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#### METHOD TO EXTRACT STRESS-STRAIN FUNCTIONS FROM PURE TORSION OR PURE BENDING EXPERIMENTAL TESTS

N. Connesson<sup>1</sup>, G. Anthérieu, D. Favier

Univ. Grenoble Alpes, Lab. TIMC-IMAG, Grenoble, France

**Abstract**: A mathematical methodology has been developed to extract stress-strain relations from pure torsion tests. This method has also been developed to extract the compression stress-strain relation from uniaxial and pure bending experimental tests. The extraction method has been experimentally tested on pure copper wire specimens; the extracted stress-strain relations proved to be fully satisfactory, validating thus the proposed method.

#### 1. Introduction

Stress-strain relations are usually experimentally identified during pure traction, pure compression or pure shear tests. Each of these tests presents its own experimental challenges. For example, buckling prevents reaching a wide range of compression stress on slender specimens: identifying the compression stress-stress relation on a satisfying range is difficult in this case. Yet, it has been observed that a higher compression stress range can be reached locally by simply applying pure bending load to these slender specimens thanks to the experimental setup developed in [1]. The measured experimental data (*i.e.* the bending moment versus curvature) contains information about the stress-strain compression relation; the aim of this work is to develop a method to successfully extract this information form experimental results. The proposed method has also been straightforwardly adapted to identify shear stressshear strain relations from pure torsion test. In this abstract, only the latter is described for concision and simplicity sake.

#### 2. Method and Results

During a torsion test, the applied and measured torque can be written:

where  $\sigma_{r\theta}(\gamma)$  is the searched shear stress-shear strain relation,  $\gamma = \frac{\theta r}{L}$  is the shear strain field, dS is an elementary surface of the specimen section S,  $\vec{u_z}$  is a unity vector normal to section, and r is the distance between a point M and the specimen center. L is the specimen length and  $\theta$  is the specimen second extremity rotation relatively to the first extremity.

The shear stress-shear strain relation  $\sigma_{r\theta}(\gamma)$  is searched as a linear combination of *n* cubic splines  $S_k$ ,  $k \in [1; n]$  written :

$$\sigma_{r\theta}(\gamma) = \sum_{k=1}^{n} q_k S_k \qquad \text{Equ. (2)}$$

where  $q_k$ ,  $k \in [1; n]$  represents the *n* unknown to be identified. These unknowns  $q_k$  are searched so as to minimize the function  $\phi^{tors}$  defined in the least mean square sense using every experimental measures  $\overline{M_o^{tors}}(t_i), i \in [1; p]$ . This function can be written :

<sup>&</sup>lt;sup>1</sup> Corresponding author

E-mail address: nathanael.connesson@imag.fr (N. Connesson)

$$\phi^{tors}(q_k) = \sum_{i=1}^p \left( \overline{M_o^{tors}}(t_i) - \iint_S \sum_{k=1}^n q_k \, r \, S_k \, dS \, \overrightarrow{u_z} \right)^2 \qquad \text{Equ. (3)}$$

The same method can be applied to identify the compressive stress-strain relation from pure bending experimental results provided the tensile stress-strain relation has been previously measured.

The experimental input data are presented figure 1. The identified results for 9 splines in torsion and 5 splines in flexion are presented figure 2.



*Figure 1.* Input experimental data on pure copper wire ( $\phi$ =0.6mm) (a) Pure torsion test results, (b) Pure uniaxial tensile test results, (c) Pure bending test results.



Figure 2. Identified results (a) shear stress-shear strain relation  $\sigma_{r\theta}(\gamma)$  identified using the pure torsion test results, (b) compressive stress-strain relation  $\sigma_{zz}(\varepsilon_{zz})$  identified using both the pure bending and tensile test results.

#### 3. Conclusions

Shear stress-shear strain relation  $\sigma_{r\theta}(\gamma)$ : for validation purpose, the identified shear stress-shear strain relation has been plotted in the Von Mises space (not presented here) and overlaps with the experimental tensile test results: the results are fully satisfactory.

**Compressive stress-strain relation**  $\sigma_{zz}(\varepsilon_{zz})$ : the identified compression stress-strain relation is symmetrical to the tensile stress-strain relation, which was the expected result [2]. Further method validation will be presented on numerical tests along with an analyze of the noise impact on the identification.

#### References

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