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# Six-Port Reflectometer in WR15 Metallic Waveguide for Free-Space Sensing Applications

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**Abstract** — This work describes the design, fabrication and measurements of a six-port reflectometer in metallic waveguide technology for operation around 60 GHz. The system integration is based on WR15 building blocks. An in-situ linearization of the detectors associated to a vector calibration procedure is provided to determine the calibrated IQ components from the measured voltages. Near-field free-space distance measurements from contact to stand-off distance of two free-space wavelengths are shown to validate the technique proposed.

**Index Terms** — Six-port, reflectometer, IQ demodulation, millimeter-wave, distance measurement,

## I. INTRODUCTION

The six-port technique has been introduced in the 1970s as a simple technique for measuring power and reflection coefficient in the microwave regime [1]. Since then, a variety of six-port systems have been exemplarily demonstrated in metallic guide, substrate integrated waveguide (SIW), planar and monolithic forms [2]-[8]. Each technology presents own advantages and drawbacks in terms of circuit size, power consumption, immunity to temperature/hygrometry variations, fabrication facility, system integration, measurement performance and cost [8]. Therefore, the choice of the technology is mainly driven by the requirements of the targeted application.

This work presents a fully WR15 metallic waveguide six-port reflectometer operating at 60 GHz for near-field sensing applications, i.e. near-field high precision distance measurement. Unlike planar technologies systems, waveguides are highly shielded to provide isolation between nearby signals. As they rely on air as a dielectric, the technology reduces the need for consistency in the dielectric material and presents better immunity to environmental variations. Furthermore, the building blocks of the six-port circuit can be easily connected each other as they are inherently matched. As the size is directly related to the operation wavelength, millimeter-wave frequency operation is preferred to reduce the circuit size.

## II. SIX-PORT IQ DEMODULATOR

This section describes the design, fabrication and test of the six-port IQ demodulator. The proposed architecture and picture of the fabricated system are given in Fig. 1.

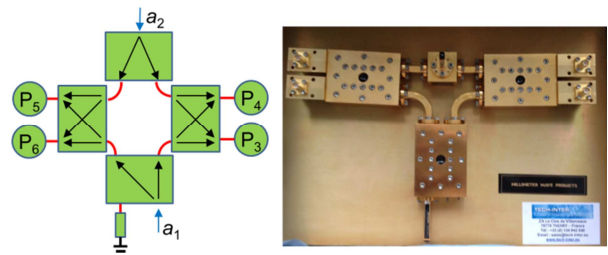


Fig. 1. (a) Structure of the six-port IQ demodulator. (b) Photograph of the WR15 waveguide six-port IQ demodulator.

The circuit is implemented using three 90° hybrids with 20 dB isolation and 6 % bandwidth around 60 GHz, a four port hybrid tee with one arm connected to a match termination for basic power splitting and four power detectors with typical video sensitivity of 500 mV/mW and tangential sensitivity of -50 dBm. Interconnecting bends and twists are used for system integration. The reference millimeter-wave signal  $a_1$  [fig. 1(a)] can be provided by a miniature high stability phase-locked source Mi-WAVE™ 957 ( $P_{LO} = 11$  dBm) or a frequency synthesizer Keysight™ E8257D.

The first step concerns the linearization of the electrical response of the power detectors to correct deviation from quadratic response. For this experiment, the RF port (signal  $a_2$ ) of the six-port demodulator is connected to a match termination to make the electrical response depending only of the LO source signal  $a_1$ . We present in Fig. 2 the detected voltages  $V_1$  to  $V_4$  measured for a source power varying from 10  $\mu$ W to 10 mW at 60 GHz.

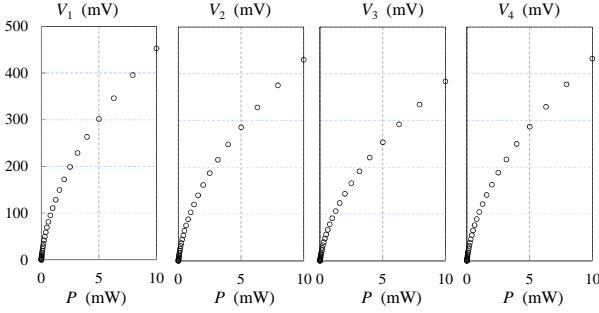


Fig. 2. Detected voltages as a function of the input millimeter-wave LO power –  $F = 60$  GHz.

From Fig. 2, the linearity is degraded by distortions. The linearization procedure consists to interpolate the measured data using a polynomial function. In this study, a 5<sup>th</sup> order polynomial is used. As an example, the interpolation model for the voltage  $V_1$  is given by

$$P_1 \text{ (mW)} = -1.43 \times 10^{-13} V_1^5 + 1.66 \times 10^{-10} V_1^4 - 8.04 \times 10^{-8} V_1^3 + 5.98 \times 10^{-5} V_1^2 + 4.02 \times 10^{-3} V_1 + 1.36 \times 10^{-2}.$$

The next step consists of verifying the performance in mixing mode. In this configuration, the millimeter-wave signal  $a_2$  with amplitude  $A_{RF}$  is combined with the signal  $a_1$  with amplitude  $A_{LO}$ . The theoretical powers  $P_3$  to  $P_6$  are given by

$$P_3 = |0.5(a_2 + a_1)|^2 \quad (1)$$

$$P_4 = |0.5(a_2 - ja_1)|^2 \quad (2)$$

$$P_5 = |0.5(a_2 - a_1)|^2 \quad (3)$$

$$P_6 = |0.5(a_2 + ja_1)|^2 \quad (4)$$

The 60 GHz LO and RF input signals are both obtained by the synthesizer using a power splitter. The source power is set to 11 dBm. The RF signal amplitude  $A_{RF}$  and relative phase-shift  $\Delta\Phi$  are respectively adjusted with precise WR15 waveguide variable attenuator (MI-WAVE 510V/385) and phase-shifter (MI-WAVE 528V/385) as shown in Fig. 3. The IQ components are defined as

$$I = A_{RF} \cos(\Delta\Phi) \sim P_3 - P_5 \quad (5)$$

$$Q = A_{RF} \sin(\Delta\Phi) \sim P_6 - P_4 \quad (6)$$

A spatial (related to the spatial phase-shift  $\Delta\Phi$ ) Fourier analysis is considered to correct the general forms given by (5) and (6) into the models (7) and (8) that encompasses mismatching and non-linear effects [9].

$$P_3 - P_5 = y_0 + y_1 I + y_2 Q + y_3 I^2 + y_4 Q^2 + y_5 (I^2 - 3IQ^2) + y_5 (Q^2 - 3I^2Q) \quad (7)$$

$$P_6 - P_4 = y'_0 + y'_1 I + y'_2 Q + y'_3 I^2 + y'_4 Q^2 + y'_5 (I^2 - 3IQ^2) + y'_5 (Q^2 - 3I^2Q) \quad (8)$$

These equations rely the powers to polynomial combinations of  $I$  and  $Q$  through eight real calibration

constants  $y_i$  and  $y'_i$ . More information about the model construction is given in [9].

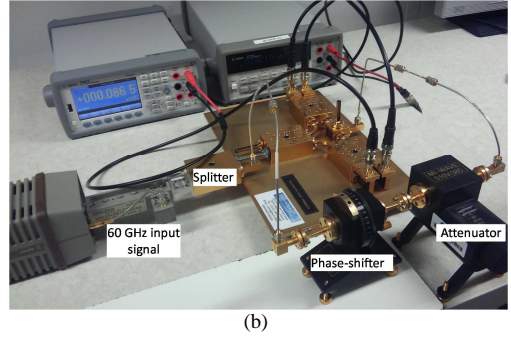
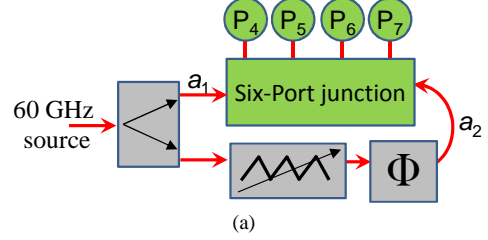


Fig. 3. Experimental test bench arrangement for IQ measurements.

The calibration coefficients  $y_i$  and  $y'_i$  are determined by fitting the measured powers to the models (7) and (8). For comparison purposes, the calibration constants are determined for the 1<sup>st</sup> ( $y_3 = y_4$  and  $y_5 = y_6 = y_7 = 0$ ), the 2<sup>nd</sup> ( $y_6 = y_7 = 0$ ) and the 3<sup>rd</sup> orders. Table I reports the parameters obtained for  $P_3 - P_5$ . The 3D fitting according to the 3<sup>rd</sup> order model is also illustrated in Fig. 4. These results show that the spatial non-linearity effect has relatively low impact. However, metrological applications that require a high degree of accuracy can benefit from a 3<sup>rd</sup> order model that achieves a determination coefficient of nearly 1 computed on 259 points. Equivalent result has been found for  $P_6 - P_4$ . The calibration has been also validated in the frequency band 55-75 GHz.

TABLE I. CALIBRATION COEFFICIENTS ESTABLISHED FOR  $P_3 - P_5 - F=60$  GHz.

Coefficient	Parameter	Order 1	Order 2	Order 3
$Y_0$	1	-0.2457	-0.2457	-0.2457
$y_1$	I	0.6575	0.6592	0.6593
$y_2$	Q	-1.1466	-1.1466	-1.1466
$y_3$	$I^2$	-0.0102	-0.0504	-0.0504
$y_4$	$Q^2$		0.0321	0.0321
$y_5$	IQ	—	-0.0152	-0.0152
$y_6$	$I^3 - 3IQ^2$		—	-0.0001
$y_7$	$Q^3 - 3I^2Q$	—	—	-0.0128
$r^2$		99.80%	99.88%	99.89%

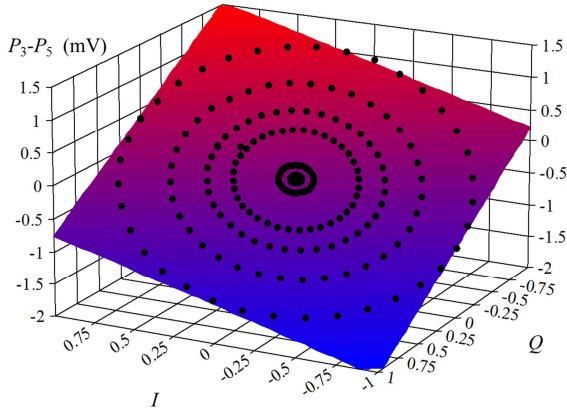
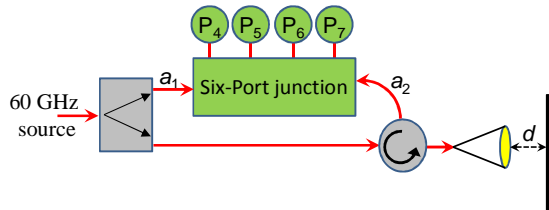


Fig. 4. IQ demodulation at 60 GHz: 3D complex interpolation – F=60 GHz. (● Measured data).

## II. DISTANCE SENSING APPLICATIONS

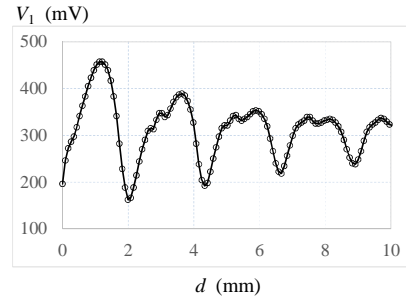
A distance measurement sensor based on the six-port demodulator associated to WR15 power divider, circulator and horn antenna is given in Fig. 5. The antenna with vertical polarization has been tested with stand-off  $d$  from contact to 10 mm to a metallic target. For example, detected voltage  $V_1$  as a function of  $d$  shows the spread propagation losses that increase with  $d$ . Furthermore, resonances are related to wave recombination between the reflected wave by that target, the guided reflected wave at the antenna input (mismatch) and the free-space source match term (reflection of the received wave by the antenna). A dedicated free-space calibration method that takes into account these two effects can be implemented to derive the distance as a function of the measured voltages [10]. Complementary results will be shown in the last version of the paper.



(a)



(b)



(c)

Fig. 5. Free-space distance measurement – F = 60 GHz. (a) and (b) Experimental test bench. (c) Detected voltage  $V_1$  as a function of the stand-off  $d$ .

## V. CONCLUSION

A 60 GHz six-port IQ demodulator in WR15 guide technology has been designed and tested. On this basis, a free-space six-port reflectometer has been described for close distance measurement in the cm range. Preliminary experiments show propagation of spherical waves combined with free-space stationary waves. Future work will provide all necessary calibration procedure for accurate extraction of distance and precision analysis.

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