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# Heat Flux estimation in WEST divertor with embedded thermocouples

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**Abstract.** The present paper deals with the surface heat flux estimation with embedded thermocouples (TC) in a Plasma Facing Component (PFC) of the WEST Tokamak. A 2D nonlinear unsteady calculation combined with the Conjugate Gradient Method (CGM) and the adjoint state is achieved in order to estimate the time evolution of the heat flux amplitude and decay length  $\lambda_q$ . The method is applied on different synthetic measurements in order to evaluate the accuracy of the method. The synthetic measurements are generated with realistic values of  $\lambda_q$  and magnitudes as those expected for ITER.

## 1. Introduction

Understanding heat flux deposition processes on Plasma Facing Components (PFC) is essential for PFC designs in order to allow reliable high power steady state plasma operations. In ITER, the PFCs will experience extreme heat and particle loads in steady state. WEST (W for tungsten Environment in Steady-state Tokamak) provides an integrated platform for testing the ITER divertor components under combined heat and particle loads in a tokamak environment [1]. One of the main objectives of the WEST project is to study the behavior of ITER-like actively cooled tungsten (W) Plasma Facing Units (PFU), in order to mitigate the risks for ITER [2]. The PFU should withstand heat fluxes close to the heat fluxes during ITER operations, which are expected to be around  $10 \text{ MW.m}^{-2}$  in steady state. It is therefore necessary to be able to measure these high heat fluxes in order to know their true amplitude and spatial distribution on the PFC surface. To achieve these objectives several thermal diagnostics (IR camera, calorimetry, embedded fibers Bragg grating and thermocouples) are planned for WEST and especially in the lower divertor where the ITER-like components will be integrated.

In the first part of the paper, the WEST lower divertor and the PFCs with embedded thermocouples (TC) are described (section 2). Then, the conjugate gradient method associated with a spatial a priori knowledge on the heat flux is presented for the estimation of the time evolution and the decay length  $\lambda_q$  of the heat flux (section 3). The results and the accuracy of the method with synthetic data are discussed based on 2D (section 4) and 3D modelling (section 5).

## 2. WEST lower divertor

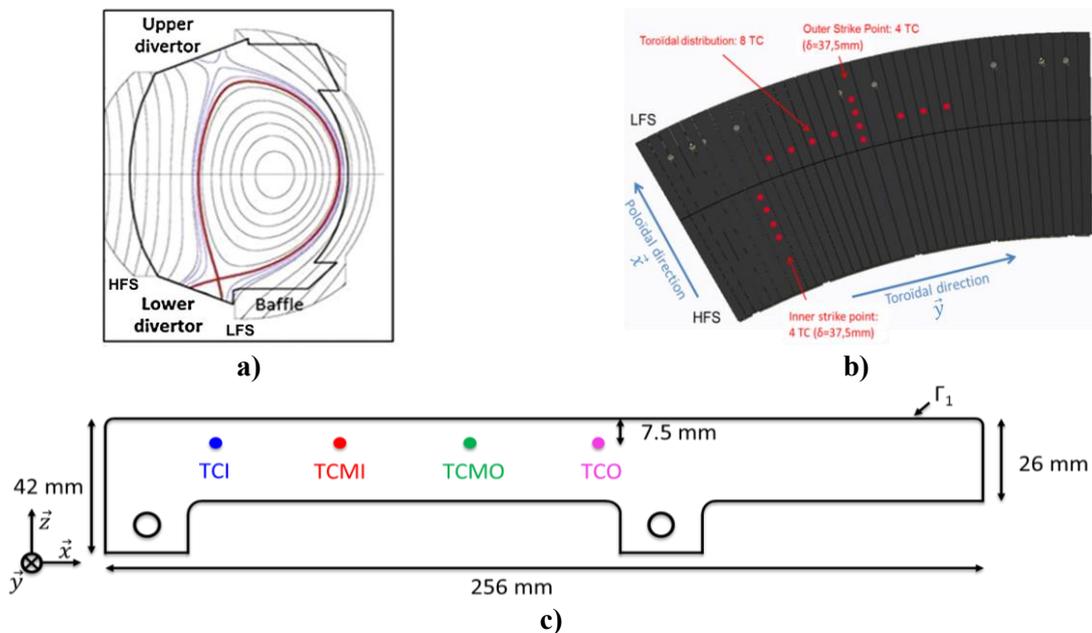
The main interaction between plasma and wall takes place in the divertor. The WEST lower divertor target is located at the bottom of the chamber (figure 1a). Its role is to sustain the power conducted through the X-point to the strike points. The WEST divertor consists of 12 independent toroidal sectors of  $30^\circ$  (one sector is represented in the figure 1b), each composed of 38 PFUs for a total of 456 to form a toroidal ring structure. The complete building of the actively cooled divertor, with W monoblocks, will take several years, longer than the other changes required. As a consequence, it has been decided to begin the operations sooner, by using a mix of actively cooled PFCs (bulk W) in combination with non-actively cooled W coated graphite PFCs (W-coating are  $15\mu\text{m}$  thick) [3]. The operation with non-



actively cooled PFCs is a good opportunity to monitor the temperature with embedded measurements. The PFU is divided into two Plasma Facing Components (PFCs), one in a Low Field Side (LFS) called the outer PFC and one in the High Field Side (HFS) called the inner PFC. Then it will be progressively replaced by the ITER-like W PFU, made of W monoblocks bonded to a copper alloy tube [4]. At the start, one sector will be a mix of actively cooled ITER-like W PFU and inertial graphite components with W coating (full inertial components in the 11 other sectors).

A total of 20 TCs is embedded in the inertial graphite PFCs (red point in the figure 1b) in order to study the heat load pattern on the divertor in the toroidal (ripple effect due to 18 superconducting toroidal field coils with periodic heat flux every 20°) and poloidal (heat flux decay length due to the Scrape Off Layer (SOL) physic) directions. Here we present the use of the 4 TCs embedded in the outer PFC at the maximal heat flux location in the toroidal direction [3]. The 4 TCs will be named TC Inboard (TCI), TC Middle Inboard (TCMI), TC Middle Outboard (TCMO), TC Outboard (TCO) and they are respectively at the poloidal coordinate 31, 68.5, 106 and 143.5mm ( $x=0$  is the left side of the PFC).

The divertor X-point configuration allows access to a wide range of plasma equilibrium. In this paper we will focus on a particular configuration called Far X-Point (FXP), with X-point localized around 7cm above the divertor (figure 1a). In this configuration the heat flux profile along the poloidal direction is very peaked at the strike point locations (intersections of red line and lower divertor in the figure 1a). The main parameter of the peaked distribution of the heat flux is the value of  $\lambda_q$ , the characteristic decay length of the heat flux density in the SOL which is expected to vary between 2.5 and 10mm.



**Figure 1.** **a)** Poloidal magnetic field configuration (Far X-Point) in the WEST Tokamak. **b)** Lower divertor view. **c)** 2D sketch of the PFC with 4TCs (the surface exposed to the plasma is on the top).

### 3. Heat flux estimation by the Conjugate Gradient Method with adjoint state

#### 3.1. Direct problem

In the paper,  $x$  represents the poloidal direction,  $y$  the toroidal direction and  $z$  the depth in the PFC. Figure 1c shows the geometry and the dimensions. The PFC is made of graphite coated on top and side with a thin tungsten deposit ( $< 30 \mu\text{m}$ ). Due to the thin layer of the coating in regard to the time step (50ms) of the study, it will be taken into account only by the change of the emissivity at the surface. The dependency of the thermal properties of graphite with temperature is taken into account. The tiles are mounted onto the support plate by the round holes at the bottom of the PFC. Moreover, the WEST

chamber is under high vacuum condition during operation (no convection exchanges). The PFC exchanges a radiative heat flux with the surrounding surfaces that are assumed to behave like the blackbody at  $T_{rad}=T_0$ , the emissivity of the graphite and the W coating is assumed known (respectively  $\varepsilon_G=0.8$  and  $\varepsilon_W=0.3$ ). The domain is initially at the same temperature, then the boundary surface  $\Gamma_1$  is subjected to a heat flux  $\phi(x, y, t)$ . Furthermore for a single PFC the heat flux is quite uniform in the toroidal direction (variation under 10%). This leads us to assume the heat transfer problem as a bi-dimensional problem (in x and z). This simplification allows us to save computing time and the accuracy of 2D versus 3D calculations will be studied in this paper. The mathematical formulation of this transient heat conduction problem is given as follows (for clarity we note  $T = T(x, z, t)$ ):

$$\begin{aligned} \rho C p(T) \frac{\partial T}{\partial t} - \vec{\nabla} \cdot (\lambda(T) \vec{\nabla}(T)) &= 0 & \text{in } \Omega & \quad (1a) \quad -\lambda(T) \frac{\partial T}{\partial n_2} = \varepsilon_W \sigma (T^4 - T_{rad}^4) & \text{on } \Gamma_2 & \quad (1d) \\ -\lambda(T) \frac{\partial T}{\partial n_1} &= \varepsilon_W \sigma (T^4 - T_{rad}^4) - \phi(x, t) & \text{on } \Gamma_1 & \quad (1b) \quad -\lambda(T) \frac{\partial T}{\partial n_3} = \varepsilon_G \sigma (T^4 - T_{rad}^4) & \text{on } \Gamma_3 & \quad (1e) \\ T &= T_0 & \text{in } \Omega & \text{ at } t=0 & \quad (1c) \end{aligned}$$

This mathematical formulation (as the adjoint and sensitivity problem) is solved by the finite element method with the software CAST3M.

### 3.2. Inverse problem

We denote  $p$ , the function to be determined, in our case this function is the heat flux  $\phi(x, t)$ :

$$p(x, t) = \phi(x, t) \quad (2)$$

Four internal temperatures are measured by type N thermocouples (figure 1), embedded at 7.5mm from the surface, with acquisition time step of 50ms. The objective of the inverse analysis is to determine the heat flux given the unsteady embedded measurement at the TC locations. We note  $Y(x, z, t)$  the temperature data taken over time by the four TCs in the PFC. The inverse heat conduction problem consists in the determination of  $p(x, t)$  minimizing  $T(x, z, t) - Y(x, z, t)$ . For this, we define the cost function which is the following quadratic criterion:

$$J(p) = \frac{1}{2} \int_0^{t_f} \sum_{i=1}^4 (T(x^i, z^i = 7.5mm, t) - Y(x^i, z^i = 7.5mm, t))^2 dt \quad (3)$$

The Conjugate Gradient Method (CGM) is the iterative process used to estimate the function  $\mathbf{p}$  by minimizing the cost function  $J(\mathbf{p})$ . The CGM calculates the new iterate  $\mathbf{p}^{n+1}$  from the previous iteration  $\mathbf{p}^n$  (with  $n$  the iteration number), by:

$$\mathbf{p}^{n+1} = \mathbf{p}^n - \gamma^n \mathbf{d}^n \quad (4)$$

where  $\gamma^n$  is the step size, determined by the resolution of the sensitivity problem, and  $\mathbf{d}^n$  is the direction of descent given by:

$$\mathbf{d}^n = \nabla J(\mathbf{p}^n) + \beta^n \mathbf{d}^{n-1} \quad \text{with } \mathbf{d}^0 = \nabla J(\mathbf{p}^0) \quad (5)$$

where  $\nabla J(\mathbf{p}^n)$  is the gradient of the cost function, determined by the resolution of the adjoint problem and the conjugation coefficient  $\beta^n$  is computed with the Polak-Ribière-Polyak's version of the CGM. The sensitivity and adjoint problem will not be developed in this paper, the reader can refer to previous work to see the details [5].

### 3.3. Heat flux profile

In our case with only four TCs, we need a priori information on the unknowns to solve the inverse problem. Eich et al. showed for the JET and ASDEX divertors [6] that the spatial distribution of the heat flux in the outer side can be expressed by a heuristic formulation, built with IR thermography during Carbon-wall operations, defined by:

$$p(x, t) = \phi(x, t) = \phi_M(t) \exp \left[ \left( \frac{c}{2} \right)^2 - \frac{x-x_0}{\lambda_q f_x} \right] \operatorname{erfc} \left( \frac{c}{2} - \frac{x-x_0}{c \lambda_q f_x} \right) \quad \text{with } \phi(x > 143mm, t) = 0 \quad (6)$$

where  $x$  is the target coordinate,  $x_0$  is the strike point location,  $\lambda_q$  is the power decay length inside the scrape off layer,  $f_x$  is the magnetic flux expansion at the PFC target and  $C$  is a constant. For the FXP configuration studied here  $f_x=3$  and  $C=0.4$ . The heat flux is set equal to 0 for  $x > 143\text{mm}$  due to the baffle (another component) shadowing which intersects the magnetic lines.

We propose here to estimate the three unknowns:  $\phi_M(t)$  the time evolution of the maximal heat flux,  $\lambda_q$  and  $x_0$  ( $f_x$  and  $C$  will be considered known and respectively equal to 3 and 0.4). In that ‘finite dimensional’ case, the only change in the methodology is the computation of the gradient. There is a component of the gradient vector for each unknown ( $\phi_M(t)$ ,  $\lambda_q$  and  $x_0$ ):

$$\nabla_{\phi_M} J(t) = \int \Psi(x, t) \exp \left[ \left( \frac{C}{2} \right)^2 - \frac{x-x_0}{\lambda_q f_x} \right] \operatorname{erfc} \left( \frac{C}{2} - \frac{x-x_0}{C \lambda_q f_x} \right) d\Gamma \quad (7)$$

$$\nabla_{\lambda_q} J = \int \int \Psi(x, t) \phi_M(t) \exp \left[ \left( \frac{C}{2} \right)^2 - \frac{x-x_0}{\lambda_q f_x} \right] \left[ \frac{x-x_0}{\lambda_q^2 f_x} \operatorname{erfc} \left( \frac{C}{2} - \frac{x-x_0}{C \lambda_q f_x} \right) - \frac{2}{\sqrt{\pi}} \exp \left[ - \left( \frac{C}{2} - \frac{x-x_0}{C \lambda_q f_x} \right)^2 \right] \frac{x-x_0}{C \lambda_q^2 f_x} \right] d\Gamma dt \quad (8)$$

$$\nabla_{x_0} J = \int \int \Psi(x, t) \phi_M(t) \exp \left[ \left( \frac{C}{2} \right)^2 - \frac{x-x_0}{\lambda_q f_x} \right] \left[ \frac{1}{\lambda_q f_x} \operatorname{erfc} \left( \frac{C}{2} - \frac{x-x_0}{C \lambda_q f_x} \right) - \frac{2}{\sqrt{\pi}} \exp \left[ - \left( \frac{C}{2} - \frac{x-x_0}{C \lambda_q f_x} \right)^2 \right] \frac{1}{C \lambda_q f_x} \right] d\Gamma dt \quad (9)$$

with  $\Psi(x, t)$  solution of the adjoint problem [5]. This leads to have one step size per parameter, the three step sizes are calculated by solving three different sensitivity problems [7].

### 3.4. TC step response

When a thermocouple (TC) is submitted to a rapid temperature change, it takes some time to reach the true temperature. This TC time-response  $\tau$  can be characterized through a simple first order equation giving its step response  $u(t)$  defined by:

$$u(t) = 1 - \exp \left( - \frac{t}{\tau} \right) \quad (7)$$

where  $\tau$  is the time constant defined as the duration required for the sensor to exhibit a 63% change from an external temperature step [8]. In our process operating condition (1mm sheathed type N TC embedded in a hole with graphite adhesive) we have  $\tau = 400\text{ms}$  ( $\tau = 200\text{ms}$  for a convective exchange into a water bath). We take into account the TC time-response by convoluting the temperature calculated at the TC location with the TC step response  $u(t)$ .

## 4. 2D feasibility study

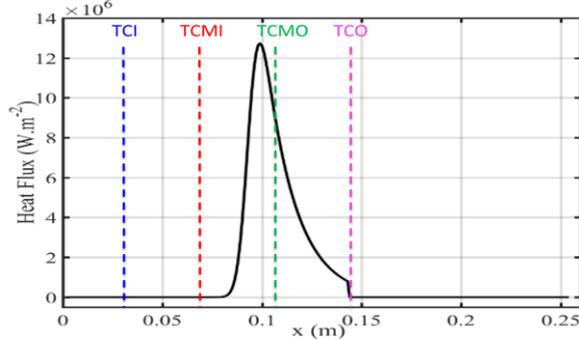
The objective of this section is to show the accuracy of the present approach in predicting  $\phi(x, t)$  with the TC measurements using the right expression of the heat flux spatial distribution. For this we generate synthetic measurement with the same expression of the heat flux than the one used for the estimation. Also we study the effect of the time response of the TCs and its impact on the estimation.

### 4.1. Synthetic measurements

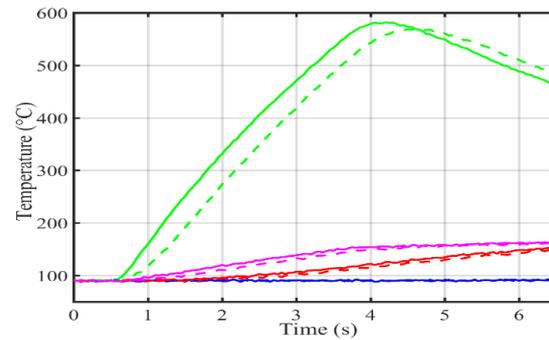
In order to avoid the ‘‘inverse crime’’ (same model used to synthesize numerical data and to inverse them) we synthesized the measurement by solving the direct problem (equation 1) with the software ANSYS (with different mesh and smaller time step) while we use CAST3M for the estimation. The heat flux used to synthesize the measurements is calculated with the equation 6 for three values of  $\lambda_q$  (2.5, 5 and 10mm). In the rest of the section we will show the results for  $\lambda_q=5\text{mm}$  and we summarize the results for all  $\lambda_q$  in the table 1. For  $\lambda_q=5\text{mm}$  we have  $x_0=93.4\text{mm}$  and  $\phi_{max}=12.73\text{MW.m}^2$ . The value of  $\phi_{max}$  is due to the shaping of the graphite PFC which have a tilt of  $1^\circ$  in comparison to the ITER-like PFU (with completely flat surface). Because of this tilt, when the ITER-like PFU is submitted to 10 MW.m<sup>2</sup> the graphite PFC receives 12.73MW.m<sup>2</sup> in the FXP configuration. The resulting heat flux is shown in the figure 2.

At  $t=0\text{s}$  the PFC is at a uniform temperature  $T_0=90^\circ\text{C}$  The simulated time is 6.5s and the time evolution of the imposed heat flux consists in a step of 3s (minimum duration in order to reach the

thermal equilibrium of the actively cooled Iter-like PFU) starting at  $t=0.5s$ . The continuous lines in the figure 3 shows the evolution of the noisy temperature (Gaussian distribution with standard deviation  $\sigma=1^\circ C$  that is the maximal order of magnitude expected) at the TCs location with a perfect time response of the TCs ( $\tau=0$ ) and the dotted lines show the noisy temperature taking into account the time response ( $\tau=400ms$ ). As expected the TCMO has the maximal heating while the TCI has a heating level lower than noise measurement.



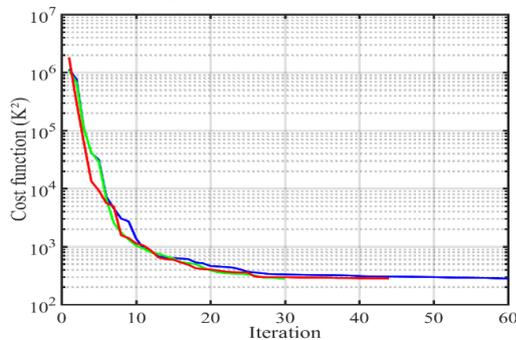
**Figure 2.** (—) Exact  $\phi(x)$  with  $\lambda_q=5.0mm$  (equation 6) with TCs poloidal locations (dotted lines)



**Figure 3.** Temperature simulation performed with ANSYS  $\tau = 0$ : (—) TCI (—) TCMi (—) TCMO (—) TCO,  $\tau = 400ms$ : (---) TCI (---) TCMi (---) TCMO (---) TCO with  $\sigma = 1^\circ C$  for  $\lambda_q=5.0mm$

#### 4.2. Estimation results

We present here the results of the inversion using the synthetic measurement for  $\lambda_q=5mm$  in three cases: 1) for  $\tau=0$ , 2) for  $\tau=400ms$  but neglected during the inversion, 3) for  $\tau=400ms$  taken into account during the inversion.

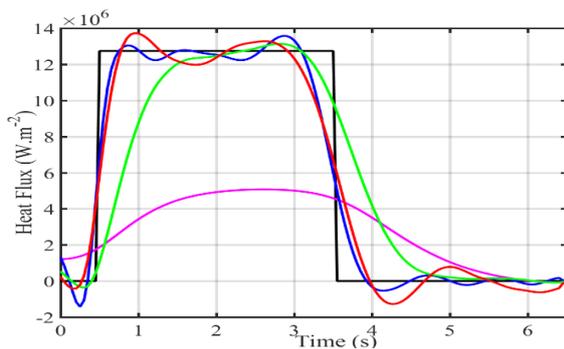


**Figure 4.** (—)  $\tau = 0$  (—)  $\tau = 400ms$  neglected (—)  $\tau = 400ms$  for  $\lambda_q=5.0mm$

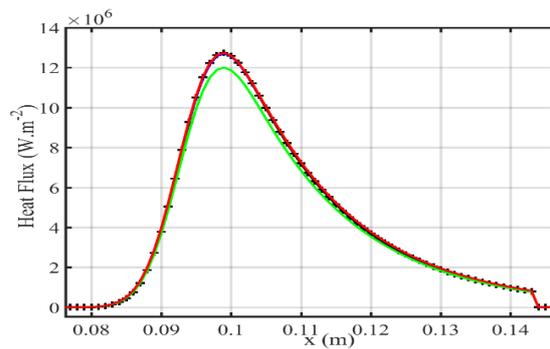
The initial guess of the parameters is set to:  $\lambda_q=10mm$  (twice of the exact value),  $x_0=80mm$  and  $\phi_M(t)$  is determined with a deconvolution method using the TCMO measurements with a 1D quadrupole model and Tikhonov regularization (magenta in figure 5) [9]. Figure 4 presents the evolution of the cost function with respect to the number of iterations for the three cases. We can see that the needed number of iterations is lower than the number of parameters to estimate (131 for  $\phi_M(t)$  and one for  $\lambda_q$  and  $x_0$ ). The computational time for a single iteration is about 10min.

Figure 5 and 6 show the estimated heat fluxes function with respect to the time and the poloidal location  $x$  (focused on the heat flux region). We note respectively that the time dependence and the spatial distribution of identified heat fluxes are well recovered for all cases except when the synthetic measurement are computed with the TC response time  $\tau=400ms$  that is neglected for the inversion. In this case the step variations are delayed with the order of magnitude of  $\tau$  but the spatial variation is still recovered thanks to the good estimations of  $\lambda_q$  and  $x_0$ .

Table 1 summarizes the results for each values of  $\lambda_q$ . We observe that the estimation of  $\lambda_q$  is done with an error less than 3% for all cases and especially for  $\lambda_q=2.5mm$  where the heat flux is the most peaked.  $\phi_{mean}$  is the average of the heat flux at the maximum location for  $0.9 < t < 3.1s$ . These results show the accuracy of this approach to estimate the intensity of the heat flux and his decay length if we have the right a priori spatial distribution of the surface heat flux. We also notice that the time response of the TCs can be taken into account to improve the estimation of  $\phi_M(t)$ .



**Figure 5.** (—)  $\phi_{exact}(t)$ , (—)  $\phi_{init}(t)$ ,  $\phi_{estimated}(t)$ : (—)  $\tau = 0$  (—)  $\tau = 400ms$  neglected (—)  $\tau = 400ms$  for  $\lambda_q=5.0mm$



**Figure 6.** (-+-)  $\phi_{exact}(x)$ ,  $\phi_{estimated}(x)$ : (—)  $\tau = 0$  (—)  $\tau = 400ms$  neglected (—)  $\tau = 400ms$  for  $\lambda_q=5.0mm$

**Table 1.** Results of the estimation for all  $\lambda_q$  and  $\tau$ . Exact values are given in the first line.

	$\phi_{mean}$ (MW.m <sup>-2</sup> )	$\lambda_q$ (mm)	$x_0$ (mm)	$\phi_{mean}$ (MW.m <sup>-2</sup> )	$\lambda_q$ (mm)	$x_0$ (mm)	$\phi_{mean}$ (MW.m <sup>-2</sup> )	$\lambda_q$ (mm)	$x_0$ (mm)
	12.73	2.5	93.11	12.73	5.0	93.4	12.65	10.0	94
$\tau = 0$	12.733 +0.02%	2.528 +1.12%	93.02 -0.1%	12.705 -0.2%	5.076 +1.52%	93.36 -0.04%	12.658 +0.06%	10.252 +2.52%	94.19 +0.2%
$\tau = 400ms$ neglected	12.132 -4.7%	2.483 -0.68%	93.12 +0.01%	12.002 -5.72%	5.059 +1.18%	93.36 -0.04%	11.941 -5.6%	10.252 +2.52%	94.17 -0.18%
$\tau = 400ms$	12.931 +1.58%	2.491 -0.36%	93.07 -0.04%	12.747 +0.13%	5.071 +1.42%	93.36 -0.04%	12.613 -0.29%	10.276 +2.76%	94.15 +0.16%

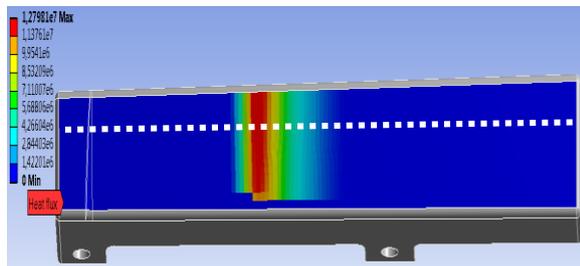
## 5. Study of 3D effects

The objective of this section is to determine the accuracy of the present approach in predicting  $\phi(x, t)$  using a 2D modeling for the inversion but using synthetic TC measurements generated with a 3D modeling. In this 3D modeling, the surface heat flux  $\phi(x, y)$  is the output of the PFCFlux code [3] that takes into account the 3D geometry of the PFC and the magnetic equilibrium.

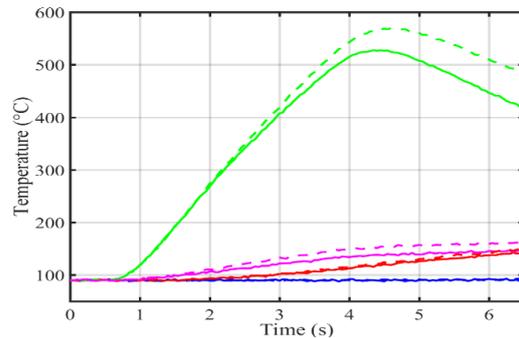
### 5.1. Synthetic measurements

The heat flux  $\phi(x, y)$  is computed with the PFCFlux code in the FXP configuration for all values of  $\lambda_q$  at the mid-plane with the distribution of the equation 6 with  $f_x=1$ . As described in [3], PFCFlux is a software dedicated to the calculation of the conducted power along the magnetic field lines assuming purely parallel transport (no cross-field transport) from the mid-plane to the PFC surface. Based on ray tracing techniques, it is able to simulate the magnetic shadowing between adjacent PFC's. One of the particularity of this calculation is to take into account the variation of the magnetic field angle of incidence along the PFC which is not taken into account in the equation 6. The computed heat flux for  $\lambda_q=5mm$  is shown in the figure 7 with the representation of the poloidal cross section of the 2D modeling, one can note at the bottom of the surface the shadowing ( $\phi = 0$  in blue) due to the previous PFC (about 3 mm). In addition, it appears also that the side of the PFC are not submitted to heat flux due to their shaping 2mm round edge.

Figure 8 shows in continuous lines the synthetic measurement generated with ANSYS in 3D using the heat flux computed with PFCFlux with the same time evolution as previously (step of 3s) and  $\tau=400ms$ . The dotted lines represent the synthetic measurement generated with ANSYS in 2D used before. As expected the discrepancies between the 3D and 2D modeling increase with time, the 3D heating is lower than the 2D one (about 10% after 3s) and the cooling rate is higher. This can be explained with the little wetted areas in the 3D modeling due to the shadowing effects and the PFC curved side (2mm round corner with no heat load).



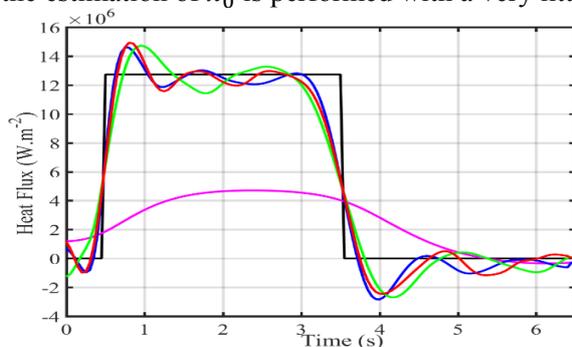
**Figure 7.**  $\phi(x, y)$  ( $\text{W} \cdot \text{m}^{-2}$ ) calculated by PFCFlux for  $\lambda_q=5.0\text{mm}$  at the mid-plane, white dotted line is the cross section of the 2D modelling (TCs location)



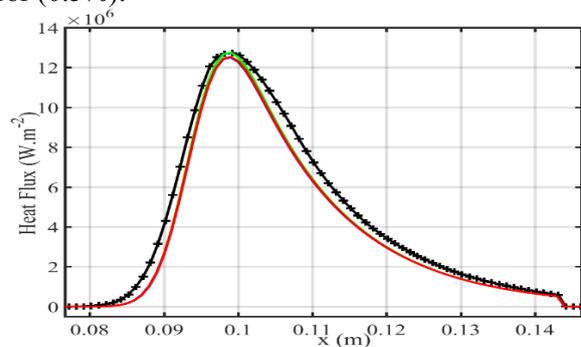
**Figure 8. simulated by ANSYS in 3D:** (—) TCI (—) TCMI (—) TCMO (—) TCO, simulated by ANSYS in 2D: (---) TCI (---) TCMI (---) TCMO (---) TCO all with  $\tau = 400\text{ms}$ ,  $\sigma = 1^\circ\text{C}$  and  $\lambda_q=5.0\text{mm}$

### 5.2. Estimation results

We present here the results of the inversion using the 3D synthetics measurement for  $\lambda_q=5\text{mm}$  with three levels of noise: 1)  $\sigma=0.25^\circ\text{C}$ , 2)  $\sigma=1^\circ\text{C}$ , 3)  $\sigma=2^\circ\text{C}$ . The initial guess of the parameters is set by the same way as previously:  $\lambda_q=10\text{mm}$ ,  $x_0=80\text{mm}$  and  $\phi_M(t)$  with a deconvolution method using the TCMO measurements (magenta in figure 9) [9]. Figure 9 and 10 show respectively the estimated heat fluxes versus time and versus the poloidal location. We note that the dynamic is well recovered with a little under estimation of the heat flux about 2% and a little negative heat flux in the cooling phase to correct the higher inertial cooling of the 3D modeling. We can see the equivalent estimation with the different noise levels showing the robustness of the method in regard of noise measurements. Figure 10 shows also an under estimation of the  $\lambda_q$  of the heat flux for the three cases, this error is about 12% (4.4mm estimated instead of 5mm imposed in the PFCFlux code). Despite of the errors on  $\lambda_q$  and  $\phi_M(t)$ , the estimation of  $x_0$  is performed with a very little error (0.5%).



**Figure 9.** (—)  $\phi_{exact}(t)$ ,  $\phi_{estimated}(t)$ : (—)  $\sigma = 0.25^\circ\text{C}$  (—)  $\sigma = 1^\circ\text{C}$  (—)  $\sigma = 2^\circ\text{C}$  for  $\lambda_q=5.0\text{mm}$



**Figure 10.** (—)  $\phi_{exact}(x)$ ,  $\phi_{estimated}(x)$ : (—)  $\sigma = 0.25^\circ\text{C}$  (—)  $\sigma = 1^\circ\text{C}$  (—)  $\sigma = 2^\circ\text{C}$  for  $\lambda_q=5.0\text{mm}$

**Table 2.** Results of the estimation for all  $\lambda_q$  and  $\sigma$ . Exact values are given in the first line.

	$\phi_{mean}$ ( $\text{MW} \cdot \text{m}^{-2}$ )	$\lambda_q$ (mm)	$x_0$ (mm)	$\phi_{mean}$ ( $\text{MW} \cdot \text{m}^{-2}$ )	$\lambda_q$ (mm)	$x_0$ (mm)	$\phi_{mean}$ ( $\text{MW} \cdot \text{m}^{-2}$ )	$\lambda_q$ (mm)	$x_0$ (mm)
	12.73	2.5	93.11	12.73	5.0	93.4	12.65	10.0	94
$\sigma = 0.25^\circ\text{C}$	13.372	2.155	93.97	12.505	4.399	93.92	11.562	9.174	94.048
	+5.04%	-13.80%	+0.92%	-1.77%	-12.02%	+0.56%	-8.6%	-8.26%	+0.05%
$\sigma = 1^\circ\text{C}$	13.154	2.211	93.9	12.534	4.39	93.959	11.546	9.170	94.086
	+3.33%	-11.56%	+0.85%	-1.54%	-12.2%	+0.6%	-8.73%	-8.3%	+0.09%
$\sigma = 2^\circ\text{C}$	13.807	2.103	94.079	12.750	4.368	93.951	11.395	9.170	94.049
	+8.46%	-15.88%	+1.04%	+0.16%	-12.64%	+0.59%	-9.92%	-8.3%	+0.05%

Table 2 summarizes the results for each values of  $\lambda_q$ . We observe that the estimation of  $\lambda_q$  is done with errors from 8.3% for  $\lambda_q=10\text{mm}$  to 16% for  $\lambda_q=2.5\text{mm}$ . This error has been quantified here for each parameter, in the range of expected values of  $\lambda_q$  including the 3D thermal effect (shadowing, wetted area, finite size and shaping of the PFC). These results show that the assumptions of our model (2D, heuristic formulation for the spatial distribution of  $\phi$ ) lead to acceptable errors on the estimated heat flux.

## 6. Conclusion

In this paper, 2D nonlinear unsteady calculations are used with the Conjugate Gradient Method and the adjoint state, for the heat flux estimation on the divertor graphite PFCs of the WEST tokamak. The combination of the heuristic target heat load profiles [6] (mainly constructed with IR thermography during Carbon-wall operation period) with an inverse heat flux calculation using the embedded TCs data, makes it possible the estimation of the maximum intensity  $\phi_M(t)$ , the decay length ( $\lambda_q$ ) and the strike point location ( $x_0$ ) of the surface heat flux on the divertor PFCs. It should be noted that no a priori information on the time evolution of the heat flux is needed for the estimation. This work is a positive evolution from previous studies [5] where only one embedded thermocouple was used for inversion making it mandatory knowledge of the true values of  $\lambda_q$  and  $x_0$ . Here, the use of multiple embedded thermocouples makes it possible to simultaneously identify  $\lambda_q$  and  $x_0$  together with  $\phi_M(t)$ .

Application to synthetic measurement generate with 2D modeling has been firstly introduced in order to study the accuracy of the method and the consideration of the time response of the TCs. We notice the good accuracy of this approach to estimate the intensity of the heat flux (< 2%) and his decay length (< 3%) if we have the right a priori heat flux spatial distribution. Finally we applied the method to synthetic measurement generated with 3D modeling and heat flux  $\phi(x,y)$  calculated with a dedicated code (PFCFlux [3]) taking into account the shadowed and wetted areas of the PFC. The results showed that the assumptions of our model (2D, heuristic formulation for the spatial distribution of  $\phi$ ) lead to acceptable errors on the heat flux estimation for the range of expected values of  $\lambda_q$  (errors on  $\lambda_q$  estimation go from 8.3% for  $\lambda_q=10\text{mm}$  to 16% for  $\lambda_q=2.5\text{mm}$ ).

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