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ON THE ISSUE OF THE PEMFC OPERATING FAULT IDENTIFICATION:

GENERIC ANALYSIS TOOL

BASED ON VOLTAGE POINTWISE SINGULARITY STRENGTHS

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Abstract. The purpose of this article is to study the portability of a non-intrusive and free of any external / internal disturbance diagnosis tool devoted to the monitoring of the State of Health (SoH) of PEM Fuel Cell (PEMFC) stack. The tool is based on a thorough analysis of the stack voltage signal using a multifractal formalism and wavelet leaders. It offers well-suited signatures indicators on the SoH of the Fuel Cell. Some relevant descriptors extracted from these patterns (singularity features) are used in the frame of Machine Learning approaches to allow the PEMFC fault identification. The proposed diagnosis strategy is evaluated with two different PEMFC stacks. The first one is designed for automotive applications and the second one is dedicated to stationary use (micro combined heat and power - µCHP application).

1. Introduction

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Fuel cells (FC) are considered as a promising alternative way for energy conversion [1]. To ensure their durability, reliability 53 and safety, many fault diagnosis and fault tolerant control 54 methods have been proposed. These methods can be classified 55 into two groups: model-based methods [2-5] and data-driven 56 methods [6-8]. The methods of the first group are very 50 cumbersome and complex because they require an in-depth 57 knowledge of the multi-physical mechanisms (thermal, 58 electrical, electrochemical, and fluidic ones) which can occur 59 in FC systems. They are based on numerous parameters 60 governing its operation, and their values are difficult to 61 estimate. Some model-based methods allows a deeper 62 understanding of the FC physics but they might be not suitable to provide an accurate / quantitative description of the FC 63 performances. Hence, the data-driven techniques attract more 64 and more attention because of their simplicity regarding the 65 implementation and the good performances obtained without profound system structure knowledge. They are supported by 66 efficient signal processing methods as: Fourier transform [9], 67 multi-resolution analysis [10, 11], singularity analysis [12, 13]. 68 For fault identification and isolation tasks, some works use 69 Electrochemical Impedance Spectra (EIS) as normal or faulty 70 operation signatures to supply artificial intelligence algorithms 71 (based for instance on fuzzy logic [14] or neural networks [15]) 72 or conventional pattern recognition approaches (based on 73

Support Vector Machines (SVM) [16], k-nearest neighbors (knn) [13] methods).

This work aims at studying the portability of an innovative data driven approach dedicated to PEMFC diagnosis, named singularity analysis. This method consists in analyzing the pointwise singularities stamped in the stack voltage signal for various FC operating conditions. The singularity features are then summarized in the form of concave arcs estimated thanks to a set of mathematical equations, baptized multifractal formalism [17-19]. The advanced analysis tool, named Voltage Singularity Spectrum (VSS) is then obtained using a non-intrusive manner and without affecting in any way the FC operation. Indeed, no external additional AC-solicitation has to be superimposed to the existing DC load current as it is the case in the usual EIS operation mode.

This paper is organized as follow. Section 2 deals with the experimental work and environment conducted with two PEMFC stacks. In section 3, a brief mathematical foundation of the singularity measurement is given. In section 4, we show how it is possible to make the singularity spectrum combined with Machine Learning techniques as a PEMFC diagnosis tool. Then, the portability of the proposed tool is discussed. Main conclusions are given in Section 5.

2. Experimental

2 Synopsis of the investigated PEM Fuel Cells

In our study, two PEMFC stacks are experimented to evaluate 31 3 the portability of the proposed diagnosis tool. The first one is 5 an 8 cells stack designed for automotive applications and 6 manufactured by CEA (Alternative Energies and Atomic 7 Energy Commission). The second one is a 12 cells stack 8 dedicated to stationary application (micro combined heat and 9 power - µCHP application). It is designed and marketed by 10 Riesaer Brennstoffzellentechnik GmbH and Engineering GmbH, Germany. 11

12 The first stack (PEMFC_{Auto}) is made of metallic gas distributor plates. The electrode active surface of a cell is equal to 220

cm². It is fed by air at cathode and pure hydrogen (H₂) at anode. 32
 A summary of the FC nominal operating conditions is given in
 Table 1. The stack operates with a nominal current of 110 A. 33

17 A picture of the stack is shown in Fig. 1(a).

18 The second stack (PEMFC $_{\mu CHP}$) is fed by air at cathode, and at 35 anode by a fuel mixture (75 % of H₂ and 25 % of carbone 36

20 dioxide -CO₂) simulating a reformat. It is made of graphite gas
21 distributor plates. The electrode's active surface is 196 cm². 37

The stack operates with a nominal current of 80 A. A picture 38 of the stack is given in Fig. 1(b). A summary of the FC nominal 39

operating parameters and other main characteristics are given $\frac{1}{40}$

25 in Table 2.

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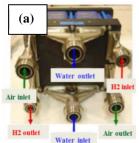
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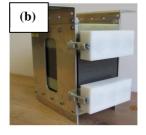


Fig. 1. Pictures of the two investigated PEMFC stacks: a) 8 cell stack designed for automotives (PEMFC_{Auto}), b) 12 cell stack designed for μCHP operation (PEMFC_{uCHP}).

Table 1. PEMFC_{Auto} nominal operating conditions.

| | | |
|---|---------|-------------|
| Coolant flow: deionized water | 2 1/min | 5 |
| Anode stoichiometry rate (H ₂) | 1.5 | — 5 — 5 |
| Cathode stoichiometry rate (air) | 2 | — 5 — 5 |
| Absolute pressure for H ₂ and air inlets | 150 kPa | — 5 — 6 |
| Max. anode - cathode pressure gap | 30 kPa | —_ 0 6 |
| Temperature of the cooling circuit | 80°C | 6 |
| | | 6 |

| Anode and cathode relative humidity rate | 50 % |
|--|-------|
| Nominal Current | 110 A |

Table 2. The PEMFC μ CHP nominal operating conditions.

| Coolant flow: deionized water | 3 l/min |
|---|---------|
| Anode stoichiometry rate (H ₂ & CO ₂ mix) | 1.3 |
| Cathode stoichiometry rate (air) | 2 |
| Absolute pressure for H ₂ and air inlets | 150 kPa |
| Max. anode - cathode pressure gap | 20 kPa |
| Temperature of the cooling circuit | 75°C |
| Anode and cathode relative humidity rate | 50 % |
| Nominal Current | 80 A |

Experimental process

The above described PEMFCs were experimented with testbenches developed in the FC platform of Belfort, France. It includes mainly:

- a complete gas conditioning sub-system including gas humidifiers at anode and cathode,
- a test stand section dedicated to the control of the temperature inside the stack and including the FC primary water circuit.
- an electric / electronic management sub-system,
- an electronic load.

The monitoring and the control of the FC testbenches parameters are done through National Instruments materials and a dedicated software. A Human-Machine Interface (HMI) was also developed in-lab using Labview TM.

The purpose of the experimental protocol was to introduce different controlled health states into the PEMFC stacks by configuring various operating parameters. Two PEMFC health states were set: no stack failure state (when the FC is operating under normal parameters) and with stack failure state (when the FC is operating under abnormal / severe parameters).

Different scenarios of FC system failure were associated to the changing of different setting physical parameters through the control-command interface of the testbenches, namely: cathode stoichiometry rate (FSC), anode stoichiometry rate (FSA), gas pressure (P), cooling circuit temperature (T) and relative humidity level (RH).

The set of the tests performed, with the two stacks and according to the degrading operating parameters, is reported

in Table 3.

Table 3. The set of FC operating conditions applied during the experimentation of the two stacks. The underlying parameter values correspond to the introducing faults. The notation 'ND' means that the FC experiment is not done.

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| Parameters value | Ref | DFSC | DFSA | DP | DT | DH | DCO |
|------------------|-----|------|------|----|----|----|-----|

| | Auto | μСНР | Auto | μСНР | Auto | μСНР | Auto | μСНР | Auto | μСНР | Auto | μСНР | Auto | μСНР |
|----------------------|------|------|------|------------|------|------------|------|-----------|-----------|------------------------|-----------|----------|-----------|------|
| FSC | 2 | 2 | 1.3 | 2.6 1.6 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| FSA | 1.5 | 1.3 | 1.5 | 1.3 | 1.3 | 1.5 1.2 | 1.5 | 1.3 | 1.5 | 1.3 | 1.5 | 1.3 | 1.5 | 1.3 |
| P (bar abs) | 1.5 | 0.1 | 1.5 | 0.1 | 1.5 | 0.1 | 1.3 | <u>ND</u> | 1.5 | 0.1 | 1.5 | 0.1 | 1.5 | 0.1 |
| T (°C) | 80 | 70 | 80 | 70 | 80 | 70 | 80 | 70 | <u>75</u> | <u>72</u> <u>65</u> | 80 | 70 | 80 | 70 |
| RH (%) | 50 | 50 | 50 | 50 | 50 | 50 | 50 | 50 | 50 | 50 | <u>ND</u> | 46 54 | 50 | 50 |
| Presence of CO (ppm) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | <u>10</u> | ND |

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3. Singularity measurement

Multifractals are the distribution of singularities, all lying on interwoven sets of varying fractal dimensions Multifractals arise in a variety of physical signals in the forms 29 5 of self-similar sub-sets of samples, such as Multifractional $\frac{1}{30}$ 6 Brownian Motion (MBM) signal [21], signals in turbulence 31 7 [22], and temporal series in finance [23].

The singularity analysis, also named "multifractal analysis" 33 allows the characterization of data by describing globally and 34 10 geometrically the fluctuations of local regularity, usually 35 11 12 measured by means of the Hölder exponent h.

13 It describes the time (t) based fluctuations of the signal given 37 by a function X(t). This is achieved by comparing the local variations of X(t) around fixed time position t_0 , against a local ³⁸ 15 power law behavior: $X(t_0)$ is said to belong to $C^{\alpha}(t_0)$ with

 $\alpha \ge 0$ if there are a positive constant C and a polynomial P, satisfying $\deg(P) < \alpha$, such that $|X(t) - P_{t_0}(t)| \le C|t - \alpha|$ $t_0|^{\alpha}$. 19

20 The Hölder exponent is defined as the largest α such as: $h(t_0) = \sup\{\alpha : X \in C^{\alpha}(t_0)\}.$

22 In practice, when $h(t_0)$ takes a value which tends to zero, the 23 signal exhibits a strong singularity at t_0 (Fig. 2).

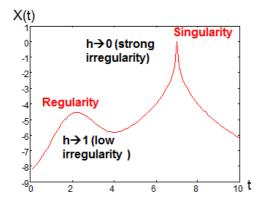


Fig. 2. Illustration of two pointwise regularity measures in the signal X(t) quantified by the Hölder exponent h.

The singularity strength regarding the variability of the regularity of X(t) vs. t is usually described through the socalled singularity spectrum. Building a singularity spectrum consists in associating to each Hölder exponent h the Hausdorff dimension D(h) of the sets of points which exhibit the same value of *h*:

$$h \mapsto D(h)$$

An example of singularity spectrum is given in Fig. 3.

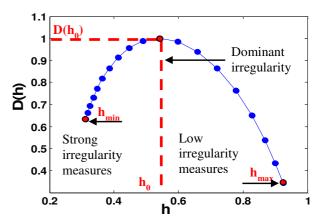


Fig. 3. Example of a singularity spectrum D(h).

The numerical implementation of the mathematical formula can be achieved using the wavelet leaders multifractal formalism. Detailed descriptions of the theoretical and practical relevance, and benefits of the use of wavelet leaders for singularity analysis are depicted in [17-19].

4. Voltage Singularity Spectrum as diagnosis tool 31

In this work, we propose to study the portability of the new diagnosis tool based on the investigation of singularity measurements stamped in FC stack voltage signals. Indeed, measuring local singularities on voltage signals provides suitable information about the evolving dynamics of non-stationary and non-linear processes involved in FC systems. We assess the generalization and the usefulness of the proposed VSS by establishing the diagnosis on two databases

For the stack PEMFC_{Auto}, 10 scenarios are analyzed (normal and abnormal conditions including one fault or more complex situations with 2 or 3 faults occurred simultaneously).

issued from the two investigated PEMFC stacks.

For the stack PEMFC $_{\mu CHP}$, 9 operating conditions (normal and abnormal conditions) are studied.

In this aim, we use 30 voltage profiles for each FC operating 35 condition; each voltage profile covers 1000 voltage samples acquired at a frequency f_a =11Hz (Fig. 4) using the monitoring 37 data system of the FC experimental test bench.

To perform the VSS, the analyzing wavelet is selected as 40 Daubechies 3 ('Db3') function (with 3 vanishing moments, 41 Fig. 4).

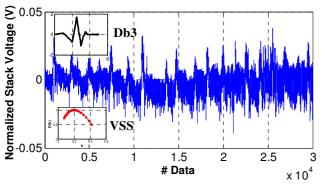


Fig. 4. Stack voltage signal scanned by Daubechies wavelet (Db3) for VSS computing.

32 An example of a set of 30 VSS is shown in Fig. 5.

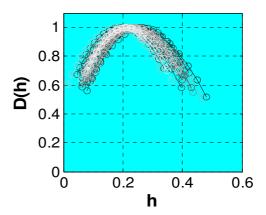


Fig. 5. Typical VSS computed on 30 profiles covering 1000 stack voltage samples.

Singularity features are then used to supply the Machine Learning approach, named k Nearest Neighbors (kNN). To improve the performance of the fault classification method, the Minimum Redundancy - Maximum Relevance (MRMR) technique [24] is used to select some relevance features offering the best classification rates.

Actually, 20 VSS / class are used to generate the learning database and the 10 others serve as test data to evaluate the performances of the classifier. Each VSS contains 38 features (19 h data and 19 D(h) data). So, by applying the MRMR method on the full feature set (38 features) of the VSS, the good classification rate obtained using the top 6 selected features is about 89.4 % for the stack PEMFC_{Auto}, separating 10 classes (10 FC operating conditions).

For the second stack PEMFC $_{\mu CHP}$, 9 classes are discriminated with a success of 95.5 %.

The best results of the classification rates of the different operating conditions studied are embedded in confusion matrixes given by Tables 4 and 5, for the stacks PEMFC_{Auto} and PEMFC_{μ CHP} respectively.

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Table 4. Confusion matrix of the good classification rates obtained with MRMR and kNN from the VSS computed with the stack voltage signals of the PEMFC_{Auto}. The studied FC operating conditions are: Ref: normal conditions - DFSC: cathode flow fault (slight air starvation) - **DFSA**: anode flow fault (slight H₂ starvation) - **DP**: gas pressure fault (lower gas pressure) - **DT**: cooling circuit temperature fault (lower stack temperature) - DCO: carbon monoxide poisoning (H₂+CO).

| Class | C_0 | C_1 | C_2 | C_3 | C_4 | C_5 | C_6 | \mathbf{C}_7 | C_8 | C ₉ |
|------------------|-------------|------------|------------|-----------|------------|------------|------------|----------------|------------|----------------|
| Ref | <u>87.5</u> | 0 | 0 | 12.5 | 0 | 0 | 0 | 0 | 0 | 0 |
| DFSC | 0 | <u>100</u> | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| DFSA | 0 | 0 | <u>100</u> | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| DP | 50 | 0 | 0 | <u>50</u> | 0 | 0 | 0 | 0 | 0 | 0 |
| DT | 0 | 0 | 0 | 0 | <u>100</u> | 0 | 0 | 0 | 0 | 0 |
| DCO | 0 | 0 | 0 | 0 | 0 | <u>100</u> | 0 | 0 | 0 | 0 |
| DFSC & DP | 0 | 0 | 0 | 0 | 0 | 0 | <u>100</u> | 0 | 0 | 0 |
| DFSA & DP | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 71.43 | 28.57 | 0 |
| DFSC & DFSA | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | <u>100</u> | 0 |
| DFSC & DFSA & DP | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | <u>100</u> |

With: $C_0 \equiv \widehat{Ref}$, $C_1 \equiv \widehat{DFSC}$, $C_2 \equiv \widehat{DFSA}$, $C_3 \equiv \widehat{DP}$, $C_4 \equiv \widehat{DT}$, $C_5 \equiv \widehat{DCO}$, $C_6 \equiv DF\widehat{CS}$ & DP, $C_7 \equiv DFSA \& DP, C_8 \equiv DFSC \& DFSA, C_9 \equiv DFSC \& \widehat{DFSA} \& DP.$

Table 5. Confusion matrix of the good classification rates obtained with MRMR and kNN from the VSS computed with the stack voltage signals of the PEMFC_{µCHP}. The studied FC operating conditions are: **Ref**: normal conditions - **DFSC**': cathode flow fault (air over-supply) - **DFSC** : cathode flow fault (slight air starvation) - **DFSA** : anode flow fault (H₂ over-supply) - **DFSA** : anode flow fault (H₂ starvation) - **DT**': cooling circuit temperature fault (higher temperature) - **DT**₂: cooling circuit temperature fault (lower stack temperature) - **DRH**': dew temperature fault (higher dew temperature) - **DRH**_{\scripts}: dew temperature fault (lower dew temperature).

| Class | C_0 | C_1 | C_2 | C_3 | C_4 | C_5 | C_6 | \mathbf{C}_7 | C_8 |
|-------------------|------------|------------|------------|-----------|-----------|-----------|------------|----------------|------------|
| Ref | <u>100</u> | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| DFSC ⁷ | 0 | <u>100</u> | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| DFSC∖ | 0 | 0 | <u>100</u> | 0 | 0 | 0 | 0 | 0 | 0 |
| DFSA ⁷ | 0 | 0 | 0 | <u>90</u> | 0 | 10 | 0 | 0 | 0 |
| DFSA | 0 | 0 | 0 | 0 | <u>90</u> | 0 | 0 | 0 | 10 |
| DT [/] | 0 | 0 | 0 | 20 | 0 | <u>80</u> | 0 | 0 | 0 |
| DT∖ | 0 | 0 | 0 | 0 | 0 | 0 | <u>100</u> | 0 | 0 |
| DRH [/] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | <u>100</u> | 0 |
| DRH√ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | <u>100</u> |

With: $C_0 \equiv \widehat{Ref}$, $C_1 \equiv \widehat{DFSC}$, $C_2 \equiv \widehat{DFSC}$, $C_3 \equiv \widehat{DFSA}$, $C_4 \equiv \widehat{DFSA}$, $C_5 \equiv \widehat{DT}$, $C_6 \equiv \widehat{DT}$, $C_7 \equiv \widehat{DRH}$, $C_{8} \equiv DRH_{\lambda}$.

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As we can see, the proposed diagnosis strategy identifies 30 successfully several complex operating faults (i.e. slight 31 deflections from the nominal operating conditions, and even 32 combination of faults) for both PEMFC_{Auto} and PEMFC_{µCHP}.

5. Conclusions

In this study, VSS are computed on voltage signals acquired under different FC operating conditions (normal and abnormal, i.e. more or less severe, deviations from the normal conditions) with considering situations that combine 2 or 3 faults simultaneously. Two stacks are investigated: a PEMFCAuto stack that is designed for automotive applications and a PEMFC_{uCHP} stack, dedicated to stationary ones.

34 Singularity features extracted from the estimated VSS are 35 classified using Machine Learning approach, named k-Nearest 36 Neighbors (kNN).

- 1 The obtained classification results show that the proposed 51
- 2 PEMFC diagnosis tool allows identifying simple operating ⁵²
- 3 faults and more complicated situations that contain several 53
- 4 fault types. The diagnosis are realized on two different test 55
- 5 stands, for different stack sizes, powers and technologies, with 56
- 6 different targeted environments of power application.
- 7 In this paper, we demonstrate that the singularity analysis of 59
- 8 voltage signal offers a generic diagnosis tool for the PEMFC 60
- 9 SoH monitoring. One key-point of the method is that the VSS 61
- 10 can be estimated from the "free" evolution of the stack voltage $\frac{62}{63}$
- 11 and without affecting in any way the FC operation: no external $\frac{63}{64}$
- 12 additional solicitation is required to reveal the SoH patterns.

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- 17 "Decentralized energy production" project, directed by
- 18 EFFICACITY, the French R&D Institute for urban energy 73
- 19 transition.

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21 References

- 22 [1] Fuel Cell Industry Review 2015: 80 23 http://www.fuelcellindustryreview.com.
- [2] Buchholz, M. and Brebs V., Dynamic Modelling of a Polymer 82
 Electrolyte Membrane Fuel Cell Stack by Nonlinear System 83
 Identification. Fuel Cells 7, 392-401, 2007.
- [3] Mainka, J., Maranzana, G., Thoaq, A., Dillet, J., Didierjean, S. 85
 and Lottin O., One-dimensional Model of Oxygen Transport 86
 Impedance Accounting for Convection Perpendicular to the 87
 Electrode. Fuel Cells 12, 5, 848-861, 2012.
- [4] Chevalier, S., Auvity, B., Olivier, J.C., Josset, C., Trichet D. and 89
 Machmoum M., Multiphysics dc and ac models of a pemfc for 90
 the detection of degraded cell parameters. *International Journal* 91
 of Hydrogen Energy, 38, 26, 11609-11618, 2013.
- [5] Petrone, R., Zheng, Z., Hissel, D., Péra, M.C., Pianese, C., 93
 Sorrentino, M., Becherif, M., et al, A review on model-based 94
 diagnosis methodologies for PEMFCs. *International Journal of* 95
 Hydrogen Energy, 38, 7077-7091, 2013.
- 39 [6] Zheng, Z., Petrone. R., Péra, M.C., Hissel, D., Becherif, M., 97
 40 Pianese, C., et al. A review on non-model based diagnosis 98
 41 methodologies for PEM fuel cell stacks and systems. 99
 42 International Journal of Hydrogen Energy, 38, 21, 8914-8926.
 43 2013.
- 44 [7] Giurgia, S., Tirnovan, S., Hissel, D., Outbib, R., An analysis of 101 fluidic voltage statistical correlation for a diagnosis of PEM fuel cell flooding. *International Journal of Hydrogen Energy*, 38, 11103 4689-4696, 2013.
- 48 [8] Li, Z., Outbib, R., Hissel, D., Giurgia, S., Data-driven diagnosis 49 of PEM fuel cell: A comparative study. Control Engineering 50 Practice, 28, 1-12, 2014.

- [9] Chen, J. and Zhou, B. Diagnosis of PEM fuel cell stack dynamic behaviors. *Journal of Power Sources*, 177, 83-95, 2008.
- [10] Rubio, M.A., Bethune, K., Urquia, A., St-Pierre, J. Proton exchange membrane fuel cell failure mode early diagnosis with wavelet analysis of electrochemical noise. *International Journal* of Hydrogen Energy, 41, 14991-15001, 2016.
- [11] Yousfi-Steiner, N., Hissel, D., Moçotéguy, P., Candusso, D., Non intrusive diagnosis of polymer electrolyte fuel cells by wavelet packet transform. *International Journal of Hydrogen Energy*, 36, 740-746, 2011.

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- [12] Benouioua, D., Candusso, D., Harel, F., Oukhellou, L. PEMFC stack voltage singularity measurement and fault classification. *International Journal of Hydrogen Energy*, 39, 36, 21631-21637, 2014.
- [13] Benouioua, D., Candusso, D., Harel, F., Oukhellou, L. The dynamix multifractality in PEMFC stack voltage signal as a tool for the aging monitoring. *International Journal of Hydrogen Energy*, 42, 2, 1466-1471, 2017.
- [14] Hissel, D., Candusso, D. and Harel, F. Fuzzy-Clustering durability diagnosis of Polymer Electrolyte Fuel Cells dedicated to transportation applications. *IEEE Transactions on Vehicular Technology*, 56, 5, 2414-2420, 2007.
- [15] Kim, J., Lee, I., Tak, Y., Cho, B.H. State-of-Health diagnosis based on hamming neural network using output voltage pattern recognistion for a PEM fuel cell. *International Journal of Hydrogen Energy*, 37, 5, 4280-4289, 2012.
- [16] Li, Z., Outbib, R., Giurgia, S., Hissel, D., Jemei, S., Giraud, A., Rosini, A. Online implementation of SVM based fault diagnosis strategy for PEMFC systems. *Applied Energy*, 164, 284-293, 2016.
- [17] Jaffard, S., Lashermes, B., Abry, P. Wavelet leaders in multifractal analysis, in Wavelet Analysis and Applications. Ed. Birkhäuser Verlag, 2006.
- [18] Wendt, H., Abry, P. Multifractality Tests Using Bootstrapped Wavelet Leaders. *IEEE Transactions on Signal Processing*, 55(10), 4811-4820, 2007.
- [19] Benouioua, D., Candusso, D., Harel, F., Oukhellou, L. Multifractal analysis of stack voltage based on wavelet leaders: A new tool for PEMFC diagnosis. *Fuel Cells*, 17, 2, 217-224, 2017.
- [20] Mandelbrot, B. B., *Fractals Geometry of Nature*. Edition. Freeman, San Francisco, 1982.
- [21] Balança, P., Some sample path properties of multifractional Brownian motion. Stochastic Processes and their Applications, 125, 10, 3823-3850, 2015.
- [22] Chevillard, L., Castaing, B., Lévêque, E., Arneodo, A. Unified multifractal description of velocity increments statistics in turbulence: Intermittency and skewness. Physica D, 218, 77-82, 2006.
- [23] Grech, D., Alternative measure of multifractal content and its application in finance. Chaos, Solitons and Fractals, 88, 183-195, 2016.
- [24] <u>Hanchuan Peng's web site</u>. Information on mRMR (minimum Redundancy Maximum Relevance Feature Selection). http://penglab.janelia.org/proj/mRMR/. 2014.