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Dynamics of non-wetting drops confined in a Hele-Shaw cell

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We experimentally investigate the sedimentation of a non-wetting drop confined between two parallel walls. The whole system is immersed in a bath of liquid of low viscosity and a lubricating film may be dynamically formed between the drop and the walls of the cell. Depending on the thickness of the film and on the viscosity ratio between the droplet and the surrounding liquid, viscous dissipation localizes either in the lubrication layer or in the bulk of the drop. The velocity of the droplet is non-trivial as the thickness of the lubricating layer may depend on the interplay between interfacial tension and viscous dissipation. Interestingly, thin films whose nanometer thickness is set by long range intermolecular interactions may lubricate efficiently the motion of highly viscous droplets. We derive asymptotic models that successfully capture the settling velocity of the drop in the different regimes observed experimentally. The effect of partial wetting is finally illustrated by a sharp increase of the velocity of the drops that we attribute to a wetting transition.

1. Introduction

Droplet dynamics in confined media is a major issue for petroleum engineering as oil extraction commonly involves the displacement of microdroplets through pores of the same scale. The formation of such emulsions stems from various interfacial instabilities such as viscous fingering (Saffman & Taylor 1958; Homsy 1987), splitting in the porous network (Jung *et al.* 2016), snap-off (Gauglitz & Radke 1990; Dangla *et al.* 2013), or capillary instabilities in gradients of confinement (Pihler-Puzovic *et al.* 2012; Al-Housseiny *et al.* 2012; Dias & Miranda 2013; Keiser *et al.* 2016). The resulting multiphase flows generally involve large deformations of the interfaces (Zinchenko & Davis 2017), which in turn modify the flow dynamics and make theoretical predictions of pressure losses complex. Droplet dynamics is however not limited to multiphase flows in porous media. Understanding the motion of a droplet in a confined environment is for instance crucial for digital microfluidics systems, which are currently blooming (Baroud *et al.* 2010; Seemann *et al.* 2012). Such confined droplets may even constitute a model system to describe the motion of biological cells in narrow environments (Zhou *et al.* 2007; Preira *et al.* 2013).

Numerous studies have been dedicated to model systems consisting of isolated droplets or bubbles moving in a uniform channel (Baroud *et al.* 2010). One of the fundamental questions concerns the peculiar viscous dissipation in the vicinity of menisci and contact lines (Snoeijer & Andreotti 2013). Pioneering advances in the field were achieved by

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Landau & Levich (1942) and Derjaguin (1993) who first described the coating of a plate withdrawn from a bath of wetting liquid. This mechanism is dictated by a balance of viscous stresses and surface tension. Bretherton (1961) adapted this problem to the case of a long bubble moving in a capillary tube filled with a wetting liquid. Later works extended this seminal study to the general case of viscous drops (Schwartz *et al.* 1986; Hodges *et al.* 2004). The recent development of digital microfluidic techniques has motivated numerous works on the dynamics of viscous drops confined in Hele-Shaw cells (Shen *et al.* 2014; Huerre *et al.* 2015; Zhu & Gallaire 2016; Ling *et al.* 2016; Yahashi *et al.* 2016). A particular attention has been devoted to the lubricating role of the films of liquid separating the drop from the walls of the cell.

Eri & Okumura (2011) investigated experimentally the settling of non-wetting drops in a Hele-Shaw cell, in the limit where viscous dissipation inside the drop dominates the resistance to the motion. Building up on these results, Yahashi *et al.* (2016) point out the crucial effect of lubricating films between the drop and the walls, in the regime of weakly confined drops. In the present paper, we explore experimentally and theoretically the effect of strong confinement and viscosity ratio between the drop and external liquids.

Drops of dense silicone oil sediment in a vertical Hele-Shaw cell filled with a solution of surfactant of lower viscosity. Depending on the confinement and on the contrast of viscosity, different flow regimes are observed as a function of the ability of the solution to lubricate the displacement of the droplet. In the following sections, we first present the experimental setup and describe the evolution of the sedimentation velocity as a function of the confinement and of the viscosity of the droplets in the ideal case where the surrounding liquid perfectly wets the wall of the cell. In the next section, we discuss these experimental data with different analytical models accounting for a self-lubrication effect. We then illustrate the case of partial wetting and demonstrate how the system may undergo a wetting transition with a dramatic impact on the droplet dynamics. We finally conclude and point out possible implications of our work for the study of the rheology of confined emulsions as encountered in petroleum engineering.

2. Experiments

2.1. Experimental setup

A Hele-Shaw cell made of two parallel glass slides separated by a gap of thickness e ranging from 0.03 to 1 mm is filled with a surfactant solution and maintained vertically (Figure 1a). The solution is composed of 4.5 % in mass of a commercial dishwashing soap (Paic Citron, from Colgate-Palmolive) in deionised water. This concentration is large in comparison with the critical micellar concentration of the soap ($\text{cmc} \simeq 0.05\%$ in mass, determined with the standard Wilhelmy plate method). Such high concentrations should limit gradients in the local surfactant concentration at the interface and thus tend to hinder Marangoni effects. All experiments are conducted at room temperature (20°C) for which the density and viscosity of the surfactant solution are $\rho_w = 997\text{ kg.m}^{-3}$ and $\mu_w = 1\text{ mPa.s}$, respectively.

A drop of fluorinated silicone oil (poly(3,3,3)-trifluoropropylmethylsiloxane, from Gelest, Inc.) is inserted into the gap of the cell. The oil density ρ_o varies from 1220 to 1250 kg.m^{-3} depending on the selected viscosity μ_o ranging from 180 to 18000 mPa.s . The presence of surfactant molecules ensures a non-wetting condition for the oil droplet. In addition, while the interface between pure water and oil is very sensitive to contamination, the large excess of surfactant molecules also impose a reproducible value of the interfacial tension. The radius R of the drop, typically millimetric, is larger than

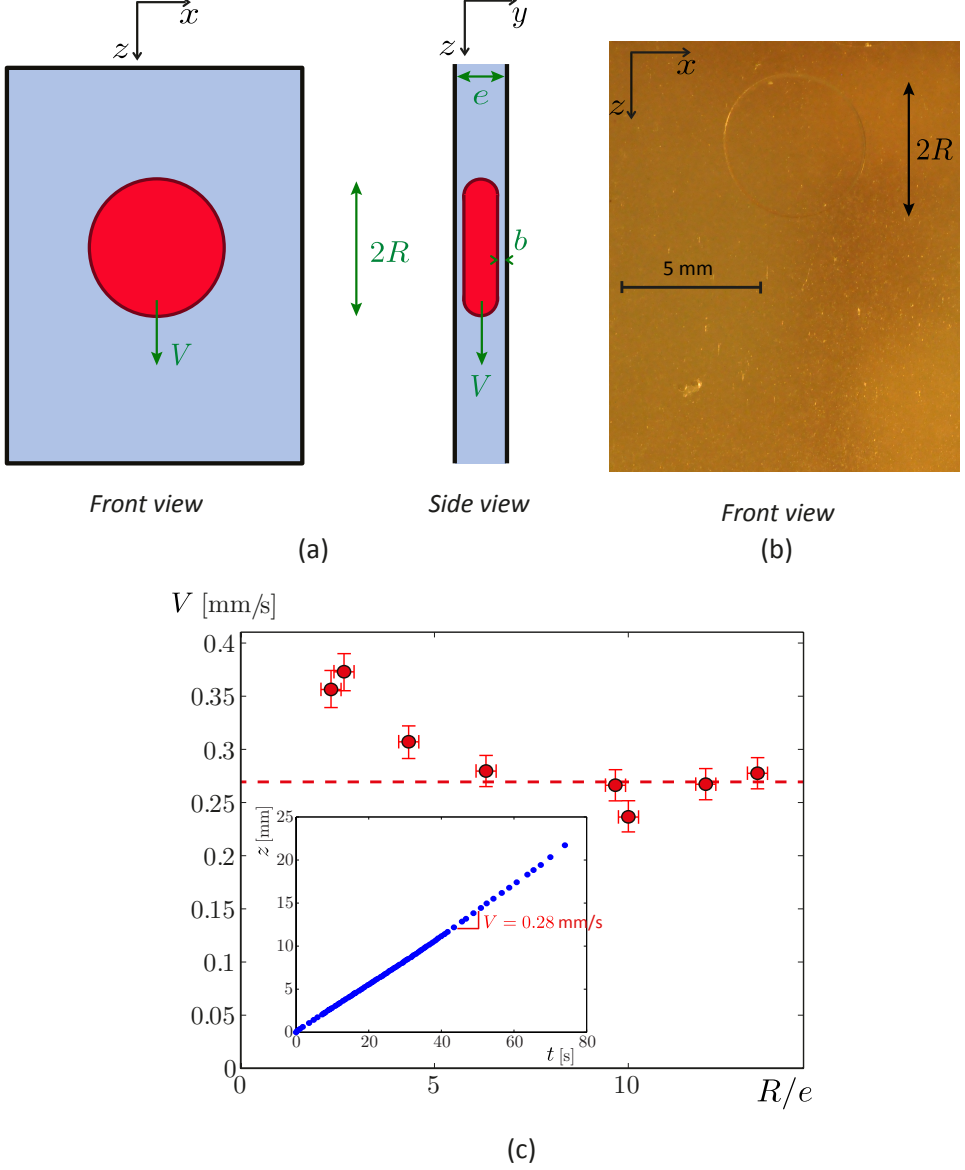


FIGURE 1. (a) Front and side views of the experimental setup: A droplet of fluorinated silicone oil of radius R is introduced in a Hele-Shaw cell of inner gap e immersed in a bath of surfactant solution, and sediments under its apparent weight. A thin layer of solution of thickness b separates the drop from the walls of the cell. (b) Photograph representing the front view of a droplet (top of the picture) of radius $R \simeq 2.5$ mm and of viscosity $\mu_o = 1500$ mPa.s, moving down in a cell of gap thickness $e = 400 \mu\text{m}$. That circular shape has been observed for all droplets, regardless of their velocity. (c) Evolution of V as a function of the ratio R/e , for $\mu_o = 1500$ mPa.s and $e = 400 \mu\text{m}$. For $R/e > 5$, V does not depend significantly on R/e . Inset: typical trajectory of a drop exhibiting a steady velocity (for $\mu_o = 1500$ mPa.s and $e = 400 \mu\text{m}$).

$2e$, so that the volume of these strongly confined puddles is approximately $\Omega = \pi R^2 e$. As the surfactant solution totally wets the cell walls, a thin layer of solution of average thickness b separates the drop from the wall. The water/oil interfacial tension γ is measured with the sessile drop method and is between 5 and 6 mN/m depending on the oil viscosity. Under these conditions, the denser oil drop settles down under gravity at a constant velocity V (see inset of Figure 1b). The sedimentation velocity weakly depends on the size of the drop. We interpret the weak dependence of the velocity as a result of geometry. While droplets adopt the shape of pancakes for high confinement, they tend to be spherical when $e \geq 2R$. As a result, we do not observe any significant evolution for $R/e > 5$. All experiments are thus conducted within this limit.

2.2. Sedimentation velocity

We represent in Figure 2 the evolution of the settling velocity V of confined droplets as a function of the gap e for various values of the oil viscosity μ_o . Regardless of μ_o , V jumps by almost 5 orders of magnitude as e increases from 30 μm to 1 mm.

Interestingly, V appears very weakly dependent on μ_o for low values of e ($e < 50 \mu\text{m}$). In an intermediate regime $50 \mu\text{m} \lesssim e \lesssim 700 \mu\text{m}$, V is a decreasing function of μ_o . Finally, for $e \gtrsim 700 \mu\text{m}$, the settling velocity becomes independent of the oil viscosity. The overall dependence of the drop velocity with its viscosity (see figure 2) is thus weaker than the simple inverse relationship that intuition might suggest. This result is in strong contrast with the opposite case of droplets that totally wet the walls (Reyssat 2014).

Different regimes are observed as a function of the confinement. Two trends are obtained for the lowest gaps ($e \lesssim 500 \mu\text{m}$). While the evolution of the settling velocity seems roughly proportional to e for the highest viscosity, we observe a variation with e^2 for droplets of low viscosity. However, all data tend to collapse in the same curve for larger gaps. The dependence with the gap then follows $V \propto e^6$, which is particularly striking.

3. Lubrication model

The weak dependence of the velocity with the viscosity of the drops suggests that viscous dissipation occurs not only in the drop but also in the thin films of solution separating the droplet from the walls of the cell. The aim of the present section is to identify the lubricating role of these films in the droplet dynamics.

3.1. General analytic expression for the drop velocity

We assume that a confined drop has the shape of a thick disc of volume $\Omega = \pi R^2 e$, since the film thickness b is much smaller than the gap e . The apparent weight of this drop thus writes:

$$F_g = \Delta\rho g \pi R^2 e \quad (3.1)$$

where $\Delta\rho = (\rho_o - \rho_w)$ and $g = 9.81 \text{ m.s}^{-2}$ is the gravitational acceleration. This driving force is balanced by friction forces acting at the surface of the drop. However, due to the large value of the viscosity ratio μ_o/μ_w , we disregard in the following derivations the drag induced by bulk flows of surfactant solution around the drop. We also neglect the friction in the peripheral menisci of surfactant solution around the drop. Both assumptions are justified in Appendix A. Those negligible friction forces may however become dominant in the dynamics of foams (Cantat 2013) or confined bubbles (Reyssat 2014), where the viscosity ratio is conversely very small. In our experiments, the remaining source of friction corresponds to viscous stresses on the walls of the cell over the area $2\pi R^2$ covered

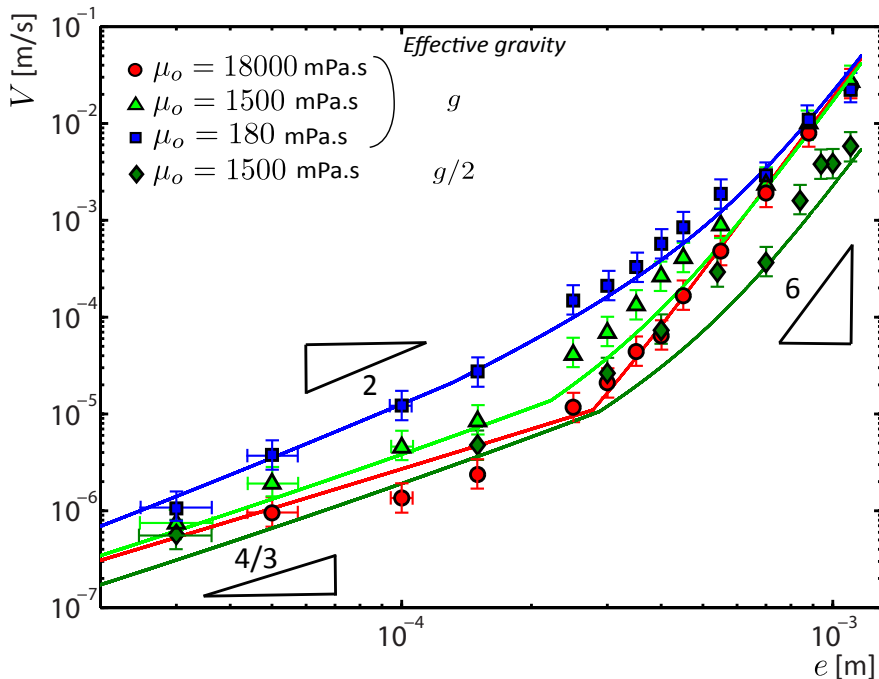


FIGURE 2. Evolution of the velocity of the confined drop V as a function of the gap of the cell e . The blue squares, green triangles and red circles correspond respectively to $\mu_o = 180$ mPa.s, $\mu_o = 1500$ mPa.s and $\mu_o = 18000$ mPa.s. The dark green diamonds correspond to drops of viscosity $\mu_o = 1500$ mPa.s moving with a moderate gravity of magnitude $g/2$, obtained by inclining the cell with an angle of 30° with respect to the horizontal. The straight lines represent the resolution of the implicit Equation 3.19.

by the drop. Since both the driving force and the resistance are proportional to R^2 , the droplet velocity should be independent of the size of the droplet as confirmed by the experiments. We expect this force balance to be valid for large drops, typically within the limit $R/e > 5$ as illustrated in Figure 1. Smaller droplets are less confined by the wall, which changes their dynamics (they tend to move faster than larger ones). The drops are separated from the glass slides by a film of water whose average thickness b is set dynamically by a balance between viscous and interfacial forces. As in the classic problem of a bubble penetrating in a capillary tube, we expect b to be a function of the capillary number $Ca_w = \mu_w V / \gamma$, where μ_w is the viscosity of water, V the velocity of the drop and γ the interfacial tension between the oil and the surfactant solution (Bretherton 1961). In our experiments, Ca_w varies between 10^{-7} and 10^{-2} . However, in contrast with air bubbles, the viscosity of the drop μ_o cannot be neglected when compared with μ_w . Indeed following Schwartz *et al.* (1986), b should also slightly depend on the viscosity ratio μ_o / μ_w .

The velocity profile in a cross section of the Hele-Shaw cell is sketched in Figure 3a. We assume in the following derivations that the flow is directed along the direction of the average velocity V and only varies across the section of the cell. We neglect the two-dimensional component of the flow at the periphery of the drop, as well as transversal flows linked to the formation of “catamaran”-like dimples in the shape of the drops, as described by Huerre *et al.* (2015) and Zhu & Gallaire (2016). We finally define as V_{int} the velocity at the interface, $y = \pm(e/2 - b)$, where $y = 0$ corresponds to the center of the cell.

We now derive the flow profile across the channel. In the region $|y| < (e/2 - b)$, the flow in the droplet follows a standard parabolic profile of average velocity V :

$$v_{drop}(y) = \frac{3}{2}(V - V_{int}) \left[1 - \left(\frac{y}{e/2 - b} \right)^2 \right] + V_{int} \quad (3.2)$$

In the complementary region $e/2 - b < |y| < e/2$, the thin lubricating film undergoes a simple shear flow with a no-slip boundary condition along the walls of the cell:

$$v_{film}(y) = V_{int} \frac{e}{2b} \left(\frac{2|y|}{e} - 1 \right) \quad (3.3)$$

At the oil-film interface ($|y| = e/2 - b$), the continuity of the tangential viscous stress in the drop and in the film imposes $\mu_o \frac{\partial v_{drop}}{\partial y} = \mu_w \frac{\partial v_{film}}{\partial y}$. As $b \ll e$, this leads to:

$$6\mu_o \frac{V - V_{int}}{e} = \mu_w \frac{V_{int}}{b} \quad (3.4)$$

We finally obtain for the velocity at the interface:

$$V_{int} = \frac{V}{1 + m} \quad (3.5)$$

with $m = \mu_w e / 6\mu_o b$. The dimensionless parameter m , quantifies the slipping of the drop with respect to the solid wall: while the limit $m \gg 1$ indicates very inefficient lubrication ($V_{int} = 0$), $m \ll 1$ conversely corresponds to full slip ($V_{int} = V$).

The shear stress exerted by the film of water and the resisting the motion of the drop is $\mu_w V_{int}/b$. Integrating this stress over the area $2\pi R^2$ on both sides of the drop provides the friction force $F_f = 2\pi R^2 \mu_w V_{int}/b$ acting on the drop. Inputting Equation 3.5 leads to:

$$F_f = \frac{2\pi R^2 \mu_w V}{b(1 + m)} \quad (3.6)$$

We finally deduce the droplet velocity from the balance of F_f with the apparent weight:

$$V = \frac{\Delta \rho g e b}{2\mu_w} (1 + m) \quad (3.7)$$

which may also be rewritten as:

$$V = \frac{\Delta \rho g e^2}{12\mu_o} \left(\frac{1}{m} + 1 \right) \quad (3.8)$$

We now describe the asymptotic limits corresponding to $m \gg 1$ and $m \ll 1$, respectively.

3.2. Inefficient lubrication: $m \gg 1$

In the limit $m \gg 1$, the film does not play any significant role. Since $b \ll e$ the flow inside the droplet is described by a classical Poiseuille velocity profile:

$$v(y) = \frac{3}{2}V \left(1 - \left(\frac{2y}{e} \right)^2 \right) \quad (3.9)$$

Integrating the resulting viscous stress over the interface of the drop gives $F_f = 12\mu_o V \pi R^2 / e$, which finally leads to the sedimentation velocity:

$$V_{Pois} = \frac{\Delta \rho g}{12\mu_o} e^2, \quad (3.10)$$

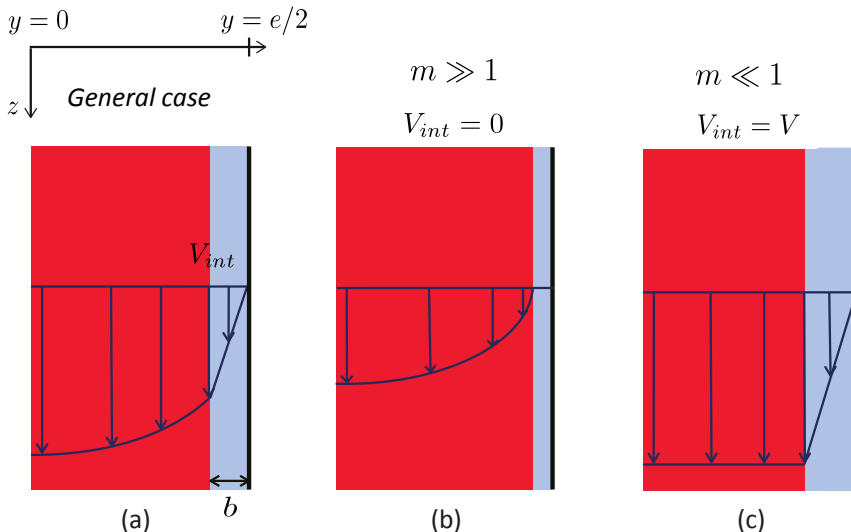


FIGURE 3. a) Velocity profile in a cross section of a half cell, for an intermediate value of the ratio $m = \mu_w e / 6 \mu_o b$. The origin of the y -coordinates is here taken in the middle of the gap, where the z -component of the velocity is maximal. b) Velocity profile in the limit $m \gg 1$. The film of water plays no lubricating role and the droplet undergoes a classical Poiseuille flow. c) Velocity profile in the limit $m \ll 1$. The drop moves as a solid plug and the film of water undergoes a Couette flow of shear rate V/b .

which can also be directly obtained by considering $m \gg 1$ in Equations 3.7. and 3.8. This prediction describes very well the experimental data corresponding to the oil of the lowest viscosity ($\mu_o = 180 \text{ mPa.s}$) and small values of Ca_w , *i.e.* high confinement (Figure 2), with no adjustable parameter (see also the dimensionless Figure 4). However, velocities measured with oils of higher viscosity or cells of larger gaps are higher than predicted in this asymptotic regime. In the following sections, we describe how the surrounding fluid can enhance the mobility of the droplet.

3.3. Full lubrication: $m \ll 1$

In the limit $m \ll 1$, the drop is simply translated as a solid block along the cell, while the lubrication film undergoes a Couette flow of shear rate V/b . The resisting force acting on the plug is thus given by:

$$F_f = 2\pi R^2 \frac{\mu_w V}{b} \quad (3.11)$$

However, the thickness b of the lubrication film should also depend on the dynamics. In his seminal work, Bretherton (1961) describes the film left behind a bubble moving in a capillary tube at velocity V . The thickness of the deposited film follows a non-linear law: $b = 1.34 r Ca_w^{2/3}$, where r is the radius of the tube and the capillary number, $Ca_w = \mu_w V / \gamma$, which compares (thickening) viscous stresses with (thinning) surface tension. This law is in very good agreement with experimental results within the range $10^{-5} \lesssim Ca_w \lesssim 10^{-2}$. At higher capillary numbers, the thickness of deposited the film tends to saturate as it becomes comparable with the radius of the tube (Taylor 1961; Aussillous & Qu  r   2000; Klaseboer *et al.* 2014). In the opposite limit of low Ca_w , repulsive intermolecular interactions become dominant when the thickness of the film falls under a few hundreds of nanometers (Israelachvili 2011). Disjoining pressure may then stabilise nanometric films (Bergeron & Radke 1992) and lead to a saturation of

the coating thickness to a value b_{Π} of the order of tens of nanometers, as first proposed by a referee of Bretherton's paper (Bretherton 1961). This effect was later modelled by Teletzke *et al.* (1988) and Chaudhury *et al.* (2014) and directly observed in a recent study by Huerre *et al.* (2015).

The work of Bretherton (1961) has also been extended to the motion of non-wetting viscous drops, which is relevant to our situation. Schwartz *et al.* (1986), Hodges *et al.* (2004) and more recently Balestra *et al.* (2017) have shown both theoretically and numerically that Bretherton's law should be corrected by a multiplying prefactor P depending of the ratio μ_o/μ_w . Indeed, the finite viscosity of the drop amplifies viscous stresses and results into thicker films. In the range of experimental parameters corresponding to our experiment, P should be close to $2^{2/3}$, which corresponds to the asymptotic value for very viscous drops ($\mu_o/\mu_w \rightarrow \infty$), also derived by Bretherton.

Although the 2D geometry of the present problem is more complex than for the axisymmetric case of capillary tubes (Burgess & Foster 1990; Reichert *et al.* 2018), we propose to extrapolate Bretherton's law to the case of droplets confined in a Hele-Shaw cell, as properly derived by Park & Homsy (1984). The gap of the cell e then replaces the radius r of the capillary tube. However, the moving contact line is not perpendicular to the velocity, except at the apex of the drop. As a consequence, the film separating the drop of oil from the wall is not rigorously uniform, as shown experimentally by Huerre *et al.* (2015). However, we assume in the following that the average thickness of the lubricating layer is set by a relation of the form:

$$b_{Br} = \alpha e C a_w^{2/3} \quad (3.12)$$

where α is a numerical factor of the order of unity.

Nevertheless, we expect such a law to fail for low values of $C a_w$. In this limit, we assume b to be equal to a value b_{Π} dictated by the disjoining pressure in the film (Teletzke *et al.* 1988; Chaudhury *et al.* 2014). The actual value of b_{Π} depends on the type of interactions involved in the disjoining pressure Π_D . In the case of ideal van der Waals forces, we expect the pressure in the film to be $\Pi_D = -A/6\pi b_{\Pi}^3$, where A is the Hamaker constant (Israelachvili 2011). Balancing this pressure with the Laplace pressure $2\gamma/e$ thus leads to:

$$b_{\Pi} = \left(\frac{-A e}{12\pi \gamma} \right)^{1/3} \quad (3.13)$$

Considering $A \sim -10^{-20}$ J, $\gamma \sim 5 \cdot 10^{-3}$ mN/m and $e \sim 50 \mu\text{m}$, we obtain a typical estimate of $b_{\Pi} \sim 10$ nm. Nevertheless, molecular interactions are not limited to van der Waals forces. Other terms such as electrostatic repulsion may also play a role in the disjoining pressure and lead to other expressions for the film thickness. However, we expect the order of magnitude of b_{Π} to remain on the order of a few tens of nanometers. Studying in detail the evolution of such thin films is beyond the scope of the current work. As detailed below, our experiment nevertheless constitutes a way to probe such thin films. We hope our study will motivate future investigations.

In the following sections we describe the regimes corresponding to both Bretherton and van der Waals limits.

3.3.1. Bretherton film limit: $b > b_{\Pi}$ (self-lubrication)

Inputting Bretherton's law in Equation 3.11 provides the friction force acting on the drop:

$$F_f = \frac{\mu_w^{1/3} \gamma^{2/3} V^{1/3}}{\alpha e} 2\pi R^2 \quad (3.14)$$

Interestingly, the friction force is a sub-linear function of the velocity, as discussed in more details at the end of the paper. Balancing this force with gravity, we obtain:

$$V = \frac{\alpha^3}{8} \frac{(\Delta\rho g)^3}{\mu_w \gamma^2} e^6 \quad (3.15)$$

As mentioned earlier, α should be independent of the viscosity ratio, since $\mu_o/\mu_w > 100$ in our experiments (Schwartz *et al.* 1986; Hodges *et al.* 2004; Balestra *et al.* 2017). Within this limit, V should almost be independent of μ_o and be proportional to e^6 as observed experimentally (Figure 4). Fitting the experimental data with equation 3.15 provides an estimate of the numerical prefactor $\alpha = 0.7 \pm 0.05$. This regime is very similar to the self-lubrication behavior observed in self-propelled droplets in capillary tubes (Bico & Qu  r   2002) and in sedimenting droplets in Hele-Shaw cells (Yahashi *et al.* 2016).

Rescaling Equation 3.15 by the velocity V_{Pois} (Equation 3.10), we obtain the dimensionless velocity \tilde{V} :

$$\tilde{V} = \frac{3\alpha^3}{2} \frac{\mu_o}{\mu_w} \left(\frac{e}{\ell_c} \right)^4 \quad (3.16)$$

This dependence of the rescaled velocity \tilde{V} on $(e/\ell_c)^4$ may be observed on the dimensionless graph, on the Figure 4.

3.3.2. Van der Waals film limit: low Ca_w

In this regime, $b = b_{II}$ which leads to a friction force $F_f = 2\pi R^2 \mu_w V/b_{II}$. We thus expect the settling velocity of the droplet to be:

$$V = \frac{\Delta\rho g b_{II}}{2\mu_w} e = \frac{\Delta\rho g}{2\mu_w} \left(\frac{-Ae^4}{12\pi\gamma} \right)^{1/3} \quad (3.17)$$

As in the previous regime, the velocity is independent of μ_o , but is now proportional to $e^{4/3}$. Experimental data are in fair agreement with this prediction for strongly confined drops ($e < 200 \mu\text{m}$) of the highest viscosity, as illustrated in Figure 2. Adjusting Equation 3.17 leads to an estimation of the Hamaker constant $A \simeq -2 \cdot 10^{-20} \text{ J}$. This evaluation of A corresponds to thicknesses b_{II} ranging from 10 to 30 nm depending on the confinement, which is comparable to the values reported by Huerre *et al.* (2015). Rescaling Equation 3.17 by the velocity V_{Pois} (Equation 3.10), we obtain the dimensionless velocity \tilde{V} for the van der Waals limit:

$$\tilde{V} = \left(\frac{18}{\pi} \right)^{1/3} \frac{\mu_o}{\mu_w} \left(\frac{-A}{\gamma e^2} \right)^{1/3} \quad (3.18)$$

3.4. Configuration diagram

The three regimes described in the previous section correspond to different asymptotic solutions of the equation:

$$V = \frac{\Delta\rho g e}{2} \left(\frac{e}{6\mu_o} + \frac{\max(b_{II}; b_{Br})}{\mu_w} \right) \quad (3.19)$$

where b_{Br} and b_{II} are respectively defined by Eqs. 3.12 and 3.13. We arbitrarily assume that $b = \max(b_{II}; b_{Br})$. Although the transition between both film regimes is actually smoother, we found this simple interpolation to be in good agreement with experiments. The implicit Equation 3.19 can be solved numerically and captures correctly the experimental data obtained for different values of viscosity ratio and effective gravity, as represented in Figure 2.

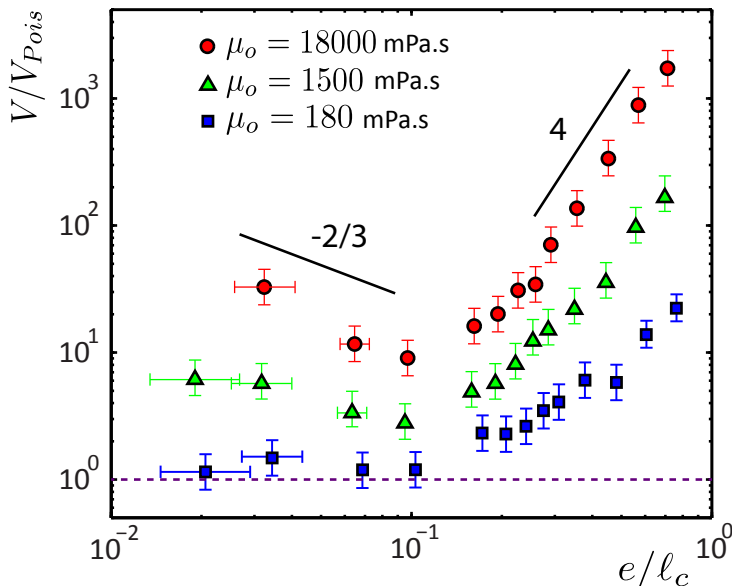


FIGURE 4. Dimensionless velocity $\tilde{V} = V/V_{Pois}$ as a function of the rescaled gap thickness e/ℓ_c , with ℓ_c the capillary length. The purple dashed line corresponds to the Poiseuille regime characterized by $\tilde{V} = 1$. For most of the experimental measurements, the rescaled velocity \tilde{V} is larger than unity, which enhances the lubricating role of the films of water between the drop and the walls.

Using equation 3.10, Equation 3.19 may be rewritten in a dimensionless implicit form:

$$\tilde{V} = 1 + 6 \frac{\mu_o}{\mu_w} \max \left(\left(\frac{-A}{12\pi\gamma e^2} \right)^{1/3} ; \frac{\alpha}{12^{2/3}} \left(\frac{\mu_w}{\mu_o} \right)^{2/3} \left(\frac{e}{\ell_c} \right)^{4/3} \tilde{V}^{2/3} \right) \quad (3.20)$$

In figure 4 we plot the dimensionless velocity \tilde{V} as a function of confinement e normalized by the capillary length ℓ_c . The lubricating properties appear clearly here, as $\tilde{V} \geq 1$ for all data points. The drops of the most viscous oils ($\mu = 18000$ mPa.s) are always fully lubricated, either by a Bretherton film ($\tilde{V} \propto e^4$) or by a van der Waals film ($\tilde{V} \propto e^{-2/3}$). Less viscous oils benefit less from the lubricating properties of water films. In particular, for oils less viscous than about 200 mPa.s, the regime dominated by dissipation in the drop is clearly observed ($\tilde{V} = 1$, blue squares in figure 4).

Describing the problem in terms of configuration diagram may be useful to get a global view of the different regimes. For a given oil viscosity, two or three regimes may be observed as the gap is increased. For very high confinement the thin film of water acts as a lubricant and the settling velocity is proportional to $e^{4/3}$ in the case of an ideal van der Waals film, as defined in Equation 3.17. In the opposite limit, self lubrication plays a leading role and leads to V proportional to e^6 as described by Equation 3.15. Between both regimes, the effect of the film may be negligible and the droplet undergoes a classical Poiseuille flow with a velocity varying with e^2 (Equation 3.10). We define as $e_{4/3 \rightarrow 2}$ and $e_{2 \rightarrow 6}$ the characteristic gaps at the transitions from the regimes $V \propto e^{4/3}$ to $V \propto e^2$ and $V \propto e^2$ to $V \propto e^6$, respectively. Both characteristic gaps are readily deduced by equating the corresponding velocities:

$$\frac{e_{4/3 \rightarrow 2}}{\ell_c} = \left(\frac{\mu_o}{\mu_w} \right)^{3/2} \left(\frac{-18}{\pi} \frac{A}{\gamma \ell_c^2} \right)^{1/2} \quad (3.21)$$

and

$$\frac{e_{2 \rightarrow 6}}{\ell_c} = \left(\frac{2}{3\alpha^3} \frac{\mu_w}{\mu_o} \right)^{1/4} \quad (3.22)$$

where $\ell_c = (\gamma/\Delta\rho g)^{1/2}$ is defined as the capillary length, whose value is generally of the order of 1 mm (in our particular system, $\ell_c \simeq 1.5$ mm).

However a direct transition from the regime $V \propto e^{4/3}$ to $V \propto e^6$ can also be observed if $e_{4/3 \rightarrow 2} > e_{2 \rightarrow 6}$. This transition is characterized by the following gap:

$$\frac{e_{4/3 \rightarrow 6}}{\ell_c} = \left(\frac{-16}{3\pi\alpha^9} \frac{A}{\gamma\ell_c^2} \right)^{1/14} \quad (3.23)$$

This direct transition is only observed for the highest viscosity ratios:

$$\frac{\mu_o}{\mu_w} > \left(\frac{\pi^2}{486\alpha^3} \frac{\gamma^2 \ell_c^4}{A^2} \right)^{1/7} \quad (3.24)$$

In our system, the numerical value of the right hand side of Equation 3.24 is of the order of 1650, which is in fair agreement with our experimental observations. Indeed we can clearly define two regimes ($V \propto e^2$ and $V \propto e^6$) for $\mu_o = 180$ mPa.s, and two regimes ($V \propto e^{4/3}$ and $V \propto e^6$) for $\mu_o = 18000$ mPa.s. However, the two low-velocity regimes $V \propto e^{4/3}$ and $V \propto e^2$ seem transitional in the intermediate case $\mu_o = 1500$ mPa.s (Figure 2). We present in Figure 5, the configuration diagram corresponding to these different transitions. In the case of high contrast of viscosity, the deposited film plays the role of a lubricant, which leads to settling velocities proportional to e and e^6 for respectively strong and weak confinements. Conversely, dissipation is concentrated in the bulk of the droplet when the contrast in viscosity is modest, which results in a velocity proportional to e^2 .

4. Partially wetting drops: lubrication film properties recovered through a wetting transition

In contrast with the ideal complete wetting situation described so far, practical configurations commonly involve partial wetting. In such cases, we do not expect to obtain any lubricating film below a certain value of Ca_w (Marchand *et al.* 2012), which should strongly affect the droplet dynamics. We performed a series of experiments where the solution of surfactant is replaced by ethanol. In this system, ethanol partially wets the walls of the cell with a receding contact angle of the order of 30° . The viscosity of ethanol is $\mu_w = 1.2$ mPa.s at 20°C .

In Figure 6, we plot V as a function of e for drops of oil of respective viscosities $\mu_o = 180, 1500$ and 18000 mPa.s. At the lowest values of e (most confined cells), V tends to follow the regime described by Equation 3.10 (dashed lines), which corresponds to a Poiseuille flow without any lubrication. In contrast with the previous experiments conducted with a wetting solution, this regime is obtained with oils of all viscosities, which confirms the absence of a lubricating film. As the thickness of the cell is increased, we observe a jump in the velocity for a critical thickness. This jump is particularly dramatic for the most viscous oils: the velocity increases by two orders of magnitude for the oil of viscosity 18000 mPa.s. Beyond this critical thickness, the settling velocity follows the self-lubrication regime described by Equation 3.15. We interpret the jump as the consequence of a wetting transition: a lubricating film is deposited as Ca_w reaches a critical value. This critical velocity has been discussed in simpler geometries for a

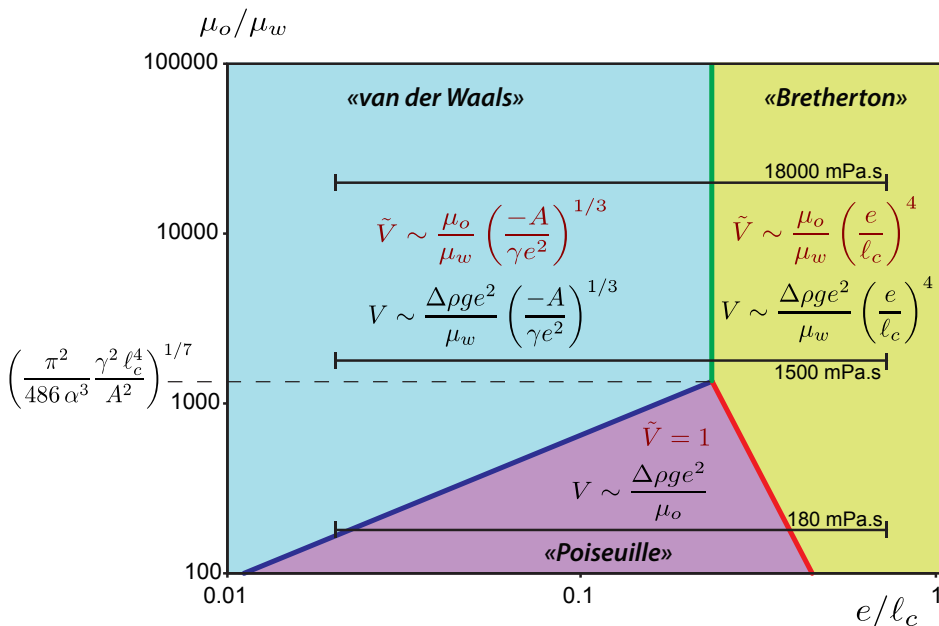


FIGURE 5. Configuration diagram describing the different asymptotic regimes as a function of the gap of the cell and of the viscosity ratio. The range of parameters explored in our experiments are represented with the horizontal lines corresponding to the different oil viscosities. Depending on the viscosity ratio, one or two transitions can be observed. The frontiers between each regime are represented by colourful lines. Blue, green and red lines correspond respectively to Equations 3.21, 3.22 and 3.23. In each domain, the asymptotic expression of the velocity V corresponds to the scaling of Equations 3.17 (cyan domain), 3.15 (yellow domain) and 3.10 (magenta domain). The scaling of the rescaled expression $\tilde{V} = V/V_{Poise}$ is written in brown, and correspond respectively to Equations 3.18, 3.16 and by definition $\tilde{V} = 1$.

variety of viscosity contrasts (Eggers 2001; Lorenceau *et al.* 2003; Snoeijer *et al.* 2006; Marchand *et al.* 2012). In the present case, the deposited fluid is much less viscous than the oil in the drops, which is reminiscent from the air entrainment problem. In this limit, Eggers and Lorenceau *et al.* found that the critical velocity for entrainment depends logarithmically on the viscosity ratio, while Marchand *et al.* rather suggest a stronger power-law dependence on the viscosity of air. However, in our experiments the component of the velocity normal to the contact line varies along the boundary of the drop (Burgess & Foster 1990). This component decreases from the front to the sides of the drop, which should delay or smoothen the transition. We also observe an important scattering of the experimental data due to a high sensitivity to local imperfections. As a general trend, smaller drops tend to undergo the transition for lower gaps than larger drops. Following the steps of the recent works of Hammoud *et al.* (2017) and Zhao *et al.* (2018), a better characterization of this transition may be achieved in the axisymmetric geometry of a capillary tube.

5. Conclusion

Our experimental study describes the sedimentation velocity of a droplet of viscous oil in a Hele-Shaw cell filled with a less viscous solution ($\mu_o/\mu_w \gg 10$). Depending on the confinement and on the wetting properties of the solution, different regimes are

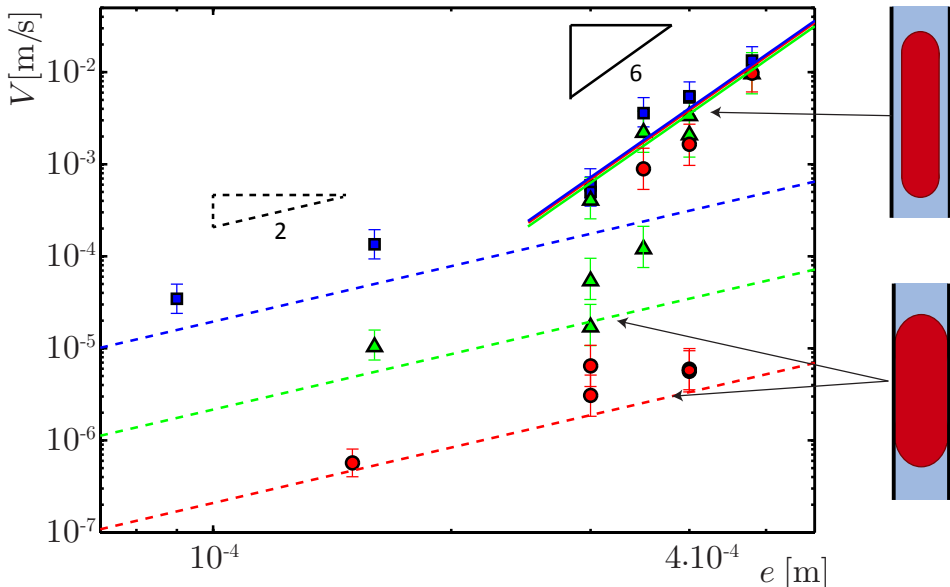


FIGURE 6. Settling velocity V as a function of the gap of the cell e for partially wetting drops of oil in a cell filled with ethanol. Blue squares, green triangles and red circles correspond respectively to $\mu_o = 180$ mPa.s, $\mu_o = 1500$ mPa.s and $\mu_o = 18000$ mPa.s. We interpret the important jump observed beyond a critical gap to be a consequence of a wetting transition. The dotted lines correspond to the “Poiseuille regime” (equation 3.10) and the solid lines correspond to the “self-lubricated” regime with a Bretherton film (equation 3.15, with $\alpha = 0.7$)

observed. In particular, we demonstrated a possible self-lubrication effect of the droplet by the solution, which dramatically amplifies the sedimentation mobility. In the absence of lubrication, the sedimentation velocity scales as $\Delta\rho g e^2 / \mu_o$. However, self-lubrication leads to a velocity proportional to e^6 in the case of low confinement and to a velocity proportional to $e^{4/3}$ for high confinements (in the case of a wetting solution). Although we mainly focused on the case of a perfectly wetting carrying liquid, we observe a stiff signature of a wetting transition in the case of partial wetting.

This work may also provide some insight into the rheology of dense emulsions in confined environments. Such a situation is indeed common in petroleum engineering when the size of oil droplets is of the same scale as the pores of the reservoirs. By analogy with standard rheology data, we can define an effective viscosity $\mu_{eff} \sim \Delta\rho g e^2 / V$ and express it as a function of the apparent shear rate V/e . The three different regimes presented in Figure 5 correspond to the following expressions:

- Lubrication through the thin van der Waals film: $\mu_{eff} \sim \mu_w e / b \Pi \sim \mu_w \left(\frac{\gamma e^2}{-A} \right)^{1/3}$,
- Absence of lubrication: $\mu_{eff} = \mu_o$,
- Lubrication through the Bretherton film: $\mu_{eff} \sim (\mu_w \gamma^2 e^2)^{1/3} (V/e)^{-2/3}$.

If the apparent shear rate could be increased as a control parameter, the confined emulsion would thus appear as a shear thinning fluid. The effective viscosity is constant at low shear rate and displays a power law behavior with an exponent $-2/3$ for high shear rates. Such a behavior is reminiscent of classical works on the rheology of foams and concentrated emulsions, although dissipation in Plateau borders tends to lead to a lower exponent (Princen & Kiss 1989; Denkov *et al.* 2008; Cantat 2013; Cohen-Addad & Höhler 2014).

In our model, we assumed the lubricating film to be uniform in order to simplify the description of the system,, which is not rigorous as demonstrated experimentally by Huerre *et al.* (2015). Nevertheless, we hope that our work will motivate further investigations where the thickness profile and, more generally, the impact of the 2D geometry of the droplet will be taken into account.

Finally, our experiments demonstrate the critical role of the lubricating film of water in the dynamics of highly viscous drops. As a perspective, it might be expected that any variation of the thickness of that film, induced by e.g. rough (Seiwert *et al.* 2011) or slippery (Li *et al.* 2014) walls, could hinder the self-lubrication regime (equation 3.15) and thus dramatically modify the mobility of the drops.

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Appendix A

We here justify our choice to neglect the resisting contribution of the flow of water in the front and rear menisci as well as in the bulk around the drop.

Dissipation in the bulk of water surrounding the drop

The resisting force resulting from the flow of water around the drop scales as $F_w^{bulk} = 12\pi\mu_w VR^2/e$ which has to be compared to the friction force $F_f = 2\pi R^2\mu_w V_{int}/b$, exerted by the walls on the drop. Using Equation 3.5, we obtain: $F_w^{bulk}/F_f = 6b(1+m)/e$. As plotted in Figure 7a, this ratio is at most 2.10^{-1} within the range of our experimental parameters. The contribution of viscous dissipation in the bulk of the surrounding water to the overall friction force can thus be neglected.

Dissipation in the front and rear menisci

Following recent work on the motion of wetting droplets in Hele-Shaw cells (Reyssat 2014) or on the dissipation involved in the displacement or deformation of foams (Cantat 2013; Sauret *et al.* 2015; Viola *et al.* 2016), we expect the friction force resulting from the flow in the advancing and receding menisci of water around the drop to follow $F_w^{menis} \simeq 20\gamma RCa_w^{2/3}$. Comparing Equation 3.6 with this force yields: $F_w^{menis}/F_f \simeq 3b(1+m)Ca_w^{-1/3}/R$. As plotted in Figure 7b, this ratio is of the order of 0.2 for the largest gaps, but lower than 0.1 for more confined drops, which justifies that the contribution of the menisci may be neglected in the overall estimation of the friction.

Inertial resistance of water

The inertial resistance of the displaced water also hinders the motion of the drop and scales as $F_i \sim \rho_w V^2 Re$. The comparison of inertia to the friction force acting on the surface of water written in Equation 3.6 leads to $F_i/F_f = \rho_w Vbe(1+m)/\mu_w R$, which can be viewed as the relevant Reynolds number. For our experiments, this Reynolds number remains smaller than 1 as long as $e < 1$ mm, which justifies neglecting the contribution

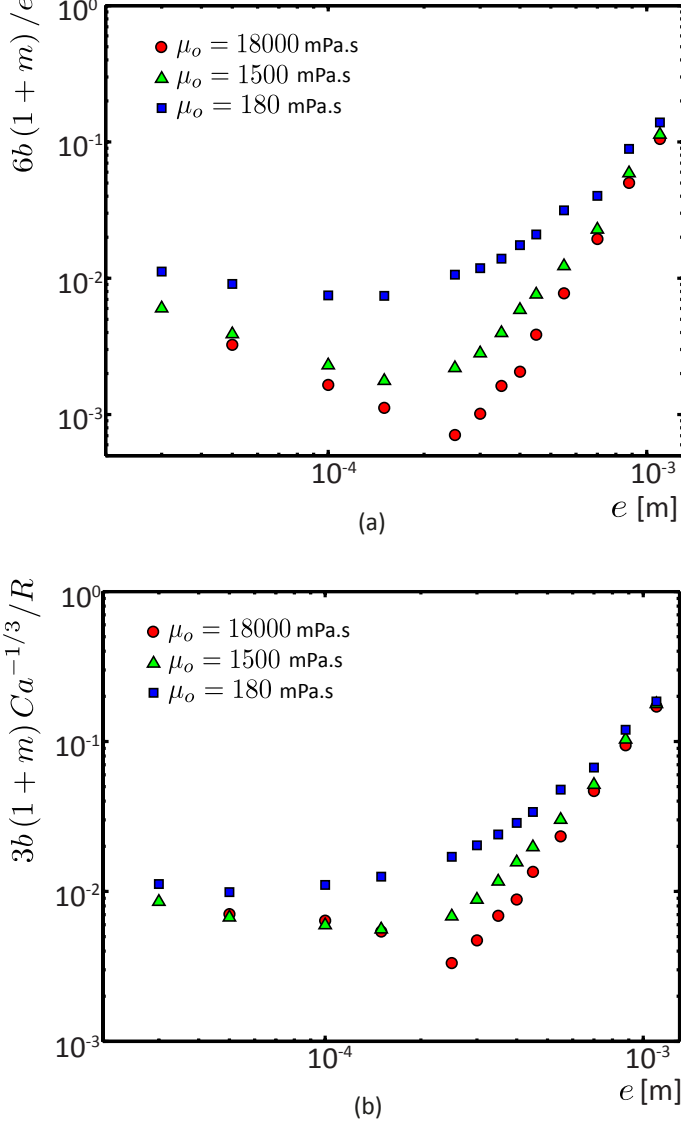


FIGURE 7. (a) Ratio of the viscous force from the bulk of the surrounding liquid to the force exerted by the lubrication film as a function of e . Blue squares correspond to $\mu_o = 180$ mPa.s, green triangles to $\mu_o = 1500$ mPa.s, and red circles to $\mu_o = 18000$ mPa.s. The ratio roughly corresponds to $6b(1+m)/e$, and its value is smaller than 0.2 for all the experiments, so that the contribution of the surrounding liquid is negligible. (b) Ratio of the viscous force in the menisci at the periphery of the drop to the force from the lubrication film as a function of e . $F_w^{menis}/F_f \simeq 3b(1+m)Ca_w^{-1/3}/R$, is smaller than 0.2 for all the experiments and the contribution of the menisci may be neglected.

of inertia in the fluid surrounding the drop in the overall drag force. For $e > 1$ mm the drop velocity is observed to saturate as inertial resistance starts to dominate.

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