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## **Computational Filterability and dewatering determination based on shape and size distribution of solid suspensions**

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### **ABSTRACT**

Dewatering after filtration is an important issue, as it determines the transferability and the final cost of dewatering for the product. Any optimization in the dewatering step will improve the process. This paper shows the effect of particle properties such as shape factor and size distribution on dewatering efficiency. An experimental plan was established to show the influence of the working pressures (filtration and dewatering pressures) on residual moisture and dewatering time. This plan was repeated on four calcium carbonate particle shapes: needles, plates, spheres, and cubes. The first data from these experiments showed that the volume shape factor of the particle has no effect on cake behavior during dewatering. The same-shaped iso-response curves of residual moisture as a function of the filtration pressure and the dewatering pressure were obtained for each particle shape. It was also shown that raising the dewatering pressure can in fact lead to a wetter cake if this pressure is higher than the cake filtration pressure. This fact points out a counterproductive phenomenon that the industrial operator has to avoid.

The experimental considerations were compared to a model for dewatering based on work by Tarleton and Wakeman combined with a specially-developed filtration model. This combination enabled the computation of cake resistance and compressibility, as well as cake dewatering behavior, using easily measurable parameters. It can serve the industrial process in the choice of the appropriate liquid-solid separation device, and provide information as to the pressure conditions necessary to obtain the wettest cake possible for a time-fixed dewatering or to see if a wet target can be reached and in how much time.

### **KEYWORDS**

Deliquoring, Pressure Filtration, Modeling, Solid-liquid-separation, Suspension

## **1. Introduction**

Once the cake is built after filtration, industrial needs to reduce the residual moisture to get a dryer cake.

The deliquoring helps to cut down the costs of drying and improves the transferability of the cake between the different steps of the process. Knowing the optimal deliquoring pressure will also improve the productivity of the process and increase the profits of an industrial application.

The residual moisture after filtration has to be linked with particle properties such as Particle size Distribution or shape factor.

This paper aims at studying the variation of the behavior of the cake during deliquoring as a function of the shape factor. A model for dewatering based on work by Tarleton and Wakeman (2007) combined with a specially-developed filtration model will also be presented. This combination enabled the computation of cake resistance and compressibility, as well as cake dewatering behavior, using easily measurable parameters.

## 2. Simulation procedure

The simulation of deliquoring is based on work by Tarleton and Wakeman (2007). The first step is to consider Darcy's law combined with Ergun's equation (Equation 1):

$$k = \frac{1}{\alpha\rho_s(1-\varepsilon)} = \frac{\varepsilon^3 D^2}{180(1-\varepsilon)^2} \quad (1)$$

Thanks to equation 1, the effective particle diameter can be calculated:

$$D = \sqrt{\frac{180(1-\varepsilon)}{\alpha\rho_s\varepsilon^3}} = 13.4 \sqrt{\frac{(1-\varepsilon)}{\alpha\rho_s\varepsilon^3}} \quad (2)$$

Wakeman proposes a correlation to calculate the irreducible saturation thanks to this effective diameter and a calculation of the capillary number (Equation 3 and 4):

$$Ca = \frac{\varepsilon^3 D^2 (\rho_l g L + \Delta P)}{(1-\varepsilon)^2 L \sigma} \quad (3)$$

$$S_\infty = 0.155(1 + 0.031Ca^{-0.49}) \quad (4)$$

If the objective is to calculate the residual moisture obtained in a cake after a fixed time and pressure of deliquoring, the dimensionless time and pressure are calculated:

$$\tau = \frac{k p_b}{\mu \varepsilon (1 - S_\infty) L^2} t_d \quad (5)$$

$$p^* = \frac{\Delta P}{p_b} \quad (6)$$

The product  $\tau p^*$  can be linked with the reduced saturation thanks to an experimental curve.

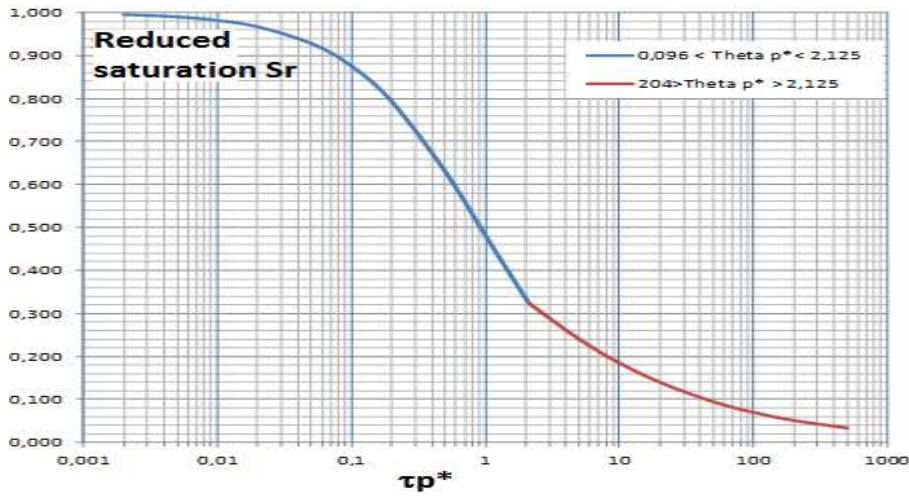


Figure 1: Correlation between reduced saturation and the product of the time and pressure adimensional

The reduced saturation is obtained and the saturation  $S$  calculated. This saturation gives access to the residual moisture in the cake:

$$S_r = \frac{S - S_\infty}{1 - S_\infty} \quad (7)$$

$$S = \frac{(1 - \varepsilon) \rho_s}{\varepsilon \rho_l} \frac{H}{1 - H} \quad (8)$$

If the residual moisture is the target and the deliquoring time needed is wanted, the calculation can be done by calculating  $S_r$ , having the product  $\tau p^*$  thanks to the curve and calculating the deliquoring time  $t_d$ .

### 3. Experimental considerations

A study of the influence of the particle shape on cake deliquoring is proposed thanks to multiple synthesis of calcium carbonate. Four shapes were obtained: spheres, cubes, platelets and needles.

The values of cake residual moisture as a function of filtration and deliquoring pressure were measured. For instance, Figure 2 presents the iso-responses curves for calcium carbonate spheres.

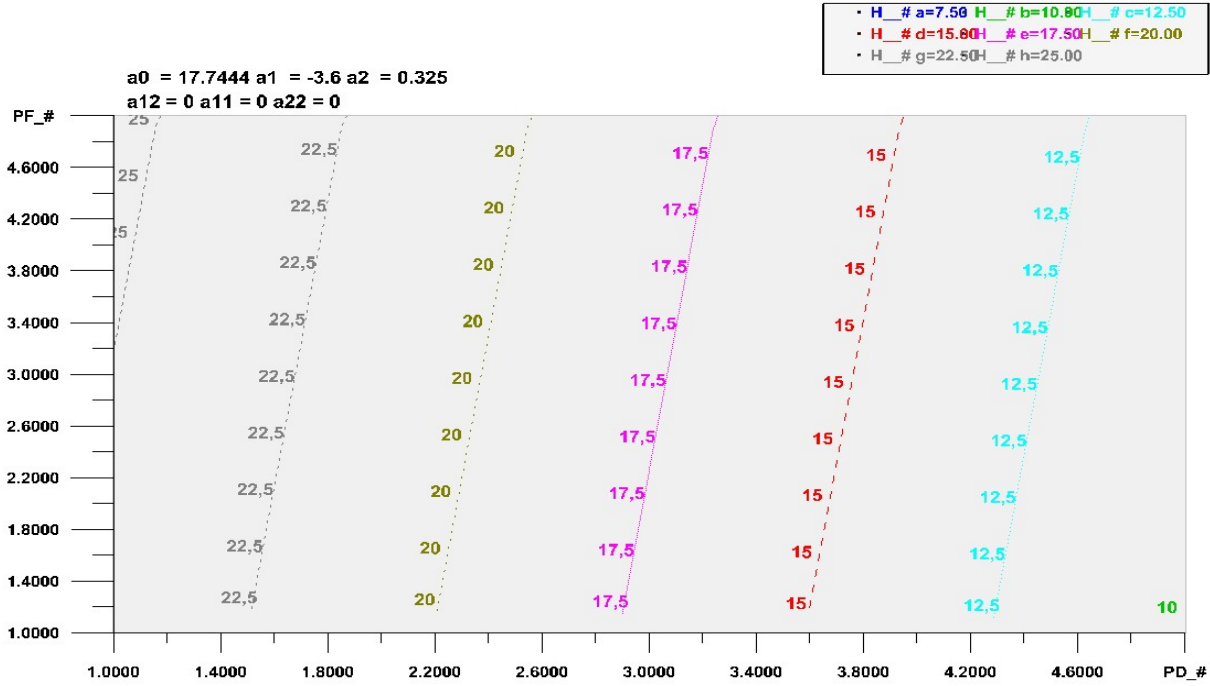


Figure 2: Isoresponses curves of residual moisture as a function of deliquoring and filtration pressure

The table 1 summarizes the results for each shape.

Table 1: Experimental results of residual moisture measurements

Shape	Deliquoring Pressure	Filtration Pressure		
		1	3	5
Spheres	1	23.3	24.0	24.6
	3	18.8	19.8	20.3
	5	9.0	9.7	10.1
Cubes	1	21.0	25.7	31.4
	3	14.8	19.3	25.1
	5	9.0	14.5	18.4
Platelets	1	34.3	38.2	43.0
	3	32.8	36.8	40.2
	5	30.2	34.7	39.1
Needles	1	12.0	21.6	32.0
	3	8.4	18.1	27.9
	5	6.2	15.6	24.3

For each shape, a linear polynomial regression is proposed:

$$H = a_0 + a_1X_1 + a_2X_2 \quad (9)$$

where X1 stands for the centered variable for deliquoring pressure and X2 for the centered variable for filtration pressure.

The table 2 gives the measured coefficients a1 and a2 for each shape:

Table 2: Polynomial coefficients for each shape

Shape	Shape factor	a0	a1	a2	a1+a2
Spheres	0.92	17.74	-3.6	0.33	-3.27
Cubes	0.81	19.91	-3.02	2.51	-0.51
Platelets	0.3	36.59	-0.96	2.08	1.12
Needles	0.17	18.46	-1.63	4.80	3.17

An analysis of the coefficients shows that the influence of deliquoring pressure is more important for shapes close to the sphere and that the influence of filtration pressure is more important for shapes far from the sphere.

#### 4. Comparison experiments/modeling

The model presented in section 2 and the experiments presented in section 3 were compared in figure 3.

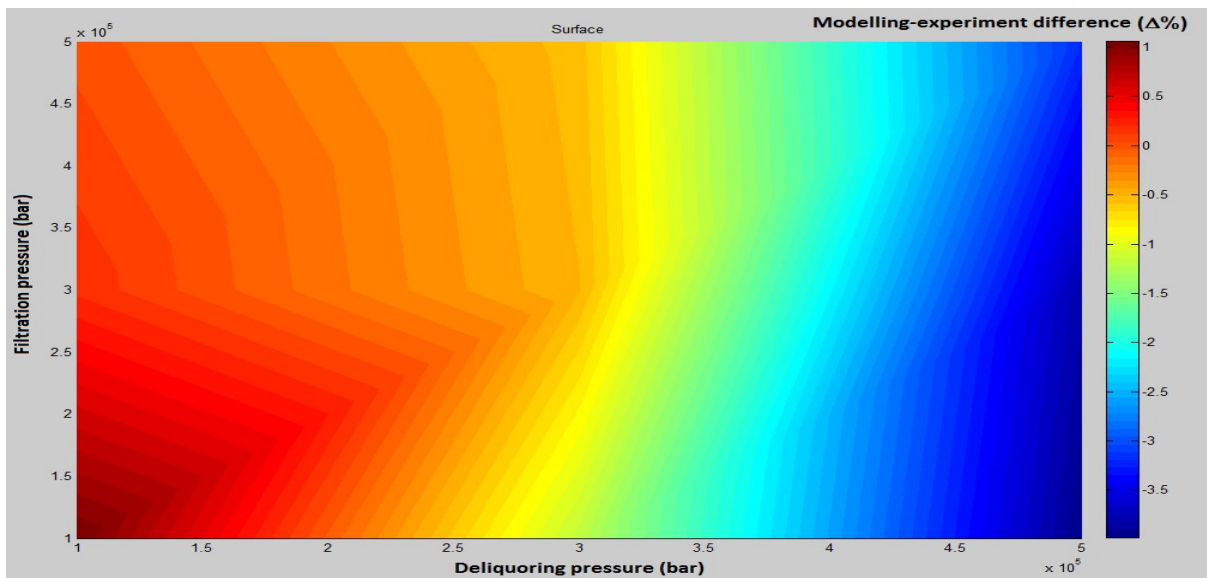


Figure 3: Comparison modelling-experiments for calcium carbonate spheres

The surface represents the difference between the modeled results and the experiments. The correlation is good and better at low pressure.

#### 5. Conclusion

The correlation between the model and the experiments is good. The effect of the shape on deliquoring has to be taken into account. This comparison gives the industrial a great tool to adapt the filtration and deliquoring pressures to the product needed, in order to improve the productivity and the dryness of the solid at the end of the separation process. The optimal pressures can be found with the Filtration Performance Test by FlowerSEP.