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# Morphogenesis of surfaces with planar lines of curvature and application to architectural design

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## Abstract

This article presents a methodology to generate surfaces with planar lines of curvature from two or three curves and tailored for architectural design. Meshing with planar quadrilateral facets and optimal offset properties for the structural layout are guaranteed. The methodology relies on the invariance of circular meshes by spherical inversion and discrete Combescure transformations, and uses parametrisation of surfaces with cyclidic patches. The shapes resulting from our methodology are called *super-canal surfaces* by the authors, as they are an extension of canal surfaces. An interesting connection to shell theory is recalled, as the shapes proposed in this paper are at equilibrium under uniform normal loading. Some applications of these shapes to architecture are shown.

*Keywords:* super-canal surface, fabrication-aware design, cyclidic net, architectural geometry, structural morphogenesis, façade

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## 1. Introduction

### 1.1. Constructive geometry in architecture

The construction of architectural shapes is subject to technological constraints that highly impact the economy of the cladding and structure. The study that aims at expressing technological requirements as geometrical constraints is often referred to as *fabrication-aware design* in the computer science community, whereas architects or engineers speak of *shape rationalization* or *constructive geometry*. This topic, takes root in the eighteenth century and stereotomy, and the work of Gaspard Monge[1].

In glass or metal envelopes, the planarity of the panels is regarded as one of the most significant aspect in the design of technologically-feasible solutions, and motivated the creation of tailor-made morphogenesis strategies by engineering office Schlaich Bergermann und Partner [2] and

later by Gehry Technologies [3]. Triangular meshes are always covered with planar facets, but their high node valence makes the fabrication of the structure complicated [4]. They are also considered less transparent than quadrilateral layouts [3]. Developable panels are also of interest because cold-bending technologies for glass can be used at a reasonable cost, as illustrated by some projects of engineering office RFR [5, 6].

The geometry of the supporting structure is another indicator of the complexity of fabrication in free-form architecture. The most economical solution is to build with planar beams that meet exactly along axes. This topic is well-known by gridshell builders [7] and is covered from a mathematical perspective in [8], with a tool called '*mesh parallelism*'. Building a support structure with planar beams implies indeed the existence of a mesh which has all its edges parallel to the initial mesh.

These two construction constraints (planarity of panels

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35 and planarity of beams) can be integrated in the design 72  
 36 of free-form architecture, either in top-down [4, 6, 9] or  
 37 in bottom-up approaches [10, 11, 12, 13, 14]. The latter  
 38 approaches generate design spaces where the fabrication  
 39 requirements are fulfilled. They offer thus the possibility  
 40 to integrate constraints of a different nature early in the  
 41 design process, like structural behaviour or energy con-  
 42 sumption. This is particularly important in the context of  
 43 architectural design: fabrication is only one of the many  
 44 criteria that should be rationalised or optimised in a build-  
 45 ing envelope.

### 46 1.2. Geometrically-constrained shape generation

47 A natural way to deal with construction constraints is  
 48 to generate a design-space of shapes that satisfy the most  
 49 critical fabrication-constraints. This approach, known as  
 50 "geometrically-constrained design strategy" [15] has been  
 51 used extensively in the history of architecture. Methods  
 52 that guarantee planar quads include surfaces of revolution,  
 53 surfaces of translation [2], scale-trans surfaces [3], mould-  
 54 ing and Monge surfaces [16, 17, 18]. These surfaces can be  
 55 generated using two curves and a rule of transformation,  
 56 either translation or sweeping along Bishop's frame. The  
 57 designer controls the overall shape and its discretisation  
 58 simultaneously, which makes all these shapes easily un-  
 59 derstandable and usable [19]. Accordingly, geometrically-  
 60 constrained approaches using two curves like surfaces of  
 61 translation are very popular in the community of struc-  
 62 tural engineers [20].

63 Table 1 shows the correspondance between shape gen-  
 64 eration techniques using two or three curves and their  
 65 fabrication-aware counterpart. For example extrusion  
 66 along a curve that yields surfaces of translation and sur-  
 67 faces of revolution are good examples of fabrication-aware  
 68 shapes. Monge surfaces, that can be generated by sweep-  
 69 ing a planar curve called generatrix along a rail curve,  
 70 are also very interesting for architectural shape design. It  
 71 can be noticed that the *sweep 2 rails* command has no

fabrication-aware equivalent.

CAD generation process	Fabrication-aware shape
Extrusion along curve	Surface of translation
Revolve	Surface of revolution
Rail Revolve	Scale-trans surface
Sweep 1 rail	Monge surface* Isoradial mesh
Sweep 2 rails	-

Table 1: Kinematic method to generate free-form surfaces and their fabrication-aware equivalent, surfaces marked with asterisks are subject to additional constraints.

The objective of this work is thus to enrich the design space accessible with geometrically-constrained design strategies by proposing new shapes constructed from two and three curves. The shapes can be generated in real-time on standard computers, which eases the exploration of this design space.

The second section of this paper discusses thus the general methodology that generates super-canal surfaces, a new family of shapes for fabrication-aware design in architecture, as well as a new algorithm for the fast computation of parallel meshes. Applying the results of [21], we also show that super-canal surfaces are remarkable with respect to shell theory: their lines of curvatures are lines of principal stress under uniform normal loading. This work thus meets fabrication with equilibrium, two major aspects of architectural design. A new method for the generation of canal surfaces from two contour curves is presented in Section 4. The fifth Section introduces some inverse problems solved in with super-canal surface. A brief discussion and conclusion sum up the contributions of the present article.

## 94 2. Methodology

### 95 2.1. Möbius geometry and cyclidic nets

96 The present methodology for shape generation relies  
97 on a more general framework proposed recently for archi-  
98 tectural design [22] in the following of previous work de-  
99 veloped in [23, 24, 25, 26]. The main concept is to link  
100 discrete objects, namely circular meshes, with a smooth  
101 underlying surface. All the shapes are thus described as  
102 coarse circular meshes, which support portions of Dupin’s  
103 cyclides. Among remarkable features of cyclides, one may  
104 mention that their lines of curvature are circles and that  
105 a patch delimited by four lines of curvature on a Dupin  
106 cyclide has its four vertices inscribed within a circle. The  
107 formal potential of this framework is shown in [26], where  
108 various fitting problems on complex shapes are solved.

109 Cyclidic nets provide thus a natural way to cover com-  
110 plex shapes with circular quadrilateral meshes. Moreover,  
111 as transformations mapping circular quadrilaterals to cir-  
112 cular quadrilaterals also preserve cyclidic nets and the un-  
113 derlying parametrisation, such transformations are of par-  
114 ticular interest. Two of those will be studied in the follow-  
115 ing: Möbius transformations in Section 2.3 and Combes-  
116 cure transformations in Section 2.4. Starting from surfaces  
117 easily described with cyclidic nets, the application of these  
118 transformations creates new shapes for fabrication-aware  
119 design in architecture.

### 120 2.2. Geometrical properties of canal surface

121 Canal surfaces are a fundamental family of surfaces in  
122 the context of Möbius geometry, as this family is indeed  
123 invariant by Möbius transformations. Canal surfaces are  
124 defined as envelopes of spheres. They are commonly used  
125 as blending surfaces, either by using contour curves [27] or  
126 by joining spheres that can be manipulated by the designer  
127 [28].

128 Alternatively, canal surfaces can be defined as surfaces  
129 such that lines of curvatures are circles. The invariance of  
130 canal surfaces under Möbius transformations is obvious,

131 because inversions preserve lines of curvatures and circles.  
132 Another way to look at it is that Möbius transformations  
133 preserve both spheres and angles, therefore an envelope of  
134 spheres is preserved by inversions. Notice that the shape-  
135 generation of canal surfaces with Dupin cyclides has been  
136 studied in [29]. We use an optimisation approach intro-  
137 duced in [26] to obtain shapes with smooth parametrisa-  
138 tions.



Figure 1: Canal surface as an envelope of spheres whose centers are on a curve.

139 These surfaces are very easily parameterised by cyclidic  
140 patches, as Dupin cyclides are particular cases of canal  
141 surfaces. The  $C^1$  continuity and generalisation to  $C^0$  con-  
142 tinuity is insured by reflections according to the method  
143 described in [25].

### 144 2.3. Möbius transformations

145 The transformation at the core of the framework using  
146 cyclidic nets is the Möbius transformation or *inversion*,  
147 which is a very simple non-linear map. We recall here some  
148 of its elementary properties, and introduce the notations  
149 used in the following of this paper.

Möbius transformations preserve locally angles, and  
are thus conformal maps. They also preserves circles.  
Möbius transformations are compositions of translation,



scaling and spherical inversions. The latter transformation is defined by a center and a ratio. Consider a point  $\mathbf{C}$ , later called center of inversion, and a real number  $k$ . The inversion of center  $\mathbf{C}$  and ratio  $k$  applied to a point  $\mathbf{M}$  is a point  $\mathbf{M}'$  defined by the well-known equation:

$$\mathbf{CM}' = \frac{k}{\|\mathbf{CM}\|^2} \cdot \mathbf{CM} \quad (1)$$

In the complex plane, the inversion of ratio  $k$  with center  $\mathbf{C}$  (complex number  $z_C$ ) reads as:

$$f_{k,\mathbf{C}}(z) = z_C + \frac{k}{\bar{z} - \bar{z}_C} \quad (2)$$

An elementary property of inversions is that they are involutions, which means that Möbius transformations are their own inverse transformations. This property is used in many applications shown in this paper (see Section 4).

It can finally be noticed that the ratio  $k$  is nothing more than a scaling factor. The position of the point  $\mathbf{C}$  is the parameter that has a true impact on the shape deformation.

#### 2.4. Combescure transformations

It has just been seen that Möbius transformations allow to modify the overall appearance of circular meshes by preserving the circumcircles of all quads. Another transformation that has the same property is the mesh parallelism transformation. Two meshes are said *parallels* if they have the same connectivity and if all their edges are parallel. The transformation mapping one mesh to the other is called a *Combescure transformation* [8]. By definition, Combescure transformations preserve discrete angles. Therefore they map circular meshes to circular meshes. Combined with Möbius transformations, they offer a range of possibilities to deform circular meshes.

Two meshes related by a Combescure transformation, with respective edges ( $\mathbf{e}_i$ ) and ( $\mathbf{e}'_i$ ), have to satisfy a linear equation:

$$\forall i, \mathbf{e}_i \wedge \mathbf{e}'_i = \mathbf{0} \quad (3)$$

Solutions for this equation are usually found using Singular Value Decomposition (SVD) [8]. We introduce here a different original approach, restricted to quadrilateral meshes, but that offers a better performance than SVD. This technique takes inspiration from the one employed in [14], which is applied to the form-finding of planar quadrilaterals meshes.

#### 2.5. Efficient computation of Combescure transformations

Let us consider two parallel quadrilaterals, like the ones shown in Figure 2. Up to a translation, prescribing the lengths of two sides  $l_0$  and  $l_3$  (thick lines on the figure) is sufficient to determine a unique quadrilateral with internal angles  $\alpha, \beta, \gamma, \delta$ . The last point  $C$  (white dot on the figure) is found by intersecting two lines (dashed lines on the figure). For the sake of simplicity, we consider planar quadrilaterals in the reference plane ( $ABD$ ): the equations are written in a frame centred in  $A$  and represented by the blue arrows in the figure. The intersection is found by solving the following equation:

$$\begin{pmatrix} l_0 + l_3 \cos \alpha \\ l_3 \sin \alpha \end{pmatrix} = \begin{pmatrix} \cos \beta & \cos(\alpha - \delta) \\ -\sin \beta & \sin(\alpha - \delta) \end{pmatrix} \cdot \begin{pmatrix} l_1 \\ l_2 \end{pmatrix} \quad (4)$$

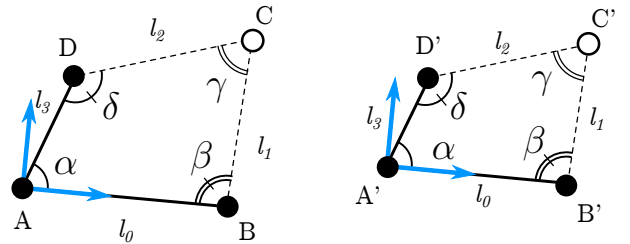


Figure 2: Two quads related by a Combescure transformation.

In the same way, prescribing the lengths of all edges on two intersecting lines, as shown in Figure 3 is sufficient to determine the entire parallel mesh. In this image, the thick lines correspond to edges which have prescribed lengths. Starting from a quadrilateral with two prescribed lengths, it is possible to apply equation (4) and find the last point of the quadrilateral (white dot). It is then possible to apply

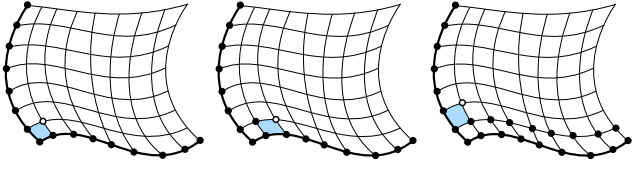


Figure 3: Propagation method for the computation of a Combescure transformation with quadrangles.

this procedure to the next quadrangle in the same row, and so forth, up to completion of each strip.

This iterative procedure is computationally efficient. The number of operations and the use of memory is proportional to the number of faces in the mesh, as the solution of the propagation requires  $NM$  applications of equation (4) for a mesh of  $N$  times  $M$  facets. The computation time also varies linearly with the number of faces, as discussed in [14]. This technique is thus more efficient than SVD, which requires assembling of matrices. The computational gain is especially important for large meshes and makes the method proposed in this paper suited for real-time applications.

### 2.6. Super-canal surface

We call *super-canal surfaces* the surfaces that are images of canal surfaces by arbitrary compositions of Combescure transformations and Möbius transformations. This name recalls the term *supercyclide* to name projective transforms of Dupin cyclides by Pratt [30]. We choose to use the same prefix even if the transformations at stake in this paper are different from the ones studied by Pratt.

The image of a circular quad-mesh by Combescure transformations and inversions remains a circular quad-mesh, but both transformations affect differently the overall shape, creating interesting formal possibilities. The two operations do not commute, so specifying the order of application of Combescure and Möbius transformation has an influence on the properties of the final shape.

Hence, the methodology proposed in the following is to reconstruct a super-canal surface from two curves assuming a composition of applications of inversions or Combescure

transforms. Rather than playing with canal surfaces and transformations, the principle of the method relies on a reverse approach which aims at finding an initially unknown canal surface that would satisfy two prescribed boundaries (see Section 5.1).

## 3. Super-canal surfaces

### 3.1. A general framework for shape generation

The method exposed above translates into a simple framework that requires two perpendicular curves as input. Indeed, canal surfaces do not have umbilical points (except poles), and consequently, their lines of curvature are necessary perpendicular. The designer thus chose a rule of construction for the surface, i.e. a specific combination of Combescure and Möbius transformations. The concatenation of transformations provides more design freedom to the end-user than the utilization of one specific transformation: this is discussed in the next sections. The identified families are proposed in Figure 4. The nomenclature for the different surfaces follows:

- the letter  $C$  denotes that the initial shape was subjected to a Combescure transformation;
- the letter  $M$  denotes that the initial shape was subjected to a Möbius transformation;
- the order of the letters gives the order of composition of the transformations:  $CM$  means that the initial shape was subject to a Möbius transformation, then a Combescure transformation;
- the name of the initial shape subject to the transformations stands at the end: for example a  $M$ -revolution surface is an inversion of a surface of revolution.

Many surfaces well-identified in the literature can be generated with this method as illustrated in Figure 4. All the common surfaces used for geometrically-constrained

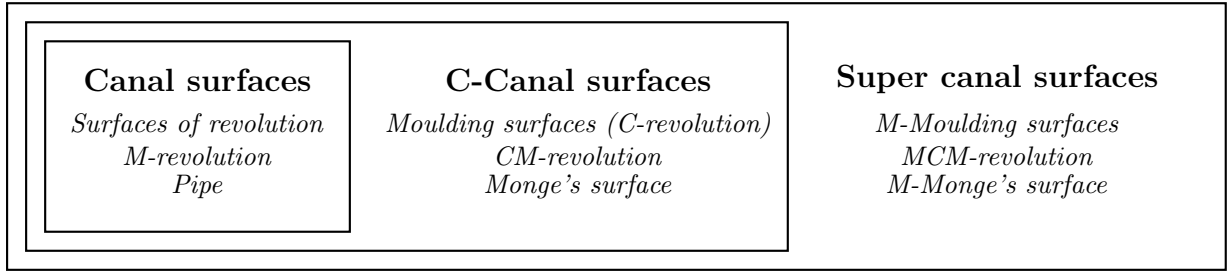


Figure 4: Super canal surfaces

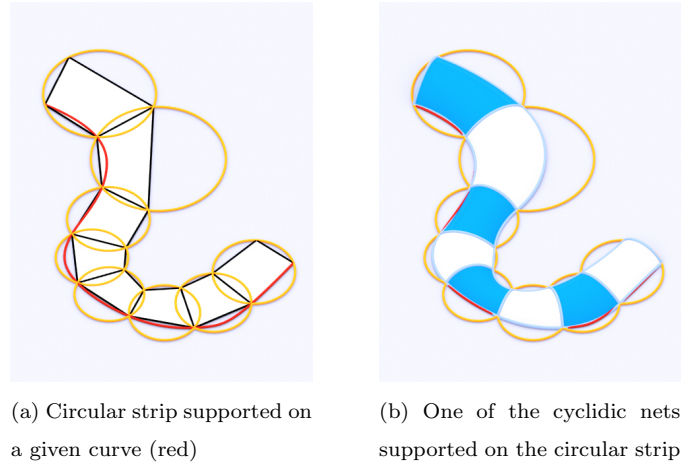
254 methods mentioned in Section 1.2 fall into the category 281  
 255 of super-canal surfaces, with the exception of scale-trans  
 256 surfaces. The curves used in surfaces of translation and  
 257 scale-trans surfaces do not correspond in general to lines of  
 258 curvatures and cannot be approached by circular meshes.  
 259 Therefore, they do not have any specific offset properties.

260 It appears that moulding surfaces and Monge sur-  
 261 faces discussed in [17] are a subset of the shapes gener-  
 262 ated by Combescure transformations of canal surfaces.  
 263 From a practical point of view, shapes with a family of  
 264 planar curves are of great interest in construction. For  
 265 that reason, we restrict the examples of application to  
 266 *CM*-surfaces, where the families of circles are trans-  
 267 formed into planar curves.

### 282 3.2. Input for design with super-canal surfaces 283

269 In the following of [3], we propose to design super-canal 284  
 270 surfaces from two curves. The simplest way to parame- 285  
 271 terise a canal surface is to take a strip of circles as input 286  
 272 parameters, as pictured in Figure 5. A two parameters 287  
 273 family of cyclidic nets can be supported on the circular 288  
 274 mesh: the choice of those parameters can be done to fulfill 289  
 275 some design requirements, like the shape smoothness, eval- 290  
 276 uated with conformal Willmore energy [31, 22]. In the ex- 291  
 277 ample of Figure 5, eight circles in the same plane are used 292  
 278 to generate a canal surface. Only the portion of the canal 293  
 279 surface above the construction plane is shown. Note also 294  
 280 that the resulting surface, made of cyclidic patches, is a 295

$C^1$  surface with curvature discontinuities between patches.



(a) Circular strip supported on a given curve (red)

(b) One of the cyclidic nets supported on the circular strip

Figure 5: A canal surface created from a coarse circular strip

282 To define the strip of circles, the user can draw manu-  
 283 ally a collection of circles, or entirely parametrised it by a  
 boundary curve and the radii of circles or a target length  
 for each border. The latter parametrisation is depicted in  
 Figure 6, whose input data follows:

1. a list of points on a curve in space;
2. one point  $\mathbf{P}$  in space defining the first circle;
3. a function describing the lengths of each edge cross-  
ing the strip (thick orange lines on Figure 6).

It is then possible to construct one unique circular strip  
 passing through the input points by propagation, in the  
 manner of [32]. The construction of a circular strip re-  
 stricts the two boundaries to be lines of curvature of the  
 resulting surface. Section 4.1 will show how this condition

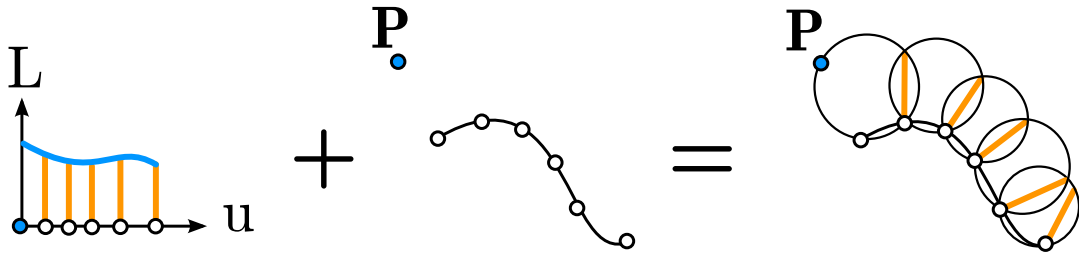


Figure 6: Parameters creating a circular strip that can support a canal surface

296 can be relaxed, while keeping the parametrisation of the 309  
 297 shapes by cyclidic nets and circular strips.

### 298 3.3. Shape smoothing

Some input data might lead to visually unpleasent results, therefore we use the strategy proposed in [26] and take the position of the vertices and the orientation of the normal vector to the cyclidic net at one node as variables for smoothness optimisation. The objective is to fit exactly one input curve. To this end, the points on this curves are parametrised by the vector  $\mathbf{u}$ . The other parameters governing the shape of the canal surface are the lengths of the edges crossing the circular strip  $\mathbf{L}$  (see Figure 6). The cyclidic net is then generated by the choice of an orthog-  
 312 onal frame, parametrised by two angles  $\lambda$  and  $\theta$ , which  
 313 are angles defining a spherical coordinate system. The  
 314 smoothness functional  $\mathcal{F}$  is finally defined as a quadratic  
 315 function of the radii of the edges of the cyclidic net  $R_{edge}$ :  
 316

$$\mathcal{F}(\mathbf{u}, \mathbf{L}, \lambda, \theta) = \sum_{\text{edges}} \frac{1}{R_{edge}^2(\mathbf{u}, \mathbf{L}, \lambda, \theta)} \quad (5)_{317}$$

299 The computation of the function is not hard, and its min-  
 300 imisation gives satisfying results and is done in real-time.  
 301 The user can specify additional constraints, like the angle  
 302 made by the normal and a reference plane. In the latter<sup>321</sup>  
 303 case, the degrees of freedom  $\lambda$  and  $\theta$  become coupled, and<sup>322</sup>  
 304 the normal rotates along a cone.<sup>323</sup>

305 Practically, the minimisation is here done by the means<sup>324</sup>  
 306 of the Broyden-Fletcher-Goldfarb-Shanno (BFGS) algo-<sup>325</sup>  
 307 rithm. Figure 7 shows the smoothing of a canal surface<sup>326</sup>  
 308 based on the proposed energy. The parameters are the

circle radii. Note that only local changes are introduced  
 310 after optimisation, and that the areas where the facets  
 311 were degenerated have disappeared.

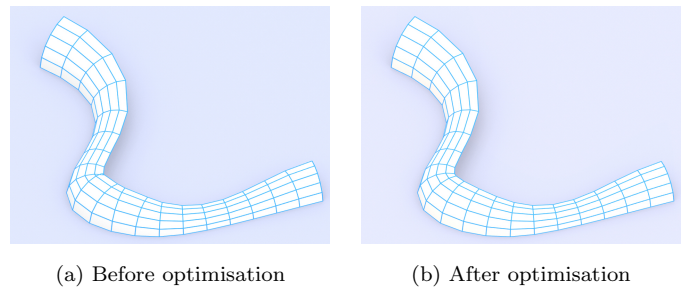


Figure 7: Optimisation of the smoothness of a canal surface.

### 3.4. Mechanical properties of super-canal surfaces

This Section discusses briefly the mechanical behaviour of super-canal surfaces. C-canal surfaces play indeed a particular role in shell theory, as Rogers and Schief proved that their lines of curvatures are also lines of principal stresses under a uniform external load [21]. This result was also proven for canal surfaces before in [33].

This induces two remarkable features for the behaviour of the shapes previously presented:

- principal stresses lines following principal curvature lines, the natural mesh of C-canal surfaces is an optimal mechanical layout for a grid structure;
- all closed shapes generated by this method are in equilibrium under uniform pressure and therefore suited for pneumatic structures.

Before showing the shape generation framework, we should make a comment on potential applications for shallow roof structures. A normal pressure load is surely very close to a uniform distributed load for surfaces with moderate curvature. It can be concluded that shallow canal surfaces are close to funicular shapes under uniformly distributed load. This kind of consideration has been documented for shallow arches: shallow circular arcs, parabolic or catenary have similar geometry and mechanical behaviour, especially buckling capacity. For more comments on this topic, the reader can refer to [34].

Furthermore, it should be recalled that in practice temporary actions are not negligible compared to the self-weight of a structure, and gridshells or thin shells are often designed with respect to non-symmetrical loads, for which lines of curvature are not principal stress lines. The finding of a structural optimum for different load case combinations is far from obvious, but its computation is not necessarily a practical design objective: just like fabrication, structural performance is not the only criterion taken into account by the architects and engineers. The integration of principal stress under self-weight can be seen as a simple way to generate a good, but not necessarily optimal structural pattern, while creating a rich design narrative referring to pioneering works of structural artists. Lines of principal stress have been used by Pier Luigi Nervi for the design of concrete ribbed slabs. Nervi did not solve an optimisation problem, but used a simple guiding principle for his design, which resulted indeed in highly efficient structures. The meshing of super-canal surfaces by their lines of curvatures combines thus constructability with structural efficiency.

## 4. Application to shape modelling

### 4.1. Generation of canal surfaces

The previous section discussed how canal surfaces can be parametrised with circular strips supporting cyclidic

nets. This generation method leads however to a strong formal restriction, as it forces the two boundaries of the strip to be lines of curvature of the resulting canal surface. The practical consequence is that the second curve is restricted to be on a developable surface passing through the first curve, whereas the designer would prefer to define it independently. This section introduces thus an original algorithm for the shape generation of canal surfaces from two curves where only one of the two curves is a line of curvature of the canal surface. The problem is illustrated in Figure 8 and it will be shown that it admits a one parameter family of solutions.

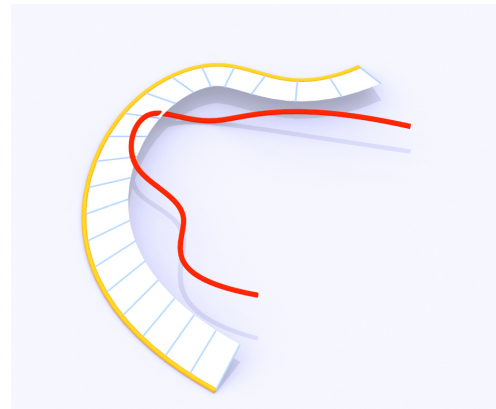


Figure 8: Input data for the curve-fitting problem. Line of curvature (orange), line to fit (red), and surface (white) containing the centers of the spheres.

### Preliminary considerations

The relevant definition of canal surfaces in this case is to consider them as the envelope of a family of spheres. Remarkable properties of canal surfaces, and of lines of curvature in general can be mentioned:

1. Canal surfaces are envelopes of spheres, and as such, the spheres generating the surface meet tangentially with any curve of a canal surface.
2. The envelope of the lines directed by the normal of the surface along a line of curvature is a developable surface.

From remark 1, we get that the locus of the centers of the spheres generating the canal surface is on the surface



388 generated by the normals of the surface. From remark  
 389 2, we get immediately that this is a developable surface.  
 390 Actually, it is a specific case of Monge surface [17]: once  
 391 one normal has been chosen, the other normals are de-  
 392 termined uniquely so that the envelope is indeed a devel-  
 393 opable surface. The locus of the centres of the spheres is  
 394 therefore controlled by one orientation parameter. This  
 395 is illustrated in Figure 9: choosing the orientation of the  
 396 normal is equivalent to choosing a surface tangent to the  
 resulting canal surface.

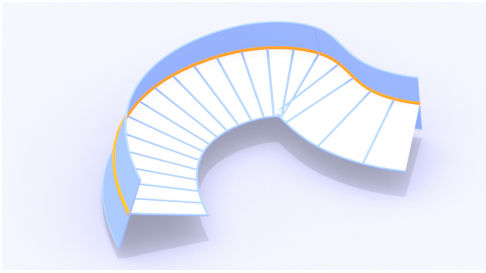


Figure 9: Line of curvature: one developable surface containing the centres of the spheres (white). The developable surface perpendicular to it (blue) is tangent to the resulting canal surface (not shown in the Figure).

397

### 398 Computation of the locus of centres

399 Consider now that a normal vector and a line of curva-  
 400 ture have been specified for the canal surface. The locus  
 401 of centres is on a developable surface. So far we did not  
 402 use any property of the second curve. We notice however  
 403 that the centres of the spheres are on the *bisector surface*  
 404 *of the two curves*. Such surface is defined as the envelope<sup>419</sup>  
 405 of the points which are equidistant to both curves. They<sup>420</sup>  
 406 have been studied in [36] for example. <sup>421</sup>

407 Therefore, the centres of the spheres can be found by<sup>422</sup>  
 408 intersecting the bisector surface of the two curves and the<sup>423</sup>  
 409 developable surface constructed from the normals. Both<sup>424</sup>  
 410 surfaces are not bounded, and it seems intuitive that they<sup>425</sup>  
 411 will have an intersection in non-degenerate cases. The<sup>426</sup>  
 412 construction of the whole bisector surface is however not<sup>427</sup>  
 413 necessary, as it is meaningful to consider a finite collec-<sup>428</sup>  
 414 tion of spheres that will construct the cyclidic net that<sup>429</sup>

parametrise the canal surface.

Consider hence the first curve discretised with  $n$  sub-  
 divisions, as depicted in Figure 10. The centres of the  
 spheres belong to  $n$  lines on the developable surface. Let  
 $\mathbf{P}_k$  be the  $k^{th}$  point on the first curve,  $\mathbf{C}_k$  the centre of  
 the bi-tangent sphere on the corresponding line and  $\mathbf{C}'_k$   
 the closest point to  $\mathbf{C}_k$  on the second curve. By default,  
 $\mathbf{C}_k$  is not on the bisector surface. Therefore, the following  
 functional is introduced and minimised.

$$F = \sum_{k=0}^n (\|\mathbf{C}_k \mathbf{P}_k\| - \|\mathbf{C}_k \mathbf{C}'_k\|)^2 \quad (6)$$

416 The positions of the  $\mathbf{C}_k$  are encoded with independent  
 417 unique parameters. Each term of the sum can thus be  
 418 minimised individually by the means of Newton's method.

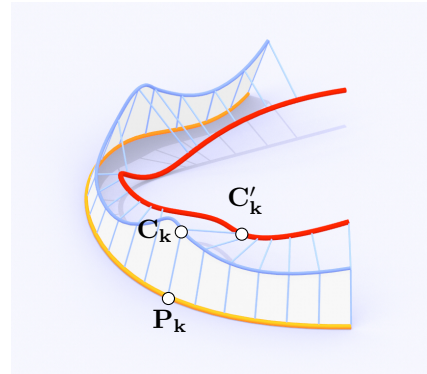


Figure 10: The curve fitting problem: the locus of the sphere centres (in dark blue) belongs to the developable surface chosen by the user, and each  $\mathbf{C}_k$  belongs to a straight line of this surface. The locus of centres is equidistant to both input curves.

### Algorithm for spheres generation

The algorithm for the generation of a canal surface from two curves follows:

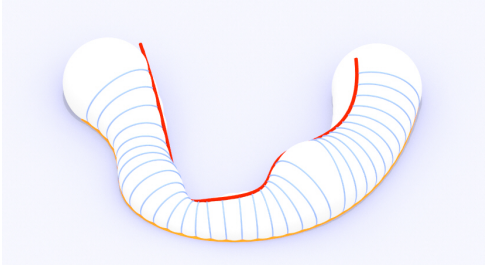
1. Select two curves, one of them being a line of curvature on the final surface.
2. Choose an orientation of the canal surface: specifying one orientation restricts the locus of centres to be in a uniquely defined developable surface.
3. Discretise the line of curvature with points  $\mathbf{P}_k$ , and generate the lines containing the centres of the spheres on the developable surface.



430 4. Initialise the  $\mathbf{C}_k$  with  $\mathbf{C}_k = \mathbf{P}_k$ .  
 431 5. Minimise Equation(6) with Newton's method.  
 432 The result is a collection of points corresponding to sphere  
 433 centres. The radius  $R_k$  of each sphere is given by the  
 434 distance  $\|\mathbf{C}_k \mathbf{P}_k\|$ .

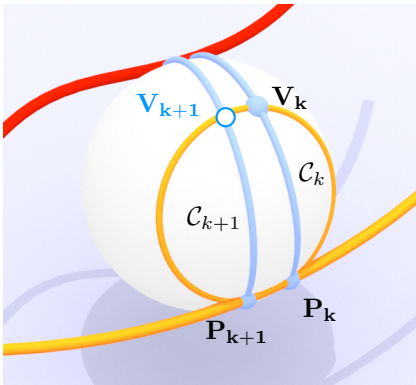
#### 435 *Generation of a supporting cyclidic net*

436 We have seen that given two curves and a supplement-  
 437 ary condition, it is possible to define one unique family  
 438 of spheres that optimally fits the two curves. Consider  
 439 now the circles  $\mathcal{C}_k$  defined as the intersection of successive  
 440 spheres  $\mathcal{S}_k, \mathcal{S}_{k+1}$ , like shown in Figure 11.  $\mathbf{P}_k$  is the point  
 441 of  $\mathcal{C}_k$  on the input curve.



465 Figure 11: A family of spheres (white) fitting two curves (red and  
 466 orange), and their successive intersection (blue).

442 It is clear that for any  $k$ ,  $\mathcal{C}_k$  and  $\mathcal{C}_{k+1}$  both belong  
 443 to the sphere  $\mathcal{S}_{k+1}$ . Consider Figure 12: choosing one  
 444 point  $\mathbf{V}_k$  on  $\mathcal{C}_k$  there is exactly one point  $\mathbf{V}_{k+1}$  on  $\mathcal{C}_{k+1}$   
 445 so that  $\mathbf{P}_k \mathbf{V}_k \mathbf{V}_{k+1} \mathbf{P}_{k+1}$  is inscribed within a circle. The



478 Figure 12: Two circles  $\mathcal{C}_k$  and  $\mathcal{C}_{k+1}$ : by choosing one point  $\mathbf{V}_k$  on  $\mathcal{C}_k$ ,  
 479 one defines a circle and a one parameter family of cyclidic patches.

445  
 446 process can be applied iteratively to generate a circular

447 strip, supporting a cyclidic net. The circles  $\mathcal{C}_k$  can be  
 448 edges of the resulting cyclidic strip because they belong to  
 449 the same sphere [25].

#### 450 *Comment*

451 The proposed method allows for the construction of  
 452 a canal surface that fits optimally two input curves. The  
 453 surface can be parametrised instantly with cyclidic patches  
 454 and covered with a circular mesh as detailed in [25]. Con-  
 455 sider indeed the collection of circles ( $\mathcal{C}_n$ ), and two consecu-  
 456 tive circles  $\mathcal{C}_n$  and  $\mathcal{C}_{n+1}$ . By construction, these circles are  
 457 co-spherical, and thus, any planar quad with vertices on  
 458  $\mathcal{C}_n$  and  $\mathcal{C}_{n+1}$  is also a circular quad. This simplifies greatly  
 459 the meshing process. The meshing algorithm is illustrated  
 460 in Figure 13.

- 461 • Choose a discretisation of the first circle  $\mathcal{C}_1$ , the  $k^{th}$   
 462 point of the  $n^{th}$  circle is noted  $\mathbf{P}_{n,k}$
- 463 • The  $\mathbf{P}_{n,1}$  are chosen so that they all belong to the  
 464 fitted curve which is a line of curvature of the result-  
 ing surface;
- 465 • Starting from  $k = 1$  and  $n = 1$ , generate the plane  
 466  $\mathcal{P}$  going through  $\mathbf{P}_{n,k}, \mathbf{P}_{n,k+1}$  and  $\mathbf{P}_{n+1,k}$  (step 1  
 in Figure 13);
- 467 • The point  $\mathbf{P}_{n+1,k}$  is the intersection between  $\mathcal{P}$  and  
 468  $\mathcal{C}_{n+1}$  (step 2 in Figure 13);
- 469 • Iterate over  $k$  (step 3 in Figure 13);
- 470 • Iterate on  $\mathcal{C}_{n+1}$  and  $\mathcal{C}_{n+2}$  (step 4 in Figure 13);

471  
 472  
 473 The tool recalls the two-rails sweep commonly used in  
 474 CAD software. One curve is a line of curvature of the re-  
 475 sulting shape. It provides proper alignment of the mesh  
 476 with the borders, which often dictate the mechanical be-  
 477 haviour of the structure.

#### 478 *4.2. Generation of closed canal surfaces*

479 The proposed construction can be extended to closed  
 480 strips with several limitations. The first one has been dis-  
 481 cussed in [22]: a closed cyclidic net gives a smooth closed

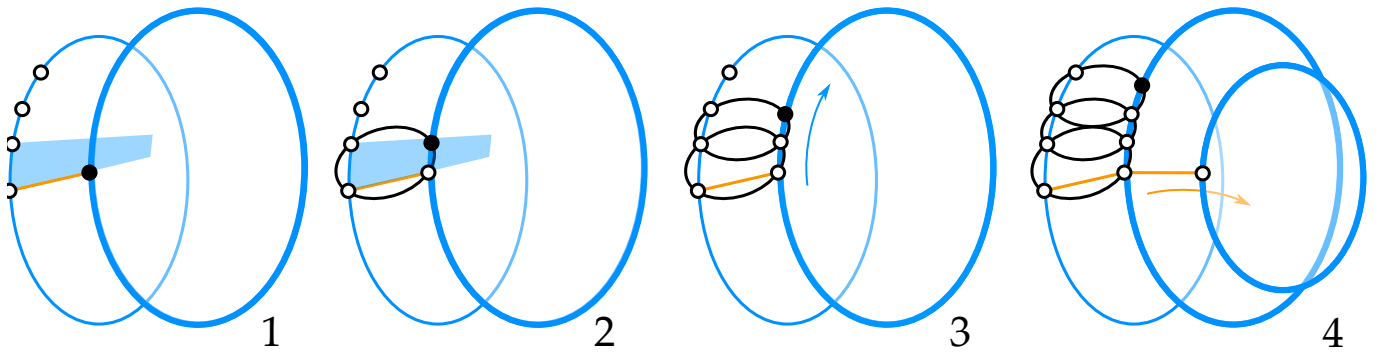


Figure 13: Meshing between two co-spherical circles (axonometry).

482 surface if and only if the discrete guide curve is a pseudo-  
 483 spherical curve (it is parallel to a curve which has all its  
 484 vertices inscribed within a sphere). The second condition  
 485 corresponds to the possibility of drawing the last circle of  
 486 the strip. Consider Figure 14: the first circle of the strip  
 487 is written  $C_0$ , the penultimate circle  $C_f$ , the initial point  
 488  $\mathbf{P}$  and the first and last point of the curve  $\mathbf{P}_0$  and  $\mathbf{P}_f$   
 489 respectively. There are two cases:

- $C_0$  and  $C_f$  belong to the same sphere, then the circle  
 going through  $\mathbf{P}$ ,  $\mathbf{P}_0$  and  $\mathbf{P}_f$  intersects the circle  
 $C_f$  in two points. This circle is the solution we are  
 looking for and is represented with dashed lines on  
 Figure 14.
- In the other cases, the spheres  $(C_0, \mathbf{P}_f)$  and  $(C_f, \mathbf{P}_0)$   
 are distinct. Their intersection is a circle intersecting  
 the circle  $C_0$  and  $C_f$  in two different points. This  
 circle is the only solution that allows the closing of  
 the circular strip, and it does not intersect  $C_0$  in  $\mathbf{P}$ .

In the first case, only the intersection of the last circle  
 and  $C_f$  is unknown. In the second case, the position of  $\mathbf{P}$   
 cannot be specified arbitrarily (as in section 2. for open  
 strips). Compared to open strips, there is therefore a loss  
 of at most two degrees of freedom for the control of the  
 shape.

Figure 15 shows a rendering of a facade covered with  
 a canal surface (the structural system supporting the can-  
 tilvering facade is not shown). Being able to model closed

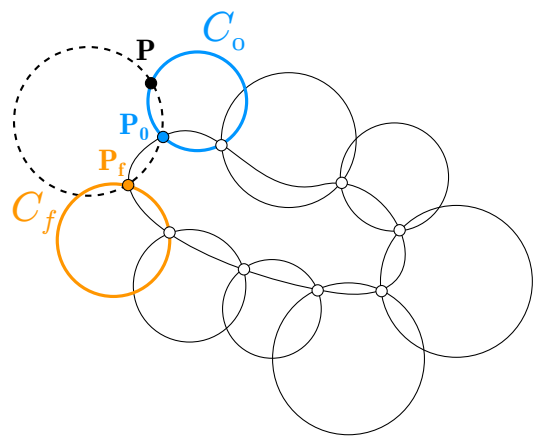


Figure 14: Problem of a closing strip

surfaces is crucial for architectural shapes, as façades are  
 usually closed.

### 4.3. Practical applications

The method presented in this paper has been used dur-  
 ing a one week workshop in 2015. Architecture and engi-  
 neering students had to design and build a 30 m<sup>2</sup> free-form  
 pavilion, the only material available was polystyrene in  
 flat rectangular sheets. The shape is a super-canal surface  
 meshed with circular quadrilaterals. The pavilion, shown  
 in Figure 16 is a grid structure with a torsion-free beam  
 layout. The offset was computed with a reflection rule sim-  
 ilar to the one generating cyclidic nets. An optimisation  
 was performed in order to minimise the height gap at the  
 nodes between beams of constant height. The fast compu-  
 tation of the space of solutions was key to the success of

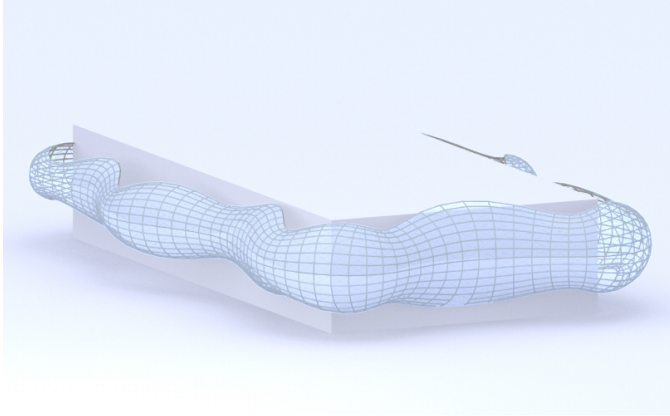


Figure 15: A visualisation of a façade as a canal surface, covered with a circular mesh.

this operation within a limited time frame (5 days).

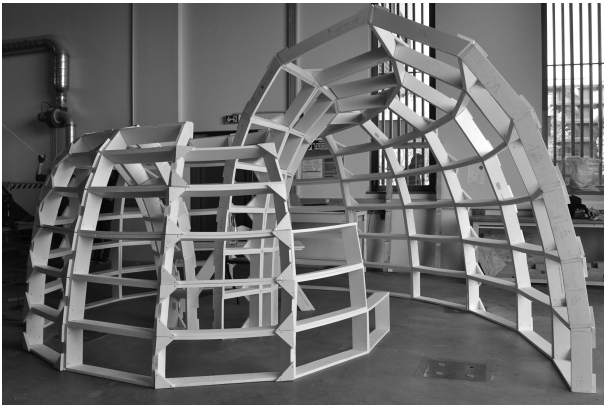


Figure 16: A prototype built with torsion free-nodes on a super-canal surface.

The tools presented in this paper were used for shape generation as well as fabrication. Hundreds of polystyrene elements were cut according to the 3D model and assembled. The planarity of the panels was considered for use as bracing elements and was validated on a  $5\text{m}^2$  model, shown in Figure 17. Flat panels used as bracing elements improve the overall stability and stiffness <sup>1</sup>.

Another exploration was performed with a timber structure, shown in Figure 18. The structure is a plated shell structures: the facets are connected along their edges without additional stiffeners. The small-scale pavilion il-

<sup>1</sup>More details and pictures can be found on <http://www.thinkshell.fr/building-freeform-2015/>.



Figure 17: A model of a canal surface with planar quadrangles used for bracing.

illustrates thus the potential offered by planar panels rather than offset properties of circular meshes, although the discrete normals of circular meshes have been used to generate planar cuts between the plates.



Figure 18: A timber plated shell structure covered with circular quadrilaterals generated with the method proposed in this paper.

The construction of those prototypes validates the use of the numerical tools presented in this paper. The user feedback allowed us to identify the most relevant way to model super-canal surfaces. In particular, the students found important to control at least one boundary curve. This explains why the method of generation of canal surfaces presented in this work focuses on the prescription of a boundary curve, and not on the curve supporting the centers of the sphere for example.

## 5. Application to inverse problems

### 5.1. Generation of *M*-revolution surfaces

The most well-known canal surfaces are surfaces of revolution. They indeed correspond to the case of a straight

553 generatrix. Surfaces of revolutions have many interest-  
 554 ing properties for applications in architecture. They are  
 555 isothermic surfaces, which means that they can be discre-  
 556 tised as Edge-Offset Meshes. Yet, isothermic surfaces are  
 557 preserved by Combescure and Möbius transformations and  
 558 they thus inherit this property.

559 In particular, we discuss here of a particular subset of  
 560 'super-surfaces of revolutions', where the center of inver-  
 561 sion and the axis of revolution are in a horizontal plane,  
 562 as shown in Figure 19. It is clear that the parallels of the  
 563 surface of revolution are vertical in this case. Since inver-  
 564 sions preserve circles and angles, we can deduce that this  
 565 family of curvature lines remain vertical after inversion.  
 566 Combescure transformations preserve planarity: applying  
 567 another Combescure transformation yields a surface with<sup>591</sup>  
 568 planar arches. This additional property is particularly in-<sup>592</sup>  
 569 teresting for applications to structural system with contin-<sup>593</sup>  
 570 uous arches and secondary structure. A specific method<sup>594</sup>  
 571 has therefore been developed to generate these surfaces.  
 572 It consists of solving the inverse problem detailed in the  
 573 following.

574 The input data for the problem are displayed in Fig-  
 575 ure 19. The user prescribes one planar curve, one circle  
 576 in the same plane comprising the ends  $\mathbf{P}_1$  and  $\mathbf{P}_4$  of the  
 577 curve, and two points  $\mathbf{P}_2$  and  $\mathbf{P}_3$  on this circle. The objec-  
 578 tive is here to reconstruct the initial surface of revolution,  
 579 therefore the problem is to find a center of inversion  $\mathbf{C}$  so  
 580 that the image of the quadrangle  $P_1P_2P_3P_4$  is an isosceles  
 581 trapezoid.

582 Isosceles trapezoids are the only cyclic quadrilaterals  
 583 that have parallel opposite edges. Notice that the prob-  
 584 lem is planar and can thus be formulated with complex  
 585 numbers. The parallelism corresponds to the fact the di-<sup>595</sup>  
 586 rection vectors are co-linear (identical up to a scaling by  
 587 a real number  $t$ ). Assigning the complex numbers  $z_1, z_2,$ <sup>596</sup>  
 588  $z_3$  and  $z_4$  to the points  $\mathbf{P}_1, \mathbf{P}_2, \mathbf{P}_3$  and  $\mathbf{P}_4$ , and writing<sup>597</sup>  
 589  $z_{j,C}$  the complex number associated to the image of  $z_j$  by  
 590 an inversion of center  $\mathbf{C}$ , we obtain equation (7):

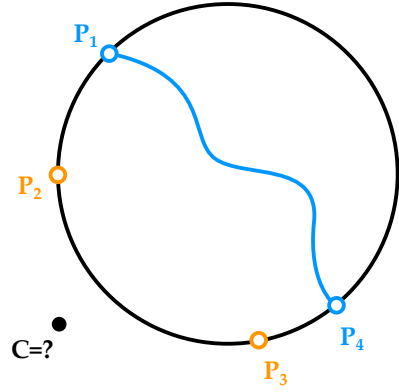


Figure 19: Problem for the practical design with inversion of surfaces of revolutions.

$$\frac{z_{2,C} - z_{1,C}}{z_{3,C} - z_{4,C}} = t \in \mathbb{R} \quad (7)$$

We can use the equation (2) to express equation (7) with respect to the  $z_j$  and obtain equation (8). It is independent of the ratio of inversion  $k$ : the position of the center of inversion is the only value of interest in this problem.

$$\frac{\left( \frac{z_2 - z_1}{(z_1 - z_C)(z_2 - z_C)} \right)}{\left( \frac{z_3 - z_4}{(z_3 - z_C)(z_4 - z_C)} \right)} = t \in \mathbb{R} \quad (8)$$

After simplifications, this equation leads to a second order equation in  $z_C$ . The general form of (8) can be written as:

$$A_t z_C^2 + B_t z_C + D_t = 0 \quad (9)$$

with

$$\begin{cases} A_t = z_2 - z_1 + t \cdot (z_4 - z_3) \\ B_t = -(1+t)z_1z_3 + (t-1)z_1z_4 \\ \quad + (1+t)z_2z_4 + (1-t)z_2z_3 \\ D_t = z_3z_4(z_2 - z_1) + tz_1z_2(z_4 - z_3) \end{cases}$$

The case of  $A_t = 0$  can occur only when the quad  $P_1P_2P_3P_4$  is already an isosceles trapezoid. In the other cases, for each value of  $t$ , there are two complex solutions giving two positions for the center of inversion in the complex plane. It is thus possible to solve this inverse problem with a straight-forward solution based on complex analysis.



602 An illustration of this problem is shown on Figure 20.<sup>628</sup>  
 603 On this image, all the facets are inscribed within circles.<sup>629</sup>  
 604 The free-form shape is thus covered with planar facets and  
 605 torsion-free nodes. Since the circle shown in Figure 20 is  
 606 in the horizontal plane, it is noticed that one family of  
 607 lines of curvature consists of planar vertical arches. The  
 608 solution proposed here can easily be extended to the case  
 609 of a spherical guide curve with two successive inversions.  
 610 Likewise, it is possible to apply this method to moulding  
 611 or Monge surfaces.

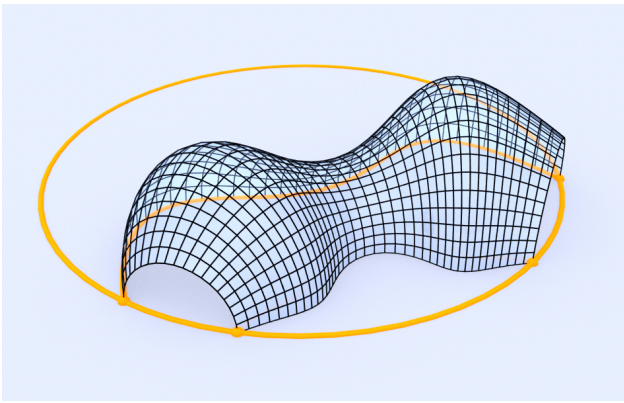


Figure 20: Surface generated by inversion of a surface of revolution,<sup>633</sup>  
 constructed from one curve and two points on a circle.

## 612 5.2. C-canal surfaces

613 We proposed an extension of the generation method  
 614 proposed in section 4.1 by adding a Combescure trans-<sup>637</sup>  
 615 form so that the can be any planar curve, and that the<sup>638</sup>  
 616 final surface is a C-canal surface. Figure 21a shows the<sup>639</sup>  
 617 three input data for the generation of a C-canal surface,<sup>640</sup>  
 618 while Figures 21b and 21c show two possible outputs. Like<sup>641</sup>  
 619 canal surfaces, the user can specify one curve, a collection<sup>642</sup>  
 620 of lengths defining indirectly a second curve, and a planar<sup>643</sup>  
 621 cross-section that is obtained by Combescure transforma-<sup>644</sup>  
 622 tion of a circle. The inputs controlled by the designer are<sup>645</sup>  
 623 thus the same as the ones described in Figure 6, with the<sup>646</sup>  
 624 control of one curve in addition.<sup>647</sup>

625 The lengths of the edges is specified for the C-canal<sup>648</sup>  
 626 surface, but at the beginning, only the canal surface can<sup>649</sup>  
 627 be computed. An optimisation procedure is thus required<sup>650</sup>

to find the canal surface that will fit the input data after  
 Combescure transformation.

Writing  $\mathbf{L}$  the target lengths for the curves crossing the  
 C-canal surface (see Figure 6), we generate first the canal  
 surface  $\mathbf{F}(\mathbf{u}, \mathbf{L})$ . There is one Combescure transformation  
 $f$  that maps the first circle of the canal surface to the  
 transverse input curves chosen while preserving one input  
 curve. After the Combescure transformation, the resulting  
 lengths  $\mathbf{L}'$  on the C-canal surface differ from  $\mathbf{L}$ . However,  
 Figure 21 shows that a canal surface and a C-canal sur-  
 face related by a Combescure transformation have similar  
 boundaries, even if they do not perfectly coincide. There-  
 fore, a local optimization algorithm (in our case BFGS)  
 can be used to minimise the error:

$$E(L_k) = \sum_k (L'_k - L_k)^2 \quad (10)$$

630 The optimisation is done for each  $L_k$  successively. This  
 631 prevents from computing the whole Combescure transfor-  
 632 mation at each iteration, but only the strip where the er-  
 633 ror is evaluated. With this precaution, the computation  
 634 remains lightweight and stable. This optimisation proce-  
 635 dure can be extended to the fitting of two curves, like done  
 636 in 4.1.

## 5.3. Meshing of super-canal surfaces

A key feature of the proposed method is that it oper-  
 ates fundamentally on smooth surfaces. It is therefore in-  
 dependent from the mesh density. Notice for example that  
 the solution of equation (9) does not require any knowl-  
 edge on the discretisation of the curves, but only the four  
 prescribed points. Therefore, re-meshing of super-canal  
 surfaces is extremely simple and detailed below.

It has already been pointed out that inversions are in-  
 volutions. Combescure transformations are linear maps  
 and can easily be inverted with the algorithm proposed in  
 Section 2.4. The computation of inverse transformation  
 is thus extremely light. These properties are used exten-  
 sively to remesh super-canal surface and is illustrated in

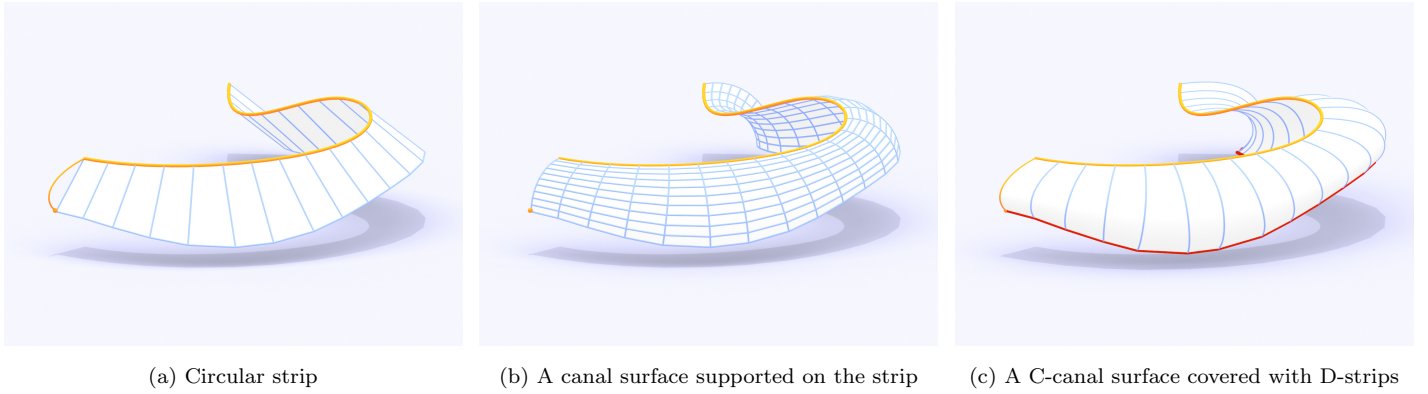


Figure 21: Generation of a C-canal surface

651 Figure 22. Given a discretisation on the guide curves, it is possible to find their image by a composition of Combescure and Möbius transformations  $f$  so that they fit with the boundaries of a canal surface. The meshing on the canal surface is done using cyclidic patches, like explained in Section 4.1. The inverse transformation  $f^{-1}$  is then computed and maps the mesh so that it fits the reference curves.

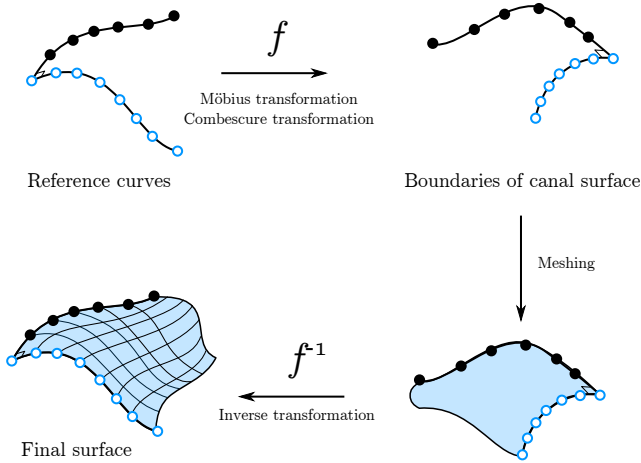


Figure 22: Remeshing procedure for a super-canal surface.

## 6. Discussion

### 6.1. Algorithmic performance

The algorithms of shape generation have been implemented in Grasshopper<sup>TM</sup>, an environment of visual

programming compatible with the modelling software Rhinoceros<sup>TM</sup>. In this section, we discuss the performance of the three operations used in our method:

- the computation of circular strips and the meshing of discrete canal surfaces;
- the computation of Möbius transformations and the solution of the inverse problems;
- the computation of Combescure transformations.

Circular strips are defined using a propagation algorithm. The problem solved at each step is the intersection of a sphere and a circle. The resulting computation time varies linearly with the number of subdivisions of the guide curve.

The computation of Möbius transformations is straight forward, as equation (1) is applied to each point of the mesh. Likewise the solution of equation (9) is obvious and requires no special numerical treatment. For that reason, Möbius transformations of meshes are as fast as the computation of simple affine transformations, like scaling or translation.

A case-study for the computation of Combescure transformations was performed. Like discussed in Section 2.4, the computation time varies linearly with the number of panels in the structure. The computation time is inferior to 20 milliseconds for a mesh with 10,000 faces, a high



		Isothermic	Planar curves	Stress lines	Circular mesh
Canal surface	revolution	Yes	Yes	Yes	Yes
	M-revolution				
	General case	No			
C-canal surface	C-revolution (moulding)	Yes			
	CM-revolution				
	General case	No			
MC-canal surface	M-moulding	Yes	No	No	
	MCM-revolution				
	General case	No			

Table 2: Properties of super-canal surfaces.

number of faces for applications in architecture. Notice that no pre-factorisation is required for the computation of the Combescure transformation: the computation time are the one experienced by the user. This is in accordance with the will to offer a maximal flexibility for the design. Applying successive Combescure transformations is therefore possible in real-time applications with our algorithm. Finally, we notice that Combescure transformations require more time than the other operations and generally governs the overall performance of the method. Notice also that Combescure transformations and Möbius transformations have to be applied twice in the reverse engineering methods presented in the previous section.

## 6.2. Properties of the structural layout

Table 2 sums up the different properties of the surfaces created with our framework. As one applies Möbius and Combescure transformations and extends the formal freedom, some properties are lost a priori. All the shapes can nevertheless be parametrised as circular meshes. As an example, it can be noticed that the lines of curvature are not necessarily lines of principal stresses under uniform pressure for MC-canal surfaces. In the most general case, there is also no guaranty that there is a family of planar curves.

Among other remarkable properties, it may be noticed

that the images of surfaces of revolution are isothermic surfaces, so that it is possible to parametrise them with conformal squares. Optimisation of the parametrisation of isothermic surfaces towards visually pleasant meshes could thus be done in the manner of [37].

Figure 23 shows a M-moulding surface. It was generated to fit two input curves, in the manner of M-revolution surfaces. The shape is visually not different from C-canal surfaces, but the curves are not planar, which increases the complexity. The analysis of Table 2 shows that C-canal surfaces are probably the best trade-off between design freedom and properties of the structural layout.

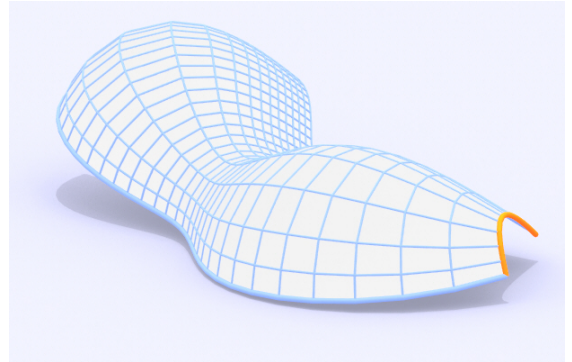


Figure 23: A M-moulding surface passing through two prescribed curves (thick lines). Only the orange curve is rigorously planar.

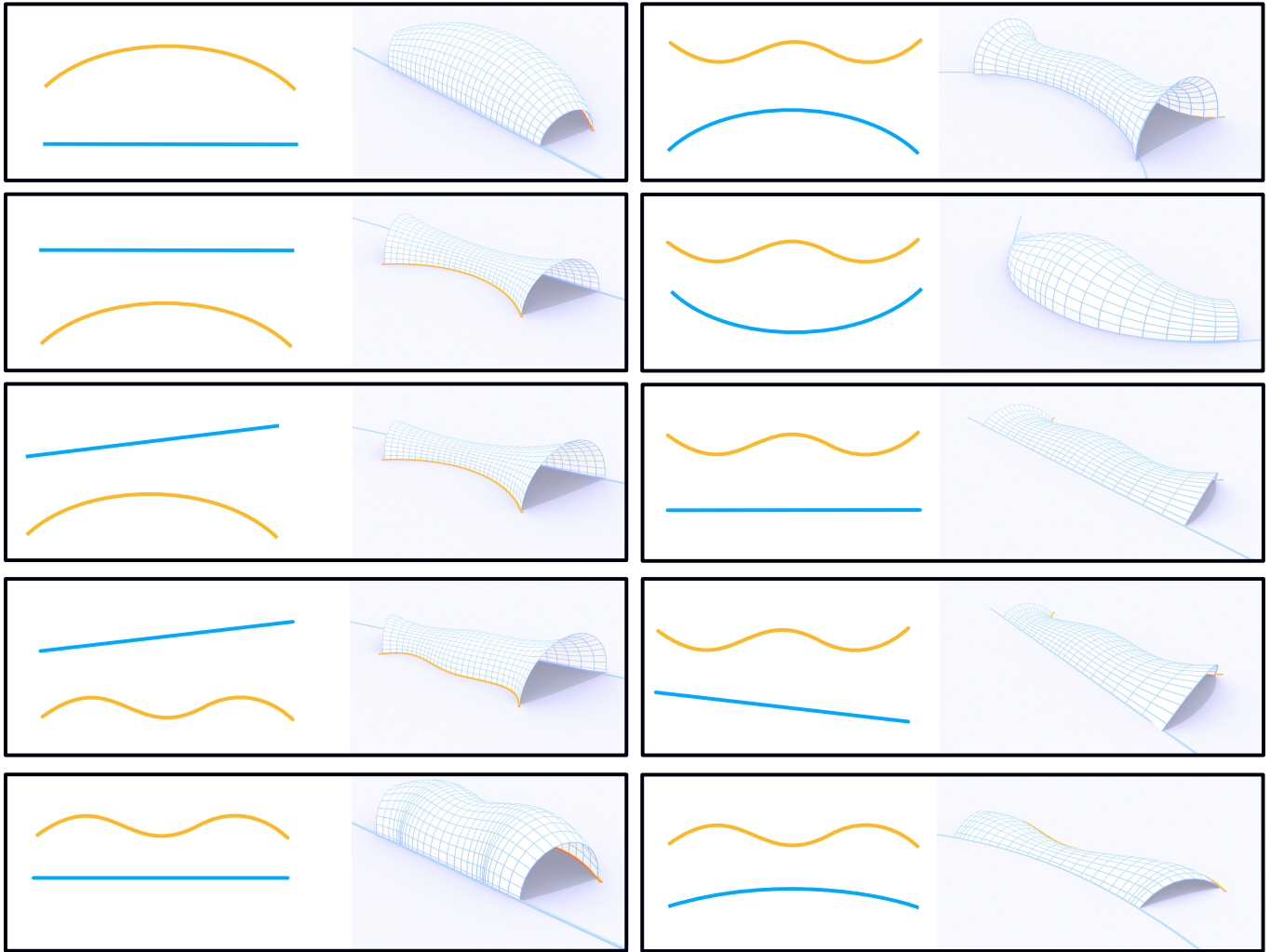


Figure 24: Canal surfaces obtained by fitting two planar curves, the orange curve is a line of curvature of the surface.

6.3. Shape explorations: potential and limitations

The generation super-canal surfaces is subject to modelling limitations discussed in this section. Figure 24 displays some canal surfaces generated by solving the two-curves fitting problem. The orange curve is a line of curvature of the resulting surface. The examples show that it is possible to properly fit a line with a doubly-curved shape, which should be of interest for practical applications.

These examples also highlight some limitations of super-canal surfaces. Consider for example the shape in Figure 25, where there is a noticeable shrinkage of panels. This concentration of lines of curvature is linked to the

properties of the *evolute* of the guiding curve.

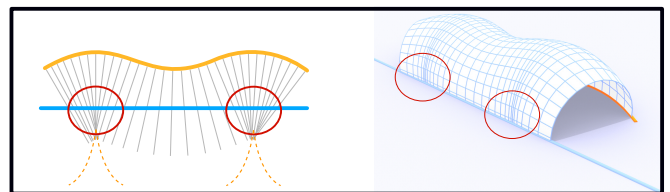


Figure 25: Concentration of lines of curvatures (circled in red) and plane view

The evolute of a curve is the locus of the center of its osculating circles. The lines obtained by sweeping along a curve intersect along the evolute, as shown in Figure 25. In Figure 25, it appears that the second curve used as an input for the fitting problem (in blue) is close to the evolute

of the first curve (in orange). As a consequence, the planes containing the circles used for the shape generation (the grey lines in the top view) converge towards the evolute and result in panel shrinkage. This practical limitation also exists for more general super-canal surfaces. The designer must limit the curvature of the control curves in order to avoid self-intersections of the surface he or she is generating.

## 7. Conclusion

This paper presented a new family of shapes for the rationalization of free-form structures and envelopes. It enriches the formal vocabulary of geometrically-constrained design approaches, and has many relevant applications, from pneumatic structures to gelzed gridshells. A connection to shell theory was recalled and showed that the surfaces created with this method are at equilibrium under normal uniform load. Moreover, the lines of curvatures that are used for discretisation of super-canal surfaces correspond to lines of principal stresses, making the meshes efficient for both fabrication and structural performance. The tools developed for the shape generation were used in the practical context of a workshop for architecture and engineering students.

The methodology for shape generation relies heavily on Möbius geometry, the geometry of circles in space. It studies the transformations of shapes by Combescure and Möbius transformations, and in that sense, it is a generalisation of Möbius geometry, which is only interested in the latter one. Like many other geometrically-constrained shapes, super-canal surfaces are generated from three curves. The underlying construction rule is more sophisticated than simple affine transformation, like translation or scaling. It also gives more degrees of freedom than scale-trans surfaces. Lack of design tools for designers and architects for complex structures has been shown by William Baker in a plenary talk at the Symposium of the IASS in 2015, which is a real prejudice to

the construction industry. Super-canal surfaces transcribe complex geometrical notions into tools easily usable as a design tool by architects and engineers as they provide insight on the buildability, the mechanical behavior under normal load of free-form structures. This illustrates the interest of using Möbius geometry for geometrical modelling in architecture. Other families of shapes could arise from this framework.

The shapes proposed in this paper could be combined with more general modelling techniques, for example see [38], who studies deformations of circular meshes by combination of compatible Möbius transformations.

## Acknowledgment

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## References

- [1] J. Sakarovitch, [Gaspard Monge founder of constructive geometry](#), in: Proceedings of the Third International Congress on Construction History, 2009, pp. 1293–1300 [cited May 2nd, 2016].
- [2] J. Schlaich, H. Schober, Glass Roof for the Hippo Zoo at Berlin, *Structural Engineering International* 7 (4) (1997) 252–254. doi: <https://doi.org/10.2749/101686697780494581>.
- [3] J. Glymph, D. Shelden, C. Ceccato, J. Mussel, H. Schober, [A parametric strategy for free-form glass structures using quadrilateral planar facets](#), *Automation in Construction* 13 (2) (2004) 187–202. doi: <https://doi.org/10.1016/j.autcon.2003.09.008>.
- [4] Y. Liu, W. Wang, H. Pottmann, J. Wallner, Y. Yong-Liang, Geometric Modeling with Conical Meshes and Developable Surfaces, *ACM Transactions on Graphics* 25 (3) (2006) 681–689. doi: <https://doi.org/10.1145/1179352.1141941>.

- [5] J. Blassel, A. Pfadler, La gare de Strasbourg, *Construction métallique* 45 (1) (2008) 15–36. [doi:https://doi.org/10.1002/stab.200490149](https://doi.org/10.1002/stab.200490149).
- [6] H. Pottmann, A. Schiftner, P. Bo, H. Schmiedhofer, W. Wang, N. Baldassini, J. Wallner, *Freeform surfaces from single curved panels*, *ACM Transactions on Graphics* 27 (3) (2008) 1. [doi:https://doi.org/10.1145/1399504.1360675](https://doi.org/10.1145/1399504.1360675).
- [7] S. Stephan, K. Knebel, J. Sanchez-Alvarez, *Reticulated Structures On Free-Form Surfaces*, *Stahlbau* 73 (2004) 562–572. [doi:https://doi.org/10.1002/stab.200490149](https://doi.org/10.1002/stab.200490149).
- [8] H. Pottmann, Y. Liu, J. Wallner, A. Bobenko, W. Wang, *Geometry of multi-layer freeform structures for architecture*, *ACM Transactions on Graphics* 26 (3) (2007) 65. [doi:https://doi.org/10.1145/1276377.1276458](https://doi.org/10.1145/1276377.1276458).
- [9] P. Bo, H. Pottmann, M. Kilian, W. Wang, J. Wallner, *Circular Arc Structures*, *ACM Transactions on Graphics (TOG)* 30 (4) (2011) 101. [doi:https://doi.org/10.1145/1964921.1964996](https://doi.org/10.1145/1964921.1964996).
- [10] Y.-I. Yang, Y.-J. Yang, H. Pottmann, N. J. Mitra, *Shape Space Exploration of Constrained Meshes*, *ACM Transactions on Graphics* 30 (2011) 124. [doi:10.1145/2024156.2024158](https://doi.org/10.1145/2024156.2024158).
- [11] S. Bouaziz, M. Deuss, Y. Schwartzburg, T. Weise, M. Pauly, *Shape-Up: Shaping Discrete Geometry with Projections*, *Computer Graphics Forum* 31 (5) (2012) 1657–1667. [doi:10.1111/j.1467-8659.2012.03171.x](https://doi.org/10.1111/j.1467-8659.2012.03171.x).
- [12] B. Deng, S. Bouaziz, M. Deuss, A. Kaspar, Y. Schwartzburg, M. Pauly, *Interactive design exploration for constrained meshes*, *Computer-Aided Design* 61 (2015) 13–23. [doi:https://doi.org/10.1016/j.cad.2014.01.004](https://doi.org/10.1016/j.cad.2014.01.004).
- [13] C. Jiang, C. Tang, M. Tomicic, H. Pottmann, J. Wallner, *Interactive Modeling of Architectural Freeform Structures*, *Combining Geometry with Fabrication and Statics*, in: P. Block, W. Wang, J. Knippers (Eds.), *Advances in Architectural Geometry*, Springer, 2014, pp. 95–108. [doi:https://doi.org/10.1007/978-3-319-11418-7\\_7](https://doi.org/10.1007/978-3-319-11418-7_7).
- [14] R. Mesnil, C. Douthe, O. Baverel, *Marionette Mesh: modelling free-form architecture with planar facets*, *International Journal of Space Structures* 32 (3-4) (2017) 184–198. [doi:https://doi.org/10.1177/0266351117738379](https://doi.org/10.1177/0266351117738379).
- [15] M. Bagneris, R. Motro, B. Maurin, N. Pauli, *Structural Morphology issues in Conceptual Design of Double Curved Systems*, *International Journal of Space Structures* 23 (2) (2008) 79–87. [doi:https://doi.org/10.1260/026635108785260560](https://doi.org/10.1260/026635108785260560).
- [16] H. Pottmann, A. Asperl, M. Hofer, A. Kilian, *Architectural Geometry*, Bentley Institute Press, 2007.
- [17] R. Mesnil, C. Douthe, O. Baverel, B. Léger, J.-F. Caron, *Isogonal moulding surfaces: A family of shapes for high node congruence in free-form structures*, *Automation in Construction* 59 (2015) 38–47. [doi:https://doi.org/10.1016/j.autcon.2015.07.009](https://doi.org/10.1016/j.autcon.2015.07.009).
- [18] S. Krivoshapko, V. Ivanov, *Encyclopedia of analytical surfaces*, Springer, 2015. [doi:10.1007/978-3-319-11773-7](https://doi.org/10.1007/978-3-319-11773-7).
- [19] R. Mesnil, *Structural exploration of fabrication-aware design spaces for non-standard architecture*, Ph.D. thesis, Université Paris-Est (2017) [cited February 14th 2018].
- [20] H. Schober, *Transparent shells - form topology structure*, Ernst & Sohn, 2016.
- [21] C. Rogers, W. K. Schief, *On the equilibrium of shell membranes under normal loading. Hidden integrability*, *Proceedings of the Royal Society of London A: Mathematical, Physical and Engineering Sciences* 459 (2003) 2449–2462. [doi:https://doi.org/10.1098/rspa.2003.1135](https://doi.org/10.1098/rspa.2003.1135).
- [22] R. Mesnil, C. Douthe, O. Baverel, B. Léger, *Generalised cyclidic nets for shape modelling in architecture*, *International Journal of Architectural Computing* 15 (2) (2017) 148–168. [doi:https://doi.org/10.1177/1478077117714917](https://doi.org/10.1177/1478077117714917).
- [23] R. Martin, J. De Pont, T. Sharrock, *Cyclide surfaces in computer aided design*, *The mathematics of surfaces* (1986) 253–268. [doi:https://doi.org/10.1016/0167-8396\(90\)90033-N](https://doi.org/10.1016/0167-8396(90)90033-N).
- [24] D. Dutta, R. Martin, M. Pratt, *Cyclides in surface and solid modeling*, *IEEE Computer Graphics and Applications* 13 (1) (1993) 53–59. [doi:https://doi.org/10.1109/38.180118](https://doi.org/10.1109/38.180118).
- [25] A. Bobenko, E. Huhnen-Venedey, *Curvature line parametrized surfaces and orthogonal coordinate systems: discretization with Dupin cyclides*, *Geometriae Dedicata* 159 (1) (2012) 207–237. [doi:https://doi.org/10.1007/s10711-011-9653-5](https://doi.org/10.1007/s10711-011-9653-5).
- [26] P. Bo, Y. Liu, C. Tu, C. Zhang, W. Wang, *Surface fitting with cyclide splines*, *Computer Aided Geometric Design* [doi:10.1016/j.cagd.2016.02.018](https://doi.org/10.1016/j.cagd.2016.02.018).
- [27] M. Bizzarri, M. Lávička, J. Vršek, *Canal surfaces with rational contour curves and blends bypassing the obstacles*, *Computer-Aided Design* 64 (2015) 55–67. [doi:10.1016/j.cad.2015.03.002](https://doi.org/10.1016/j.cad.2015.03.002).
- [28] K. Bana, K. Kruppa, R. Kunkli, M. Hoffmann, *KSpheres an efficient algorithm for joining skinning surfaces*, *Computer Aided Geometric Design* 31 (7-8) (2014) 499–509. [doi:10.1016/j.cagd.2014.08.003](https://doi.org/10.1016/j.cagd.2014.08.003).
- [29] Y. Srinivas, D. Dutta, *Intuitive procedure for constructing geometrically complex objects using cyclides*, *Computer-Aided Design* 26 (4) (1994) 327–335.

- 915 [doi:10.1016/0010-4485\(94\)90078-7](https://doi.org/10.1016/0010-4485(94)90078-7).
- 916
- 917 [30] M. J. Pratt, *Quartic supercyclides I: Basic theory*, Computer Aided Geometric Design 14 (7) (1997) 671–692.
- 918 [doi:https://doi.org/10.1016/S0167-8396\(96\)00057-X](https://doi.org/10.1016/S0167-8396(96)00057-X).
- 919
- 920
- 921 [31] A. Bobenko, P. Schröder, Discrete Willmore Flow, in: Proceedings of the third Eurographics symposium on Geometry processing, Eurographics Association, 2005, p. 101.
- 922
- 923
- 924 [32] C. Douthe, R. Mesnil, H. Orts, O. Baverel, Isoradial meshes: covering elastic gridshells with planar facets, Automation in Construction 83 (2017) 222–236. [doi:https://doi.org/10.1016/j.autcon.2017.08.015](https://doi.org/10.1016/j.autcon.2017.08.015).
- 925
- 926
- 927
- 928 [33] Z. Soyuçok, *Infinitesimal deformations of surfaces and the stress distribution on some membranes under constant inner pressure*, International Journal of Engineering Science 34 (9) (1996) 993–
- 929
- 930
- 931
- 932
- 933
- 934
- 935
- 936
- 937
- 938
- 939
- 940
- 941
- 942
- 943
- 944
- 945
- 946
- 947
- [34] S. Timoshenko, J. Gere, *Theory of elastic stability*, McGraw-Hill, New York, 1961.
- [35] D. P. Billington, *The Tower and the Bridge: the new art of structural engineering*, Princeton University Press, 1985.
- [36] G. Elber, M.-S. Kim, The bisector surface of rational space curves, ACM Transactions on Graphics (TOG) 17 (1) (1998) 32–49. [doi:https://doi.org/10.1145/269799.269801](https://doi.org/10.1145/269799.269801).
- [37] S. Sechelmann, T. Rörig, A. Bobenko, Quasiisothermic mesh layout, in: *Advances in Architectural Geometry*, Springer, 2013, pp. 243–258. [doi:https://doi.org/10.1007/978-3-7091-1251-9\\_20](https://doi.org/10.1007/978-3-7091-1251-9_20).
- [38] A. Vaxman, C. Müller, O. Weber, Conformal mesh deformations with Möbius transformations, ACM Transactions on Graphics (TOG) 34 (4) (2015) 55. [doi:https://doi.org/10.1145/2766915](https://doi.org/10.1145/2766915).