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Shear bearing capacity of RC slabs without shear reinforcement:

Design codes comparison

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Abstract

For reinforced concrete structures, as beams, slabs or walls, failure under bending is well known and its description and design is relatively internationally agreed. However for the shear failure phenomenon, there is not yet a common agreement at the international level, no consensus is reached on the subject at this time. Many parameters are involved in the shear resistance mechanism and many phenomena coexist. The shear force transfer mechanisms are sometimes complex and difficult to discern. By analyzing the different shear design codes, some shear parameters are taken into account and ignored by others, which makes that a shear effect may be omitted. In addition, different ways are adopted to take into account the different shear parameters. The main purpose of this study is to help the engineering by presenting a comparative study of all the main analytical models for the determination of shear capacity: The EN 1992-1-1:2005 standard (EC2) (**CEN, 2005**), French National Annex (**FD P 18-717, 2013**), ACI 318-14 (**ACI Committee 318, 2014**), fib Model Code 2010 (**Fib Model Code 2010, 2012**) using level of approximation LoA I and LoA II and (**CSA Committee A23.3, 2004**) both Modified Compression Field Theory (MCFT) based models, and finally the Critical Shear Crack Theory (CSCT) which is the basis of the Swiss

standard SIA 262 (SIA 262, 2003) are all examined. The results obtained are discussed regarding their agreement with eighteen shear experimental results on thick slabs (30cm, 35cm, and 40cm) and thin slabs (10cm) without shear reinforcement.

Keywords: reinforced concrete slabs; shear strength; standards results; experimental results

Nomenclature

a_v	clear shear span: face-to-face distance between the load and the support
a	horizontal distance from the axis of the load to the axis of the support
a_g	maximum diameter of aggregate
A_s	area of longitudinal tension steel
b_w	web width
b_{eff}	effective width at the support in shear
d	effective depth of the cross-section
E_c	modulus of elasticity of concrete
E_s	modulus of elasticity of reinforcement
f_{ck}	nominal characteristic cylinder compressive strength
$f_{cm,meas}$	measured cylinder compressive strength of the concrete at the age of testing
k	factor taking into account the size effect according to NEN-EN 1992-1-1:2005
k_v	factor determining the shear capacity in the fib Model Code 2010
M	bending moment at the control section
P_u	measured peak load in an experiment
V	shear force at the control section
V_{exp}	shear force at failure in the experiment
V_{EC2}	shear capacity calculated according to European NEN-EN 1992-1-1:2005
V_{France}	shear capacity calculated according to French National Annex
V_{ACI}	shear capacity calculated according to American ACI 318-14

V_{MCFT}	shear capacity calculated according to Modified Compression Field Theory
V_{MC}	shear capacity calculated according to fib Model Code 2010
V_{CSA}	shear capacity calculated according to Canadian CSA A23.3-04
V_{CSCT}	shear capacity calculated according to Critical Shear Crack Theory
β	aggregates interlocking factor in the MCFT
β_{EC2}	factor taking into account arching action in European practice
ϵ	strain in the CSCT control depth
ϵ_x	strain in the fib-Model Code 2010 control depth
γ_c	concrete partial safety factor in European practice
s_{xe}	effective crack spacing accounting for aggregate size in the fib Model Code 2010
ρ_l	ratio of flexural reinforcement in the longitudinal direction
ρ_t	ratio of flexural reinforcement in the transverse direction

1 Introduction

Structural concrete standards provide recommendations for calculating the shear strength of reinforced concrete (RC) slabs or beams are based on various parameters affecting shear strength. These parameters influence various mechanisms that jointly support the shear forces. The understanding of these different mechanisms or transmission modes of shear force which act in cracked concrete is a key element for the study of shear failures of RC members. Due to cracking, several shear mechanisms must be activated in order to guarantee the loads transmission to the supports. The shear strength of RC slabs and beams is ensured by the following main mechanisms (**ASCE-ACI Committee 445 on Shear and Torsion, 1998**): the shear stresses in uncracked concrete which involves the concrete compressive strength, the interlocking effect of aggregate which involves the aggregate size, the dowel action which involves the amount of longitudinal reinforcement, the residual tensile stresses, and an eventually arching effect. The shear parameters

considered by the codes for estimating shear strength are those related to materials, such as concrete compressive strength, aggregates size, longitudinal reinforcement ratios, geometric parameters such as the ratio a_v/d , then the member depth related to size effect phenomenon. For having safe and economical design rules, it is important to have a solid understanding of the shear behaviour of RC structures. However this is difficult because many parameters are involved in the resistance mechanism and many phenomena coexist there. In addition, the shear force transfer mechanisms are sometimes complex and difficult to discern. The complexity of the problem widely debated since the last century (**Joint Committee on Concrete and Reinforced Concrete, 1916**), (**Balázs, 2010**), (**Marí et al., 2015**) explains why there is still no unified and completely realistic theory of shear behavior of slabs and beams and that the calculation methods adopted by engineering communities are often empirical or semi-empirical.

From the examination of shear design standards, no consensus is reached allowing determining the shear capacity of RC structures in the best way. There is not yet a common agreement on the important shear parameters (**Shioya et al., 1990**), (**Brown et al., 2006**), the shear mechanisms (**Bažant et al., 2007**), (**Collins et al., 2008**) and therefore the best standard. Depending on the standards, as illustrated in **Table 1**, the effect of some shear parameters which intervene in the resistance mechanism is omitted, consequently abandoning eventually a shear aspect in the capacity calculation. In addition, the standards adopt different ways to take into account the different shear parameters. Some models for calculating shear strength are quite readily distinguishable from one another: the European standard EC2 (**CEN, 2005**), the French National Annex FNA (**FD P 18-717, 2013**), the American standard ACI (**ACI Committee 318, 2014**), the Canadian standard CSA (**CSA Committee A23.3, 2004**), the fib Model Code (**Fib Model Code 2010, 2012**), the Swiss standard SIA (**SIA 262, 2003**). These standards are for the most part based on different theoretical methods or researchers approaches. The European standard EC2 and American standard ACI 318 of an empirical nature are based on Regan's works (**Regan, 1987**) and

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(Bresler and MacGregor, 1967) works respectively. The Canadian standard CSA23.3 and fib Model Code 2010 are both derived on the Modified Compression Field Theory MCFT of (Vecchio and Collins, 1986) and the Swiss standard SIA 262 derives from the Critical Shear Crack Theory CSCT of (Muttoni, 2003). Both MCFT and CSCT based calculation models are physical (mechanical) models based on strain notion resulting in the opening of a critical shear crack and could provide a common approach for shear design. Such a method takes into account the crack lips roughness in order to apprehend their ability to transmit shear forces through aggregates interlocking effect.

Table 1 : Shear parameters considered depending on the standards

Parameters	EC2	FNA	ACI	CSA	SIA	Fib Model Code
<input type="checkbox"/> Compressive strength: f_c	<input checked="" type="checkbox"/>					
<input type="checkbox"/> Aggregate size: d_{max}	<input checked="" type="checkbox"/>					
<input type="checkbox"/> Ratio: a/d	<input checked="" type="checkbox"/>					
<input type="checkbox"/> Long. reinforcement ratio: ρ_l	<input checked="" type="checkbox"/>					
<input type="checkbox"/> Transv. reinforcement ratio: ρ_t	<input checked="" type="checkbox"/>					
<input type="checkbox"/> Size effect related to depth: d_l	<input checked="" type="checkbox"/>					

: The parameter is taken into account by the standard
 : The parameter is ignored by the standard

The main purpose of this study is to help the engineering by focusing on the different predictions provided by all the main shear design provisions in order to formulate recommendations for engineers designing RC slabs without stirrups through analytical investigation. Both the case of thick and thin slabs is studied. The following models for estimating the shear strength of RC slabs are all examined: European (CEN, 2005), French (FD P 18-717, 2013), American (ACI Committee 318, 2014), Model Code (Fib Model Code 2010) with LoA I and LoA II approximation levels, and the Critical Shear Crack Theory (CSCT). Note that the LoA II of the fib

Model Code 2010 corresponds to the Canadian standard CSA23.3 (**CSA Committee A23.3, 2004**).

The results obtained are discussed regarding their agreement with experimental results. The tests were carried out by varying on the slabs the different shear parameters, and also examining different slab configurations.

2 Shear design models

2.1 Eurocode 2 (EC2) and French National Annex (FNA) models

To estimate the shear capacity of a RC cross-section not containing shear reinforcement and without axial load, the European standard EN 1992-1-1: 2005, Section 6.2.2 (**CEN, 2005**) takes into account the effects of the longitudinal reinforcement ratio ρ_l , the concrete compressive strength f_{ck} , and a size effect through a factor k . Recommendations are also provided to take into account the influence of an eventual arch effect occurring for low values of the ratio a_v/d . Note that the influence of the concrete aggregates size is omitted. The shear strength is calculated as given by **Equation 1** (f_{ck} in MPa). It is an empirical relation, first proposed by (**Regan, 1987**) on the basis of the experimental results.

$$V_{EC2} = \text{Max} \begin{cases} [C_{Rd,c} \cdot k \cdot \sqrt[3]{100 \cdot \rho_l \cdot f_{ck}}] \cdot b_w \cdot d = V_{Rd,c1} \\ [v_{min}] \cdot b_w \cdot d = V_{Rd,c2} \end{cases} \quad (1)$$

where:

$$k = 1 + \sqrt{\frac{200}{d}} \leq 2.0$$

$$C_{Rd,c} = \frac{0.18}{\gamma_c}$$

$$\rho_l = \frac{A_{sl}}{b_w \cdot d} < 2\%$$

k is the size effect factor. When increasing the effective depth d (in mm) its value decreases, thus allowing accounting a size effect phenomenon. $C_{Rd,c}$ is an empirical factor used for characteristic

shear strength. Its value derives from comparison with experimental results of (Regan, 1987) and a reliability analysis on 176 tests (König and Fischer, 1995). b_w is the smallest width of the cross-section (in mm). In the case of slabs under concentrated load, a shear effective width b_{eff} instead of entire width b_w is used.

v_{min} represents the minimum shear stress that can be carried by the member. Its expression is based on the idea that, for low longitudinal reinforcement ratios, the shear capacity can never be less than the flexural capacity (Walraven, 2013). EN 1992-1-1: 2005 (CEN, 2005) therefore recommends:

$$v_{min_EC2} = 0.035k^{3/2}\sqrt{f_{ck}} \quad (2)$$

However, in the requirements of the French formulation FNA (FD P 18-717, 2013) another approach is adopted to calculate v_{min} :

$$v_{min} = \begin{cases} 0.23\sqrt{f_{ck}} & (3) \\ 0.053k^{3/2}\sqrt{f_{ck}} & (4) \end{cases}$$

(3) For slabs having an aptitude of transverse redistribution of loads and walls,

(4) For beams and other types of the slab.

Arching action is accounted assuming that the contribution of a load applied within $0.5d \leq a_v \leq 2d$ to the design shear force V_{Ed} may be reduced by the factor $\beta_{EC2}=a_v/2d$.

2.2 ACI 318-14 model

As European standard (CEN, 2005), the American standard (ACI Committee 318, 2014), Section 22.5.5.1, also takes into account the compressive strength of concrete f_{ck} and the longitudinal reinforcement ratio ρ_l in the estimation of the shear capacity. However, unlike the European standard which evaluates the effect of the reinforcement directly through ρ_l , the American standard considers the associated reinforcement strain (or stress) in the critical section at failure. According to (ACI Committee 318, 2014), it is not the longitudinal reinforcement ratio per se that governs the shear strength but the ratio $M/\rho Vd$. When adopting the ratio between the

moment and shear at the section, the shear strength was related to the strain demand in the longitudinal reinforcement. (Khaja and Sherwood, 2013) also confirmed this by showing that the increase of ρ_l with the simultaneous increase of a/d in order to make the ratio $M/\rho Vd$ constant will lead to shear failure stresses that are also constant (with $(a/d)/\rho = M/\rho Vd$). Note that (ACI Committee 318, 2014) does not consider both the influence of size effect and aggregate size on shear strength. For normal weight concrete ($\lambda = 1$), the shear strength is calculated as (f_{ck} in MPa):

$$V_{ACI} = \left(0.16\sqrt{f_{ck}} + 17\rho_l \frac{Vd_l}{M} \right) b_w d_l \leq 0.29\sqrt{f_{ck}} b_w d_l \quad (5)$$

Equation 5 is a semi-empirical formula recommended by (ACI-ASCE Committee 326, 1962) and developed by (Bresler and MacGregor, 1967) based on experimental results of 194 beams. The quantity Vd/M in **Equation 5** cannot exceed one. In addition, the $17\rho_l(Vd/M)$ term is generally negligible in case of practical designs according to (Bresler and Cordelis, 1963). (ACI Committee 318, 2014) also provides a simplified formula (**Equation 6**) used by most engineers that do not consider the effect of longitudinal reinforcement.

$$V_{ACI_simplified} = 0.17\sqrt{f_{ck}} b_w d_l \quad (6)$$

2.3 MCFT based models: Fib Model Code 2010 and CSA A23.3

Several shear design codes including (Fib Model Code 2010, 2012), (CSA Committee A23.3, 2004) or (AASHTO, 2004) derive from the Modified Compression Field Theory (MCFT) of (Vecchio and Collins, 1986). The concrete compressive strength, longitudinal reinforcement quantity, size effect and aggregate size are all taken into account by these models, unlike (CEN, 2005) which omits the aggregates size or (ACI Committee 318, 2014) which omits both the aggregates size and the size effect. In the MCFT approach, the failure shear stress v_{MCFT} (**Equation 7**) is determined through a factor β which characterizes the competence of the cracked concrete to transfer the shear stress by aggregates interlocking. The higher the value of β , the higher the aggregate interlock capacity.

$$v_{MCFT} = \frac{V_{MCFT}}{b_w \times d} = \beta \times \sqrt{f_c} \leq 0.25 \quad \text{with } \sqrt{f_c} \leq 8 \text{ MPa} \quad [f_c \text{ in MPa}] \quad (7)$$

The MCFT allows to find the value of β through the resolution of the equations it provides (**Vecchio and Collins, 1986**). However, solving these equations is a very time consuming effort. They require either to use tabular formats, or to perform iterations, and thus to have an appropriate computer program. In addition, many engineers prefer simple equations to tabular formats because they are more convenient for spreadsheet calculations. A simplified approach to MCFT utilizing continuous functions for shear capacity has therefore been developed by (**Bentz et al., 2006**), (**Bentz and Collins., 2006**) in which a simplified expression (**Equation 8**) was given for find the value β .

$$\beta = \frac{0.40}{(1 + 1500\varepsilon_x)} \times \frac{1300}{(1000 + s_{xe})} = (\text{strain effect term}) \times (\text{size effect term}) \quad (8)$$

In this simplified theory (SMCFT- Simplified Modified Compression Field Theory), the estimation of the factor β is founded on the fact that the crack width w is equal to the product of the mean strain normal to the crack ε and the cracks spacing s in the normal direction ($w = \varepsilon \times s$). It is known that aggregates interlocking capacity is intrinsically related to the width of the crack, the wider the crack, and the less effective the mechanism. However, the width of the cracks increases with the crack spacing and the longitudinal strain in the member (**Walraven, 1981**). Consequently, the shear capacity will decrease with all actions increasing the longitudinal strain or crack spacing as wider cracks will occur. Higher values of the longitudinal strain can be obtained, for example, by applying a tension axial load to the element, by decreasing the amount of the reinforcements or use reinforcements with low Young modulus, by increasing the ratio M/V at the section. At the opposite, the application of an axial compression load for example will reduce the cracks formation and thus increases the shear capacity. All these actions are known as "strain effect". The size effect phenomenon is also taken into account through a "size effect" term. If the size effect is now an

established experimental fact, its explanation is a complex problem in structures involving different approaches. The approach based on the fracture mechanics allows explaining the phenomenon. However, according to the MCFT, the size effect is caused by a reduction in the crack lips capacity to adequately transmit the shear forces through aggregates interlocking, due to crack opening. (Shioya et al., 1990) showed that the longitudinal cracks spacing at the mid-depth of RC beams and slabs not containing shear reinforcement tends to be about one-half of effective depth d , irrespective of the value of d . Consequently, if the depth increases, the crack spacing at mid-depth will increase and simultaneously the width of the cracks linked to the crack spacing will also increase. The parameter β in the SMCFT is therefore estimated as the product of a "strain effect term" and a "size effect term". (Lubell et al., 2009) work showed that adopt an approach by considering the effects on the shear strength of size effects and strain effects as independent effects was a conceivable simplification. s_{xe} in the expression of β is an "equivalent crack spacing factor" as defined in **Equation 9**. The longitudinal strain at the mid-depth of the member ϵ_x is calculated as defined in **Equation 10** for sections for sections without prestressing and without axial forces.

$$s_{xe} = \frac{35s_x}{(16 + a_g)} \geq 0.85s_x \quad (9)$$

$$\epsilon_x = v_{MCFT} \times \frac{1 + \frac{M}{Vd}}{2E_s \rho} = \left(\frac{\frac{M}{d} + V}{2E_s \times A_s} \right) \quad (10)$$

The crack spacing parameter s_x can typically be taken as $0.9d$ and a_g the maximum aggregate size. M is the bending moment in the control section and V the corresponding shear force. A_s is the cross-sectional area of the longitudinal reinforcements and E_s their Young modulus.

a. Fib Model Code 2010: LoA I and LoA II

This code is based on comprehensible physicommechanical models and represents a significant advance compared to empirical methods. The code (Fib Model Code 2010, 2012) contains four levels of shear strength approximation (LoA I to LoA IV) (Muttoni and Fernández,

2012) consisting in addressing a computation by increasing the level of complexity leading to more precise results. Consequently, results closer to reality should be obtained for a higher LoA. The LoA I and LoA II have been analyzed in this study. The LoA II of the **(Fib Model Code 2010, 2012)** corresponds to the SMCFT. The shear capacity for a structural member not containing shear reinforcement is calculated as indicated in **Equation 11** where k_v is a parameter with the same physical sense as β that is different depending on the level of approximation (LoA). Confronted to the LoA I, the LoA II gives a more precise value of the parameter k_v . In the LoA I, s_{xe} is assumed by simplification to be equal to 1.25 (maximum aggregate size > 9.6 mm) and the longitudinal strain is assumed to be half the yield strain of the reinforcements which leads to $\epsilon_x = 0.00125$ for reinforcements with $f_{yk} = 500$ MPa and $E_s = 200$ GPa.

$$V_{\text{Model Code}} = k_v \times \frac{\sqrt{f_{ck}}}{\gamma_c} \times b_w \times d \quad (11)$$

$$k_v(\text{LoA I}) = \frac{180}{(1000 + 1.25d)} \quad (12)$$

$$k_v(\text{LoA II}) = \beta = \frac{0.40}{(1 + 1500\epsilon_x)} \times \frac{1300}{(1000 + s_{xe})} \quad (13)$$

Note that according to fib-Model Code 2010, arching action is also accounted assuming that the contribution of point loads applied within a distance of $d \leq a_v \leq 2d$ from the face of the support to the design shear force V_{Ed} may be reduced by the factor $\beta_{\text{Model Code}} = \beta_{\text{EC2}} = a_v/2d$.

b. CSA A23.3 model

As the **(Fib Model Code 2010, 2012)**, the Canadian standard **(CSA Committee A23.3, 2004)** is also a Simplified Modified Compression Field Theory (SMCFT) based model and is equivalent to the LoA II. The shear capacity is therefore given by:

$$V_{\text{CSA}} = \frac{0.40}{(1 + 1500\epsilon_x)} \times \frac{1300}{(1000 + s_{xe})} \times \frac{\sqrt{f_{ck}}}{\gamma_c} \times b_w \times d \quad (14)$$

2.4 Critical Shear Crack Theory (CSCT)

As the (Fib Model Code 2010, 2012), the CSCT introduced and developed by (Muttoni and Schwartz, 1991), (Muttoni, 2003a), (Muttoni, 2003b), (Muttoni and Ruiz, 2008) also derives from mechanical models which enable a physical understanding of tests results. The proposed theory also considers the influence of many shear governing parameters (concrete compressive strength, longitudinal reinforcement quantity, size effect and aggregate size) and has been introduced into the Swiss code for structural concrete (SIA 262, 2003) after reasonable simplifications.

According to CSCT, the shear capacity of members not containing shear reinforcement is governed by the width and the roughness of the critical shear crack. The critical shear crack theory reflects this dependency as expressed in **Equation 15** where w is the critical shear crack width, and a_g refers to the maximum aggregate size which considers the roughness of the crack lips.

$$\frac{V_{\text{CSCT}}}{b_w d} = \sqrt{f_c} \times f(w, a_g) \quad [\text{MPa, mm}] \quad (15)$$

The CSCT assumes that the critical crack width w is proportional to the product of the longitudinal strain ε in the control section (the control depth is located at a distance $0.6d$ from the compression face) times the effective depth of element d . On the basis of these assumptions, the shear strength for elements not containing shear reinforcement is given by **Equation 17**.

$$w \propto \varepsilon \times d \quad (16)$$

$$\frac{V_{\text{CSCT}}}{b_w d \sqrt{f_c}} = \frac{1/3}{1 + 120 \frac{\varepsilon \times d}{16 + a_g}} \quad (17)$$

The longitudinal strain ε in the control section can be approximated using the linear elasticity theory, assuming that the Navier-Bernoulli hypothesis according to which the plane sections remain plane after deformation is verified (the concrete tensile strength is neglected). For sections not

subjected to axial loads, the strain in the control depth can be estimated by using the bending moment M in the control section (**Equation 18**). The compression zone depth x is calculated by **Equation 19** in which E_c refers to the Young modulus of concrete.

$$\varepsilon = \frac{M}{d \times \rho \times E_s \times \left(d - \frac{x}{3}\right)} \times \frac{0.6d - x}{d - x} \quad (18)$$

$$x = d \times \rho \times \frac{E_s}{E_c} \times \left(\sqrt{1 + \frac{2E_c}{\rho E_s}} - 1 \right) \quad (19)$$

Note that the (**SIA 262, 2003**) model is just a simplified design method based on the CSCT shear capacity expression (**Equation 17**). Some reasonable hypotheses are assumed (**Muttoni and Ruiz, 2008**). First, it is assumed to calculate ε that the depth of the compression zone x is equal to 0.35d (which is a reasonable value accounting for various reinforcement ratios and concrete strengths), thus:

$$\varepsilon = \varepsilon_s \times \frac{0.6d - x}{d - x} \cong 0.41 \times \varepsilon_s \quad (20)$$

Then the reinforcement strain ε_s is assumed proportional to the bending moment M_{Ed} . At yielding ($M_{Ed} = M_{Rd}$), its value is $\varepsilon_s = f_{yd}/E_s$ with $f_{yd} = f_{yk}/\gamma_s$ the design strength of the reinforcement. At last, the flexural strength can be estimated according to the theory of plasticity as $M_{Rd} = \rho d^2 f_{yd} (1 - \rho f_{yd} / (2 f_{cd}))$ with $f_{cd} = f_{ck} / \gamma_c$ the design concrete compressive strength. Considering these assumptions, the CSCT expression leads to the simplified expression below for (**SIA 262, 2003**).

$$\frac{V_{SIA}}{b_w d \sqrt{f_{ck}}} = \frac{0.3/\gamma_c}{1 + \frac{50}{16 + a_g} \times \frac{f_{yk}}{\gamma_s E_s} d \frac{M_{Ed}}{M_{Rd}}} \quad (21)$$

3 Experimental program

3.1 Thick slabs

To investigate the RC slabs behaviour under shear loading, an experimental campaign consisted in testing eleven full-scale thick slabs without stirrups, with various thicknesses of 30cm, 35cm and 40cm (Nana et al., 2017). It is important to note that according to Eurocode 2, section 9.3 (CEN, 2005), thick slabs are those where the depth h is higher than one fifth of the span and Euler-Bernoulli theory is not valid for these configurations of slabs. The term "thick slabs" is used here to highlight the fact that these slabs used in the nuclear power plant are thicker than those used in the standard buildings. To study the shear capacity, the slabs are subjected to a concentrated load. The shear force is favored with respect to the bending moment by applying the load near a support. At the interface between the slab and the supports, a layer of mortar was placed to ensure regular contact and consistency of the support. Regarding the boundary conditions, the slabs are simply supported on their four sides (Figure 1). The reinforcements are designed so that the failure does not occur by bending. It should be noted that the reinforcement's diameter is modified while their number is kept constant. The experimental campaign consisted of one slab (S6) of dimensions 4 m×2.6m×0.35m, another (S7) of dimensions 4 m×2.6 m×0.40 m and the nine remaining slabs of dimensions 4 m×2.6m×0.3 m. The mechanical loading system consists of a hydraulic cylinder of 200-ton capacity and the loading is applied via a rectangular plate, the dimensions of which vary according to the slabs tested. The loading application is carried out with a quasi-static speed until the slab failure. The slabs concrete properties are given in Table 3. The concrete used to design the slabs was a ready-mixed concrete from a local supplier of VICAT concrete. The maximum aggregate size was 11.2 mm (except for the slab S2B with 20mm of the maximum aggregate size). The concrete characterization tests are cylindrical specimens measuring 11 × 22 cm carried out on the day that slab testing was performed. The specimens were placed in a humid chamber regulated in moisture and temperature. The composition of the concretes made is reported in Table 2.

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Supprimé: Table 2

Table 2 : Concrete composition used for thick slabs

Designation:	BPS NF EN 2061/CN	Certification :	NF
Exhibition class:	X0 (F)	Effective Water/ Binder equivalent:	0.8
Consistency:	S3	Maximum aggregate size:	D11.2
Characteristic resistance:	C20/25	Dosage (Cement+Ecocem):	145 kg
Type and class of cement:	CEM II/A-LL 42,5 R CE NF VMO VICA	Class Chlorides:	Cl 0.40
Adjuvant type:	PRE1 0.35%		

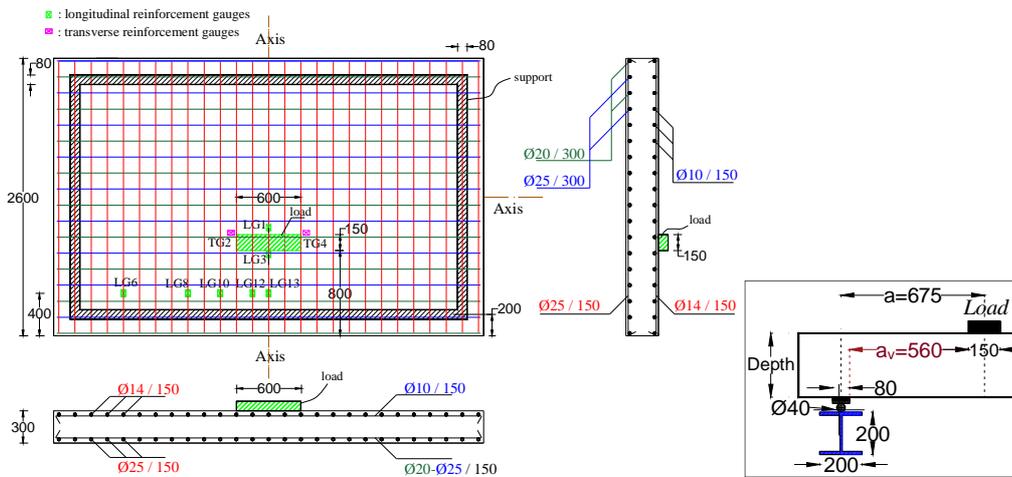


Figure 1: Reinforcement layout and test setup of thick slabs

The slabs are grouped by series. In each series, we analyze the effect of a given shear parameter. In Series I (S2, S8) the effect of concrete compressive strength, in Series II (S2, S6 and S7) the effect of a_v/d ratio, in Series III (S1, S4, and S5) the effect of longitudinal reinforcement ratio, in Series IV (S1–S3) the transverse reinforcement ratio, in Series V (S2, S2B) the concrete maximum aggregate size and finally in Series VI (S2, S9, S10) the loading plate length.

Table 3 : Properties of thick slabs

Series	Slabs	ρ_l (%)	ρ_t (%)	d_1 [mm]	d_t [mm]	a_v [mm]	a_v/d_1	Concrete class [MPa]	Maximum aggregate size [mm]	Loading plate length [mm]
I	S2	1.223	1.106	267.5	242.5	560	2.1	C20/25	11.2	600×150
	S8	1.223	1.106	267.5	242.5	560	2.1	C40/50	11.2	600×150
II	S2	1.223	1.106	267.5	242.5	560	2.1	C20/25	11.2	600×150
	S6	1.030	0.917	317.5	292.5	560	1.8	C20/25	11.2	600×150
	S7	0.890	0.783	367.5	342.5	560	1.5	C20/25	11.2	600×150
III	S1	1.223	0.854	267.5	245.0	560	2.1	C20/25	11.2	600×150
	S4	1.003	0.854	267.5	245.0	560	2.1	C20/25	11.2	600×150
	S5	1.551	0.837	270.0	250.0	560	2.1	C20/25	11.2	600×150
IV	S1	1.223	0.854	267.5	245.0	560	2.1	C20/25	11.2	600×150
	S2	1.223	1.106	267.5	242.5	560	2.1	C20/25	11.2	600×150
	S3	1.223	1.349	267.5	242.5	560	2.1	C20/25	11.2	600×150
V	S2	1.223	1.106	267.5	242.5	560	2.1	C20/25	11.2	600×150
	S2B	1.223	1.106	267.5	242.5	560	2.1	C20/25	20.0	600×150
VI	S2	1.223	1.106	267.5	242.5	560	2.1	C20/25	11.2	600×150
	S9	1.167	1.056	267.5	242.5	560	2.1	C20/25	11.2	700×150
	S10	1.117	1.010	267.5	242.5	560	2.1	C20/25	11.2	800×150

3.2 Thin slabs

Another shear experimental campaign was performed, this time on seven thin slabs of 10cm also under a concentrated load located at the proximity of the support. The tests were carried out with a structure like a floor system in which a concrete floor slab was supported by the reinforced concrete beams (Bui et al., 2017). This other experimental campaign consisted of one slab (N1) measuring 2.9 m×2.9 m×0.1m and six slabs (N2, N3, N5, N5Bis, N6, N6Bis) measuring 2.9 m×2.5 m×0.1m. The slabs are grouped by series. In each series, we study the effect of a given slab configuration under shear loading. In Series A (N1 Vs N2) the effect of the boundary conditions with slab supported on two sides instead four sides, in Series B (N2 Vs N3) the effect of loading plate length, in Series C (N5, N5Bis Vs N6, N6Bis – N5, N6 Vs N5Bis, N6Bis) the effect of both loading plate length and boundary condition by applying a lateral restraint at the two extremities of

the beam supports for N5Bis and N6Bis tests contrary to other tests where the beams are directly supported by the laboratory floor with a mortar layer placed at the interface. The reinforcement layout and the concrete properties of specimens are illustrated in **Figure 2** and **Table 5**, respectively.

The specimens were cast using ready-mixed concrete of C25/30. A maximum aggregate size of 20 mm was used. The composition of the concretes made is reported in **Table 4**.

Table 4: Concrete composition used for thin slabs

Designation:	BPS NF EN 2061/CN	Certification :	NF
Exhibition class:	XC1 (F)	Effective Water/ Binder equivalent:	0.65
Consistency:	S3	Maximum aggregate size:	D20
Characteristic resistance:	C 25/30	Dosage (Cement+Ecocec):	260 kg
Type and class of cement:	CEM II/A-LL 42,5 R CE NF VMO VICA	Class Chlorides:	CI 0.40
Adjuvant type:	SPHR3 0.40% PRE2 0.20%		

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Table 5: Properties of thin slabs

Series	Slabs	Number supports	ρ_l (%)	ρ_t (%)	d_l [mm]	a_v [mm]	a_v/d_l	Concrete class [MPa]	Maximum aggregate size [mm]	Loading plate length [mm]
A	N1	4	0.770	1.039	85	170	2.0	C25/30	20.0	1000×200
	N2	2	1.160	0.303	85	170	2.0	C25/30	20.0	1000×200
B	N2	2	1.160	0.303	85	170	2.0	C25/30	20.0	1000×200
	N3	2	1.160	0.182	85	170	2.0	C25/30	20.0	400×200
C	N5	2	1.000	0.406	85	170	2.0	C25/30	20.0	1000×200
	N5Bis	2	1.000	0.406	85	170	2.0	C25/30	20.0	1000×200
	N6	2	1.010	0.406	85	170	2.0	C25/30	20.0	400×200
	N6Bis	2	1.010	0.406	85	170	2.0	C25/30	20.0	400×200

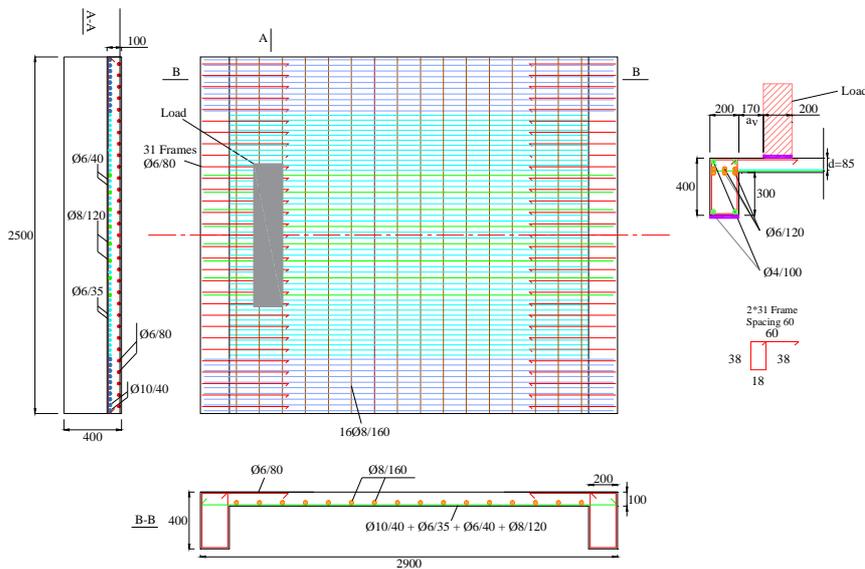


Figure 2: Reinforcement layout and test setup of thin slabs

4 Experimental results

4.1 Failure modes

The failure modes obtained for slabs are presented in **Figure 3** and **Figure 4** for thick slabs and thin slabs respectively. The first overload fracture is observed at the proximity of the support what is apparent to a one-way shear (shear failure). This cracking line whose length is equivalent to

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the shear effective width b_{eff} has a relatively larger opening than that of the other cracking lines observed. The mechanism of slabs shear failure corresponds to the appearance of this macro cracking.



Figure 3 : Thick slab failure mode: a) bottom face; b) saw-cut



Figure 4: Thin slab failure mode: a) top face; b) bottom face

4.2 Shear capacities

For slabs under concentrated load, the shear strength should not be calculated over the entire width as in the case of beams but over the effective width b_{eff} . The French code (**FD P 18-717, 2013**) and the (**Fib Model Code 2010, 2012**) adopt different approaches to calculate the effective width as shown in **Figure 5**. In the French approach, the hypothesis of a 45° load diffusion, resulting from the contour of the load zone in the direction of the supports ($b_{eff,2}$) is assumed (**Figure 5a**). Some studies showed that the shear strength determined using the French effective width recommendation has a good capacity to predict the experimental shear capacities (**Regan and Rezai-Jorabi, 1988**), (**Lantsoght et al., 2012**), (**Belletti et al., 2014**). In the present study, to

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facilitate comparisons between the design codes, the same effective width ($b_{eff,2}$) of the French approach was used. Note that the values of $b_{eff,2}$ according to (FD P 18-717, 2013) and $b_{eff,3}$ for the (Fib Model Code 2010, 2012) are very close as given in Table 6, and don't affect the results significantly.

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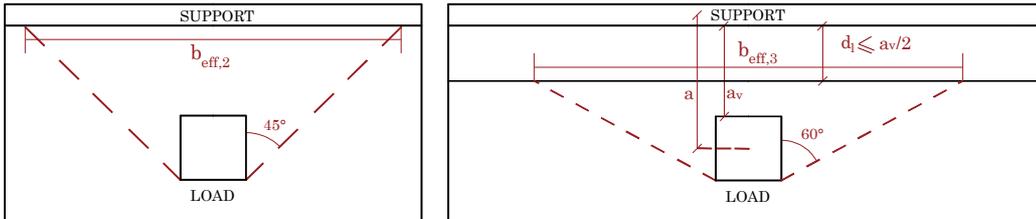


Figure 5: Determination of the effective width b_{eff} ; (a) French approach; (b) fib-Model Code 2010 approach

The peak loads values obtained from the experiments P_u and the corresponding ultimate shear loads V_{exp} are given in Table 6. For each slab, the ultimate shear loads V_{exp} is calculated from the peak loads P_u through a model using the Navier method with linear displacement hypothesis (Timoshenko and Woinowsky-Krieger, 1959). It should be noted that the slabs self-weight is not taken into account in the determination of the ultimate shear load V_{exp} , its effect is negligible compared with that of the localized load causing the failure.

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Table 6: Peak loads obtained for slabs

Slabs	a_v/d_1	ρ_l	ρ_t	$f_{cm,meas}$	$b_{eff,2}$	$b_{eff,3}$	P_u	Failure mode	V_{exp}	$V_{exp}/\sqrt{f_{cm}}$
		[%]	[%]	[MPa]	[mm]	[mm]	[kN]		[kN]	
S1	2.1	1.223	0.854	24.1	2100	2270	1111	Shear	680	139
S2	2.1	1.223	1.106	30.9	2100	2270	1220	Shear	747	134
S2B	2.1	1.223	1.106	30.5	2100	2270	1353	Shear	828	150
S3	2.1	1.223	1.349	18.8	2100	2270	1032	Shear	632	146
S4	2.1	1.003	0.854	23.9	2100	2270	1050	Shear	643	132
S5	2.1	1.551	0.837	34.6	2100	2270	1257	Shear	769	131
S6	1.8	1.030	0.917	33.2	2100	2100	1427	Shear	888	154

S7	1.5	0.890	0.783	34.2	2100	2230	1796	Shear	1135	194
S8	2.1	1.223	1.106	51.7	2100	2270	1632	Shear	999	139
S9	2.1	1.167	1.056	30.4	2200	2370	1350	Shear	825	150
S10	2.1	1.117	1.010	30.6	2300	2470	1221	Shear	745	135
N1	2.0	0.770	1.039	25.8	1740	1987	294	Shear	212	42
N2	2.0	1.160	0.303	30.4	1740	1987	308	Shear	275	50
N3	2.0	1.160	0.182	30.4	1140	1387	196	Shear	175	32
N5	2.0	1.000	0.406	30.2	1740	1987	342	Shear	305	56
N5Bis	2.0	1.000	0.406	30.2	1740	1987	351	Shear	313	57
N6	2.0	1.010	0.406	19.2	1140	1387	185	Shear	165	38
N6Bis	2.0	1.010	0.406	19.2	1140	1387	166	Shear	148	34

5 Experimental results Vs Analytical predictions

The experimental results are compared to the Eurocode 2 (EC2), French (FNA), ACI 318-14, Fib Model Code 2010 (MC) using level of approximation LoA I and LoA II and Critical Shear Crack Theory (CSCT) predictions models. The effective width according to French recommendation b_{eff} is used instead of the entire width b_w . All the partial safety factors are set equal to 1 ($\gamma_c = 1$) and the mean values of the concrete mechanical properties measured are used. The shear strength of slabs according to the fib Model Code LoA II, CSCT and ACI 318 (non-simplified expression) which are sensitive to the applied moment (with a lesser degree for ACI), are determined in a shear control section that must be specified. The bending moment and the shear force obtained at the control section are used for the calculations and predict shear failure in the region along the shear span in which the moment is higher. The control section is generally defined at a distance d (the effective depth of the specimen) from the face of the load. This potentially critical section is admitted in our study. The reinforcement's Young modulus is assumed to be 210 GPa.

The confrontation between the experimental results and the design models is shown in **Table 7**, **Table 8**, **Table 9** and **Table 10**. The average (AVG) and standard deviation (STD) of the comparison between the experimental results and the design models are shown in **Table 9** and **Table 10**. For the case of thick slabs, these results show that compared to Eurocode 2 and ACI 318-14, the French National Annex approach FNA (AVG=1.09, STD=0.08) give predictions that are very close to experimental ones. The Eurocode 2 approach also give acceptable results as this code is reasonably predicting the shear capacities (AVG=1.22, STD=0.09). However the ACI 318-14 and ACI simplified give conservative results with (AVG=1.32, STD=0.08) and (AVG=1.43, STD=0.08) respectively, the results are underestimated in all experiments. The comparison of experimental results to the EC2, French approach, and ACI 318-04 predictions is illustrated in **Figure 6** and the degree of conservatism illustrated in **Figure 10a**. In the case of thin slabs of 10cm, the same conclusions are drawn, in the sense that the closest predictions with the experimental results are obtained in the order with FNA (AVG=1.52, STD=0.17), Eurocode 2 (AVG=1.69, STD=0.14) and ACI 318-14 (AVG=1.90, STD=0.15). However compared to prediction levels for thick slabs, for thinner 10cm slabs, the predictions for all models seem more conservative. The comparison of experimental results with the predictions is illustrated in **Figure 7** and the degree of conservatism illustrated in **Figure 10b**.

Concerning the Fib Model Code 2010 with LoA II approximation level (equivalent to CSA A23.3) and the Critical Shear Crack Theory CSCT, for the case of thick slabs, the results show that both models give excellent predictions with (AVG=1.06, STD=0.11) and (AVG=1.04, STD=0.08) respectively. In the case of thin slabs, the same conclusions are also drawn with Fib Model Code 2010 LoA II (AVG=1.29, STD=0.15), CSCT (AVG=1.11, STD=0.12). However, the predictions also seem a little more conservative. As Fib Model Code 2010 and CSCT models are physical (mechanical) based models contrary to others empirical codes and, given the very good accuracy of predictions, they could provide a unified approach to shear design for one way shear. The Model

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Code 2010 with the first level of approximation (LoA I) seems to be very conservative (AVG = 1.83, STD = 0.12 for thick slabs and AVG = 2.15, STD = 0.23 for thin slabs). This seems logical as the LoA I is suitable for pre-dimensioning of structural elements, where a conservative calculation method is acceptable. The comparison of test results to the Fib Model Code 2010 (LoA I and LoA II) and the CSCT predictions are illustrated in **Figure 8**, **Figure 9** and **Figure 10**.

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Table 7: Thick slabs: experimental results Vs predictions of EC2, French approach, ACI 318–14, Model Code 2010 (MC) and Critical Shear Crack Theory (CSCT).

Test	Experiment		V with $f_{cm,meas}$						
	P_u [kN]	V_{exp} [kN]	V_{EC2} [kN]	V_{France} [kN]	V_{ACI} [kN]	$V_{ACI,simplified}$ [kN]	$V_{MC-LoA I}$ [kN]	$V_{MC-LoA II}$ [kN]	V_{CSCT} [kN]
S1	1111	680	582	625	518	469	372	661	665
S2	1220	747	633	708	576	531	421	721	726
S2B	1353	828	630	703	573	527	418	728	762
S3	1032	632	536	552	466	414	329	600	600
S4	1050	643	544	622	502	467	370	621	627
S5	1257	769	716	756	633	567	449	836	834
S6	1427	888	719	804	706	653	495	891	949
S7	1796	1135	833	931	828	767	557	930	1039
S8	1632	999	751	916	723	687	545	816	835
S9	1350	825	649	735	596	552	438	751	739
S10	1221	745	670	771	621	579	459	834	787

Table 8: Thin slabs: experimental results Vs predictions of EC2, French approach, ACI 318–14, Model Code 2010 (MC) and Critical Shear Crack Theory (CSCT).

Test	Experiment		V with $f_{cm,meas}$						
	P_u [kN]	V_{exp} [kN]	V_{EC2} [kN]	V_{France} [kN]	V_{ACI} [kN]	$V_{ACI,simplified}$ [kN]	$V_{MC-LoA I}$ [kN]	$V_{MC-LoA II}$ [kN]	V_{CSCT} [kN]
N1	294	212	139	173	124	128	122	194	231

N2	308	275	167	188	150	139	133	239	255
N3	196	175	111	123	99	91	87	134	171
N5	342	305	166	187	150	138	132	217	252
N5Bis	351	313	166	187	150	138	132	215	251
N6	185	165	94	98	81	72	69	114	137
N6Bis	166	148	94	98	81	72	69	119	138

Table 9: Thick slabs: ratios between experimental results and models predictions.

Test	Experiment		EC2 in general (EC2a)	EC2 with French approach (EC2b)	ACI 318 (ACI 318a)	ACI 318 Simplified (ACI 318b)	Model Code (LoA I) (MC I)	Model Code (LoA II) (MC II)	Critical Shear Crack Theory (CSCT)
	P_u [kN]	V_{exp} [kN]	V_{exp}/V_{EC2}	V_{exp}/V_{France}	V_{exp}/V_{ACI}	$V_{exp}/V_{ACI, simplified}$	$V_{exp}/V_{MC-LoAI}$	$V_{exp}/V_{MC-LoAII}$	V_{exp}/V_{CSCT}
S1	1111	680	1.17	1.09	1.31	1.45	1.83	1.03	1.02
S2	1220	747	1.18	1.06	1.30	1.41	1.77	1.04	1.03
S2B	1353	828	1.31	1.18	1.45	1.57	1.98	1.14	1.09
S3	1032	632	1.18	1.14	1.35	1.53	1.92	1.05	1.05
S4	1050	643	1.18	1.03	1.28	1.38	1.73	1.04	1.03
S5	1257	769	1.07	1.02	1.22	1.36	1.71	0.92	0.92
S6	1427	888	1.23	1.10	1.26	1.36	1.79	1.00	0.94
S7	1796	1135	1.36	1.22	1.37	1.48	2.04	1.22	1.09
S8	1632	999	1.33	1.09	1.38	1.45	1.83	1.22	1.20
S9	1350	825	1.27	1.12	1.38	1.50	1.88	1.10	1.12
S10	1221	745	1.11	0.97	1.20	1.29	1.62	0.89	0.95
AVG			1.22	1.09	1.32	1.43	1.83	1.06	1.04
STD			0.09	0.07	0.08	0.08	0.12	0.11	0.08
5% Percentile			1.09	1.00	1.21	1.33	1.67	0.91	0.93

Table 10: Thin slabs: ratios between experimental results and models predictions.

Test	Experiment	EC2 in general (EC2a)	EC2 with French approach	ACI 318 (ACI 318a)	ACI 318 Simplified (ACI 318b)	Model Code (LoA I)	Model Code (LoA II)	Critical Shear Crack Theory

			(EC2b)	318a)	318b)	(MC I)	(MC II)	(CSCT)	
P_u	V_{exp}		$V_{exp}/$	$V_{exp}/$	$V_{exp}/$	$V_{exp}/$	$V_{exp}/$	$V_{exp}/$	
[kN]	[kN]		V_{EC2}	V_{France}	V_{ACI}	$V_{ACI, simplified}$	$V_{MC-LoAI}$	$V_{MC-LoAII}$	V_{CSCT}
N1	294	212	1.52	1.23	1.70	1.66	1.73	1.09	0.92
N2	308	275	1.65	1.46	1.83	1.98	2.07	1.15	1.08
N3	196	175	1.58	1.42	1.77	1.92	2.01	1.30	1.02
N5	342	305	1.84	1.63	2.04	2.21	2.31	1.40	1.21
N5Bis	351	313	1.89	1.67	2.09	2.27	2.37	1.46	1.25
N6	185	165	1.76	1.69	2.04	2.29	2.39	1.45	1.20
N6Bis	166	148	1.58	1.52	1.83	2.05	2.14	1.25	1.08
AVG			1.69	1.52	1.90	2.05	2.15	1.29	1.11
STD			0.14	0.17	0.15	0.22	0.23	0.15	0.12
5% Percentile			1.54	1.29	1.72	1.74	1.82	1.11	0.95

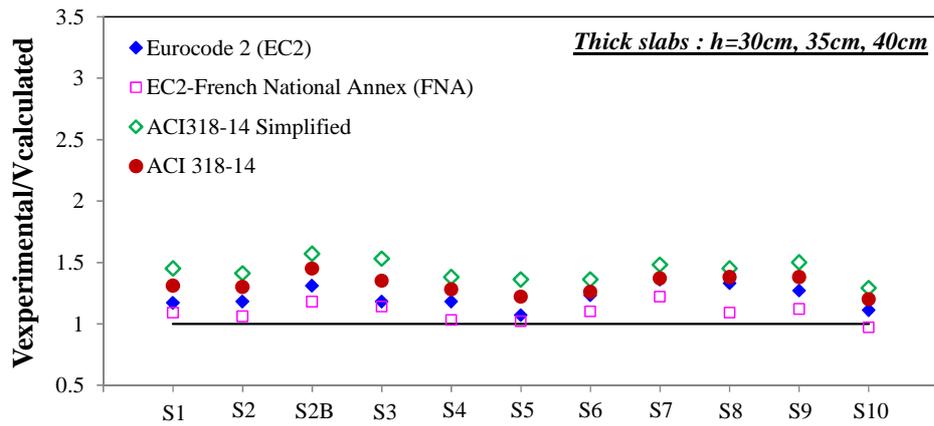


Figure 6: Thick slabs: experimental results Vs EC2, French approach and ACI 318-14.

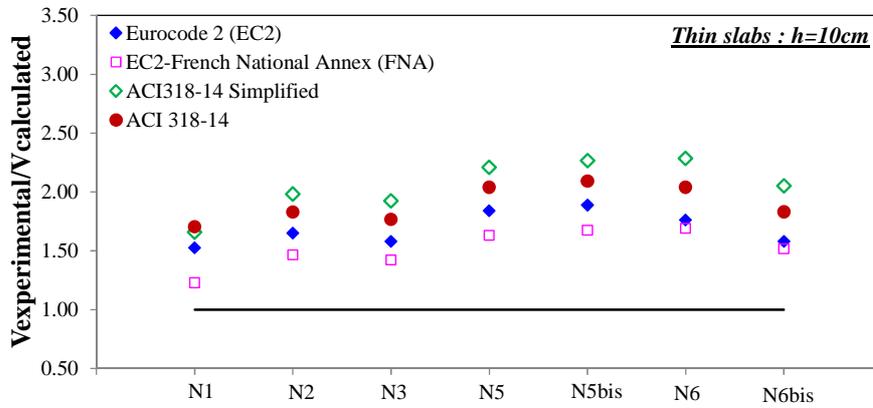


Figure 7: Thin slabs: experimental results Vs EC2, French approach and ACI 318-14.

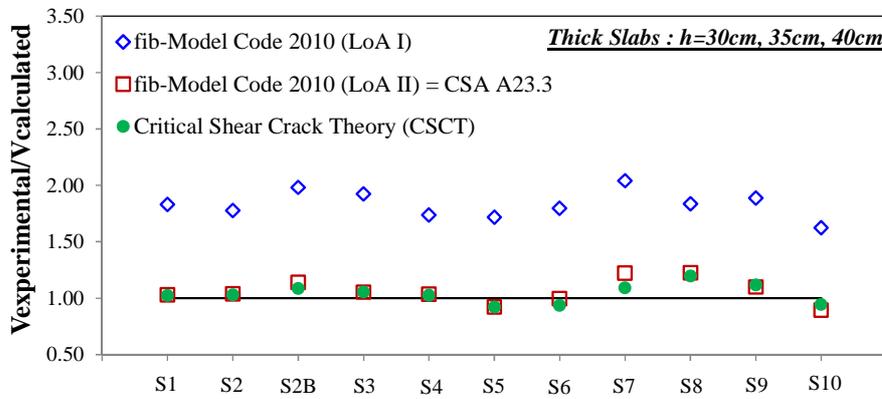


Figure 8: Thick slabs: experimental results Vs Model Code 2010 (MC) and CSCT.

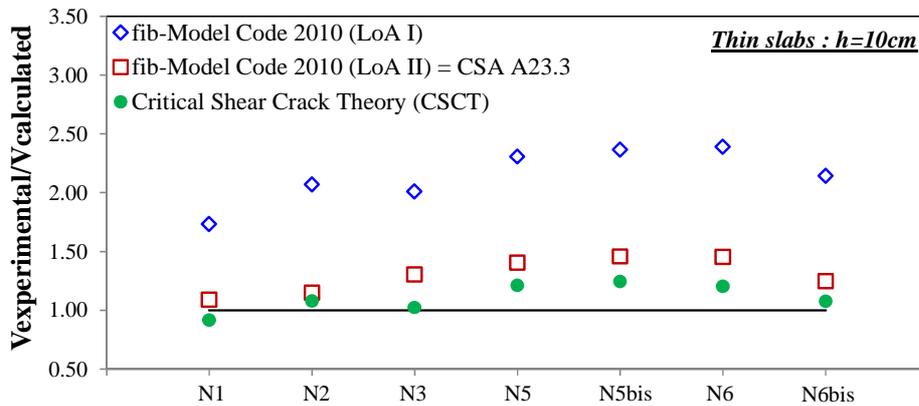


Figure 9: Thin slabs: comparisons of test results from Model Code 2010 (MC) and Critical Shear Crack Theory (CSCT).

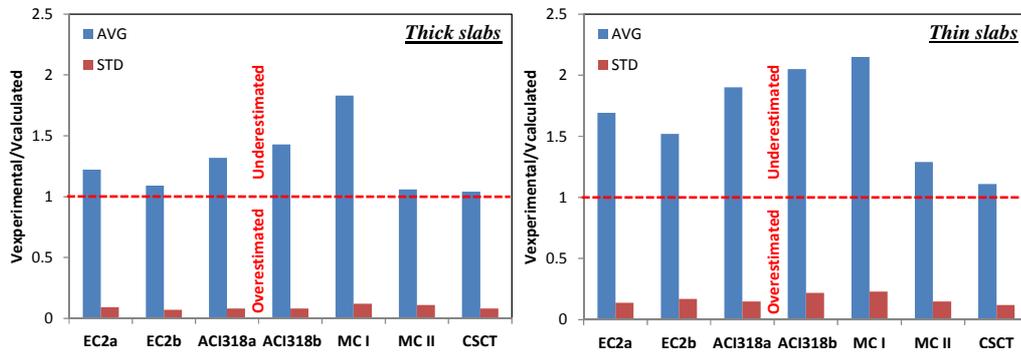


Figure 10: Comparisons between models: illustration of the conservatism degree

6 Conclusions

This paper presents a comparative study of all the main analytical methods to estimate the shear capacity of thick and thin RC slabs without stirrups. The experimental results are compared to the Eurocode 2, French National Annex, ACI 318 and its simplified version, Fib Model Code 2010 using level of approximation LoA I, LoA II, with LoA II equivalent to the Canadian standard CSA A23.3, and Critical Shear Crack Theory CSCT, basis of Swiss standard SIA 262 design models. These comparisons delivered valuable information for engineers that design thick or thin RC slabs under shear loading, as currently, there is not yet a general agreement on a design model giving the shear strength of RC structures not containing shear reinforcement. The following conclusions were drawn:

- The French National Annex approach FNA resulted in shear capacities predictions that are very close to the experimental values. However, the Eurocode 2 approach resulted in an underestimation.
- The shear strengths predicted by ACI 318-14 and ACI simplified also gave underestimations when confronted with all the experimental results.

- The Fib Model Code 2010 using level of approximation LoA II and the Critical Shear Crack Theory CSCT gave the best agreements when compared with the experimental results. The Model Code 2010 with the first level of approximation (LoA I) appeared as very conservative. The fib Model Code 2010 based on MCFT and Critical Shear Crack Theory CSCT provisions for shear represent a significant evolution in standardization with the abandonment of empirically based models in favor of physically sound models. Empirical formulations as Eurocode 2 and ACI 318 are less accurate and may neglect the role of some shear governing parameters. Therefore, MCFT based models (fib Model Code 2010, CSA, AASHTO LRFD) or CSCT based models (SIA 262) have the resources to create a modification in the way shear is treated at the international level and a unified international approach could be drawn from these models.
- Compared to prediction levels for thick slabs (30cm, 35cm and 40cm), for thin 10cm slabs, the predictions for all models seem more conservative.

In a future work, own amendments to the standard formulas should be proposed based on the experimental results. In particular a modification of the Eurocode 2, ACI 318-14, ACI simplified and Fib Model Code 2010 using level of approximation LoA I (MC I) should be proposed to make it more accurate and more physical while taking into account the effect of all shear parameters (for example, the effect of aggregates size may be taken into account).

Acknowledgements

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