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# **Phase Equilibrium of Three Binary Mixtures Containing NO and Components Present in Ambient Air.**

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## Abstract

Air contains impurities, which must be removed before its transformation and utilization. In the present work, new isothermal Vapor-Liquid Equilibrium (VLE) data are reported for three binary systems containing NO with (CO, N<sub>2</sub> or Ar) at different temperatures (between 105 and 146 K) and pressures up to 4 MPa. The compositions of the coexisting phases were experimentally determined using an apparatus based on the “static-analytic” method. The Peng-Robinson Equation of State combined with different mixing rules (classical, Wong-Sandler and Huron-Vidal) were used to represent the phase diagram (P, x, y).

**Keywords:** Vapor –Liquid Equilibrium, low temperature, thermodynamic models, measurements, phase behavior

## 1. Introduction

Air is indispensable to life and an important resource at the same time. It is approximately a ternary mixture of nitrogen, oxygen, and argon. Nevertheless, it contains variable quantities of many other substances like rare gases, CO<sub>x</sub>, hydrogen, methane, oxides of nitrogen, NO<sub>x</sub>, and of sulfur, SO<sub>x</sub>. To illustrate, Table 1 gives an example of an average volumetric distribution of the substances in the air mixture. In Table 1, distinction is made between fixed components and impurities<sup>1</sup>.

Air contains large amounts of nitrogen and oxygen. Cryogenic distillation of air is the oldest but most highly developed separation technology for the industrial production of oxygen and nitrogen. This technology has not changed fundamentally from that initially developed by Carl von Linde and Claude-Delorme at the beginning of the 20th century. The core of a conventional Air Separation Unit (ASU) is a system of two distillation columns and a reboiler-condenser in between working at about 100 K. The importance of this process depends heavily on its capability in providing extremely pure nitrogen (10 ppb of impurities) and oxygen (purity from 85% up to 99.7%) in both the liquid and vapor states. Cryogenic air separation is based on the principle of fractional distillation. This process involves liquid and vapor phases and air components are separated on the basis of differences in boiling point and of relative volatility. Consequently, the whole process is related to the VLE occurring within the distillation column, thus important information for the plant design are saturation lines of the main air components and the thermodynamics and phase equilibria of mixtures of

nitrogen, oxygen, and argon. There are currently few data available in the open literature on the thermodynamic behavior of mixtures composed of fixed components + impurities as well as mixtures composed of two impurities.

Since 1990's, the Centre of Thermodynamics of Processes has been involved in the study of the thermodynamic behavior (experimental measurements and thermodynamic calculation) of such mixtures. As examples of results obtained, we can mention the study of phase equilibria of several binary systems, O<sub>2</sub>-N<sub>2</sub>, O<sub>2</sub>-Ar and Ar-N<sub>2</sub> (VLE, Baba-Ahmed et al.<sup>2</sup>), O<sub>2</sub>-CO<sub>2</sub>, O<sub>2</sub>-N<sub>2</sub>O (solid solubility in liquid oxygen, De Stefani et al.<sup>3</sup>), O<sub>2</sub>-propane (VLLE, Houssin-Agbomson et al.<sup>4</sup>) and N<sub>2</sub>-propane (VLLE, Houssin-Agbomson et al.<sup>5</sup>). NO, CO and Ar are also impurities present with CO<sub>2</sub> after the process of CO<sub>2</sub> capture. Development of thermodynamic model to design CO<sub>2</sub> transportation process requires binary interaction parameters (Coquelet et al.<sup>6</sup>). These parameters are obtained from experimental data. In this work, VLE measurements of three binary mixtures composed of some impurities (Ar-NO, CO-NO and N<sub>2</sub>-NO,) will be presented at low temperature conditions. The Peng-Robinson Equation of State, commonly used in industry, is used to model the above systems.

## **2. Experimental set-up**

### **2.1. Chemicals**

Chemicals (nitrogen, argon, carbon monoxide and nitric oxide) were purchased from Air Liquide (France) and presented in Table 2. The chemicals were used without further purification.

### **2.2. Apparatus description**

The set-up is based on the 'static-analytic' method, for measurements at temperatures down to the normal nitrogen boiling temperature. The measured properties are: pressure, temperature and vapor and liquid compositions. A Hastelloy C276 cell (43 cm<sup>3</sup>) is placed inside a cryostat partially filled with liquid nitrogen. If the desired temperature is the normal nitrogen boiling temperature, the cell is completely immersed in liquid nitrogen. Above this temperature, the level of liquid nitrogen is maintained below the bottom of the cell. In this way, liquid nitrogen acts as the cold reservoir while a rounded heating resistance connected to a PID thermal regulator is used to achieve temperature stability within 0.1 K. Two capillary samplers Rapid On-Line Sampler-Injector (ROLSI<sup>®</sup>)<sup>7</sup> are fixed on the top of the cell, one for the liquid phase and one for the vapor phase, and allowing direct injection of samples into the carrier gas

circuit of a gas chromatograph. Efficient stirring of mixtures inside the cell is achieved using a magnetic rod driven by an external rotating magnetic field. Its rotation speed is selected through a variable speed motor.

A detail description of the setup can be found in Baba-Ahmed et al.<sup>2</sup> and Houssin-Agbomson et al.<sup>4</sup>.

### **2.3. Calibrations and uncertainty estimation**

Calibration of pressure transducer is performed against a dead weight pressure balance (Desgranges & Huot 5202S, CP 0.3–40 MPa, Aubervilliers, France). Accuracies are estimated to be within 0.005 MPa. The two platinum resistance thermometer probes (100  $\Omega$ ) are calibrated by measuring the oxygen vapor pressure at low temperatures and comparing this value to the one found in the open literature. These probes are coupled to a Hewlett Packard multi-meter. Accuracies are estimated to be within 0.1 K for both probes. The signals from the probes (temperatures and pressures) are transmitted to a data acquisition system (DAS) which is connected to a PC. The thermal conductivity detector (TCD) of a Perichrom gas chromatograph (PR-2100) is calibrated using known amounts of compounds introduced through syringes. The column used for this analytical work is a packed column molecular sieve 5A (60/80) (Restek, France).

To estimate the uncertainties in temperature, pressure and composition, we have followed the guidelines of NIST<sup>8</sup>. The uncertainty estimation procedure is fully described by Zhang et al.<sup>9</sup>. Both measurements repeatability and calibration uncertainties are taken into account. All the expanded uncertainties  $U(x)$ ,  $U(y)$  with coverage factor,  $k=2$ ) for experimental data are reported in section 4.

### **2.4. Experimental procedure**

At room temperature, the equilibrium cell and its loading lines are vacuumed. The cell is first loaded with the component having the lowest vapor pressure (NO in our study). The temperature is then set to the desired point and the system is left to reach thermodynamic equilibrium. After recording the vapor pressure of this component, the second component is introduced step by step, leading to successive equilibrium mixtures of increasing overall compositions. The two-phase (liquid and vapor) envelopes are measured with about 6 to 10 liquid and vapor points. Phase equilibrium is assumed to be achieved while temperature and pressure readings stabilized for at least 30 min. For each equilibrium condition, several samples of each phase (vapor and liquid) are withdrawn using the capillary samplers ROLSI®

and analyzed in order to determine the mole fraction of each phase and check for repeatability of measurements which must be closed or better than  $\pm 1 \%$ .

### 3. Modelling

For binary mixtures modelling, the critical parameters (temperature ( $T_C$ ) and pressure ( $P_C$ )), and acentric factor ( $\omega$ ) for each of the pure components are provided in Table 3<sup>10</sup>. The experimental VLE data were correlated using the Peng-Robinson cubic Equation of State (PR EoS)<sup>11</sup> with different mixing rules. These models were chosen in order to produce reliable correlation of the experimental data with reasonable accuracy comparable with experimental uncertainties and to represent at the best the both phases. - PR EoS incorporating the Mathias-Copeman alpha function<sup>12</sup>, combined with the classical mixing rules<sup>13</sup> (PR-EoS) as implemented in in-house software developed at CTP. - PR EoS incorporating the Mathias-Copeman alpha function, with the Wong-Sandler mixing rules<sup>14</sup> involving NRTL activity coefficient model<sup>15</sup> (PR-WS-NRTL EoS) (with non-randomness parameter  $\alpha=0.3$ ).

- PR EoS incorporating the Mathias-Copeman alpha function, with the Huron-Vidal mixing rules<sup>16</sup> with a Wilson activity coefficient model<sup>17</sup> (PR-HV-Wilson EoS)

The Mathias-Copeman alpha function coefficients for all components are listed in Table 3<sup>10</sup>. Binary Interaction Parameters (BIP,  $k_{ij}$ ) were determined directly from the VLE data by minimizing the following objective function (eq.1):

$$OF = \frac{100}{N} \left[ \sum \left( \frac{P_{exp} - P_{cal}}{P_{exp}} \right)^2 \right] \quad (\text{eq.1})$$

Where P corresponds to bubble pressure,  $_{exp}$  corresponds to experimental and  $_{cal}$  corresponds to calculated.

## 4. Results and discussion

### 4.1 VLE data for Ar-NO system

The experimental VLE data were determined at 135.80 and 146.22 K (see Table 4) and are plotted in Figure 1. The PR-EoS using the classical mixing rules is used to represent the phase diagram (P,x,y). The adjusted BIP ( $k_{ij}$ ) with and without a temperature dependency are presented in Table 5.

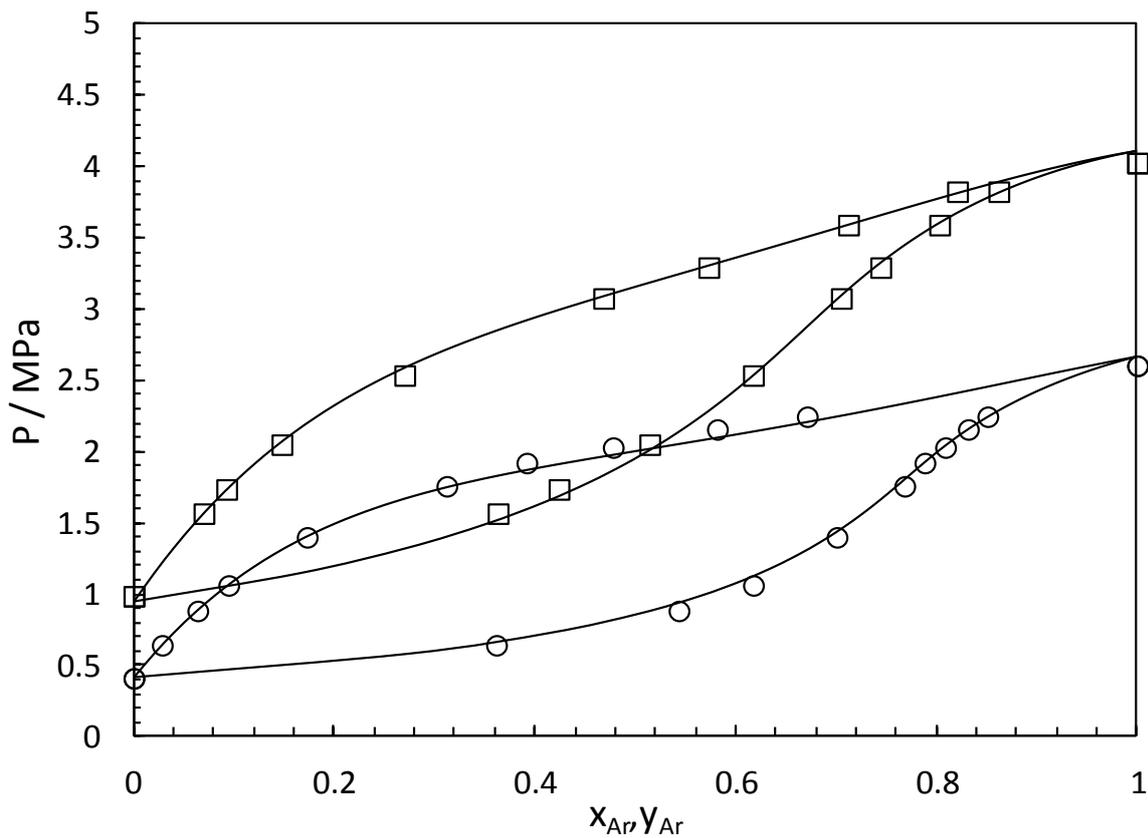
In order to quantify the fit of the models to the experimental data, the average absolute deviation (AADU) is calculated for the pressure and the vapor phase mole fractions. The deviation is defined by:

$$AADU = (100 / N) \sum |(U_{\text{exp}} - U_{\text{cal}}) / U_{\text{exp}}| \quad (\text{eq.2})$$

Where  $N$  is the number of data points,  $_{\text{cal}}$  corresponds to calculated value,  $_{\text{exp}}$  corresponds experimental value and  $U = P_i$  or  $y_i$ .

These indicators, which give information about the agreement between model and experimental results, are presented in Table 5. Regarding these indicators, taking into account a temperature dependent BIP does not improve significantly the calculated data obtained. In Figure 1,  $k_{ij}$  values used for our calculations with the PR are those obtained with a temperature dependency. PR The AADU is less than 2.3%.

**Figure 1.** Phase diagrams (P-x-y) for Ar (1) - NO (2) mixture (symbols: this work,  $\square$ : 146.42 K,  $\circ$ : 135.80 K, Black lines: PR-EoS with a temperature dependent BIP).

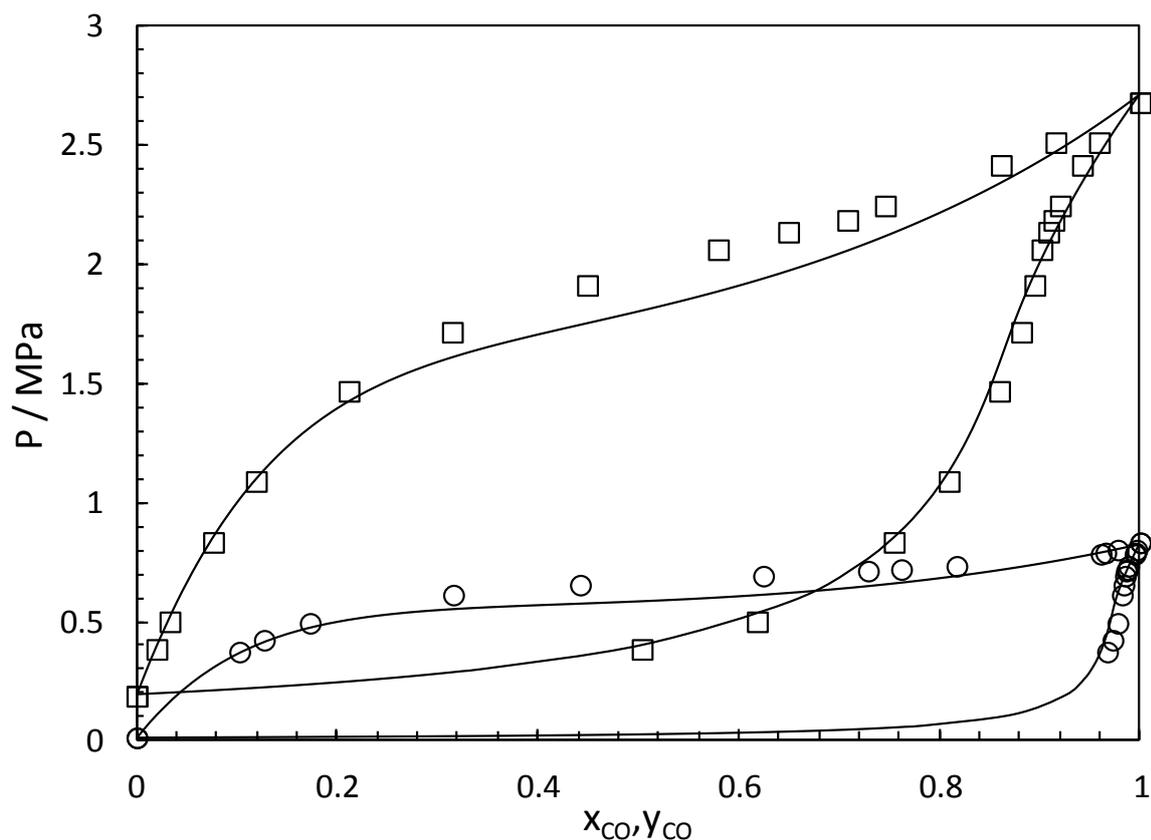


#### 4.2 VLE data for CO-NO system

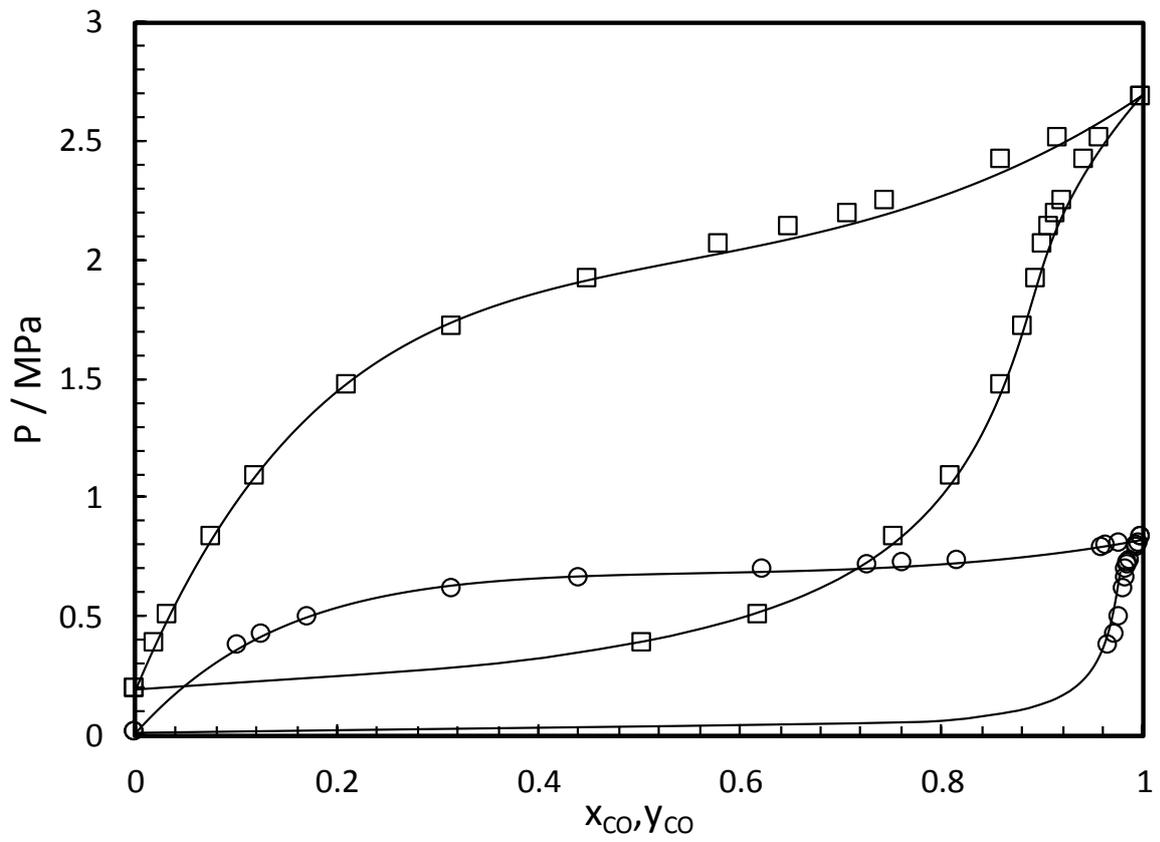
Table 6 and Figure 2 present the VLE data obtained at 105.89 and 127.32 K. A temperature dependent BIP to represent the experimental data was considered. (Table 7). At higher temperature the PR-EoS with the classical mixing rules have some difficulties representing the liquid composition (see Figure 2.a). In order to display a decent match with the experimental data (particularly for the liquid phase), the PR-WS-NRTL EoS (with non-randomness parameter  $\alpha=0.3$ ) was used. This model has 3 BIPs which give more flexibility to represent correctly the phase diagram of the system. With this mixing rule, the PR-EoS handles the representation of both phases (liquid and vapor) reasonably well. The AADU is less than 1.4%.

**Figure 2.** Phase diagrams (P-x-y) for CO (1) - NO (2) mixture (symbols: this work,  $\square$ : 127.32 K,  $\circ$ : 105.89 K, Black lines: PR-EoS with a temperature dependent BIP.

a- With classical mixing rule

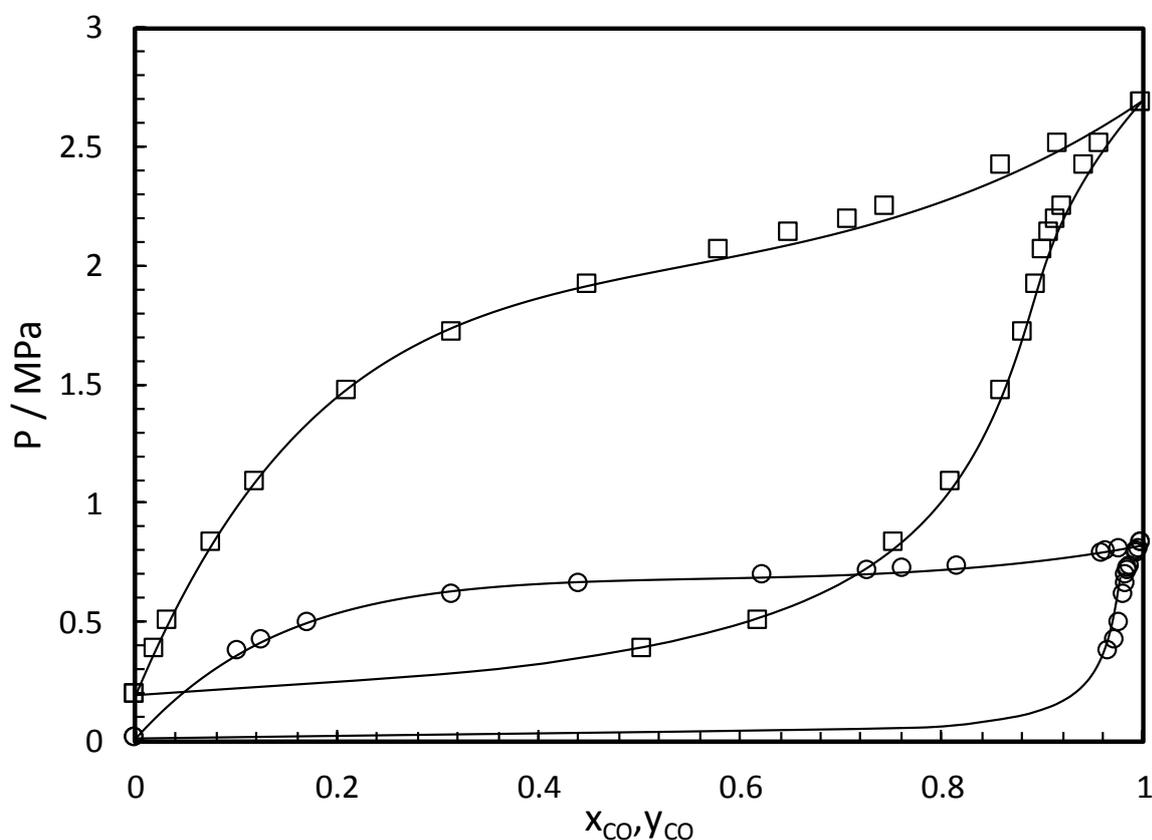


b-With Wong-Sandler mixing rule and NRTL activity coefficient model



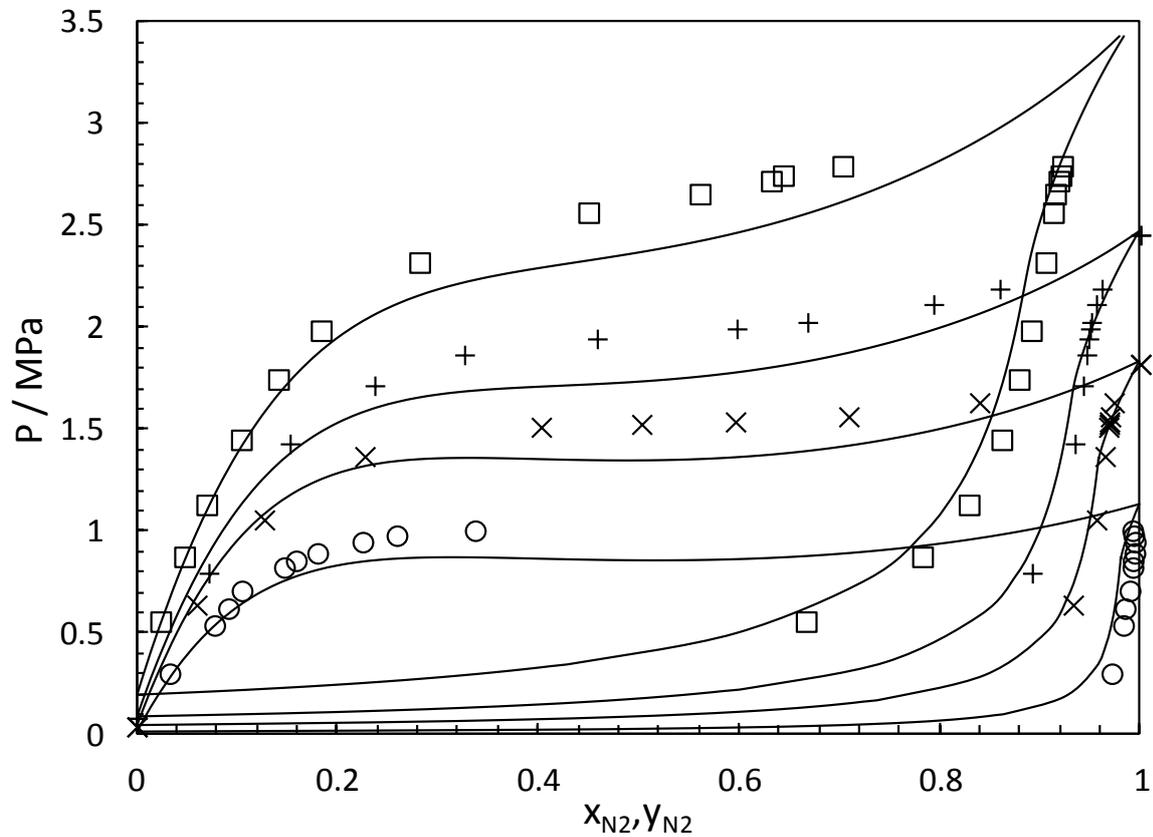
### 4.3 VLE data for N<sub>2</sub>-NO system

This system has been studied by Scheunemann et al., (1985)<sup>18</sup> at 113.85 and 119.55 K. Our new experimental data were measured at 105.69 and 127.14 K (see Table 8). Table 9 presents the BIP obtained at each temperature. For this system, the PR-EoS with classical mixing rule have some difficulties in representing the liquid composition, particularly for N<sub>2</sub> rich mixtures (Figure 3.a). A vapor-liquid-liquid-equilibrium is predicted when using the PR-WS-NRTL EoS, for the lowest temperature (Figure 3.b). To overcome this problem, the PR-HV-Wilson EoS was used. The Wilson activity coefficient model is well known not to predict liquid-liquid equilibria. The PR HV-Wilson EoS model handles the representation of both phases (liquid and vapor) reasonably well (Figure 3.c). The BIP values except at 119.55 K are an increasing function of the temperature and follow a linear behavior (Figure 4).

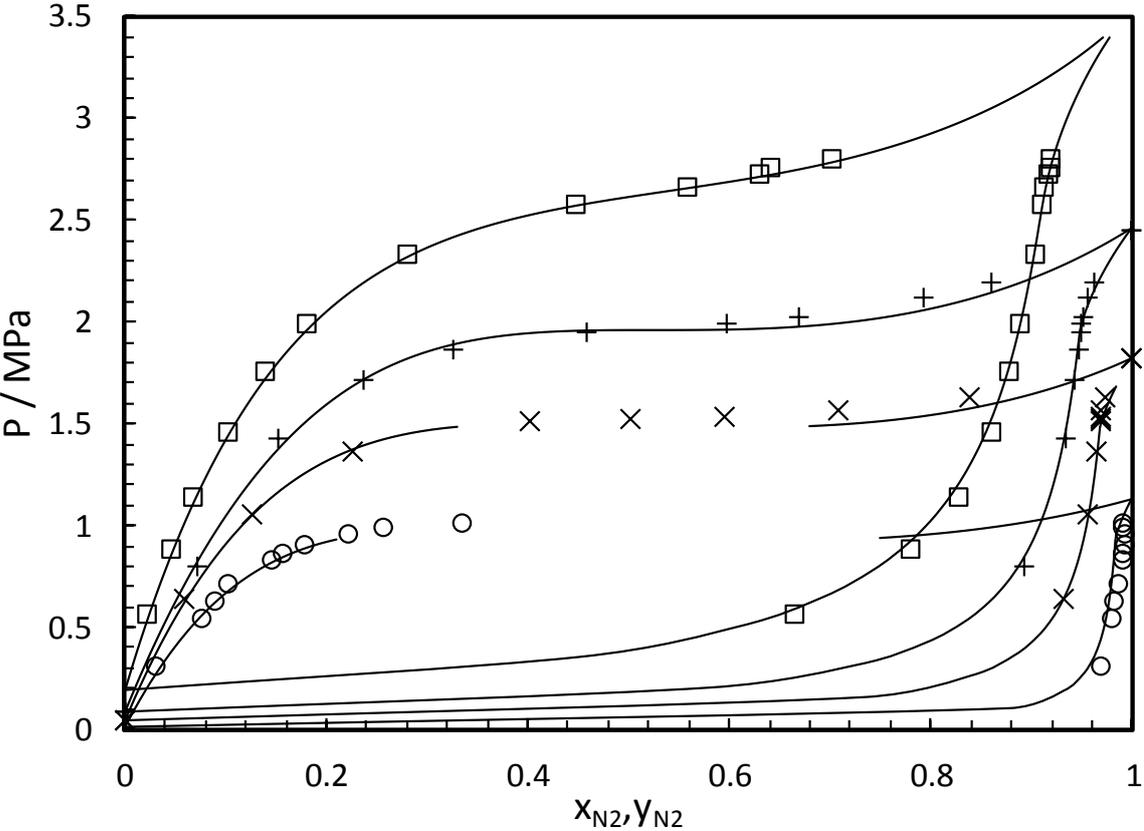


**Figure 3.** Phase diagrams (P-x-y) for N<sub>2</sub> (1) - NO (2) mixture (symbols: experimental work, □: data measured in this work at 127.14 K, ○: data measured in this work at 105.69 K, ×: Data from Scheunemann and Wagner measured at 119.55K<sup>18</sup>, +: Data from Scheunemann and Wagner measured at 113.85K<sup>18</sup>, Black lines: PR-EoS with a temperature dependent BIP).

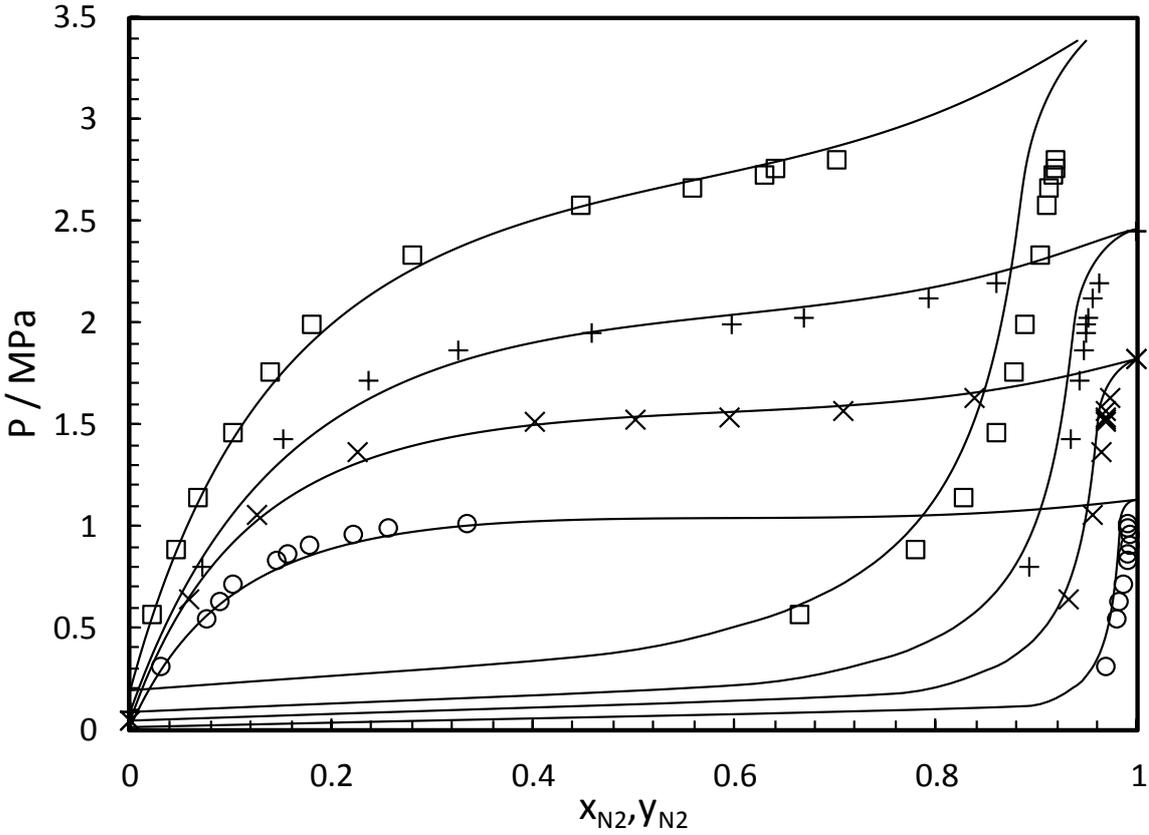
a-With classical mixing rule



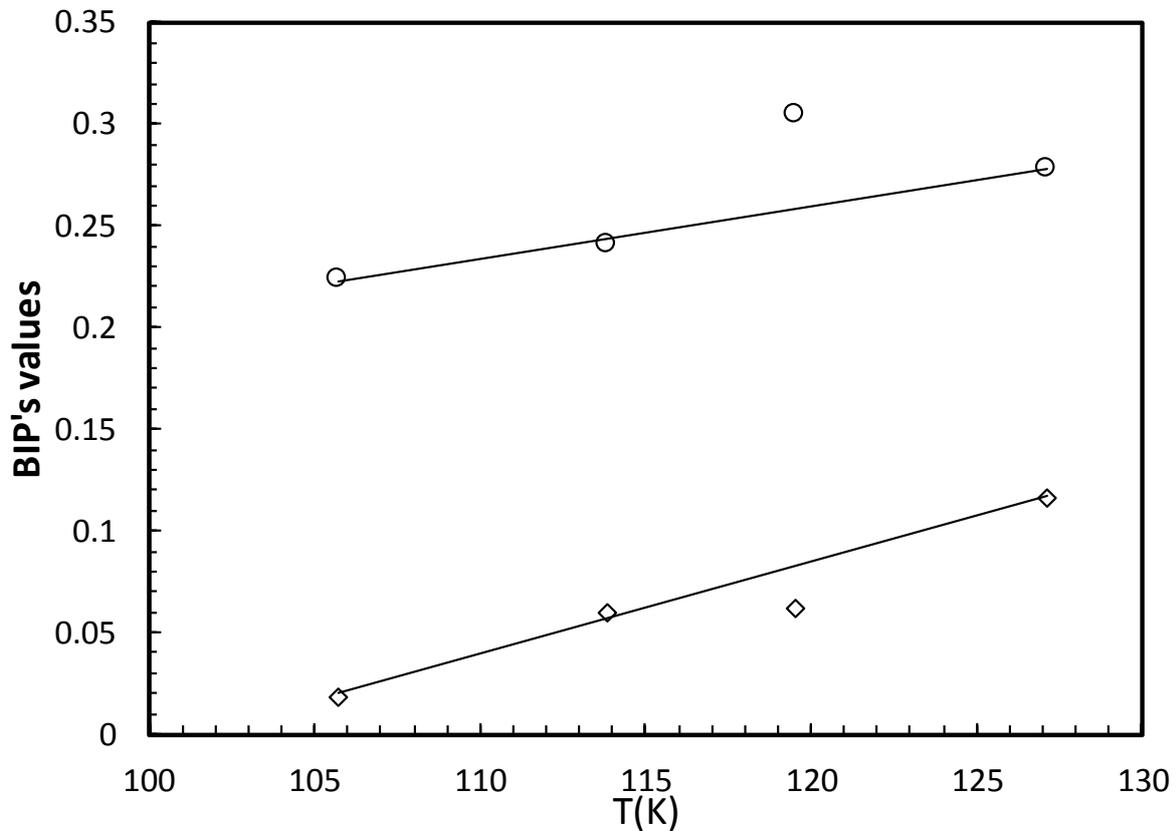
b-With Wong-Sandler mixing rule and NRTL activity coefficient model



c-With Huron-Vidal mixing rule and Wilson activity coefficient model



**Figure 4.** BIP's values with PR-WS-Wilson EoS as function of temperature. (symbols:  $\circ$ :  $\tau_{12}$ ,  $\square$ :  $\tau_{21}$ ) for  $N_2$  (1) - NO (2) mixture.



## 5. Conclusions

Phase equilibrium of binary mixtures NO with (CO,  $N_2$  or Ar) for cryogenic air separation in this paper. New experimental VLE data for these three binary systems are presented at different temperatures. Experimental data for these systems have not been previously reported in the open literature at the studied temperature. The experimental setup using a ‘static-analytic’ method is described and the uncertainties concerning the calibrations of pressure, temperature and gas chromatography detector are also given. The measured data were correlated using the PR-EoS with different mixing rules (classical, Wong-Sandler and Huron-Vidal) in function of the system studied. The new experimental data obtained in this work were used to adjust the binary interaction parameters and the chosen models seems to be adequate to fit these types of component and mixtures at these temperature conditions. As future work, we will be focusing on the improvement of PR-EoS in order to represent the thermodynamic behavior of air components.

**Acknowledgments**

This work was funded by Chevron, Linde, GALP, OMV, PETEX, Statoil, TOTAL and UK National Grid, whose support is gratefully acknowledged.

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**Figure 3.** Phase diagrams (P-x-y) for N<sub>2</sub> (1) - NO (2) mixture (symbols: experimental work,  $\square$ : data measured in this work at 127.14 K,  $\circ$ : data measured in this work at 105.69 K,  $\times$ : Data from Scheunemann and Wagner measured at 119.55K<sup>18</sup>,  $+$ : Data from Scheunemann and Wagner measured at 113.85K<sup>18</sup>, Black lines: PR- EoS with a temperature dependent BIP).

**Figure 4.** BIP's values with PR-WS-Wilson EoS as function of temperature. (symbols: experimental work,  $\circ$ :  $\tau_{12}$ ,  $\square$ :  $\tau_{21}$ ) for N<sub>2</sub>(1) - NO (2) mixture.

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**Table 8.** Vapor–liquid equilibrium pressures and phase compositions for N<sub>2</sub> (1) - NO (2) mixture (composition: y for Vapor phase and x for liquid phase, n: samples number).

**Table 9.** BIP values and deviations obtained in fitting experimental VLE data with PR-EoS (bubble pressure calculation), PR-WS-NRTL EoS (with non-randomness parameter  $\alpha=0.3$ ) and PR-HV-Wilson EoS for N<sub>2</sub> (1) - NO (2) mixture.

**Table 1:** Example of Air composition from Arpentinier et al. <sup>1</sup>.

<b>Component</b>	<b>Volumetric composition</b>
<b>Fixed components</b>	
N <sub>2</sub>	78.084 ± 0.004%
O <sub>2</sub>	20.964 ± 0.002%
Ar	0.934 ± 0.001%
CO <sub>2</sub>	0.033 ± 0.003%
Ne	1.8 ± 0.04 ppm
He	5.2 ± 0.05 ppm
Kr	1.14 ± 0.01 ppm
Xe	0.086 ± 0.001 ppm
H <sub>2</sub>	0.05 ppm
<b>Impurities (In ambient air, including dust, pollen and local pollutants.)</b>	
H <sub>2</sub> O	0.1–2.8%
CH <sub>4</sub>	1–6 ppm
CO	0.06–1 ppm
SO <sub>x</sub>	0.1–1.0%
NO <sub>x</sub>	0.52 ppm
O <sub>3</sub>	0.01–1 ppm
Rn	6 × 10 <sup>-3</sup> ppq

**Table 2:** Details of the chemicals.

<b>Chemical</b>	<b>Symbol</b>	<b>CAS number</b>	<b>Purity/volume% (by weighing)</b>
Argon	Ar	7440-37-1	99.999
Nitrogen	N <sub>2</sub>	7727-37-9	99.995
Carbon dioxide	CO	630-8-0	99.995
Nitric oxide	NO	10102-43-9	99.000

**Table 3.** Critical parameters, acentric factors and Mathias-Copeman Coefficients for the PR-EoS<sup>10</sup>.

<b>Chemical</b>	<b><math>T_c</math>/K</b>	<b><math>P_c</math>/MPa</b>	<b><math>\omega</math></b>	<b><math>MC1</math></b>	<b><math>MC2</math></b>	<b><math>MC3</math></b>
Ar	150.86	4.8980	0	0.397483	-0.282393	0.796288
N <sub>2</sub>	126.20	3.4000	0.0377	0.448322	-0.156813	0.468652
CO	132.92	3.4990	0.0481	0.451344	-0.0791691	0.464029
NO	180.15	6.4800	0.5829	1.153810	0.243750	-0.043201

**Table 4.** Vapor–liquid equilibrium pressures and phase compositions for Ar (1) - NO (2) mixture (composition: y for vapor phase and x for liquid phase, n: samples number). U(T)= 0.1 K, U(P)=0.005 MPa.

<b>T/K = 135.80</b>					
<b>P/MPa</b>	<b>y<sub>1</sub></b>	<b>x<sub>1</sub></b>	<b>U (y<sub>1</sub>)</b>	<b>U(x<sub>1</sub>)</b>	<b>ny<sub>1</sub> ; nx<sub>1</sub></b>
0.4109	0	0			
0.6432	0.3613	0.0282	2E-04	1E-04	4;6
0.8844	0.5431	0.0636	2E-04	1E-04	6;5
1.0634	0.6173	0.0944	3E-04	1E-04	5;7
1.4012	0.7006	0.173	2E-04	2E-03	6;7
1.7597	0.768	0.312	1E-03	1E-04	6;8
1.9230	0.788	0.392	1E-03	4E-03	4;4
2.0315	0.809	0.478	1E-03	4E-04	6;6
2.1587	0.831	0.581	1E-03	5E-04	5;4
2.2484	0.851	0.671	1E-03	2E-04	6;6
2.6056	1	1			
<b>T/K = 146.22</b>					
0.9878	0	0			
1.5678	0.36283	0.0698	3E-05	9E-04	6;4
1.7377	0.4235	0.0924	1E-04	2E-03	6;5
2.0521	0.51394	0.1475	7E-05	1E-03	7;5
2.5374	0.61724	0.2698	4E-05	3E-03	6;7
3.0786	0.70481	0.4680	3E-05	4E-03	6;6
3.2953	0.74408	0.5728	2E-05	3E-03	4;5
3.5934	0.8028	0.7120	1E-04	1E-03	6;5
3.8280	0.8617	0.8206	1E-04	2E-03	5;4
4.0289	1	1			

**Table 5.** BIP values and deviations obtained in fitting experimental VLE data with PR-EoS (bubble pressure calculation) for Ar (1) - NO (2) mixture.

<b>PR-EoS with classical mixing rules</b>			
<b>T/ K</b>	<b>kij</b>	<b>AAD P (%)</b>	<b>AAD y1 (%)</b>
135.80	0.1144	1.68	2.20
146.22	0.1247	1.05	1.74
no temperature dependency	0.1177	1.86	1.30

**Table 6.** Vapor–liquid equilibrium pressures and phase compositions for CO (1) - NO (2) mixture (composition: y for vapor phase and x for liquid phase, n: samples number). U(T)= 0.1 K, U(P)=0.005 MPa.

<b>T/K = 105.89</b>					
<b>P/MPa</b>	<b>y<sub>1</sub></b>	<b>x<sub>1</sub></b>	<b>U(y<sub>1</sub>)</b>	<b>U(x<sub>1</sub>)</b>	<b>ny<sub>1</sub> ; nx<sub>1</sub></b>
0.0136	0	0			
0.7847	0.99460	0.9607	4E-05	1E-04	4;4
0.8026	0.99632	0.9776	4E-05	2E-04	4;5
0.7905	0.99508	0.9653	2E-05	3E-04	4;4
0.3739	0.9671	0.10236	7E-04	6E-05	4;5
0.4236	0.97249	0.1270	1E-05	5E-04	4;5
0.4947	0.97742	0.1727	3E-05	9E-04	4;6
0.6552	0.98341	0.442	7E-05	1E-03	5;5
0.6930	0.98489	0.624	4E-05	3E-03	4;5
0.7141	0.98588	0.729	3E-05	4E-03	4;5
0.7200	0.98707	0.762	2E-05	3E-03	3;5
0.7300	0.9881	0.817	1E-04	1E-03	4;5
0.8300	1	1			
<b>T/K = 127.32</b>					
0.1883	0	0			
0.3852	0.5034	0.0198	5E-04	4E-04	5;4
0.5011	0.618	0.0329	1E-03	2E-04	4;6
0.8348	0.754	0.0763	2E-03	5E-04	6;5
1.0907	0.8092	0.1190	7E-04	2E-04	4;5
1.4696	0.85953	0.211	3E-05	1E-03	4;5
1.7178	0.8815	0.314	2E-04	1E-03	5;5
1.9145	0.8946	0.449	3E-04	1E-03	5;9
2.0645	0.9018	0.5794	2E-04	2E-04	4;4
2.1381	0.9084	0.6493	2E-04	2E-04	4;4
2.1879	0.9137	0.7082	5E-04	2E-04	4;4
2.2484	0.92010	0.74575	7E-05	9E-05	4;5
2.4190	0.9421	0.86122	2E-04	4E-05	4;5
2.5146	0.9590	0.9157	3E-04	5E-04	4;8
2.6820	1	1			

**Table 7.** BIP values and deviations obtained in fitting experimental VLE data with PR-EoS (bubble pressure calculation), PR-WS-NRTL EoS (with non-randomness parameter  $\alpha=0.3$ ) and PR-HV-Wilson EoS for CO (1) - NO (2) mixture.

PR-EoS with classical mixing rule				PR-WS-NRTL EoS				
T/ K	kij	AAD P (%)	AAD y1(%)	kij	$\tau_{12} / \text{J.mol}^{-1}$	$\tau_{21} / \text{J.mol}^{-1}$	AAD P (%)	AAD y1 (%)
105.89	-0.0081	4.89	0.49	-0.34795	3178.80	1235.00	1.60	0.53
127.32	0.0374	4.52	0.93	0.24814	61.69	1304.80	1.35	0.73

PR-HV-Wilson EoS				
T/ K	$\tau_{12}$	$\tau_{21}$	AAD P (%)	AAD y1(%)
105.89	0.30286	0.14462	1.0	0.32
127.32	0.14462	0.1164	0.89	1.55

**Table 8.** Vapor–liquid equilibrium pressures and phase compositions for N<sub>2</sub> (1) - NO (2) mixture (composition: y for vapor phase and x for liquid phase, n: samples number). U(T)= 0.1 K, U(P)=0.005 MPa.

<b>T/K = 105.69</b>					
<b>P/MPa</b>	<b>y<sub>1</sub></b>	<b>x<sub>1</sub></b>	<b>U(y<sub>1</sub>)</b>	<b>U(x<sub>1</sub>)</b>	<b>ny<sub>1</sub> ; nx<sub>1</sub></b>
0.3008	0.9713	0.0328	3E-04	4E-04	5;4
0.3558	0.9751		3E-04		4
0.4653	0.9794		2E-04		5
0.5379	0.9828	0.0774	2E-04	8E-04	4;5
0.6207	0.9845	0.0912	2E-04	9E-04	5;5
0.7078	0.9893	0.105	1E-04	1E-03	3;4
0.8226	0.99222	0.147	9E-05	1E-03	4;4
0.8555	0.99244	0.159	9E-05	2E-03	4;5
0.8922	0.99410	0.180	7E-05	2E-03	3;4
0.9474	0.99447	0.225	6E-05	2E-03	3;5
0.9791	0.99304	0.259	8E-05	2E-03	3;4
<b>T/K = 127.14</b>					
0.5568	0.667	0.0236	3E-03	3E-04	5;6
0.8751	0.783	0.0474	2E-03	5E-04	5;6
1.1304	0.829	0.0695	2E-03	7E-04	5;9
1.4500	0.862	0.104	1E-03	1E-03	5;6
1.7464	0.879	0.141	1E-03	1E-03	5;5
1.9861	0.891	0.184	1E-03	2E-03	5;5
2.3211	0.906	0.282	1E-03	2E-03	6;5
2.5660	0.9130	0.450	9E-04	3E-03	5;7
2.6573	0.9151	0.561	9E-04	3E-03	3;5
2.7213	0.9185	0.632	8E-04	3E-03	4;9
2.7482	0.9206	0.644	8E-04	3E-03	3;4
2.7944	0.9221	0.703	8E-04	2E-03	3;5

**Table 9.** BIP values and deviations obtained in fitting experimental VLE data with PR-EoS (bubble pressure calculation), PR-WS-NRTL EoS (with non-randomness parameter  $\alpha=0.3$ ) and PR-HV-Wilson EoS for N<sub>2</sub> (1) - NO (2) mixture.

PR-EoS with classical mixing rule				PR-WS-NRTL EoS				
T/ K	kij	AAD P (%)	AAD y1(%)	kij	$\tau_{12}$ / J.mol-1	$\tau_{21}$ / J.mol-1	AAD P (%)	AAD y1 (%)
105.69	-0.0004	8.02	1.31	0.0803	974.50	1244.80	1.67	1.01
113.83	0.0241	6.81	0.63	0.2368	403.22	1307.00	1.77	0.08
119.56	0.0307	7.25	0.90	0.2198	644.32	1034.50	1.75	0.09
127.14	0.0430	5.52	2.74	0.2780	-138.28	1843.70	0.29	0.78

PR-HV-Wilson EoS				
T/ K	$\tau_{12}$	$\tau_{21}$	AAD P (%)	AAD y1(%)
105.69	0.2233	0.0186	3.30	1.14
113.83	0.2413	0.0598	1.69	0.58
119.56	0.3051	0.0619	3.07	1.08
127.14	0.2782	0.1164	1.94	3.14

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