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Publishing ecular simulation of the water-triolein-oleic acid mixture: local structure and thermodynamic properties

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An artificial oil in water emulsion analogue to those found in bioresources or food matrices is simulated and studied experimentally. It is composed of one of the major natural free fatty acids (the oleic acid, OA) and the corresponding triacylglyceride (trioleic glyceride, or triolein, GTO). Because of the large time and length scales involved, the molecular simulations are done with the Martini force field, a coarse-grained model. This allowed us to study the water–OA–GTO system at different compositions with more than 20000 molecules and up to 2 μ s.

Interfacial tension was measured using the pendant drop method and compared with molecular simulation results. We observe very good agreement at high OA concentration and deviations up to 15% at low OA concentrations. The water solubility in the lipid phase is in fair agreement with experiments, between 0.03 and 0.32 mol/L, rising with the OA content.

The area occupied by OA and GTO at the interface between water and pure product fitted with experimental data ($A_{\rm OA}=36.6~{\rm Å}^2$ and $A_{\rm GTO}=152.1~{\rm Å}^2$). The consistency between simulation and experimental results allowed a structural analysis of the interface. A bilayer structure of the lipids at the water/oil interface is proposed, containing preferentially oleic acid but also triolein. Through all these results the usefulness of coarse-grained simulation for the description of water-oil interfacial organization is demonstrated. This method will be used later on to bring local information on the organization of target compounds, necessary in biomass fractionation processes or food additives formulations for example.

Keywords: oleic acid, triolein, interfacial tension, emulsion, coarse-grained simulations

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Publishing INTRODUCTION

The local organization of lipids in complex mixtures, like oil in water emulsions, is more and more needed in different application fields. Its knowledge is necessary for the development of innovative extraction and separation processes, in the context of renewable bioresources valorization (i.e. microalgae) for food, feed (polyunsaturated lipids) and energy (triglycerides)¹. For example, the many different lipids produced by microorganisms are dispersed in aqueous phase after grinding and a suitable fractionation strategy must be employed. It was shown that lipids with different unsaturated chains don't mix together and form rafts at fat globule interfaces, and that triglyceride organization at the globule interface, changing with temperature, may modify the interfacial properties ². Depending on the detailed composition, the molecules can be at the lipid droplet interface, in the lipid bulk, organized as liquid crystals or oleosome in the aqueous phase etc. and the separation procedure may vary.

Thus, the determination of the local organization (3D structure with eventual heterogeneity) will allow building fractionation strategies (for example destabilization of aggregates by shear rate or temperature variation to induce reorganization). It will help to understand the impact of molecular organization at the oil-water and liquid-solid interfaces that are key parameters for the processes.

It becomes also important to understand the behavior of the polyunsaturated lipids (ω -3 and ω -6) that have nowadays to be introduced in food matrices, because of recent nutritional recommendations. Innovative formulations containing the unsaturated fatty acids also have to prevent their oxidation or degradation. Berton *et al.*³ have shown that the oxidation of fragile unsaturated lipids depends on the nature of the water-oil droplet interface composition. A controlled local structure is therefore needed. The organization of lipids in emulsions is also very important in the domain of cosmetics and medicine, for controlled drug delivery for example.

Unfortunately, direct observation of local organization through experimental means is difficult² and/or expensive^{4,5}. Molecular simulations are becoming a tool of growing importance, applied to different systems, from simple fluids to complex biomolecules, soft-matter and nano-materials. By looking at phenomena at the molecular scale, computer simulations

Publishing ribute to a better understanding of the structure-property relationships. It is a remarkable tool to investigate the effect of small changes in molecular structure or composition onto spatial organization for e.g. surfactants in water or lipid in water emulsion stability.

One requirement for reliable molecular simulations is a correct sampling of the various degrees of freedom in the system. When using atomistic molecular dynamics, a correct sampling can be achieved if simulated times exceed the largest relaxation time in the system. In a recent paper, Skjevik et al.⁶ have used large GPU based computers to study lipid bilayer self-assembly. They have shown that the typical timescale for the formation of a phospholipid bilayer is of the order of a few hundreds of nanoseconds, a quite large value for all-atom simulations. Therefore, the timescales involved in the physical processes studied are too high to be studied systematically by molecular simulation at the atomistic level.

One route to reach larger time and length scales is to adopt coarser models where particles represent a group of atoms, typically between 3 and 10 heavy atoms (C, N, O, S, etc). By reducing the number of particles to handle (for a given physical system), simulations can be realized over a reduced computing time. Moreover, because interaction forces between particles are softer, larger timesteps can be employed during the simulations. Finally, accessible timescales can be increased by two or more orders of magnitude, depending on the details of the coarse-graining procedure.

The second requirement for molecular simulation is a good description of the interparticle forces. These forces are described empirically by simple functions of the particle positions. The set of parameters plus the analytical force expressions is called the force field (FF). In recent years, many efforts have been made to derive coarse-grained (CG) force fields adapted to different types of molecules (see e.g.⁷). However, when dealing with lipids, the Martini FF appears to be one of the most used and validated⁸. As every coarse-grained force field, dynamics is usually faster than real one, although a global time scaling factor seems to apply when using the Martini force field. As mentioned by Baron et al.⁹, thermodynamic properties could be reproduced provided the CG model is re-parameterized on the basis of the some liquid-phase properties. Recently, Bereau and Kremer¹⁰ proposed an automated parameterization procedure for common small organic molecules. The method was able to reproduce the water-octanol partitioning free energy of more than 650 neutral compounds with a deviation of the order of magnitude of the thermal energy at room temperature. One of the advantages of the original Martini force field is its limited set of parameters,

Publishiwgich make it relatively easy to adjust or optimize the interactions¹¹. Although it was designed primarily for lipids (free fatty acids, triglycerides, phospholipids, cholesterol etc.^{12,13}) extensions to proteins have been proposed¹⁴ as well as carbohydrates¹⁵.

Recently, Neyt et al.¹⁶ compared atomistic and coarse-grained (Martini force field) predictions for the interfacial tension (IT) at the oil-water interface. They mention that CG models are able to reproduce qualitatively the effect of the salinity on the interfacial tension of the system, although a more developed calibration should be necessary for more quantitative results. Ndao et al.¹⁷ applied the same methodology to the prediction of interfacial tension in several organic molecule-water systems. They also insist on the need for a re-parameterization to better match the interfacial tension. They emphasize the fact that liquid-liquid interface equilibration is an issue which can be partially resolved using CG rather than all-atoms models.

In this work, an artificial oil in water emulsion analogous to those found in bioresources or food matrices is simulated, composed of a limited number of compounds: oleic acid and the corresponding triacylglyceride, trioleic glyceride, or triolein. Before studying oil mixtures in water, force field parameter for the OA head is calibrated against the water-OA interfacial tension. Then we investigate molecule organization, mainly at the interface, and its impact on a macroscopic parameter, the interfacial tension of the mixture. Results are compared with our experiments and results from literature (interfacial tension, water solubility in oil, area per molecule). We demonstrate the relevance of the CG simulation to describe the water-oil interfacial behavior of organic compounds.

II. METHODOLOGY

A. Experiments

Experiments were performed to measure the interfacial tension. The oily mixtures were composed of pure glyceryl trioleate (purity grade $\geq 99\%$, 885.43 g mol⁻¹, Sigma-Aldrich) and oleic acid (purity grade $\geq 99\%$, 282.46 g mol⁻¹, Sigma-Aldrich). The proportion of each compound was adjusted with an automatic pipette and verified through weighting. The oleic acid proportion in the organic phase was 0, 5, 10, 20, 40, 60, 80,100 $\%_{v/v}$. The density of glyceryl trioleate, oleic acid and water are respectively 0.910 kg L⁻¹, 0.890 kg L⁻¹

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Publishi(figure ma-Aldrich data) and 0.99786 kg L^{-1} . The density of a mixture GTO-OA (40/60v/v) was measured at 0.904 kg L^{-1} .

The interfacial tension between oil and water was measured using the pendant drop method (Drop Shape Analyser DSA 30, Krüss) at a constant temperature of 295 K. A pendant water drop was formed with a clean disposable syringe filled with ultrapure water associated to a needle (diameter 1.8 mm) inside a 8 mL cuve made of quartz filled with lipid phase, so that the drop profile allow a mathematical analysis with a model based on the Young-Laplace equation coupled with the calculation of the pressure difference between inside and outside the drop ^{18,19} (equation 1). The shape factor defined by Song¹⁹ was > 0.5 to minimize the interfacial tension error. The experimental densities of oil and water were input parameters and were supposed constant. Equilibrium was reached after a few minutes. Finally, the interfacial tension was obtained from the equation 1. The schematic droplet profile is presented in figure 1.

$$\gamma \left(\frac{1}{R_1} + \frac{1}{R_2} \right) = \frac{2\gamma}{R_0} + \Delta \rho gz \tag{1}$$

with γ , the interfacial tension, R_0 , R_1 and R_2 , curvature radii of the non-spherical interface, $\Delta \rho$, the density difference between water and oil, g, the gravitational acceleration, z, the vertical height measured from the datum plane.

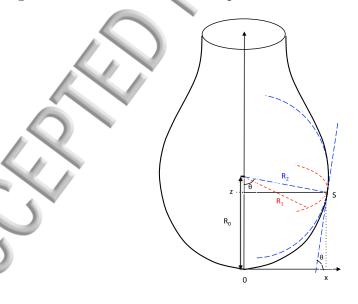


Figure 1: Pendent drop with curvature radii R_0 , R_1 and R_2 at an arbitrary point S on a convex surface



Molecular Coarse Grained Simulations

We used the MARTINI force field ¹³ to describe interactions between all particles in the system. The Martini force field has been optimized to reproduce partitioning free energy of a large number of chemicals between polar and non-polar phases. Each particle represents a small number of atoms, typically 3 or 4 heavy atoms. The force field considers only four main types of interaction sites and up to 18 subtypes. Hence, the use of MARTINI force field first requires to represent the molecules of interest into coarse-grained particles and to associate them with the correct subtype. The force field parameters are given in the supplementary information.

$1. \quad Modeled \ molecules$

In this work, four water molecules are modeled as a single P_4 particle. In order to prevent the coarse-grained water model from freezing, so called "antifreeze" water particles have been introduced at a mole fraction of 0.1 in water ¹³. Anti-freeze particles are of subtype BP_4 with identical parameters as P_4 particles. The antifreeze effect is obtained by scaling up the Lennard-Jones parameters between BP_4 and P_4 particles. The Lennard-Jones size parameter σ is changed to 0.57 nm and the interaction energy parameter ε is equal to 5.6 kJ mol⁻¹.

The cis-9-Octadecenoic acid (OA) is composed of a carboxylic head and a long hydrophobic tail with one unsaturated bond. At the MARTINI coarse-grained level, it is composed of three particle types and a total of five particles, as shown in figure 2a. The OA tail is modeled with three C_1 beads and one slightly more polar bead of type C_3 to account for the unsaturation. We considered that the acid head -CH₂COOH is neutral of main type P. From the paper by Marrink et al.¹³, the most natural choice would be the type P_3 which corresponds to acetic acid. However, other choices are possible. In a study of pH effect on oleic acid aggregates, Bennett et al.^{20,21} used parameters adapted from aspartic acid from the MARTINI 2.1 force field¹³. The amino-acid region is modeled as a P_3 bead in aspartic acid whereas it is described as P_1 in serine, threonine, lysine and glutamic acid. We found a model for palmitic acid where the head group is represented by a P_4 bead²². Therefore, as will be shown below, we decided to select the correct subtype by comparison between the experimental and the simulated interfacial tension of the pure OA with water interface.

Publishingery P subtype was studied, but P_5 which is more polar than water. OA molecule will then be described as: P_i - C_1 - C_3 - C_1 - C_1 .

Glyceryl trioleate parameters are taken as provided by Timu Vuorela on the MARTINI web site²². This parameter set is based on standard MARTINI 2.1 force field plus angle potential refinement as described in Vuorela *et al.*²³. A schematic of the GTO molecule along with the coarse-grained types is given in figure 2b. Each bead represents four heavy atoms, but the glyceryl bead, composed of three heavy atoms only. Each tail is described by a non-polar group of subtype N_a corresponding to the ester, followed by an OA tail (-C₁-C₃-C₁-C₁) leading to a general coarse-grained structure: C₁(-Na-C₁-C₃-C₁-C₁)₃.

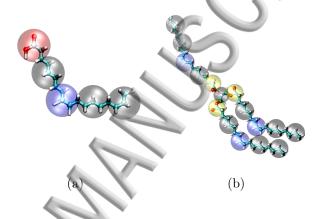


Figure 2: Schematic of (a) OA and (b) GTO molecules at both atomistic and coarse-grained description levels. Each coarse-grained particle contains four heavy atoms. Particle types are P (red), N_a (yellow), C_1 (black) and C_3 (blue).

2. Simulation tools

Molecular dynamics simulations were done with the LAMMPS code²⁴. We controlled LAMMPS input parameters in order to reproduce precisely the interactions that were used during force field optimisation. Thus, dispersion-repulsion interactions are described using the Lennard-Jones 12-6 potential with energy and forces vanishing at a cut off distance r_c . This is implemented in LAMMPS using a standard shift function (third-order polynomial)⁹. The Lennard-Jones potential was shifted between $r_{\rm shift} = 0.9$ nm and $r_c = 1.2$ nm. Lennard-Jones interactions also apply between second (and more) nearest neighbors inside each molecule. Bonded interactions between adjacent beads are described by an harmonic

Publishipg ential of the corresponding bead distance and chain bending is represented using an harmonic potential of the cosine of angles between adjacent bonds. Equations of motion are integrated using the velocity-Verlet algorithm as implemented in LAMMPS with a time step of 20 fs. During NVT simulations and $NP_{zz}T$ simulations (see below), a time constant of 40 ps is used for the thermostat and a time constant of 400 ps is used for the barostat.

3. Simulation

In this work, the influence of the oil phase composition onto the oil–water interfacial tension, γ , is studied. For all studied systems, the water amount is constant and roughly represents one third of the system volume. Nine different systems were simulated with different OA to GTO ratio. Detailed compositions are given in table I. The initial OA molar fraction was calculated according to equation 2 using the initial amount of OA and GTO molecules in the simulation box, n_{OA}^0 and n_{GTO}^0 , respectively.

$$x_{\rm OA}^0 = \frac{n_{\rm OA}^0}{n_{\rm OA}^0 + n_{\rm GTO}^0} \tag{2}$$

Initial configurations were built using the PACKMOL package²⁵ to speed up the equilibration part. The shape of the simulation box is parallepipedic. Box length in z direction is four times the value in x and y directions. Two interfaces are created normal to the z direction and water molecules are initially separated from oil molecules. OA and GTO molecules are randomly distributed inside the oil phase. After creation, the total energy of the box is minimized using a conjugate gradient method. Then, box volume is rescaled in order to bring the system close to the experimental density. The system is then allowed to relax for 160 ns at 300 K and 1 bar using the isothermal-isobaric algorithm of Shinoda et $al.^{26}$. More precisely, the pressure along the z axis, P_{zz} , is imposed during the run and box length in z direction is allowed to change while box lengths in x and y directions remain constant. This step enables to reach mechanical equilibrium, a crucial step before computing interfacial tension. During this $NP_{zz}T$ run, the average box length in the z direction is computed over the last 100 ns where a plateau clearly appears. This average box length is therefore applied to the simulation box. Typical box dimensions are 107 x107 x 465 Å.

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Publishifigually, a very long production run of 2 μ s is realized for each system in the NVT ensemble at 300 K and equilibrium properties are computed along the last 1.6 μ s.

Some verifications were made but not detailed in the paper: we checked that the demixing arises if we start with all species placed randomly; we verified on system 2 that the interfacial tension value and the final organization are identical if all OA molecules are initially placed at the oil—water interface or placed randomly into the oil phase; it was also verified that the temperature change between 290 and 310 K has a negligible impact on the interfacial tension.

4. Interfacial tension

Interfacial tension γ can be computed from the following expression (known as the Kirkwood-Buff expression) ²⁷:

$$\gamma_{\rm KB} = \frac{L}{2} \langle P_{\perp} - P_{\parallel} \rangle \tag{3}$$

where L is the box length in the z direction (normal to the interface) and P_{\perp} and P_{\parallel} are the instantaneous pressure components, respectively normal and parallel to the interface. The factor one half comes from the fact that two interfaces appear in the simulation box. The ensemble average is taken over the canonical ensemble. During the course of the simulation, the full pressure tensor is computed, from which instantaneous values of $P_{\perp} = P_{zz}$ and $P_{\parallel} = 1/2(P_{xx} + P_{yy})$ are deduced.

It must be noted that equation 3 is valid only in the limit where the range of interaction forces is small relative to the distance L. In the practical case of molecular simulation, it means that the simulation box must be large enough to avoid any interaction between the two oil—water interfaces. This can be checked by looking at the pressure profil along the direction normal to the interface. In this work, we used the algorithm proposed by Nakamura et al.²⁸ to compute the local pressure tensor in Cartesian coordinates in LAMMPS. In this approach, the simulation box is divided into 300 slices parallel to the interface and the pressure tensor elements are computed inside each region. The slice thickness varied between 1.55 Å and 1.58 Å depending on the system studied. Figure 3 shows the evolution of $P_{\perp}(z)$ and $P_{\parallel}(z)$, local values of pressure components in a slice around z. We observe that $P_{\perp}(z)$ is constant along the z axis, as expected for a system at mechanical equilibrium. On the contrary, large variations of $P_{\parallel}(z)$ are observed around layers 50 and 230, corresponding to the location

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Publishing the water-oil interfaces. However, both components are identical far from interfaces, indicating that the simulation box is large enough to compute the interfacial tension. In this work, the interfacial tension will be computed using the local pressure components^{29,30}:

$$\gamma_{\rm IK} = \frac{1}{2} \int_0^L \left[\langle P_{\perp}(z) \rangle - \langle P_{\parallel}(z) \rangle \right] dz \tag{4}$$

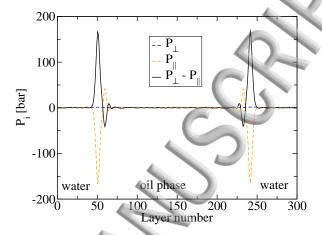


Figure 3: Local pressure components for system 7 (see table I), along the z direction. The time average normal component $\langle P_{\perp}(z) \rangle$ is constant along the z axis, as expected for a system at mechanical equilibrium. The location of interfaces can be clearly seen around layers 50 and 230, where large variations of the pressure component $\langle P_{\parallel}(z) \rangle$ occur. Layer width for system 7 is 0.156 nm.

III. RESULTS

A. Parameterization of the polar head of OA

As mentionned in section IIB, several particle types can be used to describe the polar head of OA, *i.e.* the carboxylic acid group. No unanimous opinion can be gathered because the polarity of the acidic group depends on the electron donor capacity of the lateral chain^{14,31}. In this work, we decided to test several polar head types for the oleic acid, namely types P_1 to P_4 , and to select the one giving the best estimate of the interfacial tension for the water–oleic acid binary.



| System | $n_{ m GTO}^0$ | n_{OA}^{0} | n_{W}^{0} | x_{OA}^{0} |
|--------|----------------|-----------------------|----------------------|-----------------------|
| 1 | 1874 | 0 | 15000 | 0 |
| 2 | 1780 | 300 | 15000 | 0.144 |
| 3 | 1686 | 600 | 15000 | 0.262 |
| 4 | 1500 | 1200 | 15000 | 0.444 |
| 5 | 1126 | 2400 | 15000 | 0.681 |
| 6 | 938 | 3000 | 15000 | 0.762 |
| 7 | 750 | 3600 | 15000 | 0.827 |
| 8 | 374 | 4800 | 15000 | 0.928 |
| 9 | 0 | 6000 | 15000 | |

Table I: Composition of the studied systems. n_i^0 is the initial number of molecules of species i introduced in the simulation. Considering the initial full phase separation, x_{OA}^0 is the initial mole fraction of OA in the oil phase.

We present in figure 4 the interfacial tension at the water–OA interface (system 9) computed from molecular dynamics using different polar head types. The computed values are compared with the experimental data obtained using the DSA apparatus, 11.4 ± 0.3 mN m⁻¹. It is worth noting that our value is much lower than the one reported by Demond and Lindner³², 15.59 mN m⁻¹ (see reference 3 therein, from Young and Harkins, 1928). However, it is in good agreement with recent data from Kallio *et al.*³³, 12.0 ± 0.5 mN m⁻¹.

As expected, the interfacial tension decreases as the polarity of the polar head increases and get closer to the water bead type polarity. The interfacial tension calculated with particle P_2 fits well with the experimental one. Type P_2 was thus selected for the rest of the simulations to describe the OA polar head in order to reproduce correctly the water–OA interfacial tension. This result indicates that the polar head in OA is less polar than acetic acid (P_3) which is consistent with a more important donor character of a long aliphatic carbon chain.



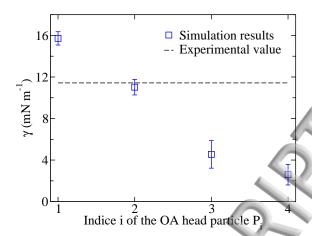


Figure 4: Interfacial tension of the water-OA mixture (system 9) versus the index i of the carboxylic acid polar bead P_i . The higher the index i, the higher the polarity of the bead.

B. Reaching the equilibrium state

Before computing any property, it is mandatory to check that simulation boxes have reached thermodynamic equilibrium. The initial configurations already contain two phases but some time is required before local concentrations reach their final values: depending on the lipid phase composition, OA and GTO molecules leave or enrich the interfaces whereas a few water molecules leave the aqueous phase and solubilize into the lipid phase. The timescale associated with these processes is rather long, even with a coarse-grained force field like MARTINI. To monitor the system behavior during the transient state, the time evolution of the number of water, OA and GTO molecules in the bulk of the lipid region was followed (see below for a precise definition of the bulk lipid region). We present in figure 5 the number of molecules into the bulk region n_i^b . As expected, the number of water molecules in the lipid phase first increases with time, OA molecules leave the bulk lipid region and migrate towards the interfaces while GTO molecules move in the opposite direction. Obviously, this process depends on temperature, phase composition and dimensions of the simulation box; though, as can be seen in figure 5, the timescale for this process is typically in the range 400-600 ns. The same range is observed for all systems studied. Moreover, the MARTINI force field has been shown to speedup dynamical processes by a factor of four^{8,13}, meaning that the "physical" time needed to reach chemical equilibrium in this system can therefore be as large as 2 μ s.



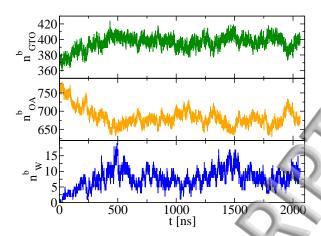


Figure 5: Time evolution of the number of water (W), OA and GTO molecules into the lipid bulk region n_i^b for system 5 (simulation timescale).

C. Local organization in the ternary mixtures

We present in figure 6 the local mass density of bead types in systems 2 and 7, *i.e.* with low and high OA/GTO ratio, respectively. The mass density profil is built using the position of each bead type along the z axis, normal to the water–oil interfaces. Each full box length is divided into 300 layers of 0.156 ± 0.001 nm. The local density is thus the mass per layer for each bead divided by the layer volume, averaged over 1.6 μ s data at equilibrium. Water (P₄ type) and anti-freeze water (BP₄ type) densities are represented explicitly along with OA head (P₂ type), OA tail (C₁ and C₃ types) beads, GTO ester groups (N_a type) and GTO tails (C₁ and C₃ types). The total density per layer is also shown.

Three distinct regions can be distinguished: the aqueous region, between layers 0-40 and 260-300, the lipid bulk region between layers 120-180 and two interfacial regions. Aqueous and lipid bulk regions are homogeneous and not perturbed by the presence of the interfaces: the total density profile is flat in the corresponding regions. We also notice that the average density of water in the aqueous region is 0.896 g cm⁻³, very close to the bulk density of water plus anti-freeze water (0.1 bead ratio BP4/P4) obtained by us using independent simulations under the same thermodynamic conditions: 0.898 g cm⁻³. For the lipid bulk region, we did independent simulations of pure OA and pure GTO and obtained equilibrium densities of 0.818 g cm⁻³ and 0.841 g cm⁻³, respectively. These values are identical within 0.1% to the OA density in system 9 (water–OA) and the GTO density in system 1 (water–OA)



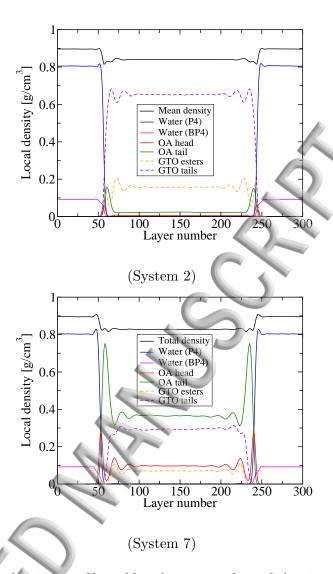


Figure 6: Local mass density profiles of bead types and total density in systems 2 and 7.

Layer width is 0.156 nm.

GTO). Therefore, as the bulk properties are reproduced in the aqueous and lipid regions, the simulation boxes are considered large enough to study at the same time bulk and interfacial properties.

Although computed densities in the water and lipid regions agree with bulk densities of the models, they are notably different from experimental values (by roughly 10% for water and 8% for the lipids). This clearly indicates some limitations of the MARTINI force field. A spurious effect was also observed concerning the local organization of P_4 versus BP_4 beads at the water–oil interface, discussed in the SI.

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Publishing No lipid molecule is totally dissolved in the aqueous phase whereas several water beads are totally dissolved in the lipid region. A fraction of oleic acid and trioleate molecules are organized at the water-oil interface. The corresponding polar beads, P_2 for OA and N_a for GTO, are in contact with water beads, whereas tail beads C₁ and C₃ are in contact with the lipid phase only. When OA and GTO are present at the interface, the P2 beads are more in contact with water beads than N_a beads. All ternary mixtures (systems 2 to 8) present the same characteristics. We also notice some interesting structure for the interfacial region. The maxima of local density of polar beads P_2 and N_a coincide with the minima of tail beads. A detailed analysis and inspection of the density profile shows that a lipid bilayer is formed by OA and GTO molecules at the water-oil interface whatever the composition of the system, even for pure GTO. This is further confirmed by the distance between the two planes of polar beads (25-30Å) compared with the length of OA molecule (14Å). Snapshots showing the bilayers for the systems 1 and 9 (pure GTO and pure OA oil phases) are presented in figure 7 and a schematic representation of the bilayers is shown in figure 8. A more quantitative analysis is given in SI, as well as movies of system 5 that demonstrate the bilayer presence, the large occupation of the interface by OA molecules, and the exchange of OA and GTO between the bulk and the interfacial layer.

D. Lipid phase composition

As mentioned earlier, water, OA and GTO local molar fractions change with time until some equilibrium is reached. The equilibrium state is characterized, in particular, by the molar fraction of the different species in the lipid bulk phase x_i^b (layers 120-180), *i.e.* the region far from the water-oil interfaces (equation 5).

Because of the limited number of molecules in the simulation box, the OA (and GTO) molar fraction in the lipid bulk region, x_{OA}^{b} can be significantly different from the *initial* molar fraction x_{OA}^{0} (equation 2) and from the interfacial molar fraction x_{OA}^{int} (equation 6).

$$x_{\text{OA}}^{\text{b}} = \frac{n_{\text{OA}}^{\text{b}}}{n_{\text{OA}}^{\text{b}} + n_{\text{GTO}}^{\text{b}}} \tag{5}$$

$$x_{\text{OA}}^{\text{int}} = \frac{n_{\text{OA}}^{\text{int}}}{n_{\text{OA}}^{\text{int}} + n_{\text{GTO}}^{\text{int}}}$$
 (6)



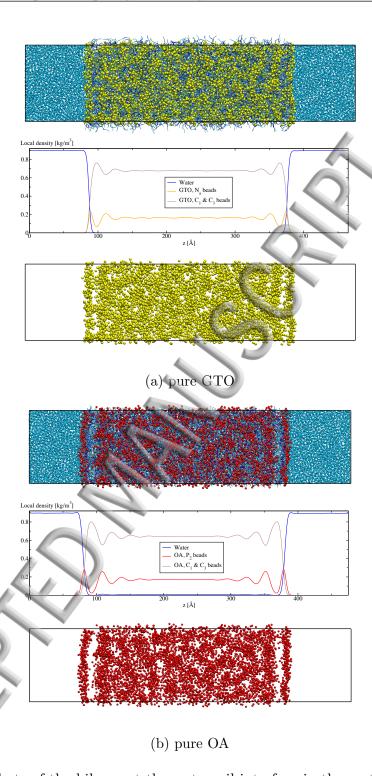


Figure 7: Snapshots of the bilayer at the water–oil interface in the systems 1 containing pure GTO oil phase (a) and 9 containing pure OA oil phase (b). The snapshots with all the beads and with only the polar beads (P_2 or N_a) are compared to the density profiles of the corresponding simulation. Snapshots produced thanks to VMD software^{34,35}



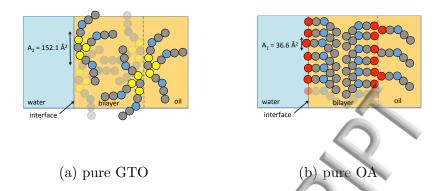


Figure 8: Graphical representation of the bilayer at the water-oil interface for the system 1 containing pure GTO (a) and the system 9 containing pure OA (b)

This is not true for macroscopic systems were the number of molecules in the bulk phase is much larger than the number of molecules at the interfaces. In macroscopic systems, the bulk phase serves as a reservoir for OA (and GTO) molecules and $x_{\rm OA}^{\rm b} \approx x_{\rm OA}^{\rm 0}$. Therefore, care should be taken to account for this difference, when comparing interfacial tension (or other composition dependent properties) obtained from molecular simulations with experimental data. We report table II the computed OA mole fraction in the lipid bulk phase and compare it with the initial value for each system. It is important to note that, although OA is not a surfactant molecule, the final bulk concentration is always smaller than the initial concentration, especially at low OA composition.

We present in figure 9 the estimation of water solubility in the lipid bulk phase as a function of OA molar fraction. Computed values are compared with measurements from Platford³⁶ and Chiou³⁷. Experimental data give water solubility in pure OA and pure GTO in the range 283-310 K. They show that water is much more soluble in OA than GTO and also that solubility strongly depends on temperature: according to Platford³⁶, solubility in OA changes from 0.13 mol L⁻¹ at 283 K to 0.26 mol L⁻¹ at 310 K and solubility in GTO changes from 0.051 to 0.1 mol L⁻¹ over the same temperature range. Water solubility in GTO given by Chiou is 0.056 mol L⁻¹ at 298 K, smaller than Platford value of 0.072 at 293 K. A single data point in a OA–GTO mixture, at $x_{OA}^b \approx 0.75$ is provided by Platford, at 310 K.

As can be seen in figure 9, molecular simulation data are in fair agreement with experi-



| System | x_{OA}^{0} | $x_{\mathrm{OA}}^{\mathrm{b}}$ |
|--------|-----------------------|--------------------------------|
| 1 | 0 | 0 |
| 2 | 0.144 | 0.105 |
| 3 | 0.262 | 0.203 |
| 4 | 0.444 | 0.362 |
| 5 | 0.681 | 0.630 |
| 6 | 0.762 | 0.720 |
| 7 | 0.827 | 0.802 |
| 8 | 0.928 | 0.917 |
| 9 | 1 | |

Table II: Initial and equilibrium OA mole fraction in the lipid bulk phase (layers 120-180).

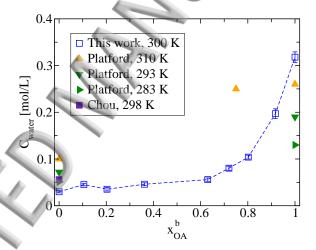


Figure 9: Water concentration versus OA concentration in the lipid bulk phase. Molecular simulation data are compared with experimental measurements from Platford 36 and Chiou 37

ments. Water solubility is lower in GTO than OA. Molecular simulation data overestimate water solubility in OA and underestimate water solubility in GTO. The solubility value in the OA-GTO mixture is not correctly predicted by simulation. Platford measured a solubility close to the one in pure OA at 310 K. Molecular simulations clearly show that water solubility strongly increases with OA concentration, though only for x_{OA}^b larger than 0.65.



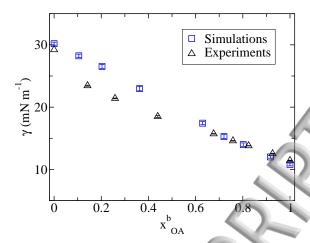


Figure 10: Measured and computed interfacial tension γ , versus OA molar fraction in the bulk region x_{OA}^{b}

Clearly, more experimental data at intermediate concentration would be required to confirm the water solubility values in OA–GTO mixtures.

E. Interfacial tension and area per molecule analysis

We present in figure 10 the computed interfacial tension between water and OA–GTO mixtures versus OA molar fraction in the bulk region. The interfacial tension γ decreases linearly with increasing OA concentration in the organic phase. This is consistent with the amphiphilic properties of OA due to the polar head and the apolar tail. A good agreement is observed between computed and experimental data shown in figure 10 for OA molar fraction above 0.6. For $0 < x_{\rm OA}^b < 0.6$, the interfacial tension is overestimated by up to 15%. However γ for water–GTO and water–OA systems are well predicted: the computed interfacial tensions for GTO and OA are respectively 30.2 ± 0.3 mN m⁻¹ and 10.8 ± 0.3 mN m⁻¹, with corresponding experimental values of 29.2 ± 0.1 mN m⁻¹ and 11.4 ± 0.1 mN m⁻¹. The disagreement observed at low OA concentration suggests that OA–GTO interactions are not well described, leading to incorrect concentrations at interfaces: OA concentration at interfaces should be larger in order to recover experimental data.

We tried to compare these values with theoretical predictions. There exists only a few methods to predict interfacial tension data for multicomponent mixtures. From a practical point of view, the Fu et~al. method³⁸ is one of the most employed for ternary mixtures. It is

Publishing of on a thermodynamic relationship established by Shain and Prausnitz³⁹. Using several assumptions, Fu et al. were able to relate interfacial tension to the mutual solubilities of the different species. Since OA or GTO and water are almost immiscible, the mutual solubilities can hardly be measured or even more computed. It is therefore difficult to estimate γ in the ternary systems from data obtained using simulation. Instead, we computed interfacial tension of binary systems, assuming that OA and GTO concentration in water is zero. The interfacial tension can thus be obtained from:

$$\gamma = -\ln(x_w^o) \frac{KRT}{A_w} \tag{7}$$

where x_w^o is the water molar fraction in the oil phase, K=0.9414 is a constant proposed by Fu et al., R is the perfect gas constant, T the temperature and $A_w=35.6 \text{ Å}^2$ per molecule, the Van der Waals surface area of the water molecule. Using water concentrations issued from molecular simulations, we obtain $\gamma_{\text{w-OA}}=25.1 \text{ mN m}^{-1}$ and $\gamma_{\text{w-GTO}}=37.8 \text{ mN m}^{-1}$. It is clear that the model proposed by Fu et al. is in disagreement with a direct computation of interfacial tensions. This may come from an incorrect value for K. As evidenced by Santos et al.⁴⁰, the constant K can differ from the one proposed by Fu et al., depending on the type of mixtures investigated. Clearly, precise molecular simulations on model systems could help to check the Fu et al. equation.

Although the computed interfacial tension is not in full agreement with measurements, we believe that these simulations contain realistic informations about the local structure at the oil–water interface. The number of OA and GTO molecules in the interfacial region were computed using the local density profiles of P_2 and N_a beads, by direct integration of their first peak at the oil-water interface. From our simulations on systems 1 and 9, the area occupied by OA and GTO at the interface between pure product and water are respectively $A_{OA}^* = 36.6 \text{ Å}^2$ and $A_{GTO}^* = 152.1 \text{ Å}^2$. The results are compared to Langmuir balance experiments that were described in the literature for OA and GTO^{41–43} and complementary experimental results (figure 11). The principle of these experiments is to spread lipid molecules as a monolayer on an water–air interface and to compress this interface with barriers. According to literature, a film of pure OA presents a compressed liquid organization with an area per molecule between 20 and 50 Å². A film of pure GTO presents an expended liquid phase with an area per molecule between 100 and 150 Å². The film collapses for lower area per molecule. In the simulation, in presence of a majority of OA at the interface, the



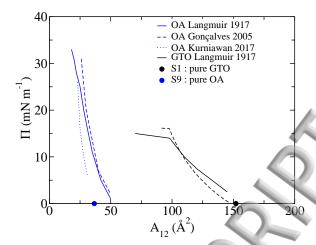


Figure 11: Surface pressure Π at the water-oil interface versus the area per molecule A_i .

compared to experimental data obtained with pure OA and pure GTO ^{41–43}

area is 36.6 Å². This result corresponds to a condensed liquid phase and correlate to the experimental results. Considering the simulations with pure GTO, the area is 152.1 Å², similar to the experimental data in the same conditions and an expended liquid phase is present.

We present in figure 12 the evolution of the global area per molecule, A, along with the excess area per molecule, A_{ex} defined as:

$$A_{\rm ex} = A - \left[x_{\rm OA}^{\rm int} A_{\rm OA}^* + (1 - x_{\rm OA}^{\rm int}) A_{\rm GTO}^* \right]$$
 (8)

where the term in braquets is an *ideal contribution*, A^* , and $x_{\text{OA}}^{\text{int}}$ represents the OA molar fraction at the interface. The excess area presents a small positive deviation, showing that the interface is slightly less compact than ideal product. The excess area reaches 5 Å² for $x_{\text{OA}}^{\text{int}} = 0.891$. However, the small values observed show that a rather good mixing of OA and GTO occurs at the interface, which seems realistic with identical hydrophobic tails.

IV. CONCLUSION

Nine systems containing oleic acid and triolein mixtures in contact with water were simulated using a coarse grained molecular simulation and the MARTINI force field. The polar bead P_2 was chosen to represent the fatty acid head in order to reproduce the experimental interfacial tension.



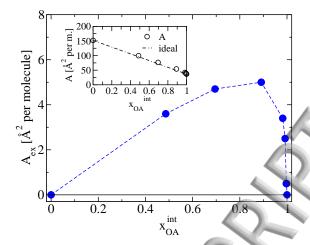


Figure 12: Excess surface per molecule, A_{ex} , versus $x_{\text{OA}}^{\text{int}}$, the molar fraction of OA at the interface. Insert: area per molecule A and ideal mixture A^* contributions.

Large simulation boxes (107 x 107 x 465 Å³) are required to ensure that the two present interfaces have no interaction. The simulations ran during 2000 ns, 500 ns to reach chemical equilibrium and 1500 ns to produce trajectories along which interfacial tension, water solubility and local densities were computed. If we account for the dynamical speedup (roughly 4) introduced by the MARTINI force field, the physical time needed to reach equilibrium is 2 μs and the production runs last for 6 μs . Such long timescales support the use of CG simulations. Inspection of density profiles suggests that a bilayer structure of the lipids exists at the water-oil interface.

Computed interfacial tensions are close to experimental values with a small deviation of maximum 15% at low OA concentrations. The water solubility in the lipid phase is in fair agreement with experiments, between 0.03 and 0.32 g L⁻¹, rising with the OA content. The surface area occupied by OA and GTO fit with experimental data; under simulation conditions OA organization at the interface is that of a compressed liquid whereas GTO behaves like an expended liquid.

Through all these results the usefulness of CG simulations for the analysis of water–oil interfacial organization is demonstrated. This method will bring local informations on the organization of target compounds, for example in biomass fractionation processes or food additives formulations.

Also, we are quite confident that this CG model can be extended to the prediction of interfacial tension and water solubility of fatty acids and triglycerides with different chain

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Publishings the (e.g. palmitic, arachidic, linoleic acids, and the triglyceride derived from these fatty acids). These quantities can be useful in order to derive new theoretical models which are really scarce in this area (water, fatty acids, triglycerides).

SUPPLEMENTARY MATERIAL

See supplementary material to obtain details on the force filed parameters, the behaviour of P₄ and BP₄ at the oil–water interface, a deepened analysis of the lipid organisation demonstrating the bilayer organization, movies that illustrate the bilayer and the evolution of local OA and GTO composition at the interface versus OA mole fraction in the oil phase.

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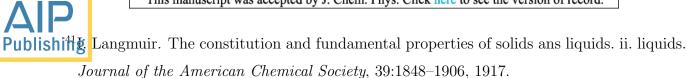
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