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A numerical model including thermodynamic equilibrium, kinetic control and surface complexation in order to explain cation type effect on chloride binding capability of concrete

Van Quan Tran^a, Anthony Soive^b, Stéphanie Bonnet^c, Abdelhafid Khelidj^c

Abstract

The impact of cation type, sulphate and pH on chloride binding is studied using a numerical model combining thermodynamic equilibrium, kinetics and surface complexation. First, the model is validated by comparing numerical and experimental results obtained on a CEM II concrete material exposed to NaCl, KCl, MgCl₂ and CaCl₂ solutions. Then, the numerical results are discussed to improve our understanding of the differences in chloride binding capability generally observed in the literature. A strong coupling between cation, pH and sulfate affecting chloride binding is highlighted. After six months of exposure, chloride binding due to Kuzel's salt formation has little effect on chloride binding capability whatever the chloride salt solution. The results also confirm the existence of a relationship between pH and chloride binding capability previously observed experimentally in the literature. When some sulfate ions are present in the chloride solution, they reduce

^a University of Transport Technology, No. 54 Trieu Khuc street, Thanh Xuan District, Hanoi. Vietnam

^b Cerema, UMR 7329 GEOAZUR, Pôle d'activités, avenue Albert Einstein CS 70499, 13593 Aix-en-Provence cedex 3. France

^c Université de Nantes, GeM, Institut de Recherche en Génie civil et Mécanique, CNRS UMR 6183, France

the chloride binding capability because of the sulfate absorption process on C-S-H.

Keywords: Concrete; Chloride binding; Thermodynamic equilibrium; Kinetic control; Surface complexation; Cation type.

1 1. Introduction

Chloride diffusion is one of the major cause of reinforcement corrosion in concrete exposed to seawater or de-icing salts. Many authors consider that corrosion initiation stage of steel reinforcement in concrete depends on the chloride threshold value which can be expressed in a number of different ways, such as: total chloride content in relation to the weight of cement (or concrete) (1), free chloride contents (2), $[Cl^-]/[OH^-]$ (3; 4). To predict the chloride concentration threshold value in cementitious materials, the performance-based approach Fib model code (5) requires the consideration of the empirical chloride binding isotherm. In this model, based on the analytical solution of the Fick's second law, the chloride binding isotherm is therefore one of the most significant input data of the Fib model code.

A survey of the literature reveals that a considerable amount of effort has been devoted in the last decade to the study of chloride binding in ce-

has been devoted in the last decade to the study of chloride binding in cementitious materials. Page et al. (6), for instance, show that the OH^- concentration (or pH) arising from the external environment significantly affects chloride binding. Tritthart (7) and Sandberg et al. (8) both experimentally demonstrate that lower pH values give higher chloride ions binding, which may be accounted for by a competition among OH^- and Cl^- ions for

the sorption sites of hydrated cement (7). Moreover, Roberts (9) and Zhu et al. (10) consider that an increase in pore solution pH enhances the solubility of chloroaluminate salt (Friedel's salt, Kuzel's salt) consequently reducing chloride binding due to chloroaluminate salt formation. Furthermore, Arva et al. (11), Page et al. (6), Delagrave et al. (12), Zhu 25 et al. (10), DeWeerdt et al. (13) and Song et al. (14) experimentally observe 26 that cations associated to chloride salts affect chloride binding capability. 27 These authors note that the maximum chloride binding capability is reached when the cementitious materials are exposed to a $CaCl_2$ solution. In a more detailed manner, Zhu et al. (10) and Song et al. (14) experimentally describe that the binding capability of chloride decreases in the order $Ca^{2+} > Mg^{2+}$ $> Na^+ \approx K^+$ when the cementitious samples are exposed to $CaCl_2$, $MgCl_2$, NaCl and KCl solutions, respectively. Wowra et al. (15) find that the Ca^{2+} cations sorption onto C-S-H surfaces increases the positive charge and in turn the chloride binding in the double electrical layer. Moreover, according to Delagrave et al. (12), the nature of the associated cation significantly affects chloroaluminate solubility and accessibility of chloride ions to sorption sites. On the basis of experimental results, Yuan et al. (16) suggest that, in the presence of Na^+ , cementitous materials have higher pH value than with Ca^{2+} and Mq^{2+} . Zhu et al. (10) demonstrate that Na^+ and K^+ may increase the pH value of pore solutions. These arguments imply that pore solution pH affects chloride binding capability. However, DeWeerdt et al. (13) experimentally prove that the relationship between the decrease in pore solution pH and the increase in chloride binding for exposure solutions like $MgCl_2$ or $CaCl_2$ is not valid when the SO_4^{2-}

ions concentration is significant. Byfors (17) and Wowra et al. (15) have previously shown that an increase in sulfate ion concentration causes a sharp decrease in chloride binding capability. DeWeerdt et al. (13) suggest that one reason might be the chloride sorption process onto C-S-H and the chloride binding due to the chloroaluminate salt formation capacity. C-S-H indeed, when exposed to MgSO4 and $MgCl_2$, fixes more SO_4^{2-} ions than Cl^- ions, leading to the decreased chloride sorption onto C-S-H. The SO_4^{2-} ions react with the AFm phase to precipitate ettringite which is more stable than the chloroaluminate salts (Friedel's salt, Kuzel's salt) and as a result chloride binding due to chloroaluminate salt formation decreases.

The experimental studies mentioned above emphasize the coupling effect of three different factors affecting chloride binding capability: cation of chloride salt, solution pH and sulfate concentration. It is, however, interesting to verify and confirm the arguments proposed through a numerical investigation. The numerical study presented in this paper is carried out through the development of a numerical model, its validation through the comparison with the experimental results found in the literature and the analysis of the chloride binding mechanism in a final section.

A number of chloride transport models are found in the literature: some models based on Fick's second law or on the multispecies ionic transport equations (18), (19) and (20), or physically and chemically coupled model (21). These models use global binding isotherms to determine the total chloride amounts as a function of the free chloride amounts. However, isotherms parameters must be calibrated on the basis of experimental data (19).

Numerical models must describe simultaneously chloride sorption and

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binding due to the chloroaluminate salt formation. Chloride sorption can be described using a surface complexation model considering the surface charge and the double electrical layer. Chloride binding due to the chloroaluminate salt formation is described by chloroaluminate precipitation/dissolution using thermodynamic equilibrium and kinetic control. The aim of this paper is to investigate the factors affecting chloride binding in concretes exposed to chloride and other ions. A reactive transport model including thermodynamic equilibrium, kinetic control and surface complexation modelling that has been previously described for chloride ingress and external sulphate attack (22; 23) is used.

First, the governing equations used to simulate the reactive transport model in saturated cementitious materials are presented: transport equations, surface complexation describing interaction on mineral surfaces, principle of thermodynamic equilibrium and kinetic laws. Then, the model input data of the model are discussed: parameters of solid species under kinetic constraints, surface complexation parameters, original mineralogical composition of hydrated cement, exposure conditions and numerical procedure, sorption reaction in thermodynamic database. Finally, the modelled results are compared with some experimental data from the literature to validate the numerical model.

2. Reactive transport modeling and input data

In this section the reactive transport modeling is exposed on several aspects, such as reactive transport equations, thermodynamic and complexation formation constants and kinetics of dissolution/precipitation. However,

the description of the model is intentionally reduced since it has been previously published and described in details for chloride transport in concrete (23) and external sulphate attack (22).

2.1. Reactive transport equations

The coupling of chemistry and transport in porous media was used to describe the mineral phases evolution in time and space. Toughreact, which is based on integral finite differences method, has been developed for this purpose by solving chemically reactive nonisothermal flows of multiphase fuids in porous media (24). A sequential iterative operator-splitting method is operated to solve the system.

In saturated condition without convection phenomena the main mechanism considered is diffusion which is coupled to chemistry according to the following equation:

$$\frac{\partial \phi C_j}{\partial t} = D_e \nabla \left(\nabla C_j \right) + q_j \tag{1}$$

where D_e is the effective diffusion coefficient of species j ($m^2.s^{-1}$) which value is the same for all species, ϕ the porosity and C_j the molar concentration of free species j in a pore solution ($mol.m^{-3}$ of solution). q_j is a source or sink term ($mol.m^{-3}.s^{-1}$) that denotes the removing or releasing species j and that is evaluated by chemical calculations. In this study, q_j combines sorption onto C- S-H surface (see paragraph 2.4), mineral dissolution/precipitation as explained in paragraphs 2.2 and 2.3 and aqueous complexation in solution.

Porosity can evolve with time by actualizing volume of each mineral species (25) that can precipitate or dissolve. Effective diffusion coefficient

can also evolve, as follows:

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$$D_e^{n+1} = \frac{\phi^{n+1}}{\phi^n} D_e^n$$

where n labels the number of the time step.

116 2.2. Thermodynamic formation constants

The thermodynamic formation constants of species are taken from CEMDATA07 and Nagra/PSI TDB thermodynamic databases (26). The thermodynamic data are exposed in Table 1. C-S-H is supposed to be a mix
of tobermorite $(CaO/SiO_2 = 0.83)$ and jennite $(CaO/SiO_2 = 1.67)$. The
Helgeson-Kirham-Flowers (HKF) model (27) is used since it gives accurate
activity coefficient with dominance of NaCl in the solution and when the
true ionic strength of the solution is close to 1 (24), as in this study.

At equilibrium, the activity product, Q_i , of the mineral species i must be equal to its equilibrium constant, K_i . Q_i writes as follows:

$$Q_i = \prod_{j=1}^{N} (\gamma_j C_j)^{\nu_j} \tag{2}$$

where γ , C, ν and N are the activity coefficient, the concentration, the stoichiometric coefficient and the number of the ionic species in the reaction, respectively.

2.3. Mineral dissolution and precipitation kinetics

Several studies have shown that a pure thermodynamic approach does not seem to be adapted for concrete exposed for several months (22; 23; 28; 29; 30). Moreover, for C-S-H the reactions can be very slow and even irreversible.

Table 1: Equilibrium constants of mineral dissolution/precipitation reactions at $25^{\circ}C$

Phase reaction	$\log K_{T_0}$
Jennite+ $2.33H^+ = 1.67Ca^{2+} + HSiO_3^- + 2.76H_2O$	-19.53
Tobermorite+ $0.66H^+ = 0.83Ca^{2+} + HSiO_3^- + 1.16H_2O$	-0.63
$Portlandite + 2H^+ = Ca^{2+} + 2H_2O$	-22.76
Monosulfoaluminate+ $12H^{+} = 4Ca^{2+} + 2Al^{3+} + SO_4^{2-} + 18H_2O$	-72.44
Ettringite+ $12H^+ = 6Ca^{2+} + 2Al^{3+} + 3SO_4^{2-} + 38H_2O$	-56.67
Hydrotalcite+ $14H^+ = 4Mg^{2+} + 2Al^{3+} + 17H_2O$	-74.68
Kuzel's salts+ $12H^+ = 4Ca^{2+} + 2Al^{3+} + 0.5SO_4^{2-} + Cl^- + 18H_2O$	-73.24
$Brucite + 2H^+ = Mg^{2+} + 2H_2O$	17.11
Chrysotile $+4H^{+} = 3Mg^{2+} + 2HSiO_{3}^{-} + 3H_{2}O$	-13.29
Sepiolite+ $2H^+ = 4Mg^{2+} + 6HSiO_3^- + 5H_2O$	-29.01

In this study, the expression of the kinetic law given by Lasaga et al. is used (31):

$$r_i = \pm k_i A_{ms,i} \left| 1 - \left(\frac{Q_i}{K_i} \right) \right| \qquad i = 1, .., N_q$$
 (3)

where r indicates dissolution or precipitation (for positive and negative values, respectively), k is the rate constant $(mol.m^{-2}.s^{-1})$. A_{ms} is the specific 137 reactive surface area $(m^2.g^{-1})$. More details can be found in Xu et al. and 138 Steefel et al. (24; 25). 139 Table 2 exposes the kinetic parameters for each mineral species. Data are 140 taken from Baur et al. for Monosulfoaluminate, ettringite and C-S-H (32), from Gali et al. for portlandite (33), from Tambach et al. for hydrotalcite (34) and from Palandri and Kharaka for brucite, gibbsite and chrysolite (35). 143 Kuzel's salt is assumed to react instantaneously because of missing data. It is to note that the simulations are performed on concretes exposed to chlorides during several months that is to say for short exposition

time compared to concrete service life. The kinetics approach is of interest to know which mineral species is susceptible to precipitate during this transient problem. The precipitation of Kuzel's salt is observed (by the model thanks to the kinetics approach) first and at low chloride concentration, while Friedel's salt is observed later and for greater concentration (36).

Table 2: Parameters describing the kinetics of mineral reactions at 25°C where k is the dissolution rate constant $(mol.m^{-2}.s^{-1})$ and A_{ms} the mineral specific reactive surface area $(m^2.g^{-1})$. Precipitation mechanism and associated constants are assumed to be similar to dissolution

Minerals	A_{ms}	k	Ref
Jennite	41.0	2.75×10^{-12}	(32)
Tobermorite	41.0	2.75×10^{-12}	(32)
Ettringite	9.8	7.08×10^{-13}	(32)
Monosulfoaluminate	5.7	6.76×10^{-12}	(32)
Portlandite	16.5	2.24×10^{-8}	(33)
Hydrotalcite	9.8	1.00×10^{-09}	(34)
Kuzel's salt		Instantaneous	
Gibbsite	9.8×10^{-4}	3.16×10^{-12}	(35)
Brucite	9.8×10^{-4}	5.75×10^{-9}	(35)
Chrysotile	9.8×10^{-4}	10.0×10^{-12}	(35)
Sepiolite		Instantaneous	

2.4. Surface complexation formation constants

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In cementitious materials, physical and chemical reactions between aqueous species and specific surface sites of mineral species can occur. These reactions mostly take place onto C-S-H (37; 38; 39). When the cementitious materials are exposed to boundary solutions, anions and cations move through the material and reactions between the ions and the surface site of C-S-H (silanol $\equiv SiOH$) appears (40). A well-known model which is used in this study is the double diffuse layer model (see (41) for a complete description).

Adsorption of X ions $(Ca^{2+}, Na^+, K^+, Cl^- \text{ and } SO_4^{2-} \text{ in the present study})$ onto the C-S-H surface can be described by the following mass action law:

$$K_{eq} = \frac{\left[\equiv SiOHX \right]}{\left[\equiv SiOH \right] \left\{ X \right\}} \exp\left(\frac{-F\psi_0}{RT} \right) \tag{4}$$

where K_{eq} is the equilibrium constant. $\{X\}$ is the activity of X ions. ψ_0 is
the potential at the surface (V). R is the molar constant $(8.354\ J.mol^{-1}.K^{-1})$ and T is the absolute temperature (K).

The sorption of Ca^{2+} , Na^+ , K^+ , Cl^- and SO_4^{2-} ions on the C-S-H surface
layer have been integrated in the database. They can be represented by
sorption reactions (see Table 3). The equilibrium constants are taken from (40) for Na^+ , K^+ , Cl^- and Ca^{2+} . That of SO_4^{2-} is supposed to be equal to
8.5. The equilibrium constants for Na^+ and K^+ are supposed to depend on C/S ratio of C-S-H whereas those for Ca^{2+} and Cl^- are not. Furthermore,
the value of the specific surface site of C-S-H is supposed to be equal to 500 $m^2 \cdot g^{-1}$ as suggested by Viallis et al. after calibration (37).

3. Concrete properties

The studied CEMII concrete is taken from the literature (14). The cement composition and the concrete mix-design are given in Tables 4 and 5, respectively. After a 90-day curing period in saturated limewater at $20\pm1^{\circ}C$,

Table 3: Equilibrium constants of the surface complexation model.

Equation	$\log K_{T_0}$	Ref
$\equiv SiOH \leftrightarrow \equiv SiO^- + H^+$	-12.7	(40)
or $\equiv SiOH + OH^- \leftrightarrow \equiv SiO^- + H_2O$		
$\equiv SiOH + Ca^{2+} \leftrightarrow \equiv SiOCa^{+} + H^{+}$	-9.4	(40)
$\equiv SiOH + Cl^- \leftrightarrow \equiv SiOHCl^-$	-0.35	(40)
$\equiv SiOH + Ca^{2+} + Cl^{-} \leftrightarrow \equiv SiOCaCl + H^{+}$	-9.8	a,b
$\equiv SiOH + Ca^{2+} + SO4^{2-} \leftrightarrow \equiv SiOCaSO_4^- + H^+$	-8.5	a,b
$\equiv SiOH_{jennite} + Na^{+} \leftrightarrow \equiv SiONa_{jennite} + H^{+}$	-13.745	(40)
$\equiv SiOH_{jennite} + K^{+} \leftrightarrow \equiv SiOK_{jennite} + H^{+}$	-13.745	(40)
$\equiv SiOH_{tobermorite} + Na^{+} \leftrightarrow \equiv SiONa_{tobermorite} + H^{+}$	-12.656	(40)
$\equiv SiOH_{tobermorite} + K^{+} \leftrightarrow \equiv SiOK_{tobermorite} + H^{+}$	-12.656	(40)
Specific surface site of C-S-H $A_{cs} = 500 \ m^2.g^{-1}$ (37)		
Sorption density of C-S-H $\Gamma_{C-S-H} = 8 \times 10^{-6} \ mol.m^{-3}$	(42), (43))
^a : Reaction on the C-S-H surface taken from (44)		

 $[^]b \colon \text{Value of} \, \log K_{T_0}$ considered in the study

some $\emptyset 100mm \times 50mm$ specimens were drilled out. The side and bottom surfaces of the cylinder specimens were sealed with epoxy resin. An immersion test was conducted to determine the penetration depth of chloride and the chloride binding isotherms in saturated conditions at 20°C under laboratory conditions. The concrete properties and experimental data are detailed in Song et al. (14).

Table 4: Chemical composition of cement, expressed as a percentage (%) (14).

Composition	SiO_2	Al_2O_3	Fe_2O_3	CaO	MgO	SO_3	Na_2O	K_2O
Content	21.70	5.09	4.32	64.64	0.92	1.08	0.21	0.53

Table 5: Concrete mix-design $(kg.m^{-3})$ (14).

Cement	Water	Sand	Gravel	w/c
312	156	746	1118	0.5

The concrete is supposed to be completely hydrated. Its mineral composition is calculated using the GEMS-software and CEMDATA07 and Nagra/PSI TDB thermodynamic databases (26). The mineralogical composition is given in Table 6.

Table 6: Mineralogical content ($mol.dm^{-3}$ of concrete)

Minerals	Content
Jennite	0.9882
Tobermorite	0.1384
Ettringite	_
Monosulfoaluminate	0.0421
Portlandite	1.6011
Hydrotalcite	0.0178

Assuming that alkalis Na and K are fully dissolved as suggested by Trotignon et al. (45), the initial chemical composition of the pore solution is calculated using the Toughreact software (24) (Table 7).

Table 7: Initial composition of the pore solution in CEMII concrete $(mol.kg^{-1})$ calculated using Toughreact at 20°C.

	Concentration $[mol/kg \text{ of pore solution}]$
Na^+	0.1366
K^+	0.2271
Ca^{2+}	0.2979×10^{-2}
Mg^{2+}	0.4057×10^{-10}
Al^{3+}	0.2348×10^{-3}
$HSiO_3^-$	0.1592×10^{-5}
SO_4^{2-}	0.2007×10^{-4}
pH	13.53

4. Results

191 4.1. Case study description

CEMII concrete is exposed to four different boundary solutions: 0.5 $mol.L^{-1}$ NaCl solution, 0.5 $mol.L^{-1}$ KCl solution, 0.25 $mol.L^{-1}$ $MgCl_2$ solution and 0.25 $mol.L^{-1}$ $CaCl_2$ solution. In order to investigate the impact of sulfate ions on chloride binding capability, solutions of 0.25 $mol.L^{-1}$ $MgCl_2 + 0.0276$ $mol.L^{-1}$ of $MgSO_4$ (SO_4^{2-} concentration in seawater) and of 0.25 $mol.L^{-1}$ $MgCl_2 + 0.276$ $mol.L^{-1}$ of $MgSO_4$, respectively, are simulated.

4.2. Numerical procedure

Only saturated concrete is considered during the simulations. Because 200 the numerical results are compared with experimental data obtained from 201 $\emptyset 100mm \times 50mm$ cylindrical specimens, one-dimensional calculations are 202 carried out. Indeed, during the immersion test, the side and bottom sur-203 faces of the cylinder specimens are sealed with epoxy resin to ensure a one-204 dimensional flow inside the cylinders as the top surface is exposed to the so-205 lutions for six months. A simple regular mesh composed of one 1000-element 206 row is used, which represents 100 mm of the specimens. The reactive trans-207 port code Toughreact (24) is used.

In the model proposed here, the only input data used to obtain chloride binding isotherms are the chemical composition of cement and the concrete mix-design. Porosity and effective diffusion data are additionally necessary coefficient when the ion profiles as a function of depth and time are required (22; 30; 23).

4.3. Chloride binding isotherms

Figures 1a,b,c and d display the chloride binding isotherms of concrete after a 6-month exposure to $0.5 \ mol.L^{-1}$ of NaCl, $0.25 \ mol.L^{-1}$ of $CaCl_2$, $0.5 \ mol.L^{-1}$ of KCl and $0.25 \ mol.L^{-1}$ of $MgCl_2$ solutions, respectively. The numerical chloride binding isotherms obtained are compared with the experimental data previously found in the literature (14).

The equilibrium computation gives a pH of 8.1 for all the chloride solutions. Further details on the pH calculation are given in (46). The fact that the experimental chloride binding isotherms for each exposed solution are successfully reproduced by the model confirms that the chloride binding

capability depends on the boundary solution type. The amount of bound chloride ions in concrete exposed to NaCl and KCl solutions are equivalent. They are larger for concrete exposed to $CaCl_2$ and $MgCl_2$ solutions. The chloride binding capability as a function of the boundary solution type decreases in the order: $Ca^{2+} > Mg^{2+} > Na^+ \approx K^+$. This result confirms the findings of Arya et al. (11), Page et al. (6), Delagrave et al. (12), Zhu et al. (10), DeWeerdt et al. (13).

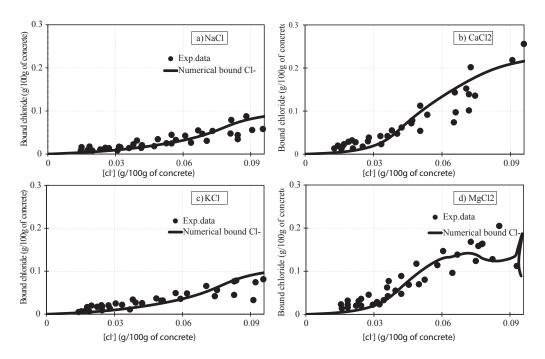


Figure 1: Chloride binding isotherm of CEM II concrete after 3 months of exposure to a) $0.5 \ mol.L^{-1} \ NaCl$ solution, b) $0.25 \ mol.L^{-1} \ CaCl_2$ solution, c) $0.5 \ mol.L^{-1} \ KCl$ solution and d) $0.5 \ mol.L^{-1} \ MgCl_2$ solution at 20° C (experimental data taken from the literature (14)).

5. Discussion

As discussed above, the model proposed in this paper can compute chloride absorption on C-S-H, chloride binding due to Kuzel's salt formation and
pH evolution. The following section provides some interpretive elements for
a better understanding of the evolution of chloride binding capability as a
function of boundary solution type. First, the chloride bound amount due
to Kuzel's salts precipitation and to surface complexation on C-S-H is highlighted. Then, the influence of cations associated with chloride from surface
complexation on C-S-H and its consequence in terms of pH is discussed. finally, additionally focus is made on magnesium and sulfate ions and their
effect on chloride binding capability.

$_{ m 242}$ 5.1. Kuzel's salt formation and surface complexation on C-S-H

Chloride ions can be adsorbed and absorbed on C-S-H. The adsorption on C-S-H are supposed to happen on two C-S-H sites in the proposed model: $\equiv SiOH$ and $\equiv SiOCa^+$. Chloride ions can also react with monosulfoaluminate to form Kuzel's salts. The numericla results of sorption of chloride ions is shown on Figures 2a, b, c, d for concrete specimens exposed to NaCl, $CaCl_2$, KCl and $MgCl_2$ solutions during six months, respectively.

The results show that the chloride quantity which reacts with C-S-H is always greater than the quantity which reacts to form Kuzel's salts. They also show that Kuzel's salts quantity is the same whatever the boundary solution type, except for the highest chloride concentration when concrete is exposed to a $MgCl_2$

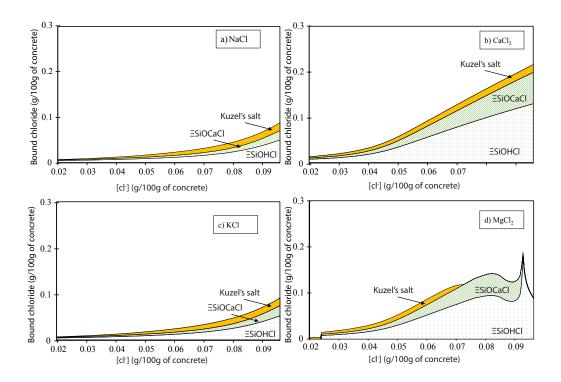


Figure 2: Chloride binding isotherm for CEM II concrete after a 6-month exposure to chloride sorption on C-S-H surface and chloride binding for a) $0.5 \ mol.L^{-1} \ NaCl$, b) $0.25 \ mol.L^{-1} \ CaCl_2$, c) $0.5 \ mol.L^{-1} \ KCl$ and d) $0.5 \ mol.L^{-1} \ MgCl_2$ solutions at 20° C, respectively. Contribution of Kuzel's salt formation and chloride sorption on C-S-H sites ($\equiv SiOHCl^{-}$, $\equiv SiOCaCl$)

solution. This latter case is discussed in Section 5.3.

56 5.2. Role of cation associated with chloride and pH

According to the chemical equations presented in Table 3, the reactions of the chloride ions bound on C-S-H to form $\equiv SiOHCaCl$ or $\equiv SiOHCl-$ are related directly or indirectly to pH. In the first case, the fixation of Cl^- and Ca^{2+} releases H^+ . In the second case, Cl^- , Ca^{2+} and OH^- are competing in order to react with $\equiv SiOH$. The reactions with Ca^{2+} and OH^- release H^+ .

Figures 3a, b, c, d show Na^+ , K^+ , Ca^{2+} concentration and pH profiles as a function of the free chloride concentration after a 6-month exposure, respectively. As expected, Na^+ , K^+ and Ca^{2+} have the highest concentrations within the concrete pore solutions exposed to NaCl, KCl and $CaCl_2$, respectively. Regarding the other ions that are not present in the boundary solutions, the profiles are equivalent whatever the exposed solution, except Ca^{2+} in the concrete specimens exposed to the $MgCl_2$ solution (cf. Figure 3c). The role of $MgCl_2$ is discussed in Section 5.3.

These results reveal that the boundary solution types causing a large amount of Ca^{2+} in the concrete pore solutions ($CaCl_2$ and $MgCl_2$) also lead to a greater amount of bound chloride on C-S-H through the formation of $\equiv SiOCaCl$ (cf. Figures 3c and 2). According to Le Chatelier's principle, a higher Ca^{2+} amount increases the number of $\equiv SiOCa^{+}$ and, consequently, leads to an increased positive and to a higher chloride ion amount bound on this surface charge. This is consistent with Wowra et al.'s proposal (15).

Figure 3d shows that the pore solution pH of the concrete specimens exposed to $CaCl_2$ and $MgCl_2$ solutions is lower than in the NaCl and KCl

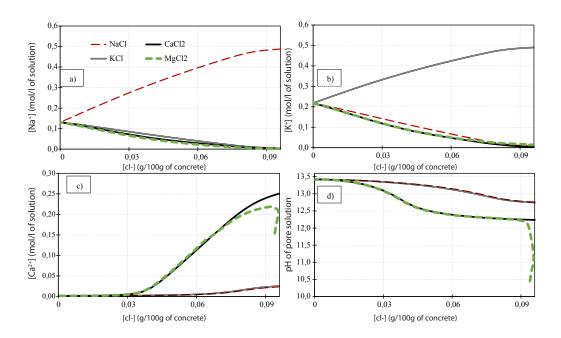


Figure 3: Concentration profile of CEM II concrete after six months of exposure to NaCl, $CaCl_2$, KCl and $MgCl_2$ solution at 20°C respectively: a) Na^+ , b) K^+ , c) Ca^{2+} and d) pH.

solutions. This observation implies that the amount of chloride ion reating with C-S-H to form $\equiv SiOHCl^-$ is larger for $CaCl_2$ and $MgCl_2$ solutions than for NaCl and KCl solutions (cf. Figure 2). This proves that the pH-chloride binding capability relationship experimentally observed in (7; 8) is verified by the model. Indeed, the higher the OH^- concentration (higher pH) in pore solution is, the larger the number of $\equiv SiOH$ transformed into $\equiv SiO^-$ according to Le Chatelier's principle. Then, the amount of $\equiv SiOH$ decreases and chloride binding capability on C-S-H decreases. This confirms OH^- and Cl^- competing for sorption on C-S-H.

In conclusion, the pore solution pH value directly affects chloride binding capability. It depends on the solid/pore solution equilibrium like portlandite dissolution/precipitation and Na^+ and K^+ concentrations. In all the cases studied, the Portlandite dissolution is numerically observed (cf. Figure 4). This is less pronounced for concrete exposed to the $CaCl_2$ solution because of higher Ca^{2+} concentrations. Nevertheless, the pH value is smaller. It may seem paradoxical considering the fact that the stronger the Portlandite dissolution, the higher the pH, but, because Na^+ and K^+ are stronger bases in the acid-base theory than Ca^{2+} and Mg^{2+} , the pore solution pH of the concrete exposed to NaCl and KCl solutions is higher than with the $CaCl_2$ and $MgCl_2$ solutions.

300 5.3. Role of magnesium

Figure 1 shows that the chloride binding isotherm with the $MgCl_2$ solution behaves differently from the other solutions. With the $MgCl_2$ solution, a peak correspond with chloride binding capability appears for a chloride concentration slightly lower than the maximal value, i.e. within the concrete. In

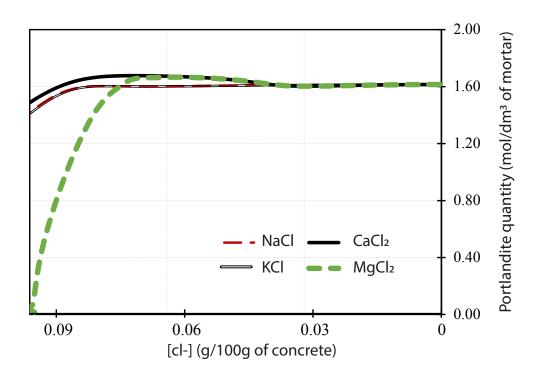


Figure 4: Portlandite amount as a function of depth for concrete specimens exposed to $NaCl, KCl, CaCl_2$ and $MgCl_2$ solutions after a 6-month exposure, respectively.

the meantime, the chloride binding capability is maximum on the concrete surface exposed to NaCl, KCl and $CaCl_2$ solutions.

The previous section demonstrates the relationship between chloride bind-307 ing capability and Ca^{2+} concentration and pH value, whereas Figure 2c shows that the Ca^{2+} concentration in concrete decreases gradually from the exposed surface towards the interior after a 6-month exposure. Moreover, the pore 310 solution pH on the surface with $MgCl_2$ exposure is the lowest of the four 311 solutions (cf. Figure 2d). An increased Mg^{2+} concentration in the exposed 312 solution indeed disturbs portlandite equilibrium and leads to the precipita-313 tion of brucite (cf. Figure 5). C-S-H (jennite and tobermorite) is also dis-314 solved and release $HSiO_3^-$, which reacts with Mg^{2+} to precipitate chrysotile. 315 The numerical observation of brucite and M-S-H (chrysotile) formation is 316 experimentally verified (47; 48; 49). C-S-H and portlandite dissolution also release a large amount of Ca^{2+} into the pore solutions. The complete dissolution of Portlandite strongly affects the pH buffering system. Consequently, with such low pH close to the exposed surface, chloride binding capability increases. However, the C-S-H dissolution causes a decrease in the number of surface charges $\equiv SiOHCl^{-}$, which reduces the ions binding capability of C-S-H on the exposed surfaces.

Furthermore, Mg^{2+} , which progresses within the concrete reacts with Al^{+3} coming from the monosulfoaluminate dissolution and precipitates hydrotalcite. As a result, the Al^{+3} concentration is no longer sufficient to precipitate Kuzel's salt despite the high chloride concentration or ettringite found just below the exposed surface. After a period of increase in the hydrotalcite amount, a small amount of ettringite and Kuzel's salt appears (cf.

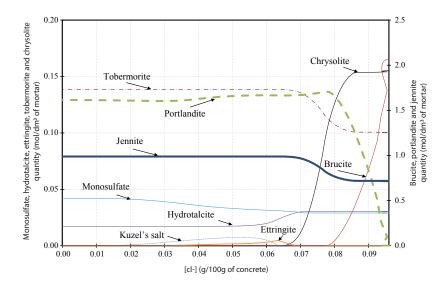


Figure 5: Mineral amount of CEM II concrete after six months of exposure in $MgCl_2$ solution at 20° C.

Figure 5). Hydrotalcite, ettringite and Kuzel's salt precipitation may be in competition with each other with high magnesium concentration.

For concrete specimens exposed to a $MgCl_2$ solution, Ca^{2+} leaching reduces the pH value and, in turn, chloride binding on $\equiv SiOH$ increases. This can be considered the most significant impact of the Mg^{2+} cation on chloride binding capability.

336 5.4. Role of sulfate

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Figure 6 displays the comparison between the chloride binding isotherms within concrete specimens exposed to 0.5 M of $MgCl_2$ solutions containing 0, 0.0276 M of $MgSO_4$ and 0.2760 M of $MgSO_4$, respectively. The chloride binding capability is different depending on the concentration in the solution. In other words, the numerical results show that the higher SO_4^{-2} the

concentration, the weaker the chloride binding capability.

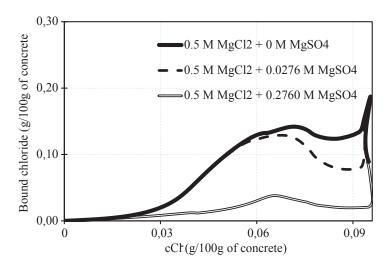


Figure 6: Chloride binding capability after six months of exposure in 0.5 M $MgCl_2$, 0.5 M $MgCl_2$ + 0.0276 M $MgSO_4$ and 0.5 M $MgCl_2$ + 0.2760 M $MgSO_4$ solution at 20°C, respectively.

This can be explained by the fact that the higher the $MgSO_4$ amount, 343 the lower the pH value (cf. Figure 7a). A comparison between the results obtained with concrete specimens exposed to $MgCl_2$ solutions without $MgSO_4$ and with 0.276 M of $MgSO_4$ shows this clearly. Another explanation is the 346 number of chloride ions that can be adsorbed on C-S-H, which decreases 347 as the amount of $MgSO_4$ increases, under all surface charge conditions: 348 $\equiv SiOHCl^-$ or $\equiv SiOCaCl$ (cf. Figures 7b and c). The same tendency is also observed as regards Kuzel's salt formation (cf. Figure 7d). 350 However, Figure 8 shows that a large amount of sulfate is absorbed on the 351 surface charge $\equiv SiOH$. Thus, a more negative surface charge $\equiv SiOCaSO_4^-$ 352 for the 0.5 M $MgCl_2$ + 0.2760 M $MgSO_4$ solution is released than the 0.5 353 M $MgCl_2$ solution and the 0.5 M $MgCl_2$ + 0.0276 M $MgSO_4$ solution. In

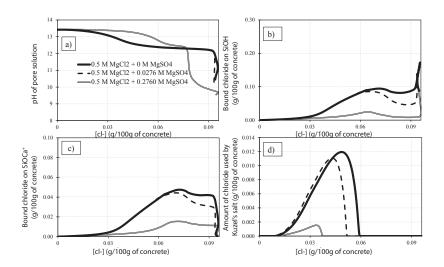


Figure 7: a) Pore solution pH and chloride binding on b) $\equiv SiOH$, c) $\equiv SiOCa^+$, d) Kuzel's salt formation after six months of exposure in 0.5 M $MgCl_2$, 0.5 M $MgCl_2$ + 0.0276 M MgSO4 and 0.5 M $MgCl_2$ + 0.2760 M MgSO4 solutions at 20°C, respectively.

addition, Cl^- and SO_4^{2-} start competing for sorption with Ca^{2+} on $\equiv SiOH$.

Because of the charge balance condition and the competition between chloride and sulfate, the number of negative surface charges $\equiv SiOHCl^-$ must
decrease. This can only happen if the chloride binding capability decreases
when the solution contains a significant amount of SO_4^{2-} .

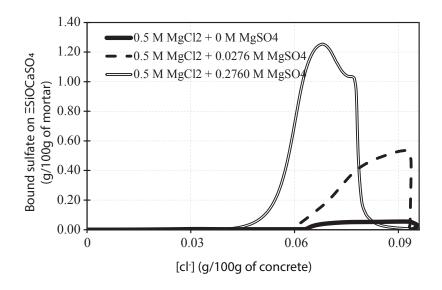


Figure 8: Sulphate binding on $\equiv SiOCaSO_4^-$

Chloride binding due to Kuzel's salt formation (cf. Figure 7d) is weakest when SO_4^{2-} concentration is highest. Ettringite formation then occurs at the expense of Kuzel's salt formation as shown in Figure 9. Results are different with the boundary solution without SO_4^{2-} . In contrast, the remaining mineral behaviors are similar. Consequently, for the 0.5 M $MgCl_2 + 0.2760$ M MgSO4 solution, Ca^{2+} leaching is not responsible for the low pH. The pH decrease is essentially due to the presence of SO_4^{2-} and to the adsorption reactions on C-S-H.

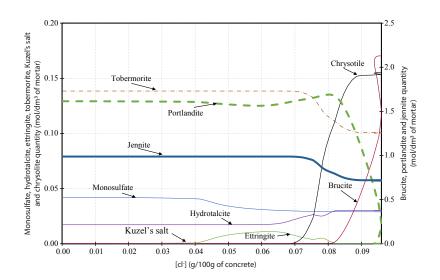


Figure 9: Mineral amount of CEM II concrete after six months of exposure in a 0.5 M $MgCl_2$ + 0.2760 M MgSO4 solution at 20°C.

6. Conclusion

In this paper a physically and chemically based multiionic model considering thermodynamical reaction kinetics and surface complexation is proposed to investigate chloride binding capability of CEM II concrete exposed to different boundary chloride solutions. Some chloride binding isotherms from the literature are compared with the numerical results for concrete exposed to NaCl, KCl, $CaCl_2$, $MgCl_2$. The presence of sulfate ions in the $MgCl_2$ boundary solution with two different concentrations is also studied.

The results underline the influence of the cation type associated to the chloride boundary solution on the chloride binding capability. As observed in the literature, the chloride binding capability decreases in the order: $Ca^{2+} > Mg^{2+} > Na^+ \approx K^+$. In addition,

the numerical results show that the highest quantity of chloride that reacts is obtained by the sorption on $\equiv SiOH$, followed by the sorption on $\equiv SiOCa^{+}$. The chloride ions quantity that reacts to form Kuzel's salts is the smallest one. This latter numerical observation is true whatever the chloride salt solution and the type of cation associated with chloride. As regards the chloride salt so-386 lution without sulfate, the competition between H^+ (or indirectly 387 pH) and Cl^- onto $\equiv SiOH$ presents the most significant effect on chloride binding capability. Indeed, the higher the pH is, the lower the chloride quantity is adsorbed on C-S-H. These conclusions also 390 confirm the relationship between pH and chloride binding capabil-391 ity observed experimentally in the literature. 392

This study also shows that the leaching of Na^+ and K^+ for the concrete exposed to a $CaCl_2$ solution and the leaching of Na^+ , K^+ and Ca^{2+} for the concrete exposed to a $MgCl_2$ solution cause a local pH decrease and, thus, an increase in chloride binding capability. Regarding the $MgCl_2$ solution, the formation of hydrotalcite is enhanced and limits Kuzel's salt precipitation. The higher the Ca^{2+} concentration is, the higher the chloride amount absorbed on $\equiv SiOCa^+$.

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Finally, the model is able to catch that when some sulfate ions are present in the chloride solution, they reduce chloride binding capability because of the sulfate absorption process on C-S-H. A more negatively charged surface $\equiv SiOCaSO_4^-$ and competition between Cl^- and SO_4^{2-} replace $\equiv SiOH$ in the presence of Ca^{2+} in the solution. This reaction releases H^+ and decreases the pH.

These first results have to be confirmed with more experimental
data on several concretes and for other ionic species than chlorides
although data is missing in the literature. In addition, on the basis of
the above study, it could be interesting to explore these findings and study
chloride binding capability of concrete exposed to seawater, in which different
cations and sulfate ions are present simultaneously.

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