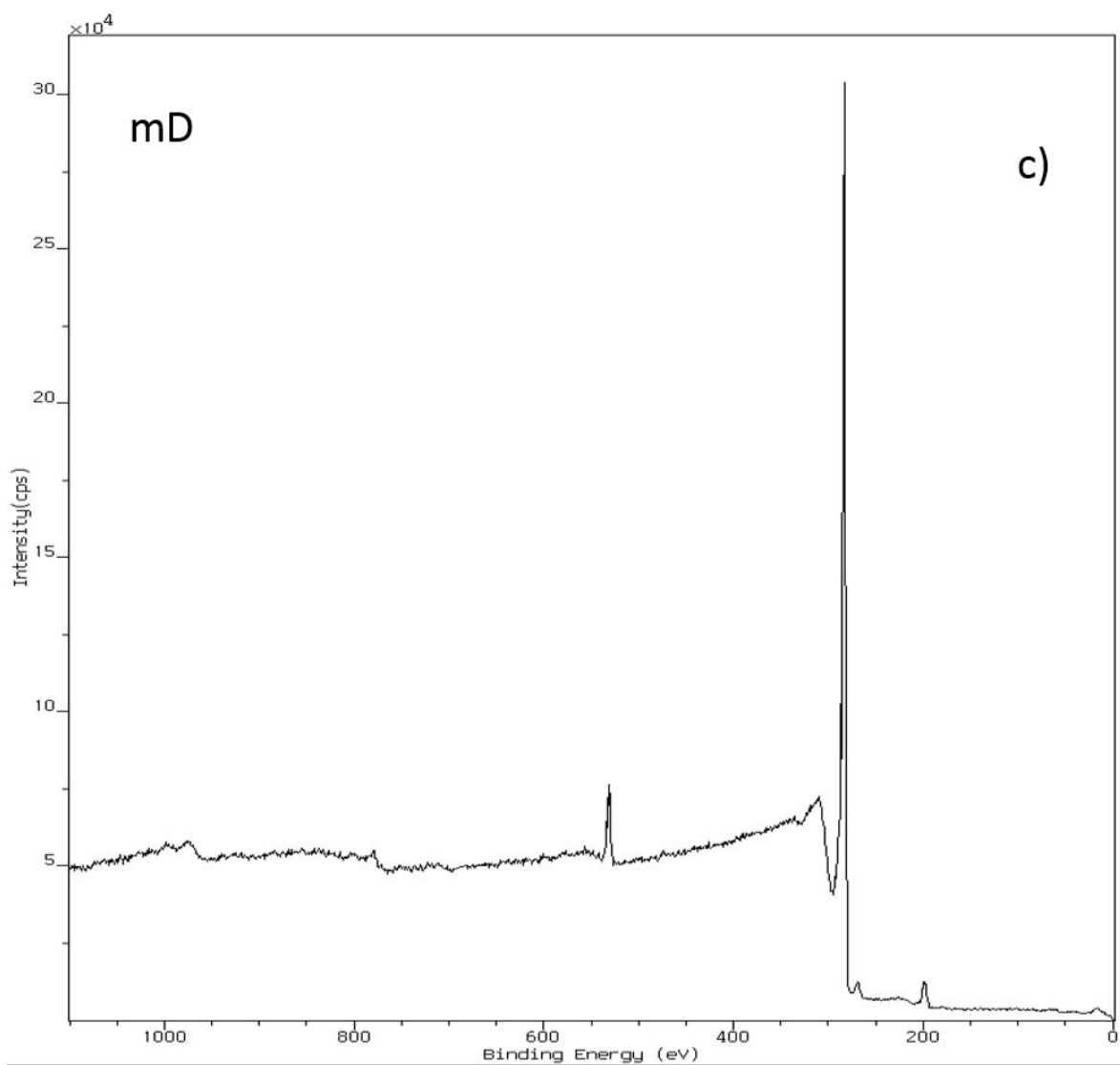
Figure S5 shows the XPS wide scans of rD (Fig. S5a), D1 (Fig. S5b), and mD (Fig. S3c)



Peak	Type	Position BE (eV)	FWHM (eV)	Raw Area (cps eV)	RSF	Atomic Mass	Atomic Conc %	Mass Conc %
Co 2p RDW	Reg	778.110	1.248	357.7	2.393	58.933	0.13	0.63
O 1s RDW	Reg	532.510	2.485	1880.5	0.760	15.999	2.24	2.91
C 1s RDW	Reg	284.210	0.759	28098.7	0.278	12.011	97.28	94.83
Mo 3d RDW	Reg	231.910	1.296	453.0	3.321	95.922	0.13	1.01
Cl 2p RDW	Reg	197.210	3.417	199.6	0.891	35.460	0.22	0.62



<i>Peak</i>	<i>Type</i>	<i>Position BE (eV)</i>	<i>FWHM (eV)</i>	<i>Raw Area (cps eV)</i>	<i>RSF</i>	<i>Atomic Mass</i>	<i>Atomic Conc %</i>	<i>Mass Conc %</i>
<i>O 1s DP8</i>	<i>Reg</i>	<i>532.010</i>	<i>2.542</i>	<i>2180.9</i>	<i>0.780</i>	<i>15.999</i>	<i>2.47</i>	<i>3.22</i>
<i>C 1s DP8</i>	<i>Reg</i>	<i>284.210</i>	<i>0.821</i>	<i>29316.3</i>	<i>0.278</i>	<i>12.011</i>	<i>96.70</i>	<i>94.39</i>
<i>Cl 2p DP8</i>	<i>Reg</i>	<i>199.860</i>	<i>1.360</i>	<i>803.0</i>	<i>0.891</i>	<i>35.460</i>	<i>0.83</i>	<i>2.39</i>



<i>Peak</i>	<i>Type</i>	<i>Position BE (eV)</i>	<i>FWHM (eV)</i>	<i>Raw Area (cps eV)</i>	<i>RSF</i>	<i>Atomic Mass</i>	<i>Atomic Conc %</i>	<i>Mass Conc %</i>
<i>O 1s DP10</i>	<i>Reg</i>	<i>532.190</i>	<i>2.732</i>	<i>3064.3</i>	<i>0.780</i>	<i>15.999</i>	<i>3.60</i>	<i>4.60</i>
<i>C 1s DP10</i>	<i>Reg</i>	<i>284.240</i>	<i>0.871</i>	<i>27809.4</i>	<i>0.278</i>	<i>12.011</i>	<i>94.94</i>	<i>91.24</i>
<i>Cl 2p DP10</i>	<i>Reg</i>	<i>199.840</i>	<i>1.450</i>	<i>1371.0</i>	<i>0.891</i>	<i>35.460</i>	<i>1.47</i>	<i>4.16</i>

Fig. S5. XPS wide scans of a) rD, b) D1 and c) mD.

## References

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- (2) Itkis, M. E.; Perea, D. E.; Jung, R.; Niyogi, S.; Haddon, R. C. Comparison of Analytical Techniques for Purity Evaluation of Single-Walled Carbon Nanotubes. *J. Am. Chem. Soc.* **2005**, *127* (10), 3439–3448. <https://doi.org/10.1021/ja043061w>.
- (3) Li, Y.; Yang, N.; Du, T.; Wang, X.; Chen, W. Transformation of Graphene Oxide by Chlorination and Chloramination: Implications for Environmental Transport and Fate. *Water Res.* **2016**, *103*, 416–423. <https://doi.org/10.1016/j.watres.2016.07.051>.