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# Theoretical Calculation of Wind (Or Water) Turbine

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## Abstract :

The Betz limit sets a theoretical upper limit for the energy efficiency of turbines energy efficiency of turbines, expressed as a maximum power coefficient of of  $16/27$ . Betz's theory is precise and is based on the calculation of kinetic energy. However, if the potential energy is taken into account potential energy, the theoretical energy efficiency of a turbine can be higher. higher. Fast wind turbines recover the kinetic energy of the wind in an optimal way kinetic energy of the wind while a large amount of potential energy is potential energy is created without being recovered. The notion of potential energy potential energy is fundamental, it is not possible to recover energy if we do not energy, if we do not create a constraint. This article examines this potential energy and the possibility for a wind turbine to transform it into into kinetic energy.

The Betz theory has been defined from the model of fast moving turbines. This theory has been generalized to slow and fast moving turbines and it has been defined as a law. The conservation of energy implies that if a variation of kinetic energy increases, the variation of kinetic energy increases, the variation of potential energy decreases. In the case of slow moving turbines, the conservation of energy applies, but not for the applies, but not for the case of fast moving turbines, however this is the reality. This paper proposes a new formulation of the power of turbines with a notion of temporal, in order to be able to verify the conservation of energy.

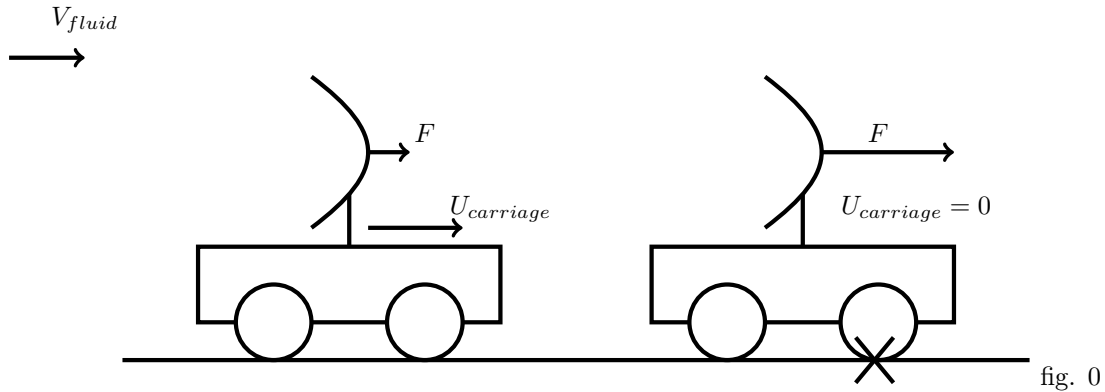
**Keywords :** Betz limit, Betz's law, Wind turbine, Tidal turbine, HAWT, VAWT.

## 1 Introduction

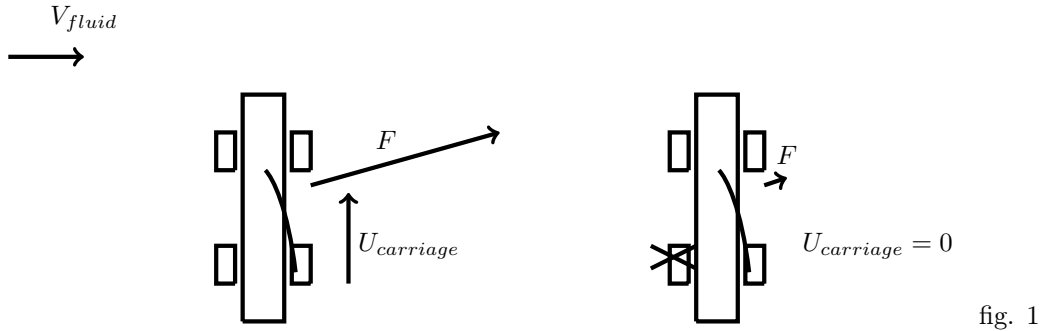
Lanchester, Betz, Joukowsky van Kuik (2007) van Kuik et al. (2015) Lanchester (1915) have defined the maximum power coefficient of wind turbines. This limit is commonly called the Betz limit. Considerable research efforts have been deployed to optimize wind turbines in order to reach this limit, for instance by optimizing the angle of incidence, the shape of the blade profile etc. One may for example refer to "Wind Energy Handbook" Burton et al. for fast moving horizontal axis wind turbines (HAWT), to "Hydrodynamic modelling of marine renewable energy devices: A state of the art review" Day et al. (2015) or to "Wind Turbine Design: With Emphasis on Darrieus Concept" Paraschivoiu (2002) for vertical axis wind turbines (VAWT).

Research has been made to reach the Betz limit: - by ducting the turbine (Georgiou (2016) Georgiou and Theodoropoulos (2016)) - by placing a water turbine in a narrow channel, which allows the water level upstream to be increased by the resistance to the advancing fluid (Quaranta (2018) (Quaranta (2018))) - by grouping turbines in wind farms in order to create an excess of power due to the proximity between machines (ducting effect) (Vennell (2013) Vennell (2013) and Broberg (2018) Broberg et al. (2018)).

The Betz limit is based on the calculation of kinetic energy. Designing a wind turbine, the energy of the fluid is taken into account in order to calculate the recoverable energy and to design a structure withstanding the stress.



A carriage with a square sail that can move freely, will be set in motion by the wind and thus be subject to very low wind stress. If the carriage is blocked, its structure will be subject to high stress.



A carriage with a modern sail that can move freely will be set in motion by the wind and subject to high stress from the wind. However, if the carriage is blocked, it will be subject to low stress on its structure.

In the case of fast moving wind turbines, when the wind increases, the turbine structure is subject to high stress.

Large wind turbines are stopped when the wind becomes too strong, not because they produce too much energy but because excessive stress could damage or destroy their structure. The stress induced in a structure is potential energy. Betz's theory does not take into account this potential energy. It exclusively takes into consideration kinetic energy.

In the case of a sailboat, the sole sail cannot recover all the energy from the wind. Betz's theory applies to the sail that can not retrieve more than  $16/27$  of the wind's kinetic energy. Many books explore the Betz limit, for instance John Kimball's "Physics of Sailing" Kimball (2009).

However, the America's Cup is a good example showing that the Betz limit can be exceeded. Indeed, a sailboat equipped with hydrofoils transforms potential energy into kinetic energy. The kinetic energy of the wind sets the boat in motion. The fluid flowing around the hydrofoils lifts the boat out of the water, thus reducing the drag and improving the efficiency. The wind power has not increased but the potential energy that applied constraints on the keel has been converted into kinetic energy by the flow of fluid around the profiles of the foils.

This article introduces the notions of kinetic and potential energy. It suggests that a vertical axis wind turbine (VAWT) with an appropriate design can transform potential energy into kinetic energy.

## 2 Preliminary considerations of Betz's theory

The German mathematician A. Betz has demonstrated that the power of a turbine is (cf. Appendix 14, Betz (1920)):

$$P_{kin} = F V = \left[ \frac{C_{kin}}{a} \frac{1}{2} \rho S V_{fluid}^2 \right] a V_{fluid} = C_{kin} \frac{1}{2} \rho S V_{fluid}^3$$

$$\text{where } V = a V_{fluid} \text{ and } C_{kin} = 4a^2(1 - a)$$

$P_{kin}$  the kinetic turbine power ( $W$ ),  
 $C_{kin}$  the kinetic power coefficient,  
 $\rho$  the fluid density ( $\frac{kg}{m^3}$ ),  
 $V_{fluid}$  the fluid velocity ( $\frac{m}{s}$ ),  
 $V$  the fluid velocity at the position of the turbine,  
 $S$  the swept area. ( $m^2$ ).

According to Betz's work (preliminarily by Lanchester), a kinetic energy approach shows that the maximum power coefficient  $C_k$  can not exceed a maximum of  $\frac{16}{27}$

$$C_{kin \text{ Betz}} = \frac{16}{27} \quad C_{kin} \leq C_{kin \text{ Betz}} \quad P_{kin \text{ maxi}} = C_{kin \text{ Betz}} \frac{1}{2} \rho S V_{fluid}^3 \quad (1)$$

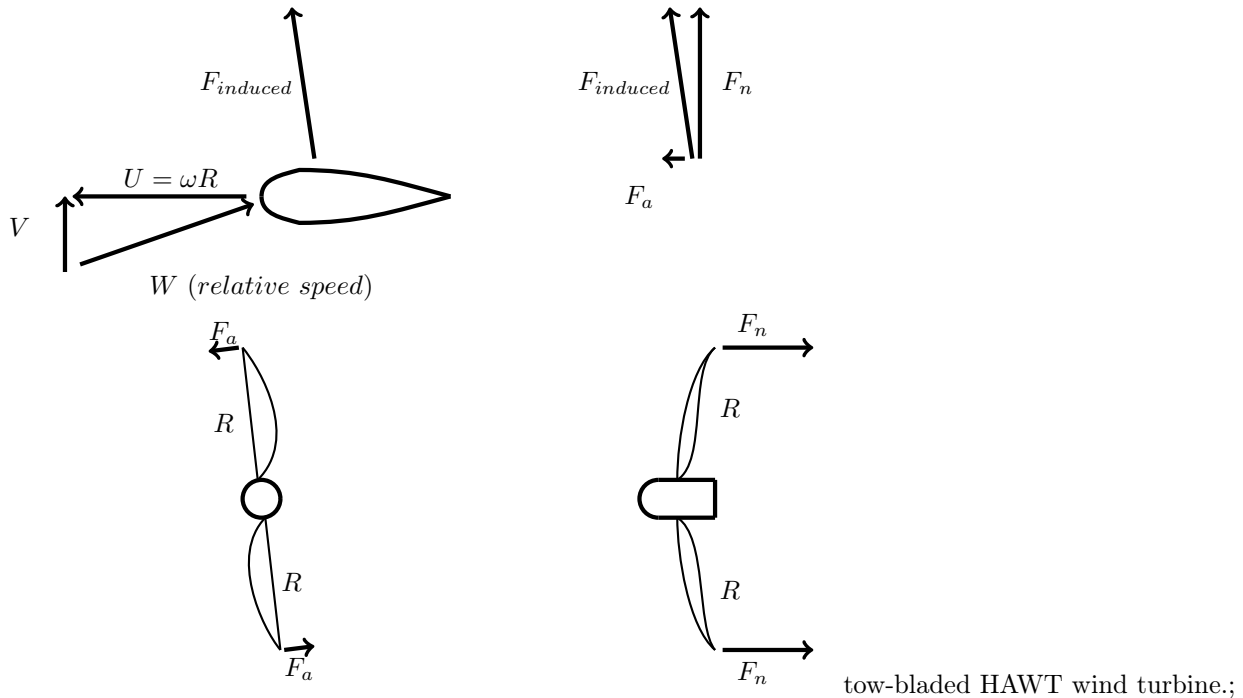


fig. 2

The relative speed due to the rotation speed of the wind turbine and the fluid speed creates an induced force  $F$  on the profile. This induced force  $F$  is composed of an axial force  $F_a$  and of a normal force  $F_n$ . The axial force  $F_a$  associated with the radius  $R$  creates a driving torque to produce energy. The normal force  $F_n$  associated with the same radius  $R$  creates a bending stress on the blade.

The power of the torque due to the axial forces and the angular rotation speed of the wind turbine is limited to  $\frac{16}{27}$  of the wind's kinetic power.

The forces  $F_n$  and  $F_a$  are associated with the same radius and have the same origin: the fluid velocity.  $F_n$  creates constraints that are the source of internal energy. These constraints are potential energy. Betz's theory does not take into account this potential energy which is as important as the kinetic energy. Betz limit is correct. However, it only takes into account kinetic energy. In order to increase the efficiency of wind

and hydrokinetic turbines, they could be designed to transform the potential energy into kinetic energy. It is necessary to dissociate slow speed turbines and fast speed turbines.

$\lambda = \frac{\omega R}{V_{fluid}}$  is an important parameter which makes a difference in the behaviour of the turbines when exposed to wind.

As for the sail, it is necessary to dissociate the navigation in thrust (square sail, spinnaker) (unstuck flow) and the navigation in smoothness (wing profile sail) (laminar flow).

## 2.1 Steady state, flow conservation and energy conservation

### 2.1.1 Flow conservation

In steady state, the fluid velocity is constant in time:  $\frac{dV}{dt} = 0$

With a constant flow, the continuity equation is obtained

$$S_1 V_1 = SV = S_2 V_2 \quad V_1 = V_{fluid}$$

### 2.1.2 Energy, power and kinetic force

The index *kin* for "kinetic" is used

$$E_{kin} = \frac{1}{2}mv^2 \quad P_{kin} = \frac{dE_{kin}}{dt} = \frac{1}{2} \frac{dm}{dt} v^2 + \frac{1}{2} m \frac{dv^2}{dt} \quad \frac{dv}{dt} = 0 \quad m = \rho s v dt \quad P_{kin} = \frac{1}{2} \rho s v^3 \quad F_{kin} = \frac{P_{kin}}{v} = \frac{1}{2} \rho s v^2$$

### 2.1.3 Energy, power and potential force

The index *pot* for "potential" is used

$$E_{pot} = m \frac{p}{\rho} \quad P_{pot} = \frac{dE_{pot}}{dt} = \frac{dm}{dt} \frac{p}{\rho} + m \frac{1}{\rho} \frac{dp}{dt} \quad \frac{dp}{dt} = 0 \quad m = \rho s v dt \quad P_{pot} = s v p \quad F_{pot} = \frac{P_{pot}}{v} = p s$$

### 2.1.4 Energy conservation (Prescott Joule (2011))

$$E_{kin} + E_{pot} = E_{kin-fluid}$$

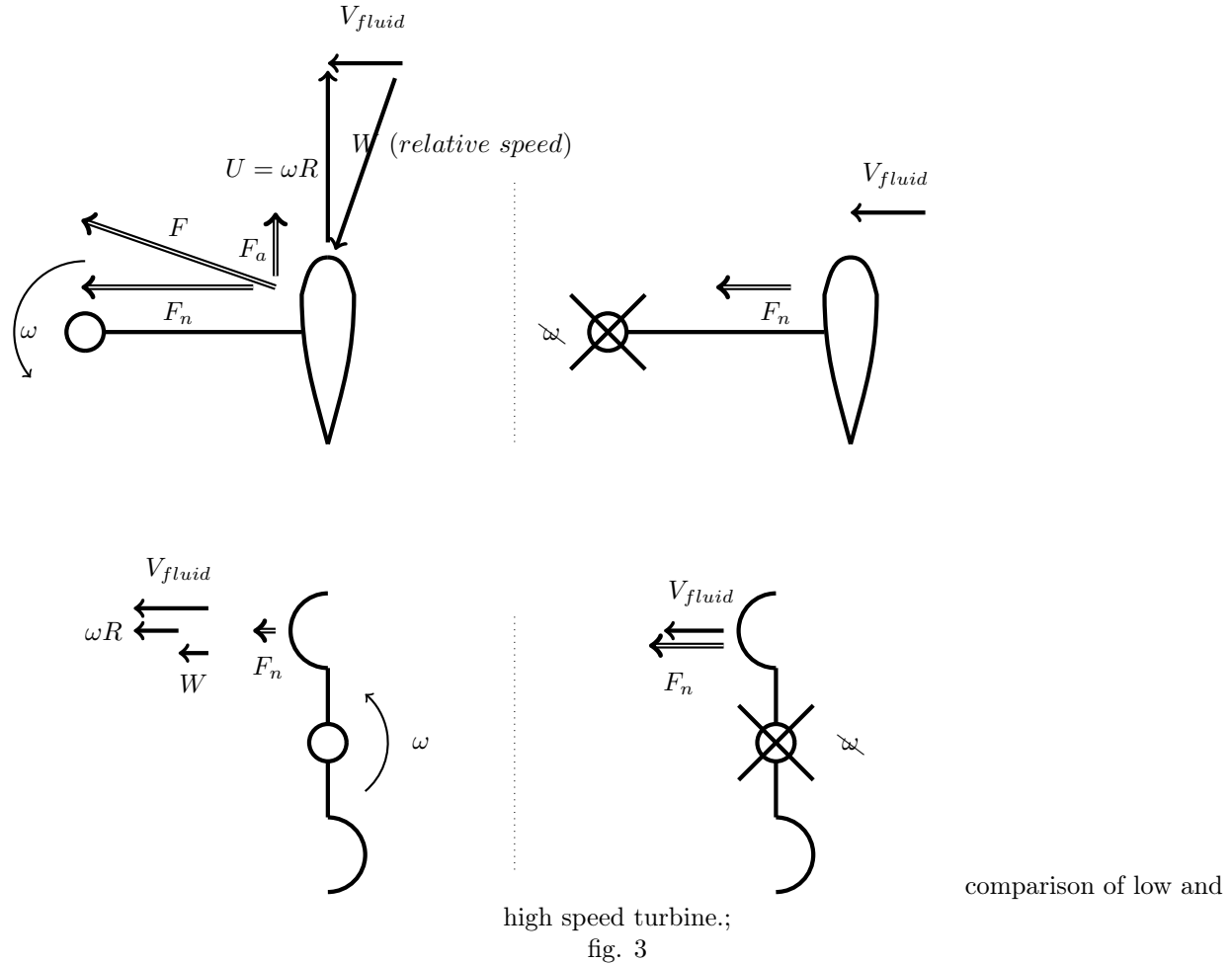
In steady state,  $\frac{dE_{kin-fluid}}{dt} = 0$

$$\Rightarrow \frac{dE_{kin}}{dt} = - \frac{dE_{pot}}{dt}$$

## 3 Difference between a low speed turbine and a high speed turbine

### 3.1 The advantage of using an airplane wing

Fast moving turbines can not be described as slow moving turbines such as Savionus. The comparison is made between the airfoil of a fast moving turbine and the cup of an anemometer.



If the movement of an anemometer is not impeded, then its cups are almost free of stress. If the rotation of an anemometer is hampered, then its cups are subject to stress. In the case of a wing profile, this effect is totally different. Indeed, the tangential rotation speed  $U$  of the profile is transverse to the flow of the fluid.

The relative speed  $W$  due to the rotation speed  $U$  and the fluid speed  $V_{fluid}$  creates an induced force  $F$  on the wing profile. The axial component  $F_a$  of this force  $F$ , combined with the radius, creates a driving torque.

For *horizontal axis wind turbines* (HAWT), this torque improves the efficiency which can then approach the Betz limit. Adding a transverse speed  $U$  will optimize the efficiency defined by Betz, but will add significant stress on the wind turbine due to the normal component  $F_n$  of force  $F$ . That's why HAWT wind turbines have to be stopped when the speed of the fluid is too high. They do not produce too much but they are subject to excessive bending stress.

**Anemometer ( $\lambda < 1$ )**

case	$U = \omega R$	$W$	$F_n$	$F_n R$
blocked	0	$= V_{fluid}$	max	0
free	$\nearrow$	$\searrow$	$\searrow$	$\nearrow$
case	$U = \omega R$	$W$	stress	torque
blocked	0	$= V_{fluid}$	max	null
free	$\nearrow$	$\searrow$	$\searrow$	$\nearrow$

case	$U = \omega R$	$W$	<i>potential energy</i>	<i>kinetic energy</i>
<i>blocked</i>	0	$= V_{fluid}$	<i>max</i>	<i>null</i>
<i>free</i>	$\nearrow$	$\searrow$	$\searrow$	$\nearrow$

### **Horizontal axis wind turbines ( $\lambda > 1$ ) (HAWT)**

case	$U = \omega R$	$W$	$F_n$	$F_a R$
<i>blocked</i>	0	$= V_{fluid}$	<i>min</i>	0
<i>free</i>	$\nearrow$	$\nearrow$	$\nearrow$	$\nearrow$

case	$U = \omega R$	$W$	<i>stress</i>	<i>torque</i>
<i>blocked</i>	0	$= V_{fluid}$	<i>min</i>	<i>null</i>
<i>free</i>	$\nearrow$	$\nearrow$	$\nearrow$	$\nearrow$

case	$U = \omega R$	$W$	<i>potential energy</i>	<i>kinetic energy</i>
<i>blocked</i>	0	$= V_{fluid}$	<i>min</i>	<i>null</i>
<i>free</i>	$\nearrow$	$\nearrow$	$\nearrow$	$\nearrow$

In the case of an anemometer, the kinetic energy varies in a direction opposite to the potential energy. This is not the case for HAWT turbines.

In the case of HAWT turbines, we must not only consider the speed of the fluid. The kinetic energy and potential energy are related to the fluid speed and to the tangential rotation speed  $U$ . The direction of  $U$  is perpendicular to the direction of the fluid.

The tangential rotation speed  $U$  is related to the fluid speed by this relation  $\lambda = \frac{U}{V_{fluid}} \quad U = \omega R$ .

In the case of an anemometer and in the case of a wing profile, we have this equation  $E_{kin} + E_{pot} = E_{kin-fluid}$ . The conservation of energy is not verified in the case of a wing profile. The variations of potential energy and energy increase when the anemometer is not blocked.

#### **3.1.1 Low speed turbines $\lambda < 1$ :**

Using the example of an anemometer with cups, when there is no resisting torque, the turbine rotates at maximum speed ( $\omega R = V_{fluid} \quad W = 0$ ), there is no energy production and the kinetic energy is at maximum. When the turbine is blocked, the stress on the turbine is at maximum ( $W = V_{fluid}$ ) and the speed of rotation is null. The potential energy is at maximum.

To obtain energy production, both kinetic and potential energy are required.

If the kinetic energy is higher than the potential energy, the energy production is limited by the potential energy.

Similarly, if the potential energy is higher than the kinetic energy, the energy production is limited by this latter.

There can be no production of kinetic energy without potential energy.

$$P_{kin-max-productive} \leq \min( P_{kin} , P_{pot} )$$

Energy production is at its maximum when the kinetic energy is equal to the potential energy. The total energy is equal to the sum of the kinetic energy and the potential energy.

$$E_{total} = E_{kin} + E_{pot}$$

Conservation of energy can be applied and verified.

$$\frac{dE_{total}}{dt} = 0 \quad \rightarrow \quad \frac{dE_{kin}}{dt} = - \frac{dE_{pot}}{dt} \quad (2)$$

The potential energy is related to the relative speed  $W$ . The kinetic energy is related to the relative speed  $\omega R$  (see Figure 2).

The tangential rotation speed must be equal to half of the fluid speed to reach optimal conditions.

$$|V_{fluid}| = |U| + |W| \quad |U| = |W| \quad U = \omega R = \frac{V_{fluid}}{2} \quad \lambda = \frac{1}{2} \quad (3)$$

To produce energy, the maximum power of the kinetic energy of a turbine at low speed ( $\lambda < 1$   $\lambda = \frac{\omega R}{V_{fluid}}$ ) is equal to

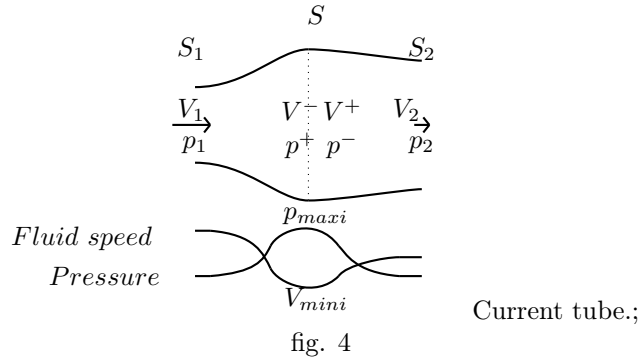
$$P_{kin \max(with \lambda < 1)} = C_{kin(with \lambda < 1)} \frac{1}{2} \rho S V_{fluid}^3 \quad C_{kin \max(with \lambda < 1)} = \frac{1}{2} \quad E_{kin} = \frac{E_{kin-wind}}{2} \quad (4)$$

For a low speed turbine, the kinetic energy of the wind is partially transformed into kinetic and potential energy.

$$E_{kinwind} \Rightarrow E_{kin} \& E_{pot} \quad (5)$$

## 4 Calculation of energy

### 4.1 Calculation of energy $\lambda < 1$



#### 4.1.1 Conservation of steady state energy applied in the area upstream of the turbine

$$\frac{1}{2} \rho S (V^-)^3 + S V^- p^+ = \frac{1}{2} \rho S_1 V_1^3 \quad \Rightarrow \quad \frac{1}{2} \rho (V^-)^2 + p^+ = \frac{1}{2} \rho \frac{S_1}{S} V_1^2$$

$$\frac{1}{2} \rho S V_{mini}^2 + p_{maxi} = \frac{1}{2} \rho S_1 V_1^2$$

$$\frac{d}{dt} \left( \frac{1}{2} \rho S (V^-)^2 + p^+ \right) = 0 \quad \Rightarrow \quad V_{mini}^2 = \frac{1}{2} \frac{S_1}{S} V_1^2$$

$$if \ S_1 = \frac{1}{2} S \ \text{then} \ V_{mini} = \frac{1}{2} V_1$$

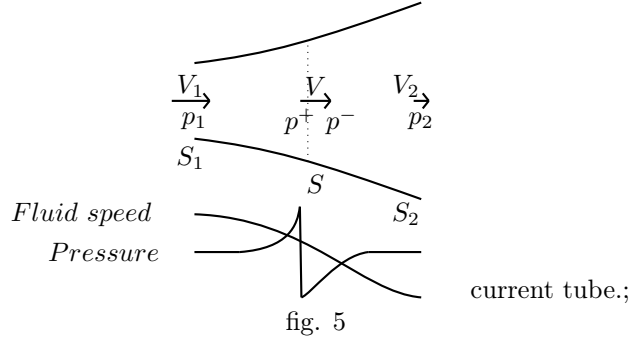
the kinetic energy of the fluid is transformed into kinetic and potential energy.

$$E_{kwind} \Rightarrow E_{pot} \& E_{kin}$$

see 3.1.1



## 4.2 Calculation of energy $\lambda > 1$



### 4.2.1 Calculation of the turbine power from the kinetic energy

The force applied to the rotor is  $F_{kin} = m \frac{dV}{dt} = \frac{dm}{dt} \Delta V = \rho S V (V_1 - V_2)$

$$P_{kin} = F_{kin} V = \rho S V^2 (V_1 - V_2)$$

$$P_{kin} = \frac{\Delta E_{kin}}{dt} = \frac{1}{2} \rho S V^2 (V_1^2 - V_2^2)$$

It is deducted  $V = \frac{V_1 + V_2}{2}$

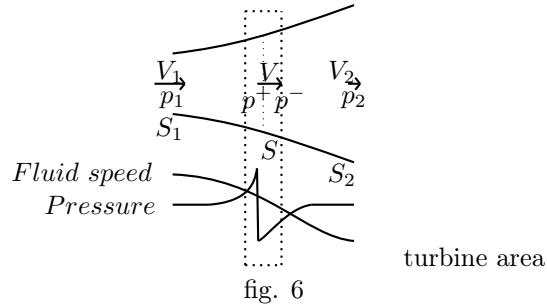
By defining  $a$  as  $a = \frac{V}{V_{fluid}}$   $V_{fluid} = V_1$   $0 \leq a \leq 1$   $V_2 = V_1(2a - 1)$   $V_2 \geq 0$   $a \geq \frac{1}{2}$

$$P_k = 4a^2(1-a) \frac{1}{2} \rho S V_{fluid}^3 \quad \text{with} \quad C_{kin} = 4a^2(1-a) \quad P_{kin} = C_{kin} \frac{1}{2} \rho S V_{fluid}^3$$

Searching for the maximum kinetic power (Betz limit) :

$$\frac{dP_{kin}}{dt} = 0 \quad a(2-3a) = 0 \quad \text{as} \quad a \geq \frac{1}{2} \quad a = \frac{2}{3} \quad C_{kin-maxi} = \frac{16}{27} = C_{kin-Betz}$$

### 4.2.2 Energy in stationary state applied in the turbine area

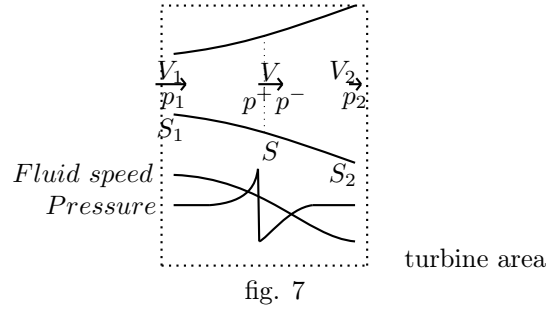


$$E_{kin+} + E_{pot+} = E_{kin-} + E_{pot-} = E_{pot}$$

$$\rho m \left[ \frac{V_+^2}{2} - \frac{V_-^2}{2} + \frac{p_+}{\rho} - \frac{p_-}{\rho} \right] = E_{pot} \quad \text{with} \quad V_+ = V_- = V$$

$$\rho m \left[ \frac{p_+}{\rho} - \frac{p_-}{\rho} \right] = E_{pot} \quad (6)$$

### 4.2.3 Energy in stationary state applied to the whole turbine



$$E_{kin_1} + E_{pot_1} = E_{kin_2} + E_{pot_2} + E_{kin}$$

$$\rho m \left[ \frac{V_1^2}{2} - \frac{V_2^2}{2} + \frac{p_1}{\rho} - \frac{p_2}{\rho} \right] = E_{kin} \quad \text{with} \quad p_1 = p_2$$

$$\rho m \left[ \frac{V_1^2}{2} - \frac{V_2^2}{2} \right] = E_{kin} \quad (7)$$

### 4.2.4 Remark

The Bernoulli equations

$$p_1 + \frac{1}{2}\rho s_1 V_1 = p^+ + \frac{1}{2}\rho s V \quad p^- + \frac{1}{2}\rho s V = p_2 + \frac{1}{2}\rho s_2 V_2$$

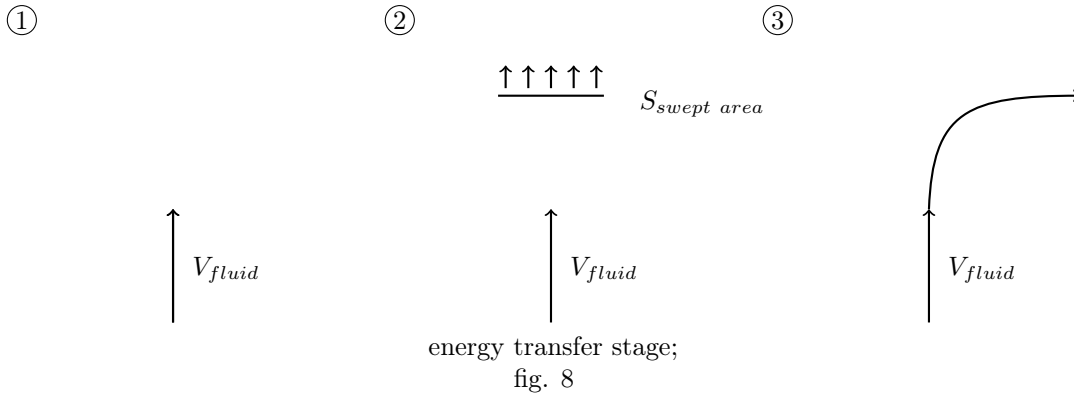
$$V_1 = V_{fluid} \quad P_1 = P_2 \quad \rightarrow \quad \frac{V_1^2}{2} - \frac{V_2^2}{2} = \frac{p_+}{\rho} - \frac{p_-}{\rho}$$

by using the equation (6),

$$E_{pot} = E_{kin}$$

The kinetic energy of the fluid is partially transformed into potential energy and then into kinetic energy

$$E_{kwind} \Rightarrow E_{pot} \Rightarrow E_{kin} \quad (8)$$



- ① Kinetic energy of the fluid
- ② Stresses are created on the turbine
- ③ The change of direction of the fluid creates a driving torque to generate energy

$$E_{kwind} \Rightarrow E_{pot} \Rightarrow E_{kin} \quad (9)$$

$$\textcircled{1} \Rightarrow \textcircled{2} \Rightarrow \textcircled{3}$$

The fluid  $\textcircled{1}$  creates stress on the surface swept  $\textcircled{2}$  by the turbine, then there is a change of direction  $\textcircled{3}$  of the fluid .

Successively, there is a transformation of energy from the kinetic energy of the fluid into potential energy, then into kinetic energy.

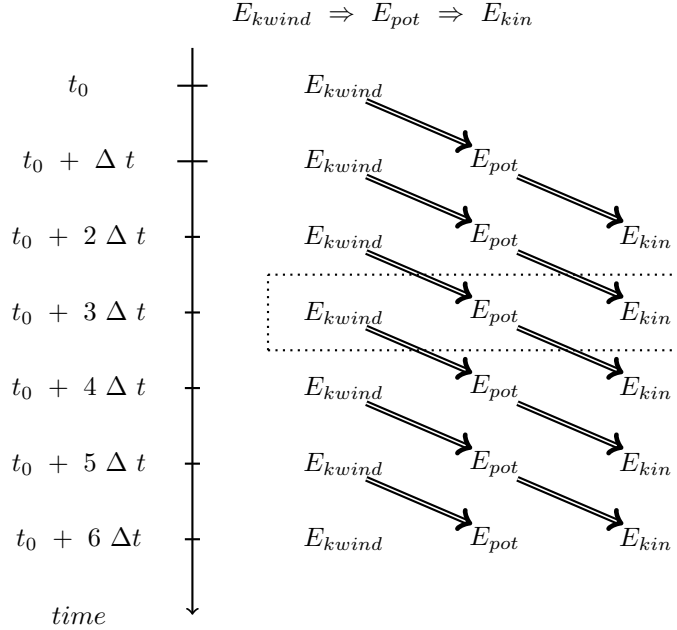


fig. 9

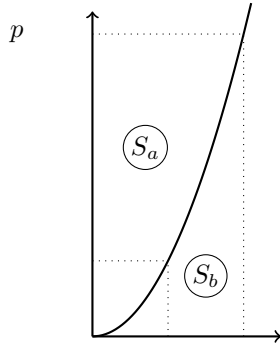
As the regime is stationary, although it is a transfer of energies, we have a summation of energies.

As there is a transfer of temporal energy  $E_{kwind}(t - 2\Delta t) \Rightarrow E_{pot}(t - \Delta t) \Rightarrow E_{kin}(t)$ , in the case of an increase in the speed of the fluid, we have successively these energy variations

$$\frac{dE_{kwind}(t - 2\Delta t)}{dt} > 0 \Rightarrow \frac{dE_{pot}(t - \Delta t)}{dt} > 0 \Rightarrow \frac{dE_{kin}(t)}{dt} > 0$$

This formulation allows to be consistent with the conservation of energy.

**remark :** The kinetic energy  $E_{kin}(v)$  and the potential energy  $E_{pot}(p)$  are not one energy and one co-energy Borel (1965) Max Marty (2005) . The pressure varies according to the square of the speed.



v fig. 10

When the fluid velocity increases, the energy variations are both positive, but the area of  $S_a$  is different from  $S_b$ .

## 5 Conversion of potential energy into additional kinetic energy

There can be energy production only if we have kinetic energy and potential energy.

For a sailboat, Betz's theory applies Kimball (2009). The fluid flow due to the wind and the forward speed of the sailboat creates an induced force on the sail. A small part of this force is used to move the sailboat forward, the other part creates stress on the sail and causes the boat to heel. Constraints are created on the keel to resist the heel. Instead of having static stresses on the keel, using hydrofoils allows a kinetic flow. This flow lifts the sailboat, creates a reaction force against the tilt and greatly improves the performance of the sailboat. The principle of transforming potential energy into kinetic energy increases performance and the wind has not been doubled.

### 5.1 Conversion of potential energy

Potential energy is the source of stress in the turbine. It is possible to convert potential energy into kinetic energy

In the case of horizontal wind turbines (HAWT, fast wind turbine type), the stress in the blades for a defined wind speed, is constant.

$$\frac{d\sigma}{d\beta} = 0$$

$\sigma$  Stress in turbine blade ( $\frac{N}{m^2}$ )  
 $\beta$  rotation angle of the blades (*rad*)

In fact, some variations of the stress exist due to gravitational forces and the differential velocity within the boundary layer depending on the elevation.

In the case of vertical axis turbines (VAWT, Darrieus type) the stress on the blades and arms depends on the rotation angle of the blades (for a given wind speed).

$$\frac{d\sigma}{d\beta} \neq 0 \quad \frac{1}{2\pi} \int_0^{2\pi} \sigma d\beta = \epsilon \quad (\epsilon \text{ small})$$

During a half-turn, the arms are submitted to compression stress whereas extending stress is dominant during the next half-turn.

In the case of a HAWT, the conversion is not possible with a dynamic mechanical system. The additional stress is constant during a rotation for a given wind speed. Alternative stress, encountered in a vertical axis wind turbine VAWT can allow the extraction of additional energy.

### 5.2 Total recoverable power of the turbine

To determine the power, one selects the power defined from the kinetic energy and, in the case of conversion of stress into a mechanical movement, the power defined from the potential energy. It is possible to convert potential energy into kinetic energy.

The total recoverable power coefficient is

$$C_{total} = C_{kin} + C_{pot}$$

$C_p = 0$  when constraints are not converted

$$P_{total} = C_{total} \frac{1}{2} \rho S V_{fluid}^3 = (C_{kin} + C_{pot}) \frac{1}{2} \rho S V_{fluid}^3$$

In the case of horizontal wind turbines (HAWT, fast wind turbine type), the power coefficient  $C_{T \text{ HAWT}}$  is

$$C_{Total \text{ HAWT}} = C_{kin} = 4 a^2 (1 - a) \quad C_{pot} = 0$$

In the case of vertical axis turbines (VAWT, Darrieus type)

the power coefficient  $C_{T \text{ VAWT Darrieus}}$  is

$$C_{Total \text{ VAWT Darrieus}} = C_{kin} = 4 a^2 (1 - a) \quad C_{pot} = 0$$

In the case of vertical axis turbines (VAWT with conversion), this stress is converted into additional energy, and the power coefficient  $C_{T \text{ VAWT with conversion}}$  is

$$C_{Total \text{ VAWT with conversion}} = C_{kin} + C_{pot} = 8 a^2 (1 - a)$$

Depending on the turbine type, the power will be different by

$$P = C_{total} \frac{1}{2} \rho S V_{fluid}^3 \quad (10)$$

$$P_{Total \text{ HAWT}} = 4 a^2 (1 - a) \frac{1}{2} \rho S V_{fluid}^3 \quad (11)$$

$$P_{Total \text{ VAWT Darrieus}} = 4 a^2 (1 - a) \frac{1}{2} \rho S V_{fluid}^3 \quad (12)$$

$$P_{Total \text{ VAWT with conversion}} = 8 a^2 (1 - a) \frac{1}{2} \rho S V_{fluid}^3 \quad (13)$$

## 6 HAWT-VAWT comparison and discussion

Following the work of Hau (2000), the power coefficient of different turbines is compared (a performance of 0.6 is applied for the supplementary energy recovery system).

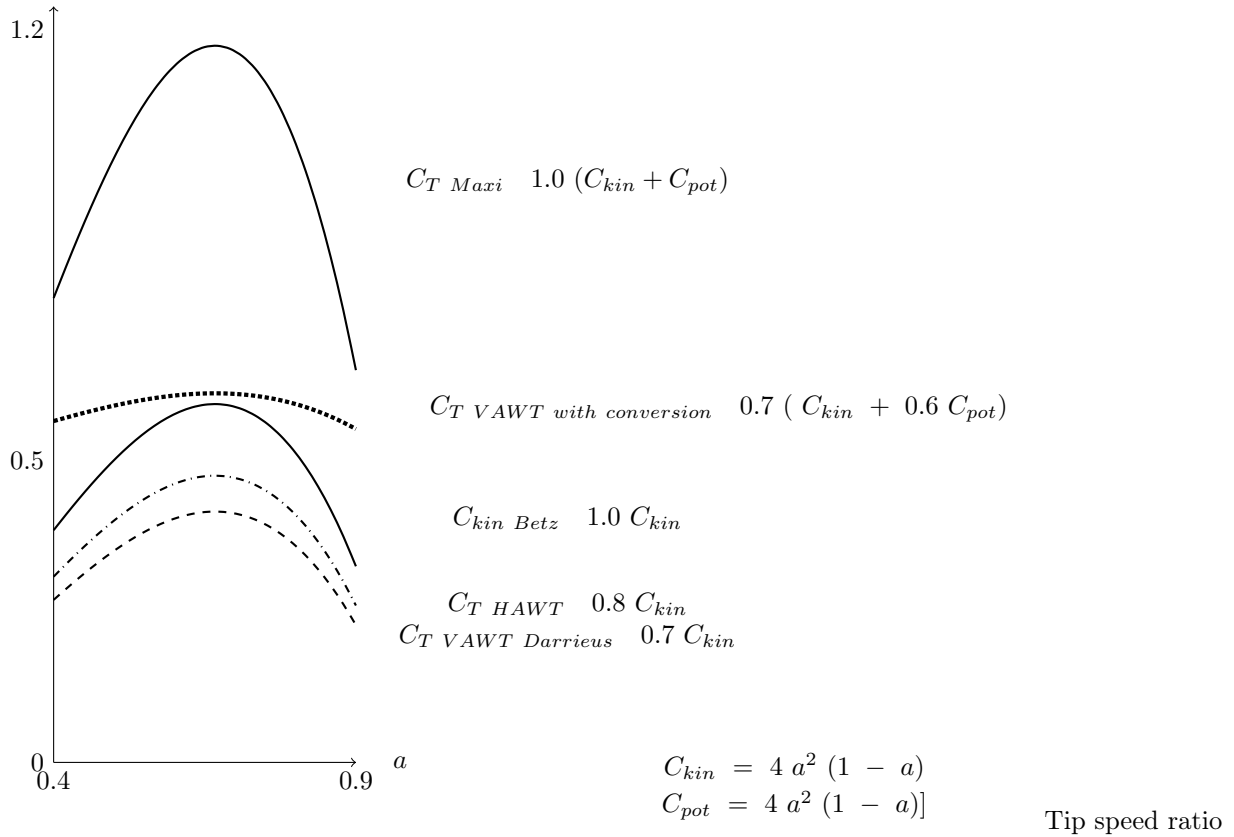
$$\text{With } a = \frac{2}{3} \quad C_{kin} \approx 60\% \quad C_{pot} \approx 60\%$$

notation  $C_{pot \text{ w.c}} = C_{pot}$  with conversion

case	Coef.	HAWT	VAWT Darrieus	VAWT with conversion
<i>perfect</i>	$C_{kin}$	60%	60%	60%
<i>perfect</i>	$C_{pot \text{ w.c}}$	0%	0%	60%
<i>perfect</i>	$C_{total}$	= 60%	= 60%	= 120%
<i>in practice</i>	$C_{kin}$	$0.8 \times 60\% \approx 48\%$	$0.7 \times 60\% \approx 42\%$	$0.7 \times 60\% \approx 42\%$
<i>in practice</i>	$C_{pot \text{ w.c}}$	0%	0%	$0.6 \times 0.7 \times 60\% \approx 25\%$
<i>in practice</i>	$C_{total}$	= 48%	= 42%	= 67%
.....				
gain/HAWT		+ 0%	-12 %	+ 39%
gain/ $C_{kin}$ (Betz)		- 20%	-30 %	+ 11%

$$\text{With } a \approx 0.8 \quad C_{kin} \approx 50\% \quad C_{pot} \approx 50\%$$

case	Coef.	HAWT	VAWT Darrieus	VAWT with conversion
<i>in practice</i>	$C_{kin}$	$0.8 \times 50\% \approx 40\%$	$0.7 \times 50\% \approx 35\%$	$0.7 \times 50\% \approx 35\%$
<i>in practice</i>	$C_{pot \text{ w.c}}$	0%	0%	$0.6 \times 0.7 \times 50\% \approx 21\%$
<i>in practice</i>	$C_{total}$	= 40%	= 35%	= 56%
.....				
gain / HAWT		+ 0%	-12 %	+ 27%
gain / $C_k$		- 20%	-30 %	+ 12%



performance curve;  
fig. 11

## 6.1 The Active lift turbine project

The "Active lift turbine" project" is an example of transformation of potential energy into kinetic energy (see preprint : Simplified theory of an active lift turbine with controlled displacement (Lecanu et al. (2016)).

$$C_{kin} = \frac{9\pi}{27} b^3 - \frac{2^3}{3} b^2 + \frac{\pi}{2} b$$

$$C_{pot} = \frac{e}{R} \lambda \left( \frac{9\pi}{27} b^3 - \frac{2^2}{3} b^2 + \frac{\pi}{2} b \right)$$

$$C_{active.lift.turbine} = \left( 1 + \frac{e}{R} \lambda \right) \left( \frac{9\pi}{27} b^3 - \frac{2^2}{3} b^2 + \frac{\pi}{2} b \right)$$

$$with \quad b = \sigma \lambda \quad \sigma = \frac{Nc}{R} \quad \lambda = \frac{R\dot{\theta}}{V_{fluid}} \quad b \leq \frac{4}{3}$$

$\sigma$  stiffness coefficient  
 $N$  Number of blades  
 $c$  Chord of profil  
 $\lambda$  Tip speed ratio  
 $e$  eccentric distance  
 $R$  Turbine radius  
 $\theta$  rotation angle of the turbine

numerical application

if  $e = 0.2$  and  $\sigma = 0.25$

$$\frac{dC_{active.lift.turbine}}{db} = \frac{d[(1 + \frac{e}{R}\frac{b}{\sigma})(\frac{9\pi}{27}b^3 - \frac{2^2}{3}b^2 + \frac{\pi}{2}b)]}{db} = 0 \quad b_1 \approx 0.84 \quad C_{active.lift.turbine} \approx .85$$

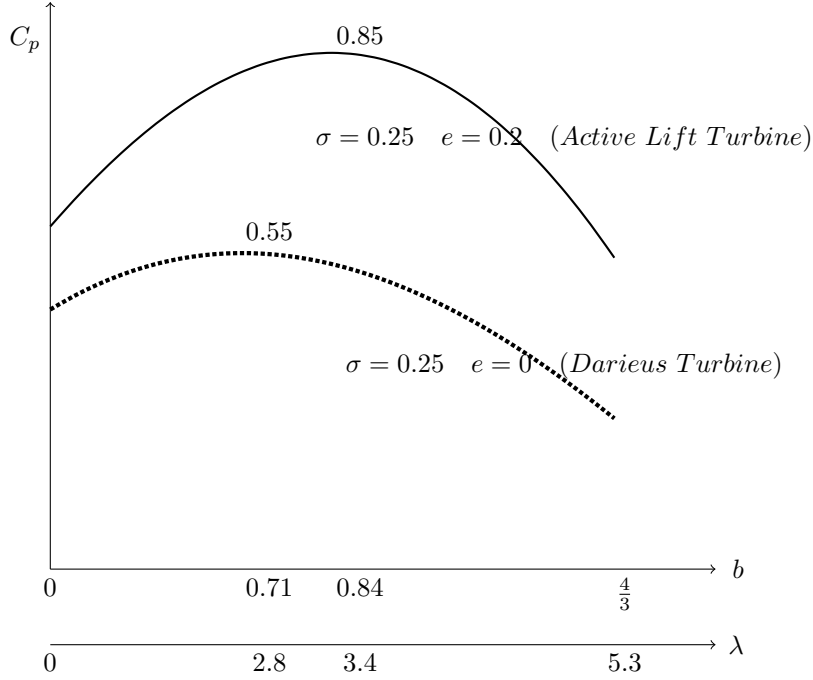


fig. 12

## 6.2 Synthesis scheme:

### 6.2.1 Low speed turbine $\lambda < 1$ :

case :  $\lambda < 1$  — turbine type Anemometer with cups  $\mathbf{E}_{kin\ wind} \Rightarrow \mathbf{E}_{pot} \ \& \ \mathbf{E}_{kin}$

For a constant wind speed, if the load of the electric generator is decreased, then we have **simultaneously** these energy variations :

$$\frac{d\mathbf{E}_{pot}}{dt} < 0 \quad \& \quad \frac{d\mathbf{E}_{kin}}{dt} > 0$$

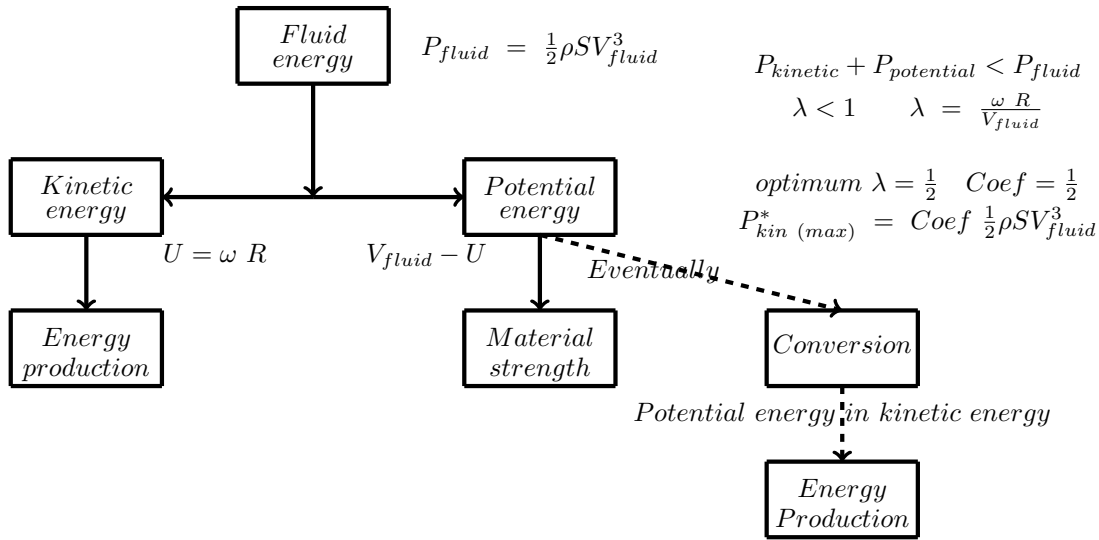


fig. 13

### 6.2.2 Fast speed turbines HAWT or VAWT $\lambda > 1$ :

case :  $\lambda > 1$  — large wind turbines HAWT or VAWT  
 Temporal transfer of energy  $E_{kwind} \Rightarrow E_{pot} \Rightarrow E_{kin}$

For a constant wind speed, if the load of the electric generator is decreased, then we have **successively** these energy variations :

$$\frac{dE_{pot}}{dt} > 0 \Rightarrow \frac{dE_{kin}}{dt} > 0$$

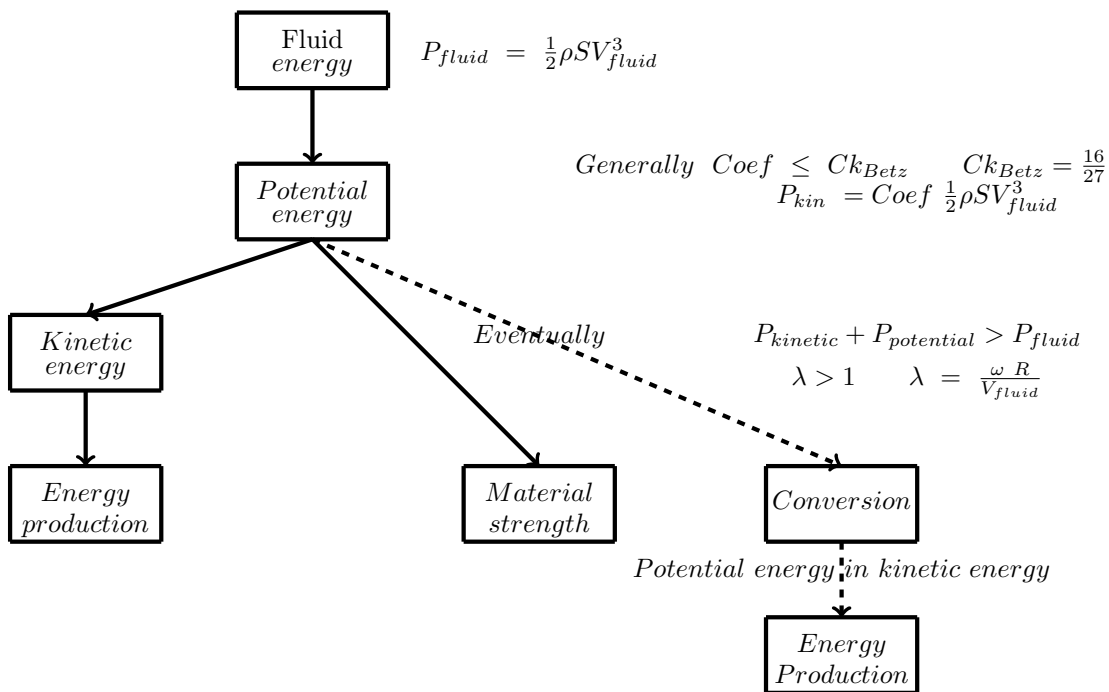


fig. 14



In the case of a turbine with a lambda lower than 1, a part of the recoverable energy, is transformed into kinetic energy and the other part into potential energy (stress in the turbine). Eventually a part of this potential energy could be transformed into kinetic energy.

In the case of a turbine with a lambda higher than 1, the recoverable energy defined by Betz, is transformed into potential energy. This energy creates kinetic but also potential energy (stress in the turbine). This is possible because a rotation speed which is higher than the speed of the fluid is created. A part of this potential energy (due to the stress) can be transformed into kinetic energy.

### 6.3 Synthesis on the extracted power:

With a mechanical conversion system, the power is, for each turbine type

$$P_{T \text{ HAWT}} = 4 a^2 (1 - a) \frac{1}{2} \rho S V_{fluid}^3$$

$$P_{T \text{ VAWT Darrieus}} = 4 a^2 (1 - a) \frac{1}{2} \rho S V_{fluid}^3$$

$$P_{T \text{ VAWT with conversion}} = 8 a^2 (1 - a) \frac{1}{2} \rho S V_{fluid}^3$$

Compared to a HAWT turbine, the gain of a VAWT Turbine with an energy recovery system is in practice from 20% to 50%.

Concerning a vertical axis turbine with a conversion system, the power factor is higher than the one defined by Betz.

In the comparative table, a yield of 0.6 was chosen for the mechanical conversion system of the potential energy into mechanical energy. By choosing an efficient technology, this yield can be greatly increased, which will improve the performance of the turbine.

The definition of the maximum power coefficient is the one established by Betz which remains valid for horizontal axis turbines HAWT but not for vertical axis turbines VAWT. The given results examined a conversion of the potential energy into kinetic energy through a mechanical system which is not applicable for horizontal axis turbines HAWT. The calculation of the powers are the sum of the powers taken into account.

**In order to obtain productive kinetic energy, kinetic energy and potential energy are needed. The maximum productive kinetic power is equal to**

$$P_{k-max-productive} \leq \min( P_k , P_p )$$

The limit of this depends on whether it is a low or high speed turbine

$$P_{k(max)} = Coef \frac{1}{2} \rho S V_{fluid}^3$$

$$\begin{aligned} Coef &= \frac{1}{2} && \text{for low speed turbines } (\lambda < 1) \\ Coef &= \frac{16}{21} && \text{for high speed turbines } (\lambda > 1) \end{aligned}$$

The maximum power coefficient for a wind or tidal turbine is

$$C_{Total \text{ maxi } \lambda < 1} = \frac{100}{100} (\approx 100\%)$$

$$C_{Total \text{ maxi } \lambda > 1} = \frac{32}{27} (\approx 118.5\%)$$

$C_{Total \text{ maxi}}$  is a limit value with  $C_{pot} \leq C_{kin}$ .

Using piezo-electric materials would make it possible to transform potential energy into electrical energy. However, in order to achieve higher efficiency, the potential energy should be transformed into kinetic energy.

Thus, the power coefficient will be  $C_{total} = C_{kin} + C_{pot}$  whatever the type of turbine.

Note : In the case of a turbine in a channel (see appendix 15 ), the maximum kinetic power coefficient is to 1. The maximum total power coefficient is then 200%.

## 7 Conclusion

The article presents a new formulation for power calculation of wind or water turbines.

Taking into account the potential energy allows to establish that the conservation of energy is well verified.

This was not the case in the formulation presented by Betz.

A new power coefficient has been defined for the turbines depending on their type, low or high speed.

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## A : Appendix

Maximum wind power recovered from kinetic energy

$$E_k = \frac{1}{2} m V^2$$

$$\frac{dE_k}{dt} = \frac{1}{2} \frac{dm}{dt} V^2 + \frac{1}{2} m \frac{dV^2}{dt} \quad \frac{dV}{dt} = 0$$

$$\frac{dE_k}{dt} = \frac{1}{2} \dot{m} V^2 = \frac{1}{2} \rho S V^3$$

V Wind speed at the turbine level

Force applied by the wind on the rotor

$$F = m \frac{dV}{dt} = \dot{m} \Delta V = \rho S V (V_{fluid} - V_{wake})$$

$V_{wake}$  streamwise velocity in the far wake

$$P = FV = \rho S V^2 (V_{fluid} - V_{wake})$$

$$P = \frac{\Delta E}{\Delta t} = \frac{\frac{1}{2} m V_{fluid}^2 - \frac{1}{2} m V_{wake}^2}{\Delta t}$$

$$P = \frac{\Delta E}{\Delta t} = \frac{1}{2} \dot{m} (V_{fluid}^2 - V_{wake}^2) = \frac{1}{2} \rho S V (V_{fluid}^2 - V_{wake}^2)$$

From these equalities

$$V = \bar{V} = \frac{V_{fluid} + V_{wake}}{2}$$

$$F = \rho S V (V_{fluid} - V_{wake}) = \frac{1}{2} \rho S (V_{fluid}^2 - V_{wake}^2)$$

$$P = FV = \rho S V^2 (V_{fluid} - V_{wake})$$

defining  $a = \frac{V}{V_{fluid}}$

$$V_{wake} = V_{fluid} (2a - 1) \quad \text{as } V_{wake} \geq 0 \quad a \geq \frac{1}{2}$$

$$P = 4a^2(1-a) \frac{1}{2} \rho S V_{fluid}^3$$

defining power coefficient  $C_k = \frac{P}{\frac{1}{2} \rho S V_{fluid}^3} = 4a^2(1-a)$

Search of maximum power coefficient

$$\frac{dC_k}{da} = 0 \quad a(2 - 3a) = 0 \quad a = 0 \quad \text{or} \quad a = \frac{2}{3}$$

$$a = \frac{2}{3} \quad C_k = \frac{16}{27} = 0.593$$

The maximum power coefficient  $C_{k_{maxi}}$  is defined by Betz

$$C_{k_{maxi}} = C_{k_{Betz}} = \frac{16}{27} \approx 60\%$$

The maximum power of the fluid is

$$P_{fluid} = \frac{1}{2} \rho S_{fluid} V_{fluid}^3$$

$$S_{fluid} = \frac{S V}{V_{fluid}} = a S$$

The power of the turbine is

$$P = \frac{C_k}{a} P_{fluid} = C_k \frac{1}{2} \rho \frac{S_{fluid}}{a} V_{fluid}^3 = C_k \frac{1}{2} \rho S V_{fluid}^3$$

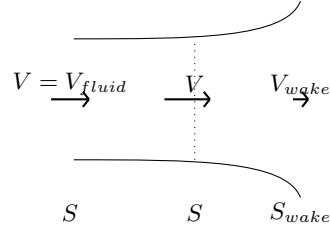
The maximum power of the turbine is

$$P_{max} = \frac{C_k}{\frac{2}{3}} P_{fluid} = \frac{8}{9} P_{fluid} = C_k \text{ Betz} \frac{1}{2} \rho S V_{fluid}^3 = \frac{16}{27} \left( \frac{1}{2} \rho S V_{fluid}^3 \right)$$

$$P_{max} = C_k \text{ Betz} \frac{1}{2} \rho S V_{fluid}^3 \tag{14}$$

## B : Appendix

Maximum wind power for a turbine in a channel (from kinetic energy)



$$E_k = \frac{1}{2} m V^2$$

$$\frac{dE_k}{dt} = \frac{1}{2} \frac{dm}{dt} V^2 + \frac{1}{2} m \frac{dV^2}{dt} \quad \frac{dV}{dt} = 0$$

$$\frac{dE_k}{dt} = \frac{1}{2} \dot{m} V^2 = \frac{1}{2} \rho S V^3$$

V Wind speed at the turbine level

Force applied by the wind on the rotor

$$F = m \frac{dV}{dt} = \dot{m} \Delta V = \rho S V (V - V_{wake})$$

$V_{wake}$  streamwise velocity in the far wake

$$P = FV = \rho S V^2 (V - V_{wake})$$

$$P = \frac{\Delta E}{\Delta t} = \frac{\frac{1}{2} m V^2 - \frac{1}{2} m V_{wake}^2}{\Delta t}$$

$$P = \frac{\Delta E}{\Delta t} = \frac{1}{2} \dot{m} (V^2 - V_{wake}^2) = \frac{1}{2} \rho S V (V^2 - V_{wake}^2)$$

From these equalities

$$V_{wake} = \frac{1}{2} V \quad S_{wake} = \frac{S V}{V_{wake}} = 2 S$$

$$F = \rho S V (V_{fluid} - V_{wake}) = \frac{1}{2} \rho S (V_{fluid}^2 - V_{wake}^2)$$

$$P = FV = \rho S V^2 (V_{fluid} - V_{wake})$$

$$P = \frac{1}{2} \rho S V_{fluid}^3$$

defining power coefficient

$$C_k = \frac{P}{\frac{1}{2} \rho S V_{fluid}^3} = 1 \quad (15)$$

## C : Appendix

Additional recovery power (from potential energy)

The fluid creates stresses in the blade. They are due to thrust force. The energy of this force is

$$E_p = m \frac{f_s}{\rho}$$

$f_s$  thrust force

For HAWT horizontal wind turbines (fast wind turbine type), the thrust force  $F_s$  are constant.

$$\frac{dE_p}{dt} = 0$$

For a VAWT, the thrust force depends on the time or the rotation angle  $F_s(t)$  or  $F_s(\beta)$   $\beta = \omega t$

$\omega = \frac{d\beta}{dt}$  angular frequency

$$\frac{dE_p}{dt} \neq 0 \quad \text{and} \quad \frac{1}{2\pi} \int_0^{2\pi} E_p(\beta) d\beta = \epsilon \quad (\epsilon \text{ small})$$

As

$$F_s = f_s S = C_x \frac{1}{2} \rho S V_{fluid}^2$$

$$E_p = m C_x \frac{1}{2} V_{fluid}^2$$

$V$  fluid speed at the level turbine

The power is

$$P_p = \frac{dE_p}{dt} \quad dm = \rho S V dt$$

$$P_p = \frac{dE_p}{dt} = \frac{dm}{dt} C_x \frac{1}{2} S V_{fluid}^2 + m C_x \frac{1}{2} S \frac{dV_{fluid}^2}{dt} \quad \frac{dV_{fluid}}{dt} = 0$$

$$P_p = a C_x \frac{1}{2} \rho S V_{fluid}^3 \quad \text{with } a = \frac{V}{V_{fluid}} \quad (16)$$

$$\frac{1}{2\pi} \int_0^{2\pi} E_p(\beta) d\beta = \epsilon \quad (\epsilon \text{ small}) \quad E_{p-max} \approx -E_{p-min}$$

the power depends on a potential energy difference

$$P_p = \frac{\Delta E_p}{\Delta t} \quad T = \frac{2\pi}{\omega} \quad P_p \leq \frac{E_{p-max} - E_{p-min}}{T} \quad P_p \leq \frac{E_{p-max}}{\pi} \omega$$

for a half-turn

$$E_p(\beta) R d\beta = dE_p \pi R$$

in particular

$$E_{p-max} = \frac{dE_p}{d\beta} \pi = \frac{dE_p}{dt} \frac{\pi}{\omega}$$

As

$$\frac{dE_p}{dt} = a C_x \frac{1}{2} \rho S V_{fluid}^3 \quad \text{and} \quad P_p \leq \frac{E_{p-max}}{\pi} \omega$$

$$P_p \leq a C_x \frac{1}{2} \rho S V_{fluid}^3$$

## D : Appendix

Variation of energy in opposite sense

Along a streamline, the Bernoulli's equation is see Bernoulli (1738)

$$\frac{p}{\rho} + \frac{v^2}{2} = \text{constant} \quad \text{with } z = 0$$

By multiplying by m

$$m \frac{p}{\rho} + m \frac{v^2}{2} = \text{constant}$$

The differential of this equation is

$$d\left(\frac{1}{2} m v^2\right) = -d\left(m \frac{p}{\rho}\right) \tag{17}$$

the variations of energy vary simultaneously and in opposite sense.

$$\text{As } \frac{dV}{dt} = 0 \quad \text{and} \quad \frac{dp}{dt} = 0 \quad p = -\frac{1}{2} \rho v^2$$

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