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Coverage and Throughput Analysis at 60 GHz for Indoor WLAN with Indirect Paths

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Abstract—The 60 GHz frequency band enables the combination of high bandwidth free of interference and very high throughput WLANs such as 802.11ad, 802.11ay and maybe 5G. Propagation loss in millimeter-wave band may be a strong limitation to deployment and practical usage, in particular in non-line of sight. For this purpose, this paper presents 60 GHz channel sounding and throughput measurement results in an indoor residential environment. The presented results are focused on non-direct multipath characteristics that could be potentially used by smart antenna solution to extend 60 GHz communications in non-line of sight.

Index Terms—60 GHz, indoor propagation, non-direct paths, path loss.

I. INTRODUCTION

Due to the rapid growth of wireless communications with increasing throughput and bandwidth, the 2.4 and 5 GHz unlicensed spectrum might be congested in a short future. The 60 GHz frequency band has regain strong interest thanks to lower cost of millimeter-wave components and the wide bandwidth available, 59-66 GHz for example in Europe. The new high end smartphones are also expected to embed the current 802.11ad standard.

Millimeter waves are promising for very high throughput WLANs, but there is still a technological issue concerning their ability to ensure non line of sight (NLOS) communications, as shadowing loss due to obstacles like walls, furniture or people might be too high. A lot of works have characterized the effects of the direct path obstruction in line of sight situations (LOS) [1], [2] but fewer works have paid attention to purely non-line of sight propagation [3]-[7]. NLOS results rely on ray model simulation [2], [8], [9] rather than on radio measurements. The IEEE 802.11ad/ay channel models [1] consider for example an obstructed line of sight for a living room scenario resulting in an additional path loss from 8 to 12 dB compared to LOS propagation. Office or lab environments are also mostly considered [2], [3], [6], [7], [9], [10] and more rarely indoor residential [4], [5]. Measurement results reveal for example the very high transmission loss through concrete walls or wooden

materials [7], [11] with up to 15 dB for wooden doors [5], [7].

The advances in smart antenna technologies and Massive MIMO solutions could break this limitation. Such solutions are full part of the future 5G radio and also 802.11ay standard currently under progress. For 802.11ad/ay, transmit and receive beamforming or beam steering enables transmitting and receiving antennas to turn their beam towards the optimal direction in term of link budget.

In this paper, we present a 60 GHz channel sounding measurement campaign performed in a typical home environment. The objective of this work is to assess indirect propagation path level that could be exploited by smart antenna solutions in order to provide NLOS coverage. The rest of this paper is organized as follows: Section II describes the measurement environment and the experimental setup. In Section III, the path loss characteristics and statistical results about indirect paths are analyzed. To complete the analysis, some throughput and coverage results obtained with current 802.11ad products are also presented. Finally, conclusions are drawn in Section IV.

II. EXPERIMENTAL SETUP AND SCENARIO

All the measurements analyzed in this paper have been carried out in a typical multi-room residential environment (6.49 m x 11.7 m x 2.6 m). The channel sounding is based on a vector network analyzer (VNA), extended to 60 GHz using up and down converters developed on our own with standard components. The following paragraphs detail the measurement setup and scenario.

A. Experimental Setup

The measurement system is shown in Fig. 1 and Fig. 2. It is composed of the transmitting (Tx) and receiving (Rx) antennas that are both sectoral vertically polarized horn antennas. The Tx antenna has a 120° 6 dB beam width in both E and H planes (Orange Labs conception), while the Rx antenna is more directive with a 20° aperture (Flann Model 25240-20). Their gain is around 7.3 dBi and 19.5 dBi respectively.

The VNA measures the S21 parameter over 2048 sub-carriers sequentially with 1 MHz frequency spacing and a 60 GHz starting frequency. Hence, a 2.047 GHz wideband is considered for further multipath analysis. It provides also more accurate average path loss estimations thanks to reduced small-scale fading compared to single carrier measurements. The large maximum delay we are able to measure (1 μ s) allows estimating the noise level as measured delays above 100 ns in our environment are nonphysical and correspond only to noise or measurement impairments. The VNA works with an intermediate frequency around 15 GHz. External up and down converters, using standard components such as multipliers, mixer and amplifiers, have been developed and added in order to transpose the signals around the expected frequencies. The 120° Tx antenna is connected to the VNA up/down converter through a 25-meter low loss (12 dB) coaxial cable, while the 20° Rx antenna is connected to the VNA up/down converter via a short cable (2 m). The transmitted power is 13 dBm at the 120° Tx antenna input, and a 20 dB low noise amplifier around 60 GHz is directly used after the 20° Rx antenna. The frequency response of all these components is measured periodically per back to back measurement 2 times per measurement day to correct temperature effects which are then removed from the raw data. Once processed, the obtained data lead to the results presented in Section III.

A laptop commands the VNA and the rotating arm controller for the 20° Rx antenna, by 6° azimuth steps around its axis. It is also used to collect the measured data. The elevation angle of the Rx antenna can be manually adjusted through a 3-way ball joint: we have considered 0°, 10°, 20°, 30° and 40° elevation angles (in direction of the ceiling).

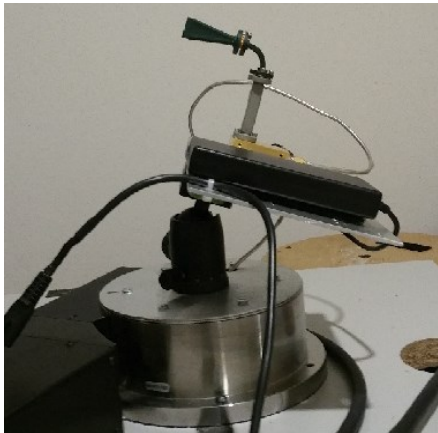


Fig. 1. 20° Rx antenna, 3-way ball joint and rotating arm.

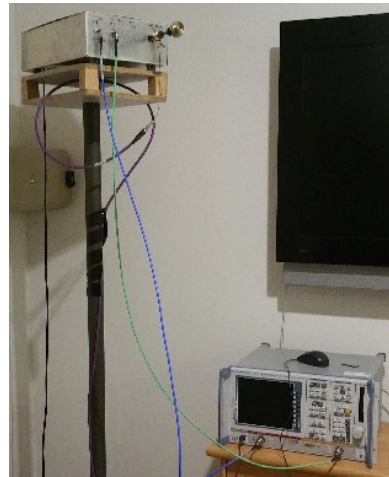


Fig. 2. 120° Tx antenna, up/down converter and VNA.

B. Measurement Scenario

On the transmitter side, one position has been chosen (T1) in the corner of the living room. The Tx antenna height is around 1.97 m, its azimuth points towards the main diagonal of the room without tilt. We have selected this Tx location in order to have most of the room in LOS, and in height for the sake of limiting human shadowing. In a practical home deployment, it is easier to have Ethernet connection near walls or corner walls than under the ceiling center contrary to office or hot spot environments. On the receiver side, 17 positions are chosen inside the apartment and 4 outside in a nearby corridor but with a strong load bearing wall separation with a closed wooden door. The Rx antenna height is equal to 1.31 m for all the 21 Rx positions. All measurements have been made in an empty environment (no people), with typical furniture (tables, chairs, TV screens, kitchen equipment, wooden cabinets) and closed wooden doors. Fig. 3 displays the Tx and Rx locations as well as the various building materials (doors, plasterboard, and concrete walls in dashed lines). Fig. 4 displays an example of measurement result in NLOS (precisely at R2, in Fig. 3) with a direct path level 10 dB lower than other non-direct paths coming from the living room. The azimuths 0° and 180° correspond respectively to the South and North.

III. CHANNEL SOUNDING RESULTS

The measurements have been processed in order to compare the path loss of the direct and indirect paths. The results are detailed in the following paragraphs. Some 802.11ad throughput measurements are also presented to complete the analysis.

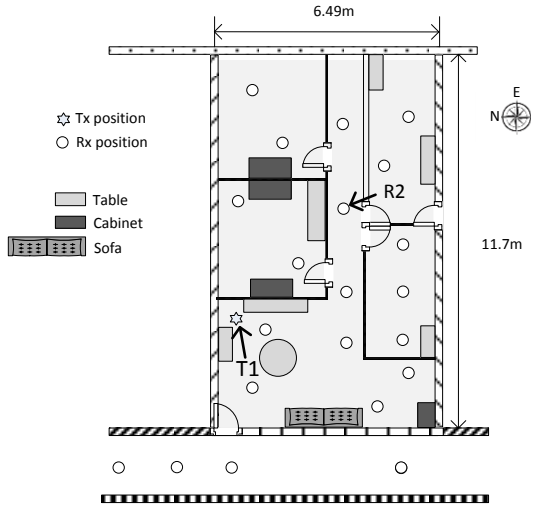


Fig. 3. Floor plan and measurement locations.

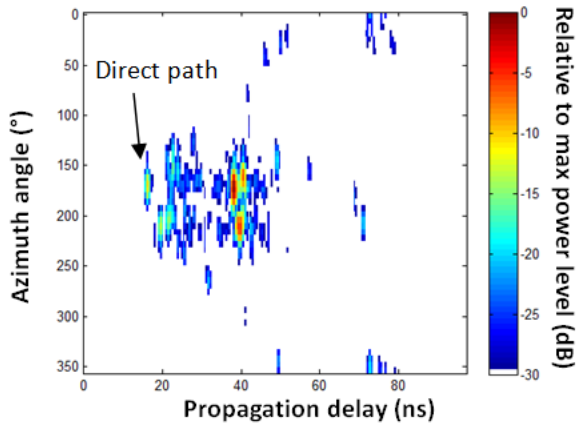


Fig. 4. Example of spatio-temporal results (at R2).

A. Path Loss Modeling

Based on the Tx and Rx locations, the direction (in terms of azimuth and elevation angles) of the direct path between the Tx and a given Rx can be computed. Then, the average path loss (over the 2.047 GHz bandwidth) corresponding to this direction can be extracted from the measurements. As the direct path is not necessarily the optimal pointing direction in NLOS, we have also searched for another direction corresponding to the highest maximum of received power in function of azimuth and elevation of the Rx antenna. Then, for each Rx location, we have compared the path loss values of these directions. A path loss model over distance [1], described by the following formula, has been also adjusted:

$$PL(d) \text{ [dB]} = PL_0(d_0) + 10n\log_{10}(d/d_0) + X_\sigma \quad (1)$$

where $PL(d)$ is the path loss value at a Tx-Rx distance equals to d , $PL_0(d_0)$ is the path loss at a

reference distance d_0 (here $d_0 = 1$ m), n is the path loss exponent that depends on the environment and characterizes the increase of the path loss with distance. X_σ reflects the other variations of the path loss caused by shadowing effects and multi-path propagation. It is a zero-mean Gaussian random variable with σ dB standard deviation. The parameters of this model (Table I), which takes into account the Tx and Rx antennas gain, are obtained by performing linear regressions between the measured path loss and the log-distance for the various cases. Fig. 5 displays the free space path loss (reference) and the established log-distance path loss models in LOS and NLOS. Table I gives the model parameters $PL_0(d_0)$, n , and σ defined above. In LOS, we get 10 to 26 dB and 16.4 dB average additional path loss for the best non-direct path compared to direct path loss. This is a bit higher than predicted by the 802.11ad living room channel model (8 to 12 dB, [1]). This difference tends to decrease a lot with increasing d . In NLOS, we get an average around 32.4 dB additional path loss compared to free space for the direct path. A detailed analysis of the angular power spectrums shows that the direct path is not in most cases the best one excepted when the direct path crosses only one plasterboard dividing wall (without any blocking furniture). Compared to the direct path direction, in NLOS, the best Rx antenna orientation towards non direct paths can benefit from 3 to 17 dB higher received power and 5 dB on average (discarding 2 Rx points outside the Tx antenna main lobe).

The NLOS results show a very high shadowing standard deviation and so, that a log-distance path loss model is not very accurate. Table II gives more details on the average transmission loss induced by the crossed walls, doors or furniture along the direct path.

The RMS delay spread has been also computed for the impulse responses (Figs. 6 and 7) associated to both Rx antenna orientations: towards Tx in direct line or towards the best non-direct path. A 20 dB dynamic has been considered between the maximum level of the impulse response and the noise floor to compute the RMS delay spread. A Hanning window has been applied in the frequency domain to reduce the side lobes level. Fig. 6 displays the RMS delay spread in function of the path loss and reveals increasing delay spread with increasing path loss in NLOS. In LOS, the RMS delay spread stays below 4 ns versus 15.8 ns in NLOS. An 802.11ad single carrier solution uses 1.76 Gsym/s and thus may suffer from high inter-symbol interference especially in NLOS, as the 802.11ad standard allows equalization up to 36 ns channel delay based on the guard interval duration for channel estimation. Much narrower antenna beams than the ones of the used antennas would be needed to reduce the delay spread in NLOS, for single carrier 60 GHz or OFDM physical layer, would have to be privileged for NLOS.

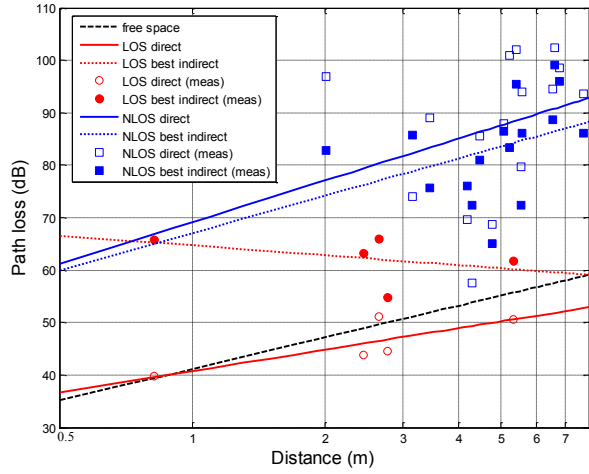


Fig. 5. 802.11ad path loss in LOS and NLOS.

TABLE I. PARAMETERS OF THE PROPOSED PATH LOSS MODELS

Model	PL_0 (dB)	n	σ (dB)
LOS – direct path	40.85	1.35	3.29
LOS – best non-direct path	64.68	-0.62	4.82
NLOS – direct path	69.15	2.64	13.49
NLOS – best non-direct path	67.1	2.36	9.01

TABLE II. TRANSMISSION LOSS FOR SOME OBSTACLES

Material	Thickness (cm)	Transmission Loss (dB)
plasterboard	7	9.8
concrete	24	40.8
wooden door	4	32.2
wooden cabinet + plasterboard	47+7	49.6

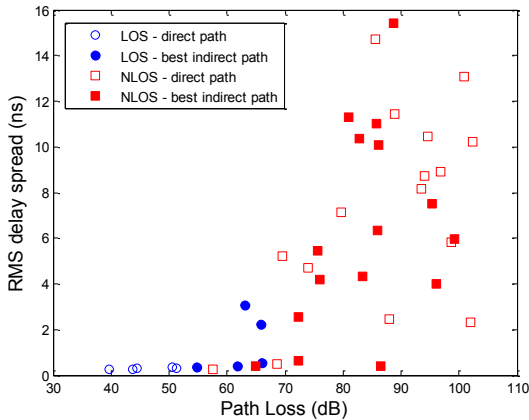


Fig. 6. RMS delay spread versus path loss.

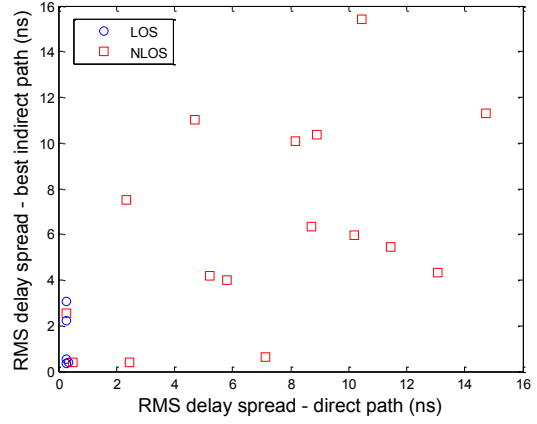


Fig. 7. RMS delay spread of the direct path versus the best indirect path.

B. 802.11ad Throughput Measurements

To complete the analysis, two devices have been equipped with Qualcomm 802.11ad mini PCIe cards, based on the Sparrow chipset, working on a single 802.11ad channel. The first one is an access point (AP), and the other one is a laptop acting as client device. This commercial solution relies on a single carrier modulation with Tx and Rx beamforming, mainly in the azimuth plane. A 12 printed elements rectangular antenna array (17 mm x 7 mm surface) has been used at both Tx and Rx sides. The EIRP was estimated around 26 dBm. Fig. 8 and Fig. 9 display respectively an example of coverage area and the 30 s averaged measured TCP throughputs (with iperf tool) between the AP (located at 1.86 m height, with 5 AP positions considered in the apartment) and the client device (at 1.2 m height) without any people presence. 8 azimuth angles of the client device have been tested, by 45° step, and the minimum, maximum and average throughput values have been extracted. In the living room, the throughput in LOS varies between 1.6 and 2.5 Gbps. In NLOS, as shown in Fig. 9, the throughput varies between 0 and 1.6 Gbps. No communication was possible in NLOS with a concrete wall or with plasterboard and blocking wooden cabinet crossing the direct path. In LOS, the system proved also quite good robustness in the random presence of up to 4 people, with a throughput generally greater than 1 Gbps. In NLOS, however it was no more possible to guarantee communications in the presence of people.

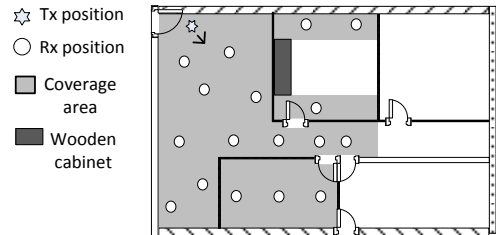


Fig. 8. Example of 802.11ad coverage area (no people).

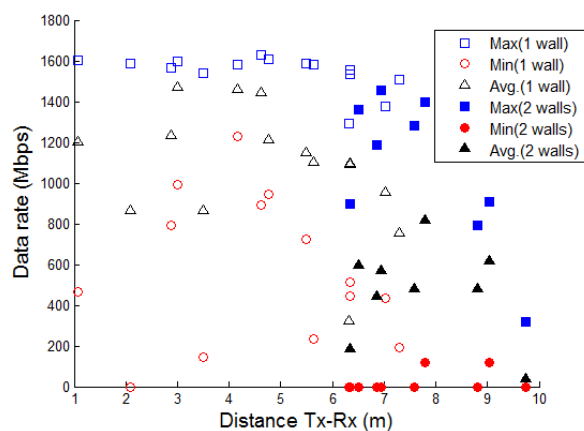


Fig. 9. 802.11ad TCP throughput in NLOS.

Based on our path loss measurements, we can infer that the tested 802.11ad equipment allows around 65-70 dB of path loss. In the case of blockage by a load bearing wall or by a wooden cabinet close to a plasterboard dividing wall, at least 25 dB are missing in the link budget to maintain communications. We expect the future 802.11ay standard improving NLOS coverage in the nearby rooms surrounding the AP as multiple antenna arrays (like Massive MIMO) would have a great benefit on the link budget. For example, 256 elements antenna array for both AP and client device would provide in theory 26.5 dB more antenna gain compared to the 12 elements antenna array tested Qualcomm equipment, but would require approximately a 25 cm² surface for planar antenna arrays. This may be sufficient to get more robust NLOS communications, at least for the less stringent blockage configurations such as one plasterboard dividing wall with wooden furniture or one plasterboard dividing wall with moving people.

IV. CONCLUSION

Herein we studied NLOS 60 GHz radio coverage based on radio and throughput measurements. In indoor residential environment, we showed that the non-direct paths have a significant level and could be exploited to extend mm-wave communications in the neighboring rooms around the access point. Future solutions like 802.11ay Massive MIMO seem well suited to improve the link budget in NLOS. Further works and measurements in various environments are needed to have more statistical results.

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