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An analytical solution to assess the *SH* seismoelectric response of the vadose zone

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SUMMARY

We derive an analytical solution of the seismoelectric conversions generated in the vadose zone, when this region is crossed by a pure shear horizontal (*SH*) wave. Seismoelectric conversions are induced by electrokinetic effects linked to relative motions between fluid and porous media. The considered model assumes a 1D soil constituted by a single layer on top of a half-space in contact at the water table, and a shearing force located at the earth's surface as the wave source. The water table is an interface expected to induce a seismoelectric interfacial response (IR). The top layer represents a porous rock in which porous space is partially saturated by water and air, while the half-space is completely saturated with water, representing the saturated zone. The analytical expressions for the coseismic fields and the interface responses, both electric and magnetic, are derived by solving Pride's equations with proper boundary conditions. An approximate analytical expression of the solution is also obtained, which is very simple and applicable in a fairly broad set of situations. Hypothetical scenarios are proposed to study and analyse the dependence of the electromagnetic fields on various parameters of the medium. An analysis of the approximate solution is also made together with a comparison to the exact solution. The main result of the present analysis is that the amplitude of the interface response generated at the water table is found to be proportional to the jump in the electric current density, which in turn depends on the saturation contrast, poro-mechanical and electrical properties of the medium and on the amplitude of the solid displacement produced by the source. This result is in agreement with the one numerically obtained by the authors, which has been published in a recent work. We also predict the existence of an interface response located at the surface, and that the electric interface response is several orders of magnitude bigger than the electric coseismic field, whereas it is the opposite using compressional waves as shown by theoretical and experimental results. This fact should encourage the performance of field and laboratory tests to check the viability of SHTE seismoelectrics as a near surface prospecting/monitoring tool.

Key words: Electrical properties; Hydrogeophysics; Permeability and porosity; Wave propagation.

1 INTRODUCTION

The seminal work of Pride (1994) completed previous efforts (Frenkel 1944) to build a solid theory to explain both the already observed conversions of seismic waves travelling in the shallow subsurface of the Earth into electromagnetic energy (Ivanov 1939; Long & Rivers 1975; Thompson & Gist 1993) and also the conversion of electromagnetic signals into travelling seismic waves. It encouraged several authors to make further studies, trying to appropriately characterize the different signals predicted theoretically and detected both in laboratories and in the

field. Among them, we can mention the work of Pride & Haartsen (1996), who derived Green's functions for electroseismics/seismoelectrics for solid and fluid displacements and the electric field; this work was extended by Gao & Hu (2010), who developed the Green's function for the magnetic field and considered moment tensors as sources. Haartsen & Pride (1997) used a global matrix method to study the so called interface response (IR) generated at interfaces of a layered Earth illuminated by electromagnetic and seismic point sources. They showed that the electromagnetic IR generated by an impinging compressional seismic wave on the interface between two layers has a pattern which in the near field can be associated with the one of a vertical electric dipole located at the interface, right beneath the seismic source. Again, Hu & Gao (2011) extended this algorithm and applied it to analyse the electromagnetic fields produced by a finite fault rupture. They observed two types of electric fields: the coseismic electric field (E-Cos), that is, the electromagnetic signal supported within the seismic wave, travelling at its speed and the post-seismic decaying variation. Garambois & Dietrich (2001), in a work where seismoelectric field signals were analysed, developed transfer functions showing that in the lower frequency band the E-Cos is proportional to the grain acceleration. They also showed that the particle velocity in a seismic shear wave and the magnetic field are related in the same way. Similarly, Pride & Garambois (2005) proved with numerical studies that compressional or shear waves crossing an interface in which any of the transport properties or elastic moduli change, give rise to electromagnetic disturbances that could be measured at the surface. Moreover, they observed that the amplitude of the converted electric field at the interface can be drastically increased if there is a thin layer of third material present at the interface, and suggested that this feature could be exploited in hydrological applications. We mention here that in Pride's theory, and therefore in all the works previously mentioned, the amplitudes of the coseismic electromagnetic signals are controlled by the properties of the porous material (the formation factor) and by the properties of the pore fluid/solid interface (the zeta potential). In the alternative seismoelectric theory proposed by Revil *et al.* (2003, 2007), the role of the latter is played by the excess charge per unit pore volume.

Seismoelectrics and electroseismics, which aim at combining the sensitivity of the electric methods to the fluid content with the spatial resolution of the seismic method, have been used to investigate hydrogeological reservoirs (Dupuis *et al.* 2007; Dupuis *et al.* 2009; Schakel *et al.* 2012; Warden *et al.* 2013), especially in arid environments (Valuri *et al.* 2012), and hydrocarbon reservoirs (Thompson *et al.* 2005; Hornbostel & Thompson 2007; Hu *et al.* 2007; Thompson *et al.* 2007; Zyserman *et al.* 2012; Guan *et al.* 2013; Zyserman *et al.* 2015). It has been shown that seismic compressional waves generate IRs with amplitudes smaller than those of the coseismic signals, which makes the former difficult to be measured. As detailed in Jouniaux & Zyserman (2016), several authors have studied how to deal with this problem. For example, Dupuis *et al.* (2007) proposed to measure the electric field within a borehole, below the interface of interest and Haines *et al.* (2007) suggested to implement off-line geometry surveys as a means of separating the IR signal from the coseismic and source related ones. Quite recently, Peng *et al.* (2017) performed a laboratory study of IRs produced by sandstone targets with different geometries, aiming at characterizing the amplitudes of the IRs produced by incident waves and their reflections at multiple interfaces, and to study the polarity reversals for different setups.

Focusing on the signals processing, Kepic & Rosid (2004) proposed to create virtual 'super gathers' as a way to obtain a dense spatial sampling, necessary to apply Radon transform filters, also called $(\tau - p)$ where τ is the intercept time of an event and p the apparent slowness, or frequency-wavenumber $(f - k)$ filters, which can be used to isolate the IRs as Strahser *et al.* (2007) have shown. More recently, Warden *et al.* (2012), aiming at better preserving the amplitude of the IRs, developed a new filtering strategy based on the fast discrete curvelet transform, getting better results than when using the Radon transform or $(f - k)$ filtering.

Most of the mentioned works were developed considering a single saturating fluid at full saturation. The effect of moisture on seismoelectrics was studied by Parkhomenko & Tszé-San (1964), Parkhomenko & Gaskarov (1971), Gaskarov & Parkhomenko (1974) and later by Ageeva *et al.* (1999), at various frequencies. However, it was not possible to deduce any transfer function as a function of water saturation. It was only in the few last years that the attempts to introduce a quantitative effect of the partial saturation in seismoelectrics/electroseismics have been undertaken (Warden *et al.* 2013; Bordes *et al.* 2015; Jardani & Revil 2015; Zyserman *et al.* 2015). Bordes *et al.* (2015) extended the original dynamic transfer function between the coseismic seismoelectric signal and the acceleration based on the works from Pride (1994) and Pride & Haartsen (1996) to partially saturated states. The transfer function was measured in sand during imbibition and drainage experiments by Holzhauser *et al.* (2016). These authors showed that the behaviour of this transfer function is complex: it is not monotonous with the water saturation, and a switch in polarity was observed at a critical saturation. This behaviour was modelled by taking into account an electrokinetic coupling dependent on the water saturation showing a non-monotonous behaviour, and using an effective fluid modulus obtained from a power law of the saturation or based on the Reuss average.

Turning now the reader's attention to the choice of the seismic source, on the one hand, we have proved in a previous work (Zyserman *et al.* 2017a) that the signal-to-noise ratio can be higher when using a shear wave source than when using a compressional source, and on the other hand, although up to now shear wave sources have not been tested in seismoelectric field studies, they have been employed in several works aiming at characterizing the shallow subsurface. Konstantaki *et al.* (2013) performed a detailed study of how a landfill can be monitored via seismic interferometry, using SH-wave sources and receivers. Later, Konstantaki *et al.* (2015) characterized a heterogeneous landfill using seismic and electric resistivity data. For the seismic analysis they used S waves, generated by a horizontal vibrator with a frequency range of 20–300 Hz. We can also mention the work by Krawczyk *et al.* (2012), who investigated the roof region of a salt diapir in Hamburg, employing a horizontal vibrator as a source, and recorded the seismic responses with SH-geophones; in Krawczyk *et al.* (2013) the authors describe several case studies of urban geophysics employing the same source-receiver system as in the previous mentioned work and in Pugin *et al.* (2013) two examples of multicomponent shallow S-wave reflection profiling were presented. Quite recently, Beilecke *et al.* (2016) carried out high resolution, near surface, shear wave reflection seismic measurements to investigate the fault structure in a CO₂ deposition site in

Australia. We mention, finally, the works of Stucchi *et al.* (2017) and Comina *et al.* (2017), integrating *SH*-wave measurements with *P* wave and Love-wave, respectively, to investigate different geological systems to assess landslide risks. The mentioned works show that there is evidence of successful usage of *SH* waves to investigate the subsoil.

We analytically show in this work – confirming numerical results mentioned above – that the use of SHTE seismoelectrics could overcome also the difficulties in measuring the IRs, because the electric coseismic signal has a remarkably smaller amplitude than that of the IR. We recall here that SHTE stands for the coupling between shear horizontal seismic waves and transverse electric fields; the other mode is the so called PSVTM, denoting the coupling of *P*- and *SV*- seismic waves with the transverse magnetic mode (Haartsen & Pride 1997; Zyserman *et al.* 2010, 2012).

Recently Zyserman *et al.* (2017a) analysed the seismoelectric conversions generated in the vadose zone when this region is crossed by a pure *SH* wave, instead of a pure compressional *P*-wave as usually studied. With this choice better spatial resolution can be achieved, due to smaller wavelengths (Krawczyk *et al.* 2012; Konstantaki *et al.* 2013, 2015). Moreover, the numerical results showed that the seismoelectric conversions induced by a shear wave source yield an electric interfacial response of about three orders of magnitude larger than the coseismic signal amplitude, leading to a possible detection of the water table by seismoelectromagnetic measurements. In the present work, these seismoelectromagnetic conversions induced in the vadose zone are analytically derived for a simple 1D model involving a step-shaped saturation profile. We are able to identify, for both electric and magnetic fields, IRs at the surface and at the water table and also the coseismic signals above and below the water table. Moreover, we can identify how these signals depend on the soil properties in a clear and simple way. We start our work describing the rock physics models we employ for the effective soil properties, afterwards we introduce the 1D SHTE seismoelectric equations and we continue presenting the analytical solution. Then, we present an approximation to the obtained analytical solution, which is quite simple and applicable in a fairly broad set of situations, making it quite useful as an interpretation tool and to test numerical codes. Then, hypothetical examples are proposed in order to analyse the obtained expressions and a parametric study is performed to study the dependence of the electromagnetic fields on various physical parameters of the media. Finally, an analysis of the approximate solution is made, together with a comparison to the exact solution.

2 THEORETICAL BACKGROUND

2.1 Effective model parameters

We describe now the rock physics models employed to get the different necessary soil parameters. We consider three different materials building the solid matrix, namely sand, silt and clay, and we call f_{sand} , f_{silt} and f_{clay} their respective volume fractions; $f_{\text{sand}} + f_{\text{silt}} + f_{\text{clay}} = 1$. The mass density of the aggregate, ρ_s , is given by the volume weighted mean of the respective components mass densities:

$$\rho_s = f_{\text{sand}}\rho_{s,\text{sand}} + f_{\text{silt}}\rho_{s,\text{silt}} + f_{\text{clay}}\rho_{s,\text{clay}}. \quad (1)$$

For the effective shear and bulk moduli of the aggregate G_s and K_s , respectively, we use the Reuss lower bound (Mavko *et al.* 2009), calculated in terms of the components volume fractions, shear moduli and bulk moduli of the solid grains as:

$$G_s = \left(\frac{f_{\text{sand}}}{G_{s,\text{sand}}} + \frac{f_{\text{silt}}}{G_{s,\text{silt}}} + \frac{f_{\text{clay}}}{G_{s,\text{clay}}} \right)^{-1}, \quad K_s = \left(\frac{f_{\text{sand}}}{K_{s,\text{sand}}} + \frac{f_{\text{silt}}}{K_{s,\text{silt}}} + \frac{f_{\text{clay}}}{K_{s,\text{clay}}} \right)^{-1}. \quad (2)$$

We use Walton model (Mavko *et al.* 2009) to estimate the solid matrix shear modulus G ; this choice is appropriate when unconsolidated soils are considered (Pride 2005; Bordes *et al.* 2015; Dupuy *et al.* 2016). It reads

$$G = \frac{1}{10} \left[\frac{3(1-\phi)^2 \hat{C}^2 P}{\pi B^2} \right], \quad \text{with } B = \frac{1}{4\pi} \left(\frac{1}{G_s} + \frac{1}{G_s + \lambda_c} \right). \quad (3)$$

In this equation, ϕ is the porosity, \hat{C} is the so called coordination number, and is related to the packing of the spheres building the solid aggregate, P is the hydrostatic pressure and λ_c is Lamé's coefficient of the effective grain material calculated as $\lambda_c = K_s - \frac{2}{3}G_s$. In this work we consider $\hat{C} = 9$ and $P = 101325$ Pa.

To deal with both saturated and partially saturated porous media within Pride's formulation for seismoelectrics, it is necessary to introduce appropriate effective properties. We perform here this task by following the same approach taken by Zyserman *et al.* (2012), Smeulders *et al.* (2013), Warden *et al.* (2013), Bordes *et al.* (2015) and Zyserman *et al.* (2015). For the effective fluid mass density, we use

$$\rho_f = \rho_w S_w + \rho_a (1 - S_w), \quad (4)$$

where ρ_w and ρ_a are the densities and S_w and $S_a = 1 - S_w$ are the saturation degrees of water and air, respectively. The bulk density ρ_b is computed as:

$$\rho_b = \phi \rho_f + (1 - \phi) \rho_s. \quad (5)$$

The effective viscosity is computed, following Teja & Rice (1981), in terms of the water viscosity η_w , air viscosity η_a and water saturation S_w using

$$\eta = \eta_a \left(\frac{\eta_w}{\eta_a} \right)^{S_w}. \quad (6)$$

Because in Biot's theory, shear stresses are decoupled from pore pressure and, hence, the shear modulus does not depend on the conditions of drainage, the shear modulus of the saturated rock matrix is assumed to be equal to G , the shear modulus of the dry matrix (Kümpel 1991).

On the other hand, we compute the absolute permeability as (Bear 1988):

$$\kappa = \frac{\eta_w K}{\rho_f g}, \quad (7)$$

where K is the hydraulic conductivity of the soil, and $g = 9.81 \text{ m s}^{-2}$ is the gravity acceleration.

In order to characterize the electrical conductivity of the effective fluid saturated solid matrix, we use the expression recently proposed by Warden *et al.* (2013), extending Pride's original formula (Pride 1994, eq. 242) to the realm of partially saturated media:

$$\sigma(S_w, \omega) = \frac{S_w^{\hat{n}}}{F} \sigma_w + \frac{2}{F} \frac{C_{em} + C_{os}(\omega)}{\Lambda}. \quad (8)$$

The first term in this equation is Archie's law for a partially saturated medium, where $F = \phi^{-\hat{m}}$ stands for the formation factor, \hat{m} being the cementation exponent and \hat{n} the Archie's saturation exponent. The electrical conductivity of water containing sodium chloride can be computed as $\sigma_w = \sum_{l=\text{Na}^+, \text{Cl}^-} (ez_l)^2 b_l N_l$, where $e = 1.6 \times 10^{-19} \text{ C}$ is the electron electric charge, and z_l is the ions' valence, taken to be one for both species. The ions' mobility b_l and concentration N_l (depending on the salinity C_0) are calculated following Carcione *et al.* (2003). The second term in eq. (8) accounts for the surface conductivity; within this expression, as Pride (1994) stated, the factor C_{em} is the excess conductance associated with the electromigration of double layer ions; $C_{os}(\omega)$ is the frequency-dependent electro-osmotic conductance due to electrically induced streaming of the excess double-layer ions. Finally, Λ is a fundamental porous material parameter related to the volume-to-surface ratio, and can be obtained from the condition $(\xi \alpha_\infty \kappa) / (\varphi \Lambda^2) = 1$ (Johnson *et al.* 1987; Pride 1994); the pore-geometry dependent factor ξ lies in the range $4 \leq \xi \leq 8$ (Pride 1994) and in this work we consider $\xi = 8$, which corresponds to a network of variable-radii tubes; $\alpha_\infty = \varphi F$ is the tortuosity. We remark here that, as in Brovelli *et al.* (2005) and Warden *et al.* (2013), the surface conductivity is assumed to be independent of water saturation, because under realistic saturation ranges (residual water saturation $S_{wr} \geq 0.1$) the thickness of the wetting phase layer on the pore surface is always larger than the Debye length. This also means that all fluid-related properties involved in the calculation of the surface conductivity and of the electrokinetic coupling – see below – are just those of water. Note that another approach, with a water saturation-dependent surface conductivity can also be considered; however, it can be observed that it does not affect significantly the seismoelectromagnetic conversions for the considered soils (Zyserman *et al.* 2017b).

We propose for the effective fluid saturated media the following electrokinetic coupling, again following Warden *et al.* (2013) and Bordes *et al.* (2015):

$$L_0(S_w) = -\frac{\phi}{\alpha_\infty} \frac{\epsilon_w \zeta}{\eta_w} \left(1 - 2 \frac{d}{\Lambda} \right) S_w^{\hat{n}} \mathcal{C}(S_w). \quad (9)$$

In this equation ζ is the zeta potential, ϵ_w is the permittivity of water, d is the Debye length and $\mathcal{C}(S_w)$ is a function relating the streaming potential coefficient obtained under partial saturation conditions to the one corresponding to full saturation conditions. This streaming potential coefficient corresponds to the electric potential difference over the pressure difference at the origin of this electrical signal. If the fluid flow does not induce an electric signal, the streaming potential coefficient is zero, and then the electrokinetic coupling L_0 is also zero, and no seismo-electromagnetic conversions are possible. For a tutorial on these effects see Jouniaux & Ishido (2012). In eq. (9), we use the following relation, which was experimentally derived from laboratory measurements of the streaming potential coefficient in partially saturated sands and displays a non-monotonic dependence with water saturation (Allègre *et al.* 2010, 2012, 2014, 2015; Fiorentino *et al.* 2017):

$$\mathcal{C}(S_w) = \left(\frac{S_w - S_{wr}}{1 - S_{wr}} \right) \left[1 + 32 \left[1 - \left(\frac{S_w - S_{wr}}{1 - S_{wr}} \right) \right]^{0.4} \right], \quad S_{wr} = 0.20. \quad (10)$$

For water saturations below S_{wr} , $\mathcal{C}(S_w)$ is set to zero. Others different available models for $\mathcal{C}(S_w)$ have already been discussed by ourselves and other authors (Strahser *et al.* 2011) as well, see Zyserman *et al.* (2017a), Perrier & Morat (2000), Allègre *et al.* (2010). We compute the zeta potential as $\zeta = 0.008 + 0.026 \log_{10}(C_0)$ (Pride & Morgan 1991), and consider a fixed salt concentration $C_0 = 5 \times 10^{-3} \text{ mol L}^{-1}$ (Table 1), such that $\zeta = -52 \text{ mV}$ throughout this work.

2.2 SHTE seismoelectric equations

We model the electromagnetic response to seismic waves generated by a shear source using the equations derived by Pride (1994). In particular, we assume that the source of the system is a shearing force located at the Earth's surface, parallel to the x -axis acting on a horizontal infinite plane (see Fig. 1). Under these assumptions both the solid and fluid phases can only undergo displacements in the x -direction, with amplitudes depending only on depth z ; no compressional waves can arise in this model and spherical spreading and Fresnel zone effects are not accounted

Table 1. Values of model parameters used in the present study. Those not shown in this table, e.g. effective fluid viscosity η , effective bulk conductivity σ , inertial coupling coefficient g_0 , can be obtained from the present ones using the formulae described in the ‘Theoretical background’ section. Values marked with a* symbol correspond to a silt loam; the constituents fractions are chosen according to the USDA soil texture classification triangle (U.S. Soil Conservation Service 1987), the hydraulic parameters are given by Carsel & Parrish (1998). The vacuum permittivity is taken to be $\epsilon_0 = 8.85 \times 10^{-12} \text{ C}^2 \text{ N}^{-1} \text{ m}^{-2}$.

Model parameters			
\hat{m}	1.35	$\rho_{s, \text{ sand}} \text{ (kg m}^{-3}\text{)}$	2600
\hat{n}	1.85	$\rho_{s, \text{ silt}} \text{ (kg m}^{-3}\text{)}$	2600
$\hat{\phi}$	0.45*	$\rho_{s, \text{ clay}} \text{ (kg m}^{-3}\text{)}$	2580
$f_{\text{ sand}}$	0.3*	$\eta_w \text{ (Pa s)}$	1×10^{-3}
$f_{\text{ silt}}$	0.55*	$\rho_w \text{ (kg m}^{-3}\text{)}$	1027
$f_{\text{ clay}}$	0.15*	$\eta_a \text{ (Pa s)}$	1.81×10^{-5}
$K \text{ (cm day}^{-1}\text{)}$	10.8*	$\rho_a \text{ (kg m}^{-3}\text{)}$	1.2
$G_{\text{ sand}} \text{ (GPa)}$	45	$\epsilon_w \text{ (F m}^{-1}\text{)}$	$80 \epsilon_0$
$G_{\text{ silt}} \text{ (GPa)}$	45	$C_0 \text{ (mol L}^{-1}\text{)}$	5×10^{-3}
$G_{\text{ clay}} \text{ (GPa)}$	6.8	$T \text{ (K)}$	298
$K_{\text{ sand}} \text{ (GPa)}$	36		
$K_{\text{ silt}} \text{ (GPa)}$	36		
$K_{\text{ clay}} \text{ (GPa)}$	20.9		

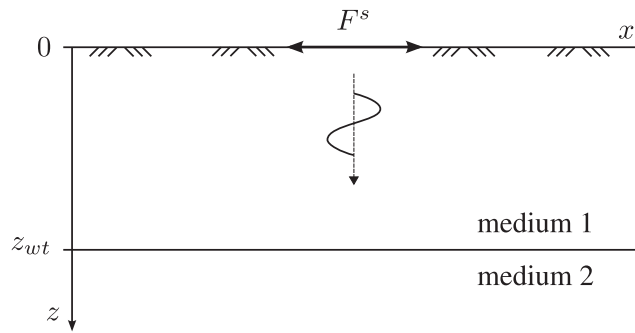


Figure 1. Schematic representation of the seismic shear plane wave travelling downwards in a two-layer 1D system. Medium 1 and medium 2 represent the vadose zone and the saturated zone, respectively, in contact at $z = z_{wt}$ (the depth of the water table).

for. If we also consider that the electroosmotic feedback can be neglected in Biot’s equations, as it is usually assumed for frequencies in the range of interest for shallow seismoelectric surveys (10 Hz to 1 kHz) (Hu & Liu 2002; Haines & Pride 2006), Pride’s equations can be written in the space-frequency domain, assuming an $e^{i\omega t}$ time dependence, as follows:

$$-\sigma E_x - \frac{\partial H_y}{\partial z} = i\omega \frac{\eta}{\kappa} L_0 u_{f,x} = j_v, \quad (11)$$

$$\frac{\partial E_x}{\partial z} + i\omega \mu_0 H_y = 0, \quad (12)$$

$$-\omega^2 \rho_b u_{s,x} - \omega^2 \rho_f u_{f,x} - G \frac{\partial^2 u_{s,x}}{\partial z^2} = F^s \delta(z), \quad (13)$$

$$-\omega^2 \rho_f u_{s,x} - \omega^2 g_0 u_{f,x} + i\omega \frac{\eta}{\kappa} u_{f,x} = 0. \quad (14)$$

In this system of equations, eqs (11) and (12) are Ampère–Maxwell’s equation and Faraday’s equation, respectively, – notice that the source of the electromagnetic fields arises due to the electrokinetic coupling –, while eqs (13) and (14) are Biot’s equations, being the right-hand side of eq. (13) the seismic source. E_x and H_y are the electric and magnetic fields, respectively, and $u_{s,x}$ and $u_{f,x}$ are the average solid and relative fluid displacements, respectively. From now on, for the sake of simplicity, we denote $u_s \equiv u_{s,x}$, $u_f \equiv u_{f,x}$, $E \equiv E_x$ and $H \equiv H_y$. The parameters in eqs (11)–(14) which remain to be mentioned are the vacuum magnetic permeability $\mu_0 = 4\pi \times 10^{-7} \text{ N A}^{-2}$ and the Biot’s low-frequency inertial coupling coefficient $g_0 = \alpha_\infty \rho_f \phi = F \rho_f$ (Biot 1956; Santos *et al.* 2004, 2005; Zyserman *et al.* 2012). The right-hand side in eq. (11) is the electric current density, source of the electromagnetic signals, and can be referred to as the viscous current density j_v , whereas σE is the conduction current. The right-hand side of eq. (13) is the shearing source acting on the surface (F^s is the shearing force per unit area).

3 DERIVATION OF THE ANALYTICAL SOLUTION

We describe here the geometry of the model, and derive the electric and magnetic fields induced by the shear wave propagation. Our analytical development of the fields allows to clearly individualize both the coseismic fields and the interfacial signals.

3.1 Electric current density

Let us consider a porous medium constituted by two regions, schematically depicted in Fig. 1 as a cut in the $x - z$ plane, being z the vertical axis (positive downwards) and x the horizontal axis. The origin of the z coordinates is located at the surface, and both regions are in contact at $z = z_{wt}$, the depth of the water table. The upper region ($0 < z < z_{wt}$) labelled as medium 1, represents a partially saturated porous rock. This space mimics the so called vadose zone where we have added the assumption that the water saturation remains constant with depth. The lower region ($z > z_{wt}$), labelled as medium 2, is completely saturated by water, and represents the saturated zone below the water table. Although the proposed model for water saturation distribution is not completely realistic, it is a simple way to describe the water content distribution near the water table, and has allowed us to derive an analytical solution to quantify the effect of the vadose zone on the electromagnetic response, as we describe below.

Biot's eqs (13) and (14) predict that the perturbation created by the shear source at $z = 0$ will propagate as a plane wave travelling downwards from the surface to the water table, as is schematically depicted in Fig. 1. Assuming the wave is harmonic with angular frequency ω and polarized in the x -axis direction, the solid and relative fluid displacements in medium 1, $u_{s,1}$ and $u_{f,1}$ will be given by:

$$u_{s,1} = U_{s,1}e^{i(\lambda_1 z + \omega t)} \text{ and } u_{f,1} = U_{f,1}e^{i(\lambda_1 z + \omega t)}, \quad (15)$$

where λ_1 is the wavenumber of medium 1:

$$\lambda_1 = \omega \left[\frac{1}{G} \left(\rho_{b,1} - \frac{\rho_{f,1}^2}{g_{0,1} - i\eta_1/(\kappa_1\omega)} \right) \right]^{1/2}, \quad (16)$$

being $U_{s,1}$ and $U_{f,1}$ the solid and relative fluid displacements at $z = 0$. From eq. (16) the S -wave velocity v_1 can be computed as $v_1 = \omega/|Re(\lambda_1)|$. We choose λ_1 such that $Re(\lambda_1) < 0$ in order to consider waves travelling downwards. The two last expressions are obtained by solving eqs (13) and (14) (see Appendix A). Following the same reasoning the solid and relative fluid displacements of medium 2 can be expressed as:

$$u_{s,2} = U_{s,2}e^{i(\lambda_2(z-z_{wt})+\omega t)} \text{ and } u_{f,2} = U_{f,2}e^{i(\lambda_2(z-z_{wt})+\omega t)}, \quad (17)$$

being λ_2 the wavenumber of medium 2 and $U_{s,2}$ and $U_{f,2}$ the corresponding displacements at the water table ($Re(\lambda_2) < 0$). Using these expressions in eq. (14), the following relations can be obtained:

$$u_{f,1} = -\frac{\rho_{f,1}}{g_{0,1} - \frac{i\eta_1}{\omega\kappa_1}}u_{s,1} \text{ and } u_{f,2} = -\frac{\rho_{f,2}}{g_{0,2} - \frac{i\eta_2}{\omega\kappa_2}}u_{s,2}. \quad (18)$$

If an SH wave impinges the interface, there will not occur mode conversions to P or SV waves. So, there will be only three waves to consider: incident SH , reflected SH and transmitted SH . Now, let us assume that the solid matrix of the porous medium is the same for both media (they only differ in fluid content). In this scenario, the shear modulus is the same for both media, and the reflection coefficient for the relative solid displacement in the case of normal incidence can be computed after Liu & Greenhalgh (2014) as follows:

$$R_{SH} = \frac{\lambda_1 - \lambda_2}{\lambda_1 + \lambda_2}. \quad (19)$$

Given that $\lambda_1 \simeq \lambda_2$, then $R_{SH} \simeq 0$, and there is no reflection from the interface. Then, the interface is virtually transparent, the wave will pass through it unaffected and the solid displacement at $z = z_{wt}$ will be the same for both incident and transmitted waves. This allows to write $u_{s,1}(z_{wt}) = u_{s,2}(z_{wt})$, which is equivalent to write $U_{s,1}e^{i\lambda_1 z_{wt}} = U_{s,2}$. Moreover, being the solid matrix the same for both regions, the hydraulic permeability will also be the same, so we can write $\kappa_1 = \kappa_2 = \kappa$.

The viscous current density j_v generated by the charges dragged by the relative fluid motion can be obtained for medium 1 as follows (see eq. 11):

$$j_{v,1} = i\omega\eta_1 \frac{L_{0,1}}{\kappa} u_{f,1} = \frac{\omega^2 \rho_{f,1} L_{0,1}}{1 + i\omega g_{0,1} \kappa \eta_1^{-1}} U_{s,1} e^{i(\lambda_1 z + \omega t)} = J_1^{wt} e^{i(\lambda_1(z-z_{wt})+\omega t)}, \quad (20)$$

where J_1^{wt} is the current density in medium 1 at the water table. In the same way we can obtain the current density in medium 2

$$j_{v,2} = i\omega\eta_2 \frac{L_{0,2}}{\kappa} u_{f,2} = \frac{\omega^2 \rho_{f,2} L_{0,2}}{1 + i\omega g_{0,2} \kappa \eta_2^{-1}} U_{s,2} e^{i(\lambda_2(z-z_{wt})+\omega t)} = J_2^{wt} e^{i(\lambda_2(z-z_{wt})+\omega t)}, \quad (21)$$

where J_2^{wt} is the current density in medium 2 at the water table. Note that, being the water content profile discontinuous at $z = z_{wt}$, the relative fluid solid displacement will be discontinuous, and so will be the current density. Note that the jump in the current density j_v is given by the difference between J_2^{wt} and J_1^{wt} . From eqs (20) and (21) this is

$$J_2^{wt} - J_1^{wt} = \left(\frac{\rho_{f,2} L_{0,2}}{1 + i\omega g_{0,2} \kappa \eta_2^{-1}} - \frac{\rho_{f,1} L_{0,1}}{1 + i\omega g_{0,1} \kappa \eta_1^{-1}} \right) \omega^2 U_{s,1}. \quad (22)$$

This difference gives a measure of the jump in the amplitude of the current density at the water table and its value is mainly controlled by the jump in water saturation, which in turn produces jumps in ρ_f and L_0 across the interface. Eq. (22) will be useful to interpret the electric and magnetic field behaviour in terms of the saturation contrast and the physical parameters of the medium.

3.2 Electric and magnetic fields

In this section, the influence of the current density as a source of electromagnetic fields is explored. Taking the first derivative with respect to z in eq. (12) and replacing the resulting expression in eq. (11), the following non-homogeneous Helmholtz equation is obtained for the electric field E :

$$\frac{d^2 E}{dz^2} + k^2 E = i\omega\mu_0 j_v, \tag{23}$$

being $k = \sqrt{-i\omega\mu_0\sigma}$ the wavenumber. Replacing eqs (20) and (21) in eq. (23) we get:

$$\frac{d^2 E}{dz^2} + k_1^2 E = i\omega\mu_0 J_1^{\text{wt}} e^{i\lambda_1(z-z_{\text{wt}})}, \quad 0 \leq z < z_{\text{wt}}, \tag{24}$$

$$\frac{d^2 E}{dz^2} + k_2^2 E = i\omega\mu_0 J_2^{\text{wt}} e^{i\lambda_2(z-z_{\text{wt}})}, \quad z > z_{\text{wt}}. \tag{25}$$

Calling \mathcal{L}_* the differential linear operator

$$\mathcal{L}_* = \frac{d^2}{dz^2} + k_*^2, \tag{26}$$

where * denotes the medium (1 or 2), and calling

$$\psi_*(z, \omega) = i\omega\mu_0 J_*^{\text{wt}} e^{i\lambda_*(z-z_{\text{wt}})}, \tag{27}$$

then, eq. (24) can be expressed as:

$$\mathcal{L}_1(E) = \psi_1(z, \omega); \tag{28}$$

it is straightforward to verify that

$$E_{1,p}(z, \omega) = -\frac{k_1^2 J_1^{\text{wt}} e^{i\lambda_1(z-z_{\text{wt}})}}{(k_1^2 - \lambda_1^2)\sigma_1} \tag{29}$$

is a particular solution to it. On the other hand, the general solution for the homogeneous equation $\mathcal{L}_1(E) = 0$ is given by:

$$E_{1,\text{hom}}(z, \omega) = A_1 e^{-ik_1 z} + B_1 e^{ik_1 z}, \tag{30}$$

where A_1 and B_1 are frequency-dependent complex coefficients. Then, the complete solution in medium 1 can be written by adding both homogeneous and particular solutions

$$E(z, \omega) = A_1 e^{-ik_1 z} + B_1 e^{ik_1 z} - \frac{k_1^2 J_1^{\text{wt}} e^{i\lambda_1(z-z_{\text{wt}})}}{(k_1^2 - \lambda_1^2)\sigma_1}, \quad 0 \leq z < z_{\text{wt}}. \tag{31}$$

Following the same procedure, the solution for the electric field in medium 2 can be obtained:

$$E(z, \omega) = A_2 e^{-ik_2 z} + B_2 e^{ik_2 z} - \frac{k_2^2 J_2^{\text{wt}} e^{i\lambda_2(z-z_{\text{wt}})}}{(k_2^2 - \lambda_2^2)\sigma_2}, \quad z > z_{\text{wt}}. \tag{32}$$

The magnetic field H can be derived from E using eq. (12), leading to

$$H(z, \omega) = \frac{k_1}{\omega\mu_0} A_1 e^{-ik_1 z} - \frac{k_1}{\omega\mu_0} B_1 e^{ik_1 z} - \frac{i\lambda_1 J_1^{\text{wt}} e^{i\lambda_1(z-z_{\text{wt}})}}{k_1^2 - \lambda_1^2}, \quad 0 \leq z < z_{\text{wt}}, \tag{33}$$

$$H(z, \omega) = \frac{k_2}{\omega\mu_0} A_2 e^{-ik_2 z} - \frac{k_2}{\omega\mu_0} B_2 e^{ik_2 z} - \frac{i\lambda_2 J_2^{\text{wt}} e^{i\lambda_2(z-z_{\text{wt}})}}{k_2^2 - \lambda_2^2}, \quad z > z_{\text{wt}}. \tag{34}$$

It is important to remark at this point that both fields are constituted by the superposition of two distinct responses. The first two terms in eqs (31)–(34), which are linked to the general solution of the homogeneous equation $\mathcal{L}_*(E) = 0$ are perturbations travelling at velocities given by $\omega/|Re(k)|$, that is, the velocity at which the electromagnetic signal travels in the soil. As it is well known, these perturbations are attributed to responses originated at interfaces between two distinct media, the so called IRs. The third terms, which are linked to the particular solutions of $\mathcal{L}_*(E) = \psi_*(z, \omega)$, can be clearly identified with the coseismic response, travelling at the same velocity $\omega/|Re(\lambda)|$ as the solid and fluid displacements. Observing the magnetic coseismic field (H-Cos), for example in eq. (33), it is clear that its origin is the current density J_1^{wt} arisen from the shearing motion of the rock matrix, which in turn drags the viscous fluid and therefore the electric charges in it. The origin of the E-Cos is, again as can be seen in the equations, the time derivative of the magnetic field, that is, the electric field is induced, through Faraday’s law, by the time variation of the magnetic field. This behaviour of the fields was conceptually discussed in, e.g. Haartsen & Pride (1997), Zyserman *et al.* (2015), Munch & Zyserman (2016). On the other hand, the situation is different for the coseismic electric field located within compressional waves, because it is created by accumulation and depletion of electrokinetic charge in regions of dilation and compression (Pride & Haartsen 1996; Haines *et al.* 2007; Jouniaux & Zyserman 2016). The unknown coefficients A_1, B_1, A_2 and B_2 should

be obtained by imposing conditions on the interface of both media at $z = z_{wt}$, and at the boundaries of the system ($z = 0$ and $z \rightarrow \infty$) as it is shown below. In order to avoid the divergence of the electromagnetic fields when $z \rightarrow \infty$, we set $B_2 = 0$ (for k_2 we choose the square root with negative imaginary part). If the Earth's surface is in contact with air, and if we assume that the air is an insulator, then the amplitude of the electric field must be constant for $z \leq 0$ in order to avoid its divergence when $z \rightarrow -\infty$, and in virtue of eq. (12) $H = 0$ for $z < 0$ (see Appendix B). Given that the magnetic field should be continuous at $z = 0$ (Appendix C shows the continuity of H at $z = 0$ and $z = z_{wt}$, see Fig. C1), we can write:

$$0 = A_1 - B_1 + \frac{\lambda_1 k_1 J_0}{(k_1^2 - \lambda_1^2)\sigma_1}, \tag{35}$$

where $J_0 = J_1^{wt} e^{-i\lambda_1 z_{wt}}$ is the current density at the surface. Both the electric and magnetic fields should be continuous at the water table (see Appendix C). The continuity condition for both fields at the water table can be, respectively, stated as follows:

$$A_1 e^{-ik_1 z_{wt}} + B_1 e^{ik_1 z_{wt}} - \frac{k_1^2 J_1^{wt}}{(k_1^2 - \lambda_1^2)\sigma_1} = A_2 e^{-ik_2 z_{wt}} - \frac{k_2^2 J_2^{wt}}{(k_2^2 - \lambda_2^2)\sigma_2}, \tag{36}$$

$$k_1(A_1 e^{-ik_1 z_{wt}} - B_1 e^{ik_1 z_{wt}}) + \frac{\lambda_1 k_1^2 J_1^{wt}}{(k_1^2 - \lambda_1^2)\sigma_1} = k_2 A_2 e^{-ik_2 z_{wt}} + \frac{\lambda_2 k_2^2 J_2^{wt}}{(k_2^2 - \lambda_2^2)\sigma_2}. \tag{37}$$

The system of eqs (35)–(37) completely determine the values for the three coefficients A_1 , B_1 and A_2 :

$$A_1 = -\frac{1}{2} \frac{\left[\frac{\lambda_1 k_1 (k_1 + k_2) e^{ik_1 z_{wt}} J_0}{(k_1^2 - \lambda_1^2)\sigma_1} - \frac{k_1^2 (k_2 + \lambda_1) J_1^{wt}}{(k_1^2 - \lambda_1^2)\sigma_1} + \frac{k_2^2 (k_2 + \lambda_2) J_2^{wt}}{(k_2^2 - \lambda_2^2)\sigma_2} \right]}{k_1 \sinh(ik_1 z_{wt}) + k_2 \cosh(ik_1 z_{wt})}, \tag{38}$$

$$B_1 = -\frac{1}{2} \frac{\left[\frac{\lambda_1 k_1 (k_1 - k_2) e^{-ik_1 z_{wt}} J_0}{(k_1^2 - \lambda_1^2)\sigma_1} - \frac{k_1^2 (k_2 + \lambda_1) J_1^{wt}}{(k_1^2 - \lambda_1^2)\sigma_1} + \frac{k_2^2 (k_2 + \lambda_2) J_2^{wt}}{(k_2^2 - \lambda_2^2)\sigma_2} \right]}{k_1 \sinh(ik_1 z_{wt}) + k_2 \cosh(ik_1 z_{wt})}, \tag{39}$$

$$A_2 = -\frac{\left[\frac{\lambda_1 k_1^2 J_0}{(k_1^2 - \lambda_1^2)\sigma_1} - \frac{k_1^2 (\lambda_1 \cosh(ik_1 z_{wt}) - k_1 \sinh(ik_1 z_{wt})) J_1^{wt}}{(k_1^2 - \lambda_1^2)\sigma_1} + \frac{k_2^2 (\lambda_2 \cosh(ik_1 z_{wt}) - k_1 \sinh(ik_1 z_{wt})) J_2^{wt}}{(k_2^2 - \lambda_2^2)\sigma_2} \right]}{k_1 \sinh(ik_1 z_{wt}) + k_2 \cosh(ik_1 z_{wt})} e^{ik_2 z_{wt}}, \tag{40}$$

with which we have the complete solutions for the electric and magnetic fields. Once the fields $E(z, \omega)$ and $H(z, \omega)$ are known for a given depth z below the surface, the time variation of these fields at that depth is obtained by the inverse Fourier transform. In the following section, hypothetical examples are proposed to analyse the electromagnetic responses predicted by the derived analytical solutions.

3.3 Approximate electromagnetic fields

Although the analytical expressions for the fields (eqs 31–34) seem to be quite simple, the involved coefficients A_1 , B_1 and A_2 are not. However, under reasonable assumptions it is possible to find a simple approximation to the solution suitable to perform an analysis of the SHTE response of the vadose zone.

Consider the ratio $(k_*/\lambda_*)^2$, given by eq. (16) and the definition of the wavenumber k_* :

$$\left(\frac{k_*}{\lambda_*}\right)^2 = \frac{i\mu\sigma_*G}{\rho_{b,*} - \frac{\rho_{*,*}^2}{g_{0,*} - i\eta_*/(\kappa\omega)}}. \tag{41}$$

We have computed this quotient for five different soil textures and for a wide range of seismic frequencies, observing that its absolute value is not bigger than 1×10^{-4} , so we can safely consider it as a very small quantity. By doing this, it is possible to make some approximations to simplify the expressions of the fields. Neglecting the ratio $(k_*/\lambda_*)^2$ against k_*/λ_* and assuming that $e^{\pm ik_1 z} \simeq 1$, which is a very good approximation when z is not higher than 10^2 m, then the electric and magnetic fields can be approximated by the following simplified expressions:

$$E(z, \omega) \simeq \frac{\omega\mu_0}{k_2} \left[\frac{J_0}{i\lambda_1} - \frac{J_1^{wt}}{i\lambda_1} + \frac{J_2^{wt}}{i\lambda_2} \right], \quad z \geq 0, \tag{42}$$

$$H(z, \omega) \simeq \frac{J_0}{i\lambda_1} - \frac{J_1^{wt} e^{i\lambda_1(z-z_{wt})}}{i\lambda_1}, \quad 0 \leq z < z_{wt}, \tag{43}$$

$$H(z, \omega) \simeq \left[\frac{J_0}{i\lambda_1} - \frac{J_1^{wt}}{i\lambda_1} + \frac{J_2^{wt}}{i\lambda_2} \right] - \frac{J_2^{wt} e^{i\lambda_2(z-z_{wt})}}{i\lambda_2}, \quad z > z_{wt}. \tag{44}$$

Note that these last expressions are simpler than those of the exact solutions, particularly the terms corresponding to the interface response; the complex coefficients A_1 , B_1 and A_2 appearing in the exact solution are no longer present in the approximate solution. The three terms between

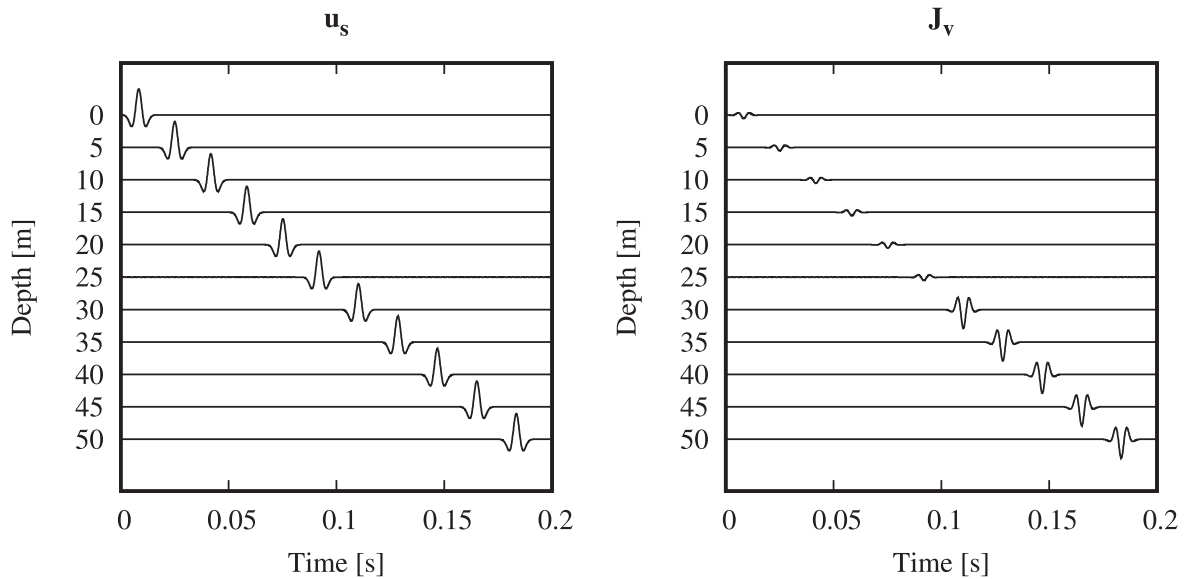


Figure 2. Time variation of the solid displacement (left) and electrical current density (right) registered at 11 receivers. The distance between receivers is 5 m. Above 25 m depth the water saturation is 0.32, and below 25 m depth the medium is fully saturated.

brackets in eqs (42) and (44) together with the first term in eq. (43) constitute the interfacial response of the approximate solution, meanwhile the last terms in eqs (43) and (44) give the coseismic response. In the following we analyse the electromagnetic responses predicted by both the exact and the approximate solutions. It is shown that the latter result is a very good approximation to the exact solution, and due to the simplicity of the mathematical expressions of the fields, they are convenient to analyse the seismoelectrical response of the vadose zone.

4 RESULTS AND DISCUSSION

We describe here the coseismic and interfacial response of the water table induced by the propagation of an *SH* wave produced by a shear source at the surface. We first show the displacement and electric current density, then the coseismic and interfacial signals of both the electric and magnetic fields. We analyse the amplitude of these electromagnetic conversions, and the effect produced by changes in water saturation, porosity, fluid viscosity and density.

4.1 Seismic waves and viscous current density analysis

To illustrate the field responses predicted by the derived analytical solution we compute, as explained before, the physical parameters given in 'Theoretical Background' section using the basic parameters listed in Table 1. Both the porous matrix properties and the effective properties of the media are computed for a silt loam, using the same soil parameters as in Zyserman *et al.* (2017a). The water table is assumed to be located at 25 m below the surface, and as the time signature of the seismic source $f(t)$ we use a Ricker wavelet with peak frequency of 120 Hz, the peak amplitude for the Ricker wavelet (located at $t = 8 \times 10^{-3}$ s) is set so that the amplitude of the solid displacement at the surface is $U_{s,1} = 1$ m. Note that this is not a realistic value for the solid displacement but it is appropriated for a qualitative analysis. The vadose zone water saturation is taken to be the mean value of the saturation profile defined by the van Genuchten model. For the silt loam (see Zyserman *et al.* 2017a) with the water table located at the same depth as above, the mean saturation value is $S_w = 0.32$.

The time variation of the solid displacement and the current density is plotted in Fig. 2 for 11 different depths measured from the surface down to 50 m depth. For visualization purposes, the fields were scaled by multiplying the u_s field and the J_v field by 4 and 1.5, respectively, so that the wavelets have almost the same amplitudes; we proceed in this way because the purpose of Fig. 2 is to analyse the time signatures of the fields but not the amplitudes, which are studied in the following sections. As it can be seen, the solid displacement u_s induced by the source at the surface travels downwards with fairly constant seismic velocity and amplitude. The current density j_v follows the same time dependence as u_s but with a sharp increase of amplitude when the water table is reached at 25 m depth. This jump in the current density was expected given the sharp contrast in water saturation. This contrast is the main contribution to the variation of the current density across the water table (see eq. 22).

4.2 Coseismic field analysis

The coseismic responses of the electric and magnetic fields are shown in Fig. 3 (left-hand panels). These fields are obtained by computing the third term in eqs (31) and (34), respectively. As we did in the previous figure, for visualization purposes the fields were scaled by multiplying

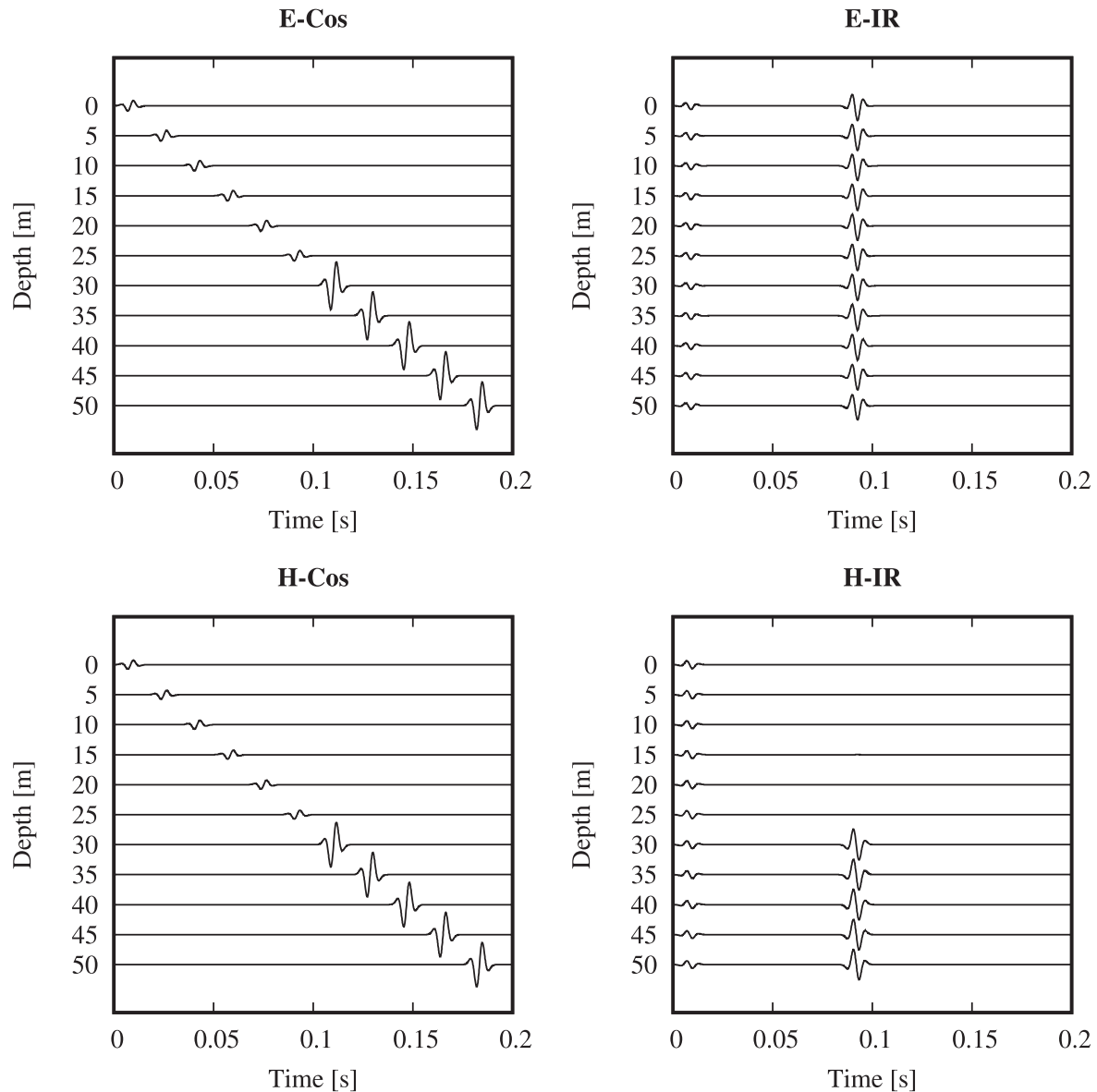


Figure 3. Time variation of the coseismic (left) and interfacial (right) responses of both electric (top) and magnetic (bottom) fields registered at 11 receivers. The distance between receivers is 5 m. Above 25 m depth the water saturation is 0.32, and below 25 m depth the medium is fully saturated.

the E-Cos field and the H-Cos field by 25 000 and 8, respectively; again, the scaling does not affect the behaviour in time of the traces. The travelling seismic wave induces a relative motion between the rock matrix and the water due to the non-zero viscosity of the latter, which produces an electric current density. This current density induces the coseismic magnetic field. The coseismic field travels with the seismic wave and therefore shows the same propagation pattern with depth. The coseismic responses of the magnetic field H-Cos and of the electric field E-Cos show the same behaviour as the current density, with higher amplitudes below the water table. Indeed the amplitudes of the coseismic fields are proportional to the current density (see the third term in eqs 31–34, respectively). We recall here that the E-Cos is originated in the time dependence of the H-Cos, through Faraday's law, eq. (12) (Zyserman *et al.* 2017a).

4.3 Interfacial responses analysis

The interfacial responses are shown in Fig. 3 (right-hand panels) and are given by the first two terms of eqs (31)–(34). The fields were scaled by multiplying the E-IR field and the H-IR field by 8 and 7, respectively. As it can be seen, two distinct events occurring at two different times are registered simultaneously at all depths (in the case of H-IR, the second event is not distinguishable over the water table because its amplitude is negligible). The first one has its peak amplitude at the same time as the seismic source (8×10^{-3} s), and for this reason is identified as an IR originated at the surface. This IR is attributed to the jump in the current density at the surface (note that the current density over the surface is zero, and at the surface it takes the value J_0). Although there is numerical evidence of the existence of this IR (Zyserman

et al. 2015; Munch & Zyserman 2016), this is the first time that its existence is predicted analytically. As it also can be seen in the figure, the interface response of the surface is registered for both the electric and magnetic fields, and depicts the same amplitude for all the receivers located both over and below the water table. A second event is registered at a time that is compatible with the time needed by the seismic wave to reach the water table, located at 25 m depth, which is $\simeq 0.083$ s for a seismic velocity of 300 m s^{-1} . Once the SH seismic wave reaches the water table, there is a discontinuity in the electric current density and therefore a strong amplitude variation in the magnetic coseismic field H-Cos. Note, however, that the total field H is continuous across the water table, as we proved in Appendix C. The jump in the current density leads to the magnetic interfacial response H-IR, and to the electric interfacial response E-IR, which travel in the porous medium at a velocity much larger than the seismic velocity and arrive at (nearly) the same time at all depths. Note that in this case, the interface response of the electric field preserves its amplitude across the water table, contrary to what we have just described happens with the magnetic field H. This is a consequence of the continuity of the tangential component of the electric field at any interface. The behaviour for the IRs of both fields confirms the novel numerical results we obtained in our previous work (Zyserman *et al.* 2017a). They are different from what is known from the analysis of seismoelectromagnetic conversions induced by compressional waves: Warden *et al.* (2013) and (Bordes *et al.* 2015; Peng *et al.* 2017) predicted through numerical modelling and observed on experiments that in this case the IRs have a very small amplitude compared to the coseismic signals.

At this point, we want to mention that in most theoretical and numerical scenarios present in the literature is affirmed that the coseismic electric field accompanying the *P* wave is larger than that of the *S* wave. However, a numerical study of Gao *et al.* (2017), based on a relation for the transfer functions for both *P* and *S* waves deduced previously (Gao & Hu 2010), showed that there are indeed realistic situations in which the *S*-wave coseismic electric field can be of the same order of magnitude as that of the *P* wave. However, this is of no concern to the relative amplitudes of the IRs generated by the *P*- and *S*-seismic waves. The origin of the IRs, associated to different physical processes (electric charge accumulation in the first case, electric currents in the second one) and how they depend on the geometry and physical parameters of the system under research, is not completely known, fundamentally for the SH-wave IRs. In this regard, a point that must not be overlooked is that the IRs generated by the arrival of *P* waves to an interface (E_P -IR) present not only the problem that the amplitude of the coseismic signal is usually stronger than the E_P -IR, but they are also recorded simultaneously for usual acquisition geometries, what makes their individualization very difficult. This situation persists even in the case in which the E_P -IR be stronger than those generated by SH waves (E_{SH} -IR). Therefore, we think that the signal-to-noise ratio E-IR/E-Cos becomes more relevant than the relative amplitude between the E_P -IR and the E_{SH} -IR fields when evaluating the possibility of individualizing the interface response. The difficulty in getting a meaningful E_P -IR from a surface-to-surface recording is well known, and it could be overcome by setting other source and receivers geometries, e.g. surface-to-borehole, as it has been proposed in the literature (Dupuis *et al.* 2009). On the other hand, the fact that for SH-wave sources the E-Cos signal is much lower than the E-IR leads in principle to a much better signal-to-noise ratio even for the surface-to-surface geometry to detect the interfacial response.

4.4 Water saturation dependence of the amplitude of the electromagnetic responses

We explore the dependence of the electromagnetic responses on the saturation S_w of medium 1. The coseismic and interfacial responses of the surface and the water table, for water saturation between 25 per cent to 40 per cent computed at $z = 10$ m (15 m over the water table) and $z = 40$ m (15 m below the water table) are shown in Figs 4 and 5, respectively. As it can be seen in Fig. 4, the amplitude of the electric coseismic field is in the range of 0.1 mV m^{-1} while the amplitude of both electric interfacial responses reaches amplitudes in the order of $0.2\text{--}0.4 \text{ V m}^{-1}$. The amplitude of the coseismic electric field is decreasing with decreasing water saturation, and the same occurs to the surface E-IR, whereas the amplitude of the water table E-IR is increasing with decreasing water saturation. The water table E-IR is therefore several orders of magnitude higher than the E-Cos and can be detected at 10 m depth or at the surface, and is enhanced if the water saturation is decreased, from a ratio of 3 orders of magnitude at saturation 40 per cent to 4 orders of magnitude at saturation 25 per cent. This behaviour is well explained in Fig. 6, where the ratio of the peak amplitudes between IR of the water table and E-Cos responses of the electric field is plotted as a function of water saturation of the vadose zone. Still in the unsaturated zone, at 10 m depth the amplitudes of the magnetic coseismic field and the magnetic interfacial response of the surface are both in the range $0.1\text{--}0.3 \text{ A m}^{-1}$, both fields are decreasing with decreasing water saturation. Although the magnetic interface response of the water table is present in the registers located above the water table, its amplitude is negligible, as can be seen from Fig. 4. The amplitudes for the H-IR of the water table are between 2 and 3 orders of magnitude lower, so that the ratio between the H-IR and H-Cos will not allow us to detect to H-IR.

In the saturated zone, at 40 m depth (see Fig. 5), the amplitude of the E-Cos is about 0.15 mV m^{-1} and the E-IR of the water table is about $0.1\text{--}0.3 \text{ V m}^{-1}$, leading to a ratio between the E-IR over the E-Cos of about 667–2000 for water saturations of 25–40 per cent, respectively. The E-IR from the water table could therefore be detected in the saturated zone. The amplitude of the coseismic magnetic field is about 0.5 A m^{-1} and the one of the H-IR of the water table is $0.2\text{--}0.4 \text{ A m}^{-1}$ for water saturations of 25–40 per cent. Therefore, the ratio between the H-IR and H-Cos is only 0.4 to 0.8, and the H-IR will be hardly detected at depth. As it can be seen, the amplitude variation of E-IR and H-IR with water saturation depicts the same behaviour. However, the amplitudes of E-Cos and H-Cos remain constant [note in eqs (32) and (34) that the expressions for the coseismic fields in the saturated zone have no dependence on the saturation of the unsaturated zone]. Note that both for $z = 10$ m and $z = 40$ m the saturation variation induces a time shift that is present in the coseismic fields and in the interfacial response of the water table, but is not in the interfacial response of the surface. We attribute this shift to a decrease in the velocity of medium 1 with

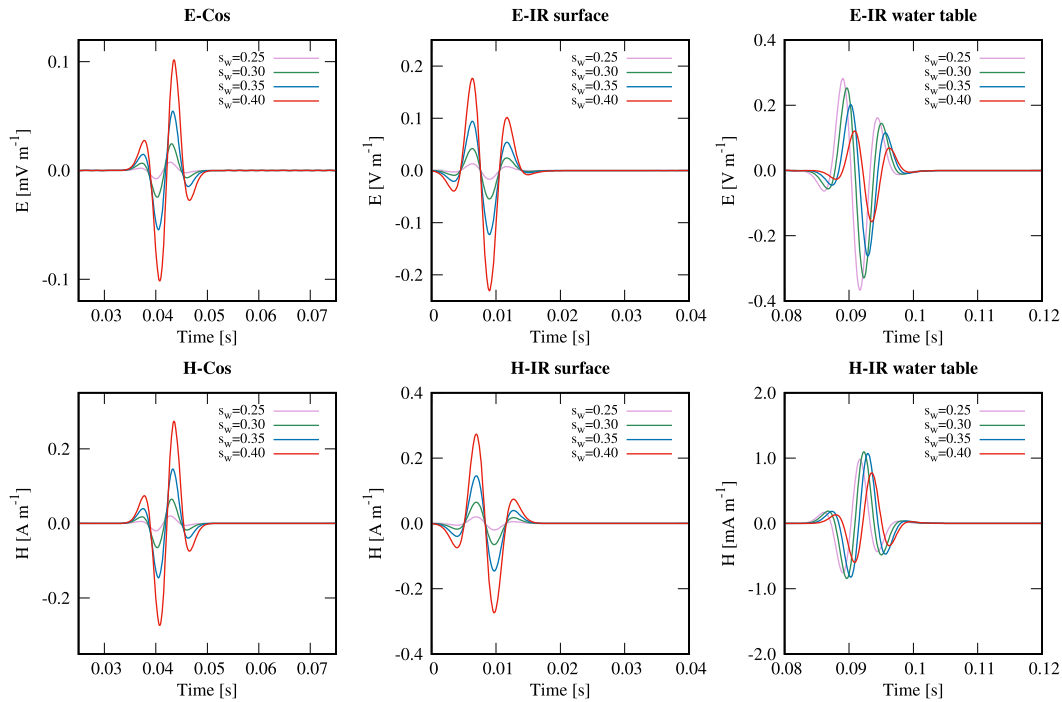


Figure 4. Time variation of the coseismic response (left), interfacial response of the surface (center) and interfacial response of the water table (right) of both electric (top) and magnetic (bottom) fields registered at $z = 10$ m (15 m over the water table) for the four different saturation values considered in this study.

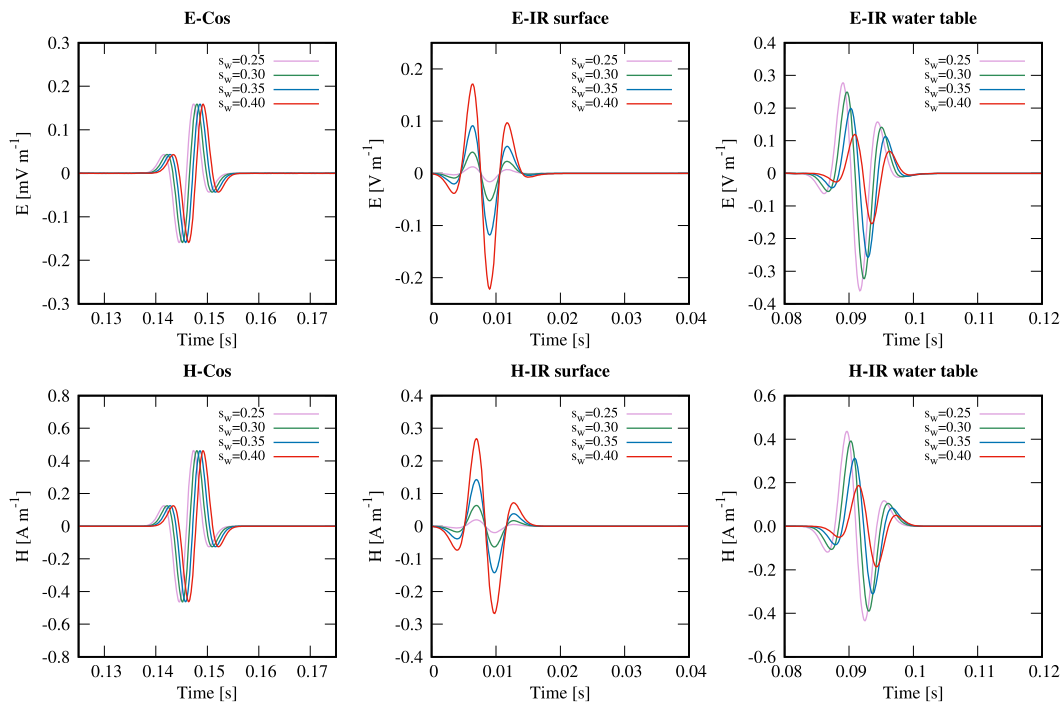


Figure 5. Time variation of the coseismic response (left), interfacial response of the surface (center) and interfacial response of the water table (right) of both electric (top) and magnetic (bottom) fields registered at $z = 40$ m (15 m below the water table) for the four different saturation values considered in this study.

the increase of water saturation; this behaviour is observed from the shear wave velocity obtained from eq. (16) and has been experimentally observed in partially saturated rocks (Mochizuki 1982). It is important to remark that this analysis allows to conclude that a SH -wave source can induce an E-IR from the water table which can be detected at surface or at depth because it is several orders of magnitude larger than the E-Cos field. We observe that an increase of the water saturation contrast between the vadose zone and the saturated zone will produce an increase in the amplitude of the water table E-IR and H-IR together with a decrease of the amplitude of the surface E-IR and H-IR.

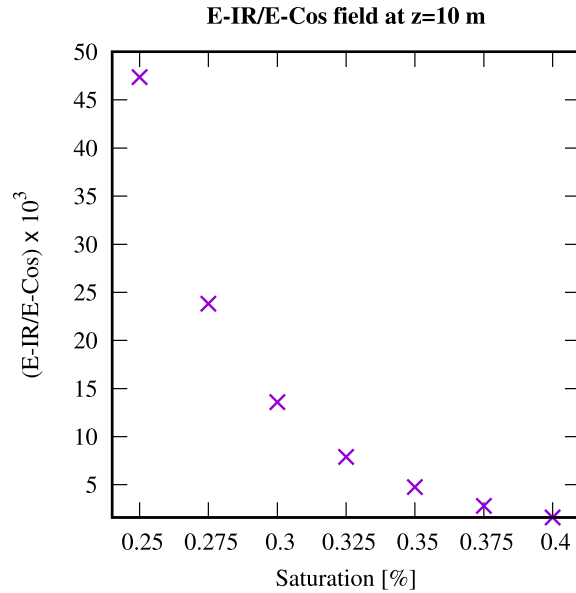


Figure 6. Ratio between the peak amplitudes of the electric interfacial response E-IR of the water table and coseismic response E-Cos computed at a receiver located 10 m below the surface and for seven different values of water saturation of the vadose zone.

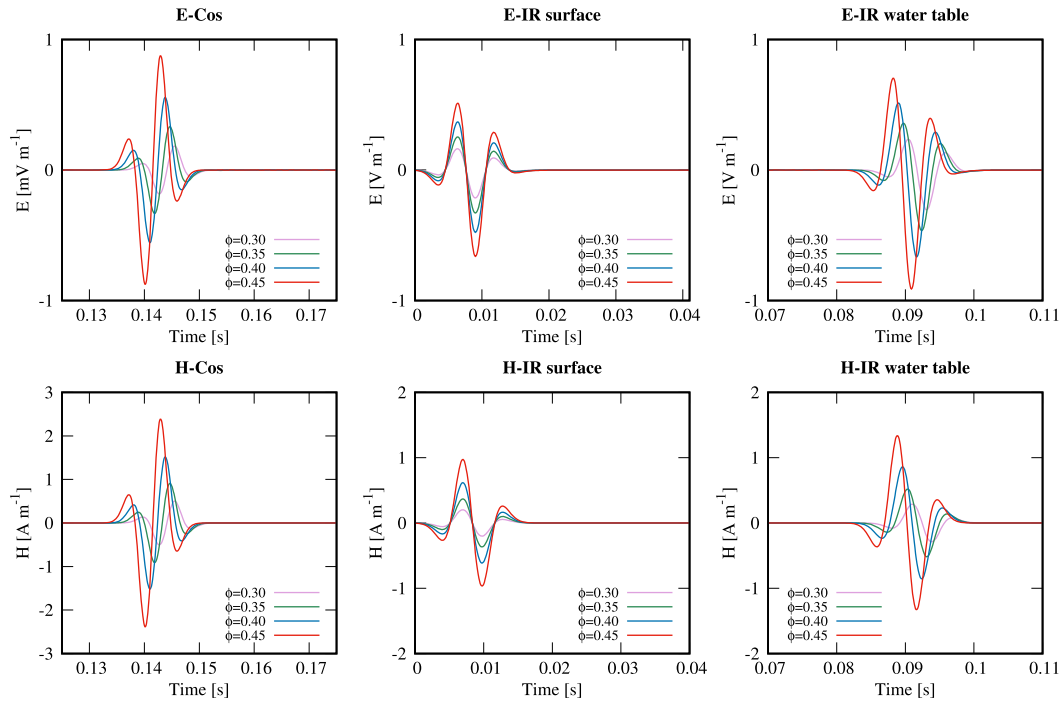


Figure 7. Time variation of the coseismic (left), interfacial response of the surface (center) and interfacial response of the water table (right) of both electric (top) and magnetic (bottom) fields registered at $z = 40$ m (15 m below the water table) for four different porosity values considered in this study.

4.5 Sensitive analysis

We analyse here the effect of changes in porosity, fluid viscosity and density on the electromagnetic conversions. The analysis is performed on time traces of the electric and magnetic fields registered at one receiver. The results observed for other depths are qualitatively the same when analyzing the effect of these parameters. In this case we choose a receiver located below the water table ($z = 40$ m) because all events can be visualized (remember that the amplitude of H-IR at the water table is almost negligible for receivers located over the water table).

The coseismic and interfacial responses for porosities between 0.30 and 0.45 computed at $z = 40$ m are shown in Fig. 7. Note that the changes in porosity produce both amplitude and time shift variations on the fields. Particularly, when the porosity is increased, the time shift of the events (with the exception of the IRs of the surface) is decreased. This is due to the small increase of seismic velocity produced when the porosity of the medium is increased; this behaviour is theoretically predicted by the shear wave velocity obtained from eq. (16) and has been experimentally observed in unconsolidated sands (Zimmer *et al.* 2007). It can also be observed in Fig. 7 that the amplitude of the

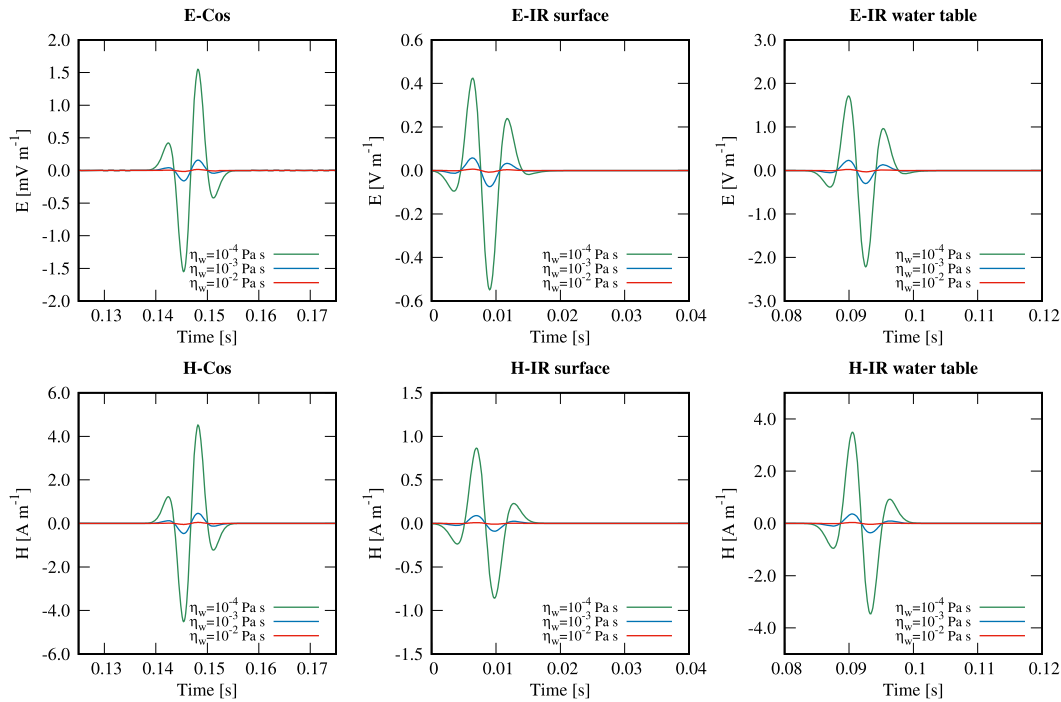


Figure 8. Time variation of the coseismic response (left), interfacial response of the surface (center) and interfacial response of the water table (right) of both electric (top) and magnetic (bottom) fields registered at $z = 40$ m (15 m below the water table) for three different viscosity values considered in this study.

electromagnetic fields shows a smooth increase with porosity that causes a higher fluid volume to be displaced, which in turn produces higher current densities. The former statement is based in an analysis of the behaviour of eq. (18) with porosity we performed but don't show here for the sake of brevity. These higher current densities increase the amplitudes of the fields, explaining the amplitude variation showed by the fields when porosity is increased.

The impact of fluid viscosity variations on the electromagnetic fields is analysed by considering time traces of the electromagnetic fields registered at $z = 40$ m for three different values of fluid viscosity (see Fig. 8). As in the case of porosity variations considered before, we choose a receiver below the surface because all events are clear and the results obtained for other traces are qualitatively the same. It is worth to mention that the variation is introduced in the viscosity of water, i.e. η_w . As it can be seen in Fig. 8, the increase of viscosity produces a decrease in the amplitude of both fields, with no time shift present in the traces. This effect is attributed to energy dissipation, which is stronger for higher fluid viscosities; this fact can be observed from eq. (18); the real part of this expression gives the amplitude of the fluid displacement, the imaginary part accounts for the energy dissipation. Then, the amplitude of the current density induced by the shear wave is lower, which in turn produces a lower amplitude coseismic response and, therefore, smaller interface responses.

Finally, we analyse the effect of fluid density variations on the electromagnetic fields by considering time traces registered at $z = 40$ m for three different values of water density (see Fig. 9). Both amplitude and time shift variations are produced when the water density is changed, and this variations are present in all the events with the exception of the IR of the surface (only amplitude variations are shown by this event). The increase of water density produces an increase in the amplitude of both fields. Note that this amplitude increase is in the same order than the one observed for porosity changes. There is a shift in time as in the case of the porosity, but again it can be attributed to variations in the seismic velocity induced by the change in fluid density. The increase of water density produces a decrease of the seismic wave velocity (see eq. 16), which in turn produces a shift towards later times of the events registered, as can be seen in the figure. The amplitude variation, however, is mainly attributed to a variation on the current density, which depends on fluid density (the current density is higher for higher fluid densities), see eqs (20) and (21).

4.6 Comparison between the exact and the approximate solutions

In this section, the exact solution given by eqs (31)–(34) is compared with the approximate solution of eqs (42)–(44) in order to evaluate the ability of the approximate solution to model the SH response of the vadose zone. Figs 10 and 11 show time traces of the electric and magnetic fields, respectively, registered at a receiver located 10 m below the surface, computed using the exact solution and its approximation. The difference between both fields is also plotted with an enlarged scale. In this case, the plot corresponds to the total field (note that, as was pointed out before, the amplitudes of E-Cos and H-IR of the water table in the unsaturated zone are almost negligible compared to the other events). As we mention in the 'Approximate solution' section, for depths up to $\simeq 100$ m, the approximations made work fairly good. As a result, the traces computed for both solutions at a depth of 10 m give a very good match, and the difference between the solution and its

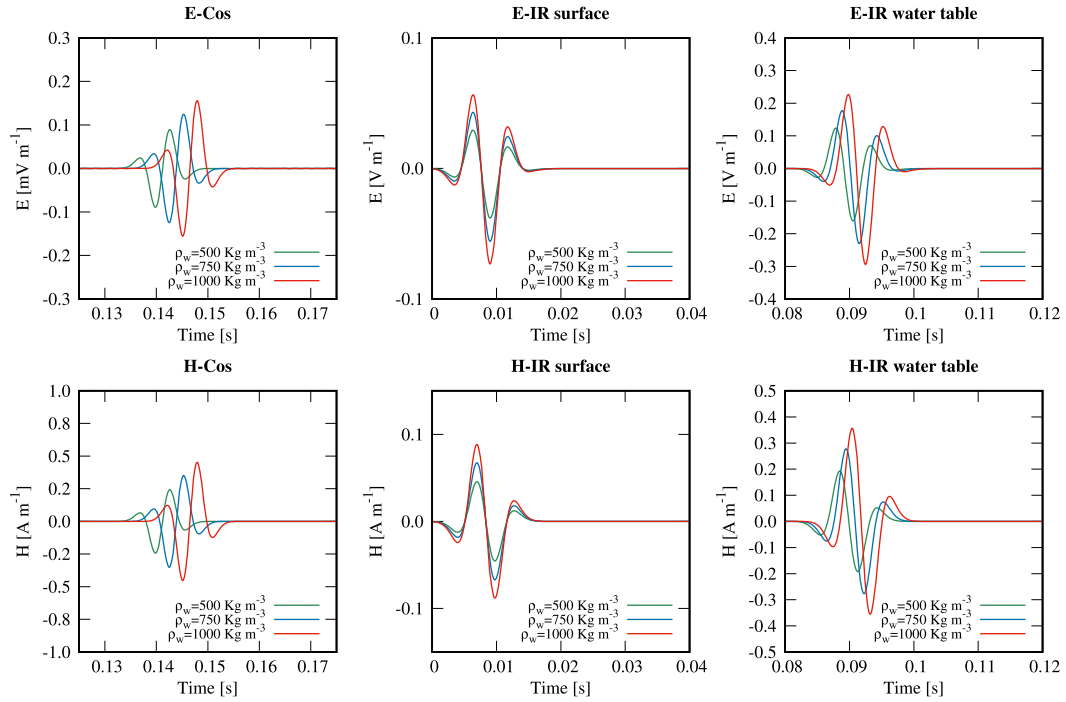


Figure 9. Time variation of the coseismic (left), interfacial response of the surface (center) and interfacial response of the water table (right) of both electric (top) and magnetic (bottom) fields registered at $z = 40$ m (15 m below the water table) for three different density values considered in this study.

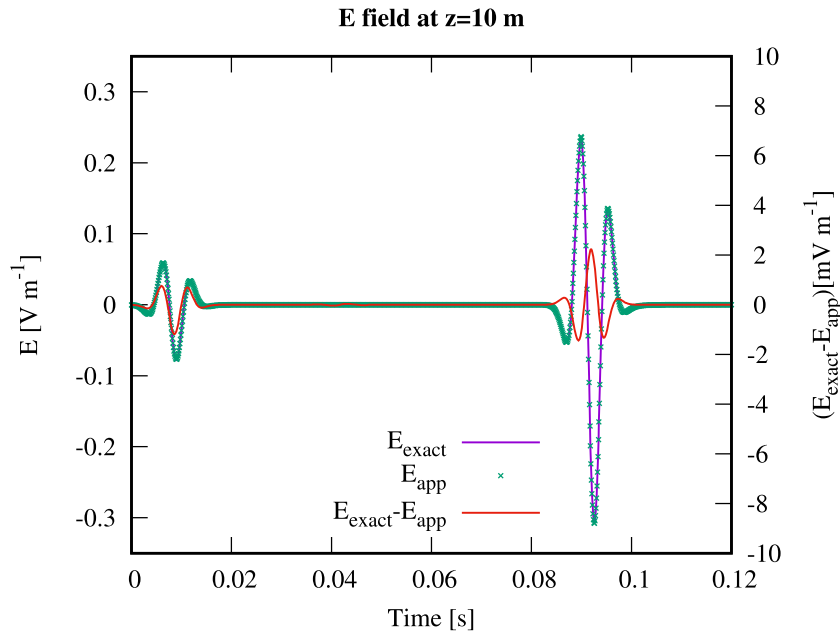


Figure 10. Comparison of the exact (E_{exact}) and approximate (E_{app}) solutions for the electric field response registered at $z = 10$ m below the surface. Note that a double scale is used; the left one to plot both analytical solutions and the right one to plot the difference between both solutions.

approximation is lower than ≈ 4 per cent of the field in both cases. Note in Fig. 11 that the event located at ≈ 0.09 s corresponds to the difference between the IR of the water table predicted by the exact solution and the one predicted by the approximate solution. The amplitude of this difference is ≈ 1 mA m^{-1} , which is almost 100 times lower than the exact solution.

The time traces of the electric and magnetic fields registered at a receiver located 100 m below the surface are shown in Figs 12 and 13. Note that for this depth, the coseismic components are no longer present within the considered time window. The coseismic component of the H field is present in Fig. 11, but the one corresponding to the E field is not visible in Fig. 10 because of its very small amplitude in comparison with the E-IR. As was expected, in the case of $z = 100$ m there is a discrepancy between both solutions, and their difference is around 25 per cent of the field. However, even for this rather big value of z , the approximate solution works fairly good. This example shows

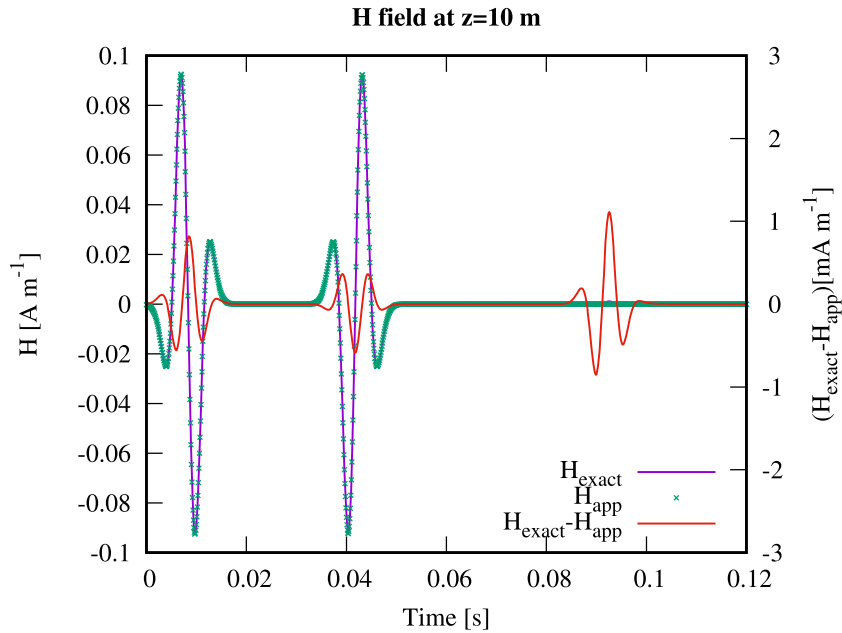


Figure 11. Comparison of the exact (H_{exact}) and approximate (H_{app}) solutions for the magnetic field response registered at $z = 10$ m below the surface. Note that a double scale is used; the left one to plot both analytical solutions and the right one to plot the difference between both solutions. The event located at ≈ 0.09 s corresponds to the IR of the water table. Note that the amplitude is $\approx 1 \text{ mA m}^{-1}$, which is almost 100 times lower than the exact solution.

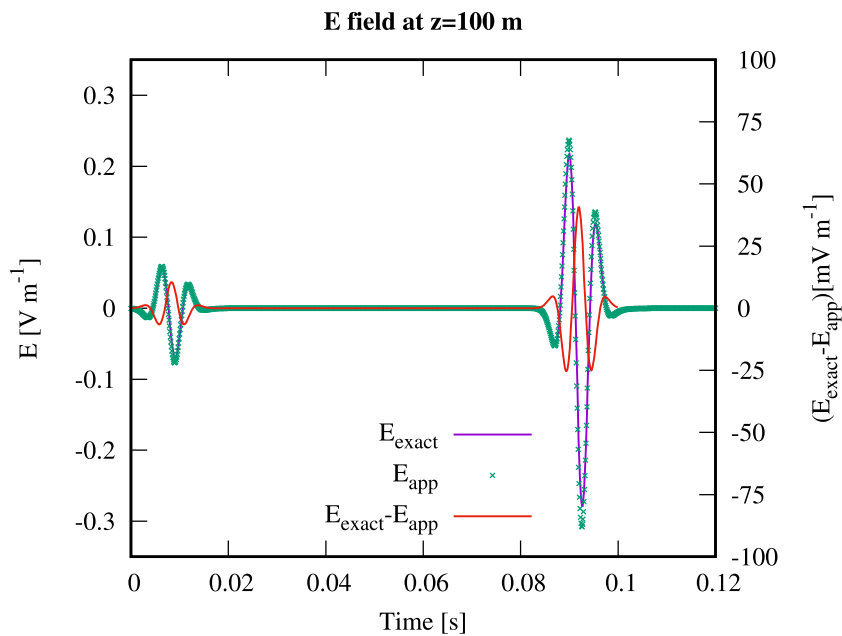


Figure 12. Comparison of the exact (E_{exact}) and approximate (E_{app}) solutions for the electric field response registered at $z = 100$ m below the surface. Note that a double scale is used; the left one to plot both analytical solutions and the right one to plot the difference between both solutions.

that the approximate solution is a very good one and in most cases, with the only restrictions imposed by the assumptions of the model, can be safely used to model the *SH* response of the vadose zone .

4.7 Analysis of the approximate solution

Finally, taking advantage of the simplicity of the analytical expressions of the approximate solution, we perform an analysis of the dependence of the electromagnetic response in terms of the physical parameters of the medium. First, let us take a look at eq. (42) which gives the approximate expression of the electric field. Note that as a consequence of the approximations made in Section 3.3, the coseismic response is absent. The reason is that, as we showed before, this component of the field is several orders of magnitude lower than the interface response. As a result, the approximated electric field is a pure IR field. The first term involving J_0 corresponds to the IR of the surface, meanwhile the

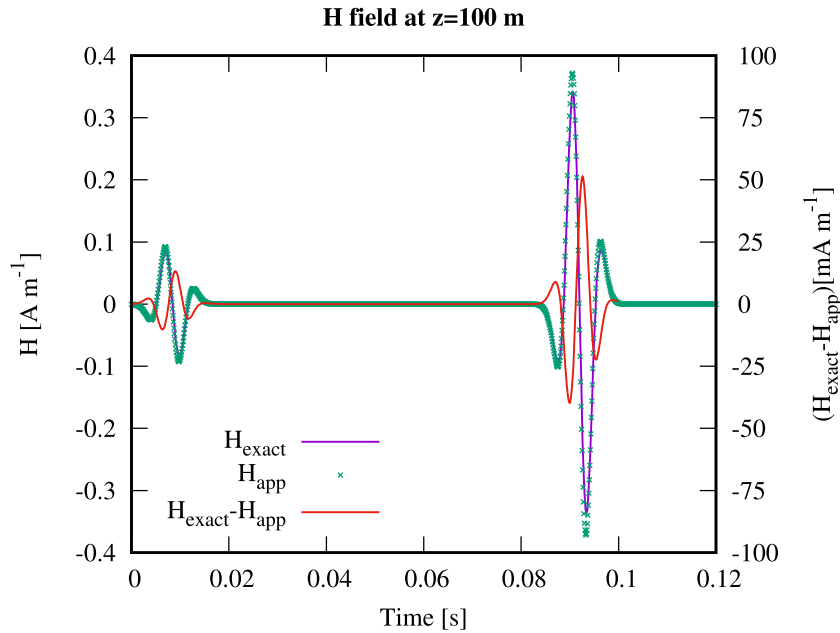


Figure 13. Comparison of the exact (H_{exact}) and approximate (H_{app}) solutions for the magnetic field response registered at $z = 100$ m below the surface. Note that a double scale is used; the left one to plot both analytical solutions and the right one to plot the difference between both solutions.

second and third terms constitute the water table IR. Note that the magnitude of the IR of the surface is proportional to J_0 , leading to stronger responses for higher values of $|J_0|$. On the other hand, the IR of the water table is proportional to the difference between $J_1^{\text{wt}}/\lambda_1$ and $J_2^{\text{wt}}/\lambda_2$, and given that the wavenumbers λ_1 and λ_2 verify $\lambda_1 \simeq \lambda_2$, this response will be mainly controlled by the difference between current densities $J_2^{\text{wt}} - J_1^{\text{wt}}$. This explains the fact that for lower water saturations, the IR of the surface tends to be lower, but the one corresponding to the water table turns to be higher: J_0 is lower for lower values of S_w , and the same occurs to J_1^{wt} . Then, given that J_1^{wt} is lower than J_2^{wt} , the difference $J_2^{\text{wt}} - J_1^{\text{wt}}$ will be higher for lower S_w .

The approximate solution for the magnetic field over the water table is given by eq. (43). As it can be seen, this field preserves the coseismic component, given by the second term, and the interface response is purely due to the surface. As was shown before, the IR of the magnetic field is almost negligible for receivers located over the water table, and it is neglected, and therefore taken out in the approximation.

Finally, eq. (44) shows the approximate expression of the magnetic field proposed for receivers located below the water table. This field contains contributions from both the coseismic field and IRs, being the latter originated at both interfaces. Note that the IR of the water table is, as in the case of the electric field, proportional to the jump in current density $J_2^{\text{wt}} - J_1^{\text{wt}}$, controlling the behaviour of the magnetic field in the same way that it does for the electric field. For low values of water saturation of the vadose zone, both J_0 and J_1^{wt} will be small compared with J_2^{wt} , and as a result, the amplitude of the IR of the water table will be almost the same as the amplitude of the coseismic response.

5 CONCLUSIONS

We found new analytical solutions – derived under the assumptions of a SH-wave seismic source acting on an infinite plane on the surface of the 1D Earth – allowing to straightforwardly study the seismoelectromagnetic interface and coseismic responses, and their dependence on the physical medium parameters. Moreover, we considered two layers, differing only in the fluid saturation. The upper one, of finite width, is partially saturated with a constant saturation and overlies a fully saturated semispace. An important feature of the obtained solution is that the interfacial and coseismic responses are explicitly given in the mathematical expressions of the electromagnetic fields, so they can be analysed separately. Another important feature is that the analytical solution predicts the existence of an IR originated at the surface. To our knowledge, this is the first time that its existence is analytically predicted. An approximation of the analytical solution was derived, which provides a simple way to interpret and analyse the dependence of the seismoelectric response on the various parameters of the medium. We showed that the approximate solution works fairly well in most cases of shallow exploration, given that the conditions under which the approximations work are valid for depths close to, but not higher than 100 m, approximately. Our analysis of the dependence of the electromagnetic response on the water saturation is in complete agreement with our previous work (Zyserman *et al.* 2017a), showing that a sharp contrast in water saturation at the water table can induce strong interfacial responses in both fields, and in the case of the electric field, the amplitude of the interfacial response is at least three orders of magnitude higher than the coseismic response in the unsaturated zone. The sensitivity analysis has shown that the considered parameters can produce variations, both in amplitude and time shift of the registered fields. The amplitude variations can mostly be explained in terms of the variation in the magnitude of the jump in the current densities at the interfaces, meanwhile the time shifts are attributed to variations in the seismic velocity induced by the variations in the considered parameters. Although these results

were obtained for a particular soil, namely a poorly consolidated silty loam, no significant change is expected in the observed qualitative behaviour of the obtained results when considering other soil textures.

Finally, it is important to mention that whether a 1D approach is performed, the question if the simplicity of the model yields characteristics only proper to 1D representation arises. One possible way to answer this question is to run 2D or 3D simulations and compare them with the 1D predictions. However, this task is far beyond the scope of this paper, although it certainly could be the subject of forthcoming studies. Despite this, the results obtained could be very accurate in modelling the electrokinetic effects induced by a pure shear wave in the case of normal incidence. Although the cylindrical/spherical spreading experienced by the wave in its way from the source to the water table would not be modelled, the physical process for the generation of the interface response will be clearly explained by the jump in current density occurring at the water table, as it is predicted by the proposed model.

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APPENDIX A

From eq. (14), it is possible to obtain the following relation between u_s and u_f :

$$u_f = -\frac{\omega^2 \rho_f}{[i\omega \frac{\eta}{\kappa} - \omega^2 g_0]} u_s. \quad (\text{A1})$$

Replacing eq. (A1) in eq. (13), one obtains:

$$\frac{d^2 u_s}{dz^2} + \lambda^2 u_s = -\frac{F^s}{G} \delta(z), \quad (\text{A2})$$

where λ is given by eq. (16). Using Laplace Transform, it is possible to show that the solution for $u_s(z)$ is given by:

$$u_s(z) = \left[-\frac{F^s}{\lambda G} \sin(\lambda z) + u_s(0) \cos(\lambda z) + \frac{u'_s(0)}{\lambda} \sin(\lambda z) \right] \mathcal{H}(z), \quad (\text{A3})$$

being $\mathcal{H}(z)$ the Heaviside function. Writing the sine and cosine functions in their exponential form and regrouping terms in eq. (A3), we obtain:

$$u_{s,1}(z) = \left[-\frac{F^s}{2i\lambda G} + \frac{u_s(0)}{2} + \frac{u'_s(0)}{2i\lambda_1} \right] e^{i\lambda z} \mathcal{H}(z) + \left[\frac{F^s}{2i\lambda G} + \frac{u_s(0)}{2} - \frac{u'_s(0)}{2i\lambda_1} \right] e^{-i\lambda z} \mathcal{H}(z), \quad (\text{A4})$$

Choosing the square root of λ^2 that verifies $Re(\lambda) < 0$, then, the first term of the last equation represents a wave that travels downwards, meanwhile the second one is a wave travelling upwards. If we consider only waves travelling downwards, then the second term of eq. (A4) should vanish:

$$\left[\frac{F^s}{2i\lambda G} + \frac{u_s(0)}{2} - \frac{u'_s(0)}{2i\lambda} \right] = 0 \quad (\text{A5})$$

Using the last expression in eq. (A4), we obtain:

$$u_s(z) = u_s(0) e^{i\lambda z} \mathcal{H}(z). \quad (\text{A6})$$

Now, it remains to determine the value of the constant $u_s(0)$. If we assume that the solid matrix is in perfect contact with the source generator at the surface, then the shear stress applied by the source over the surface F^s should be equal to $\tau_{xz} = -2G_1 \epsilon_{xz} = -G_1 \frac{\partial u_{s,1}}{\partial z}$ (the minus sign indicates that the shear stress is computed taking the normal in the $-z$ -direction). Then, taking the first derivative of $u_s(z)$ with respect to z in eq. (A6) and evaluating it in $z = 0$ we can write:

$$u'_s(0) = i\lambda u_s(0) = -\frac{F^s}{G}, \quad (\text{A7})$$

which leads to the final solution for $u_s(z)$:

$$u_s(z) = U_s e^{i\lambda z} = -\frac{F^s}{i\lambda G} e^{i\lambda z}, \quad z \geq 0. \quad (\text{A8})$$

A similar expression can be obtained for $u_f(z)$ replacing eq. (A8) in eq. (A1):

$$u_f(z) = U_f e^{i\lambda z} = -\frac{\omega^2 \rho_f}{[i\omega \frac{\eta}{\kappa} - \omega^2 g_0]} U_s e^{i\lambda z}, \quad z \geq 0. \quad (\text{A9})$$

Eqs (A8) and (A9) show that the solid and relative fluid displacements are produced by a shear wave originated at the source position travelling downwards with phase velocity given by $\omega/|Re(\lambda)|$.

APPENDIX B

For $z < 0$ (over the surface) we assume that the medium is constituted by air, which is treated as a perfect insulator. Then, both the electric conductivity σ and the electric current density will be zero and Maxwell's equations (11) and (12) reduce to:

$$\frac{\partial H}{\partial z} = 0, \quad (\text{B1})$$

$$\frac{\partial E}{\partial z} + i\omega\mu_0 H = 0. \quad (\text{B2})$$

From eq. (B1), we know that H is constant. Then, from eq. (B2), $E(z) = az + b$, where a and b are complex constants. However, a must be equal to zero in order to avoid the divergence of the electric field when $z \rightarrow -\infty$. Then, E is also a constant field, and replacing it in eq. (B2) we obtain that $H = 0$ for $z < 0$.

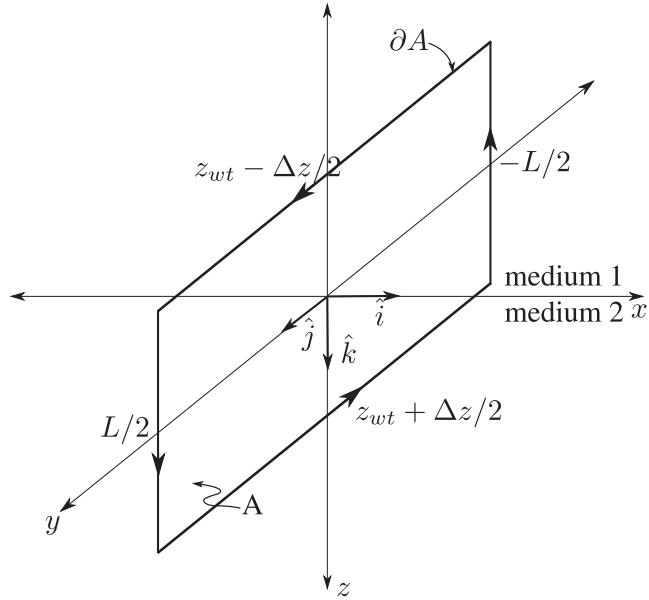


Figure C1. Continuity of H across the water table ($z = z_{wt}$) – Ampere’s law.

APPENDIX C

In this appendix, we show that the magnetic field should be continuous at the surface and at the water table. Let us assume a closed rectangular loop crossing the horizontal plane at $z = z_{wt}$, as is depicted in Fig. C1. According to Ampere’s law

$$\oint_{\partial A} \mathbf{H} \cdot d\mathbf{l} = \iint_A \mathbf{j}_v \cdot d\mathbf{A}. \quad (\text{C1})$$

For our model $\mathbf{H} = H(z) \hat{j}$, $\mathbf{j}_v = j_v(z) \hat{i}$ and $d\mathbf{A} = dA \hat{i}$, so we can write:

$$\int_{-L/2}^{L/2} H(z_{wt} - \Delta z/2) dy + \int_{L/2}^{-L/2} H(z_{wt} + \Delta z/2) dy = \int_{-L/2}^{L/2} \int_{z_{wt}-\Delta z/2}^{z_{wt}+\Delta z/2} j_v(z) dz dy. \quad (\text{57})$$

Integration over y yields

$$H(z_{wt} - \Delta z/2) - H(z_{wt} + \Delta z/2) = \int_{z_{wt}-\Delta z/2}^{z_{wt}+\Delta z/2} j_v(z) dz. \quad (\text{58})$$

Using the expressions for $j_v(z)$ given by eqs (20) and (21) we have

$$H(z_{wt} - \Delta z/2) - H(z_{wt} + \Delta z/2) = \int_{z_{wt}-\Delta z/2}^{z_{wt}} J_1^{wt} e^{i\lambda_1(z-z_{wt})} dz + \int_{z_{wt}}^{z_{wt}+\Delta z/2} J_2^{wt} e^{i\lambda_2(z-z_{wt})} dz, \quad (\text{59})$$

which gives, after integrating over z

$$H(z_{wt} - \Delta z/2) - H(z_{wt} + \Delta z/2) = \frac{J_1^{wt}}{i\lambda_1} [1 - e^{-i\lambda_1 \Delta z/2}] + \frac{J_2^{wt}}{i\lambda_2} [e^{-i\lambda_2 \Delta z/2} - 1]. \quad (\text{60})$$

Taking the limit when $\Delta z \rightarrow 0$, the right hand side of eq. (C5) tends to 0, leading to the following relation:

$$\lim_{z \rightarrow z_{wt}^-} H(z) = \lim_{z \rightarrow z_{wt}^+} H(z), \quad (\text{61})$$

which means that the magnetic field H is continuous across the water table. The same reasoning can led to the following relation valid for the continuity of the magnetic field at the surface

$$\lim_{z \rightarrow 0^-} H(z) = \lim_{z \rightarrow 0^+} H(z). \quad (\text{C7})$$

On the other hand, given that the electric field $E(z)$ is purely tangential to both the surface and the water table interfaces, and the tangential components of the electric field should be continuous across any interface, the same will be valid for the electric field.