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ON THE ISSUE OF THE PEMFC OPERATING FAULT IDENTIFICATION: GENERIC ANALYSIS TOOL BASED ON VOLTAGE POINTWISE SINGULARITY STRENGTHS

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Abstract. The purpose of this article is to study the portability of a non-intrusive and free of any external / internal disturbance diagnosis tool devoted to the monitoring of the State of Health (SoH) of PEM Fuel Cell (PEMFC) stack. The tool is based on a thorough analysis of the stack voltage signal using a multifractal formalism and wavelet leaders. It offers well-suited signatures indicators on the SoH of the Fuel Cell. Some relevant descriptors extracted from these patterns (singularity features) are used in the frame of Machine Learning approaches to allow the PEMFC fault identification. The proposed diagnosis strategy is evaluated with two different PEMFC stacks. The first one is designed for automotive applications and the second one is dedicated to stationary use (micro combined heat and power - μ CHP application).

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1. Introduction 25

26 Fuel cells (FC) are considered as a promising alternative way for energy conversion [1]. To ensure their durability, reliability 53 27 and safety, many fault diagnosis and fault tolerant control 54 28 methods have been proposed. These methods can be classified 55 29 into two groups: model-based methods [2-5] and data-driven 56 methods [6-8]. The methods of the first group are very 56 30 31 cumbersome and complex because they require an in-depth 57 32 knowledge of the multi-physical mechanisms (thermal, 58 33 34 electrical, electrochemical, and fluidic ones) which can occur 59 35 in FC systems. They are based on numerous parameters 60 governing its operation, and their values are difficult to 61 36 estimate. Some model-based methods allows a deeper 62 understanding of the FC physics but they might be not suitable 6237 38 to provide an accurate / quantitative description of the FC 63 39 performances. Hence, the data-driven techniques attract more 64 40 41 and more attention because of their simplicity regarding the 65 42 implementation and the good performances obtained without 43 profound system structure knowledge. They are supported by 66 44 efficient signal processing methods as: Fourier transform [9], 67 45 multi-resolution analysis [10, 11], singularity analysis [12, 13]. 68 46 For fault identification and isolation tasks, some works use 69 47 Electrochemical Impedance Spectra (EIS) as normal or faulty 70 48 operation signatures to supply artificial intelligence algorithms 71 49 (based for instance on fuzzy logic [14] or neural networks [15]) 72 50 or conventional pattern recognition approaches (based on 73

Support Vector Machines (SVM) [16], k-nearest neighbors (knn) [13] methods).

This work aims at studying the portability of an innovative data driven approach dedicated to PEMFC diagnosis, named singularity analysis. This method consists in analyzing the pointwise singularities stamped in the stack voltage signal for various FC operating conditions. The singularity features are then summarized in the form of concave arcs estimated thanks to a set of mathematical equations, baptized multifractal formalism [17-19]. The advanced analysis tool, named Voltage Singularity Spectrum (VSS) is then obtained using a nonintrusive manner and without affecting in any way the FC operation. Indeed, no external additional AC-solicitation has to be superimposed to the existing DC load current as it is the case in the usual EIS operation mode.

This paper is organized as follow. Section 2 deals with the experimental work and environment conducted with two PEMFC stacks. In section 3, a brief mathematical foundation of the singularity measurement is given. In section 4, we show how it is possible to make the singularity spectrum combined with Machine Learning techniques as a PEMFC diagnosis tool. Then, the portability of the proposed tool is discussed. Main conclusions are given in Section 5.

2. Experimental 1

Synopsis of the investigated PEM Fuel Cells 2

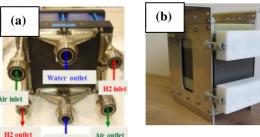
In our study, two PEMFC stacks are experimented to evaluate 31 3 4 the portability of the proposed diagnosis tool. The first one is 5 an 8 cells stack designed for automotive applications and 6 manufactured by CEA (Alternative Energies and Atomic 7 Energy Commission). The second one is a 12 cells stack 8 dedicated to stationary application (micro combined heat and 9 power - µCHP application). It is designed and marketed by 10 Riesaer Brennstoffzellentechnik GmbH and Inhouse Engineering GmbH, Germany. 11

12 The first stack (PEMFC_{Auto}) is made of metallic gas distributor

- 13 plates. The electrode active surface of a cell is equal to 220
- 14 cm^2 . It is fed by air at cathode and pure hydrogen (H₂) at anode. 37
- 15 A summary of the FC nominal operating conditions is given in
- Table 1. The stack operates with a nominal current of 110 A. 33 16 17 A picture of the stack is shown in Fig. 1(a).
- 34 The second stack (PEMFC_{μ CHP}) is fed by air at cathode, and at 3518
- anode by a fuel mixture (75 % of H_2 and 25 % of carbone 36 19 20 dioxide -CO₂) simulating a reformat. It is made of graphite gas distributor plates. The electrode's active surface is 196 cm². 37 21
- 22 The stack operates with a nominal current of 80 A. A picture 38
- of the stack is given in Fig. 1(b). A summary of the FC nominal 39 23

operating parameters and other main characteristics are given 40 24

25 in Table 2



- 26 Fig. 1. Pictures of the two investigated PEMFC stacks:
- 27 a) 8 cell stack designed for automotives (PEMFC_{Auto}),
- 28 b) 12 cell stack designed for μ CHP operation (PEMFC_{μ CHP}).
- 29

30 Table 1. PEMFC_{Auto} nominal operating conditions.

Coolant flow: deionized water	2 l/min
Anode stoichiometry rate (H ₂)	1.5
Cathode stoichiometry rate (air)	2
Absolute pressure for H ₂ and air inlets	150 kPa
Max. anode - cathode pressure gap	30 kPa
Temperature of the cooling circuit	80°C
C	

Anode and cathode relative humidity rate	50 %
Nominal Current	110 A

Table 2. The PEMFC_{μ CHP} nominal operating conditions.

Coolant flow: deionized water	3 l/min
Anode stoichiometry rate (H ₂ & CO ₂ mix)	1.3
Cathode stoichiometry rate (air)	2
Absolute pressure for H ₂ and air inlets	150 kPa
Max. anode - cathode pressure gap	20 kPa
Temperature of the cooling circuit	75°C
Anode and cathode relative humidity rate	50 %
Nominal Current	80 A

Experimental process

The above described PEMFCs were experimented with testbenches developed in the FC platform of Belfort, France. It includes mainly:

- . a complete gas conditioning sub-system including gas humidifiers at anode and cathode,
- a test stand section dedicated to the control of the temperature inside the stack and including the FC primary water circuit.
- an electric / electronic management sub-system, .
- an electronic load.

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45 The monitoring and the control of the FC testbenches 46 parameters are done through National Instruments materials and a dedicated software. A Human-Machine Interface (HMI) was also developed in-lab using Labview $^{\rm TM}$ 48

49 The purpose of the experimental protocol was to introduce 50 different controlled health states into the PEMFC stacks by 51 configuring various operating parameters. Two PEMFC health 52 states were set: no stack failure state (when the FC is operating 53 under normal parameters) and with stack failure state (when 54 the FC is operating under abnormal / severe parameters).

Different scenarios of FC system failure were associated to the changing of different setting physical parameters through the control-command interface of the testbenches, namely: cathode stoichiometry rate (FSC), anode stoichiometry rate (FSA), gas pressure (P), cooling circuit temperature (T) and relative humidity level (RH).

The set of the tests performed, with the two stacks and according to the degrading operating parameters, is reported in Table 3.

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65 Table 3. The set of FC operating conditions applied during the experimentation of the two stacks. The underlying parameter values correspond to the introducing faults. The notation 'ND' means that the FC experiment is not done. 66

Parameters	Ref	DFSC	DFSA	DP	DT	DH	DCO
value							

	Auto	μСНР	Auto	μСНР	Auto	μCHP	Auto	μСНР	Auto	μСНР	Auto	μСНР	Auto	μCHP
FSC	2	2	<u>1.3</u>	<u>2.6</u> <u>1.6</u>	2	2	2	2	2	2	2	2	2	2
FSA	1.5	1.3	1.5	1.3	<u>1.3</u>	$\frac{1.5}{1.2}$	1.5	1.3	1.5	1.3	1.5	1.3	1.5	1.3
P (bar abs)	1.5	0.1	1.5	0.1	1.5	0.1	<u>1.3</u>	ND	1.5	0.1	1.5	0.1	1.5	0.1
T (°C)	80	70	80	70	80	70	80	70	<u>75</u>	<u>72</u> <u>65</u>	80	70	80	70
RH (%)	50	50	50	50	50	50	50	50	50	50	<u>ND</u>	<u>46</u> <u>54</u>	50	50
Presence of CO (ppm)	0	0	0	0	0	0	0	0	0	0	0	0	<u>10</u>	<u>ND</u>

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2 3. Singularity measurement

Multifractals are the distribution of singularities, all lying on
interwoven sets of varying fractal dimensions [20].
Multifractals arise in a variety of physical signals in the forms 29
of self-similar sub-sets of samples, such as Multifractional 30
Brownian Motion (MBM) signal [21], signals in turbulence 31
[22], and temporal series in finance [23].

9 The singularity analysis, also named "multifractal analysis" $\frac{33}{24}$

10 allows the characterization of data by describing globally and 34

11 geometrically the fluctuations of local regularity, usually 35

12 measured by means of the Hölder exponent h. 36

13 It describes the time (t) based fluctuations of the signal given 37

14 by a function X(t). This is achieved by comparing the local 15 variations of X(t) around fixed time position t_0 , against a local ³⁸

16 power law behavior: $X(t_0)$ is said to belong to $C^{\alpha}(t_0)$ with

17 $\alpha \ge 0$ if there are a positive constant C and a polynomial P, 18 satisfying deg(P) < α , such that $|X(t) - P_{t_0}(t)| \le C|t - C|t$

19 $t_0|^{\alpha}$.

20 The Hölder exponent is defined as the largest α such as: 21 $h(t_0) = \sup\{\alpha: X \in C^{\alpha}(t_0)\}.$

22 In practice, when $h(t_0)$ takes a value which tends to zero, the 23 signal exhibits a strong singularity at t_0 (Fig. 2).



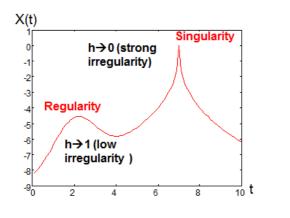


Fig. 2. Illustration of two pointwise regularity measures in the signal X(t) quantified by the Hölder exponent h.

The singularity strength regarding the variability of the regularity of X(t) vs. t is usually described through the socalled singularity spectrum. Building a singularity spectrum consists in associating to each Hölder exponent h the Hausdorff dimension D(h) of the sets of points which exhibit the same value of h:

 $h \mapsto D(h)$

An example of singularity spectrum is given in Fig. 3.

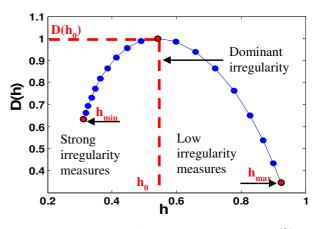


Fig. 3. Example of a singularity spectrum D(h).

41 The numerical implementation of the mathematical formula
42 can be achieved using the wavelet leaders multifractal
43 formalism. Detailed descriptions of the theoretical and
44 practical relevance, and benefits of the use of wavelet leaders
45 for singularity analysis are depicted in [17-19].

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4. Voltage Singularity Spectrum as diagnosis tool ³¹ 1

2 3 In this work, we propose to study the portability of the new 4 diagnosis tool based on the investigation of singularity 5 measurements stamped in FC stack voltage signals. Indeed, measuring local singularities on voltage signals provides 6 7 suitable information about the evolving dynamics of non-8 stationary and non-linear processes involved in FC systems.

9 We assess the generalization and the usefulness of the 10 proposed VSS by establishing the diagnosis on two databases 11 issued from the two investigated PEMFC stacks.

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- For the stack $PEMFC_{Auto}$, 10 scenarios are analyzed (normal 13
- 14 and abnormal conditions including one fault or more complex
- 15 situations with 2 or 3 faults occurred simultaneously).
- For the stack PEMFC_{μ CHP}, 9 operating conditions (normal and 16 33 17 abnormal conditions) are studied.
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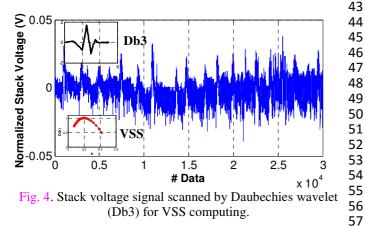
In this aim, we use 30 voltage profiles for each FC operating 3519

20 condition; each voltage profile covers 1000 voltage samples

36 acquired at a frequency $f_a = 11$ Hz (Fig. 4) using the monitoring 21 37

22 data system of the FC experimental test bench. 23

39 24 To perform the VSS, the analyzing wavelet is selected as Daubechies 3 ('Db3') function (with 3 vanishing moments, 41 40 25 26 Fig. 4). 42 27



32 An example of a set of 30 VSS is shown in Fig. 5.

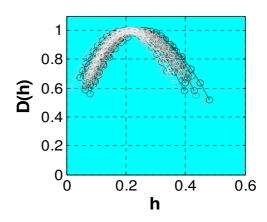


Fig. 5. Typical VSS computed on 30 profiles covering 1000 stack voltage samples.

Singularity features are then used to supply the Machine Learning approach, named k Nearest Neighbors (kNN). To improve the performance of the fault classification method, the Minimum Redundancy - Maximum Relevance (MRMR) technique [24] is used to select some relevance features offering the best classification rates.

Actually, 20 VSS / class are used to generate the learning database and the 10 others serve as test data to evaluate the performances of the classifier. Each VSS contains 38 features (19 h data and 19 D(h) data). So, by applying the MRMR method on the full feature set (38 features) of the VSS, the good classification rate obtained using the top 6 selected features is about 89.4 % for the stack PEMFCAuto, separating 10 classes (10 FC operating conditions).

For the second stack PEMFC_{uCHP}, 9 classes are discriminated with a success of 95.5 %.

The best results of the classification rates of the different operating conditions studied are embedded in confusion matrixes given by Tables 4 and 5, for the stacks PEMFC_{Auto} and PEMFC_{μ CHP} respectively.

Table 4. Confusion matrix of the good classification rates obtained with MRMR and kNN from the VSS computed with the stack voltage signals of the PEMFCAuto. The studied FC operating conditions are: Ref: normal conditions - DFSC: cathode flow fault (slight air starvation) - DFSA: anode flow fault (slight H₂ starvation) - DP: gas pressure fault (lower gas pressure) - DT: cooling

Class	C_0	C1	C_2	C ₃	C_4	C ₅	C ₆	C ₇	C ₈	C ₉
Ref	<u>87.5</u>	0	0	12.5	0	0	0	0	0	0
DFSC	0	<u>100</u>	0	0	0	0	0	0	0	0
DFSA	0	0	<u>100</u>	0	0	0	0	0	0	0
DP	50	0	0	<u>50</u>	0	0	0	0	0	0
DT	0	0	0	0	<u>100</u>	0	0	0	0	0
DCO	0	0	0	0	0	<u>100</u>	0	0	0	0
DFSC & DP	0	0	0	0	0	0	<u>100</u>	0	0	0
DFSA & DP	0	0	0	0	0	0	0	<u>71.43</u>	28.57	0
DFSC & DFSA	0	0	0	0	0	0	0	0	<u>100</u>	0
DFSC & DFSA & DP	0	0	0	0	0	0	0	0	0	<u>100</u>

circuit temperature fault (lower stack temperature) - **DCO**: carbon monoxide poisoning (H₂+CO).

With: $C_0 \equiv \widehat{Ref}$, $C_1 \equiv \widehat{DFSC}$, $C_2 \equiv \widehat{DFSA}$, $C_3 \equiv \widehat{DP}$, $C_4 \equiv \widehat{DT}$, $C_5 \equiv \widehat{DCO}$, $C_6 \equiv DF\widehat{CS \& DP}$,

 $C_7 \equiv DFSA \& DP, C_8 \equiv DFSC \& DFSA, C_9 \equiv DFSC \& DFSA \& DP.$

10 Table 5. Confusion matrix of the good classification rates obtained with MRMR and kNN from the VSS computed with the stack voltage signals of the PEMFC $_{\mu CHP}$. The studied FC operating conditions are: **Ref** : normal conditions - **DFSC**': cathode flow fault 11 (air over-supply) - **DFSC** : cathode flow fault (slight air starvation) - **DFSA** : anode flow fault (H₂ over-supply) - **DFSA** : 12

anode flow fault (H₂ starvation) - **DT**': cooling circuit temperature fault (higher temperature) - **DT**₂ : cooling circuit temperature 13

fault (lower stack temperature) - **DRH**': dew temperature fault (higher dew temperature) - **DRH**.: dew temperature fault (lower 14 dew temperature). 15

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Class	C_0	C_1	C_2	C ₃	C_4	C ₅	C ₆	C ₇	C_8
Ref	<u>100</u>	0	0	0	0	0	0	0	0
DFSC/	0	<u>100</u>	0	0	0	0	0	0	0
DFSC	0	0	<u>100</u>	0	0	0	0	0	0
DFSA'	0	0	0	<u>90</u>	0	10	0	0	0
DFSA	0	0	0	0	<u>90</u>	0	0	0	10
DT'	0	0	0	20	0	<u>80</u>	0	0	0
DT	0	0	0	0	0	0	<u>100</u>	0	0
DRH/	0	0	0	0	0	0	0	<u>100</u>	0
DRH∖	0	0	0	0	0	0	0	0	<u>100</u>
With: $C_0 \equiv \widehat{Ref}$, C_1	$\equiv D\widehat{FSC}^{\prime}, C$	$C_2 \equiv DFS$	\overline{SC} >, $C_3 \equiv$	DFSA',	$C_4 \equiv D\overline{l}$	$\widehat{FSA}_{\lambda}, C_{5}$	$\equiv \widehat{DT'}, C_{e}$	$\overline{DT_{\lambda}},$	$C_7 \equiv \widehat{DRH^{\prime}}$

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 $C_{\mathbf{g}} \equiv \widehat{DRH}_{\lambda}$

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29 As we can see, the proposed diagnosis strategy identifies 30 21 successfully several complex operating faults (i.e. slight 31 22 23 deflections from the nominal operating conditions, and even 32 24 combination of faults) for both PEMFC_{Auto} and PEMFC_{uCHP}. 33

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5. Conclusions 26

27 In this study, VSS are computed on voltage signals acquired

28 under different FC operating conditions (normal and abnormal, i.e. more or less severe, deviations from the normal conditions) with considering situations that combine 2 or 3 faults simultaneously. Two stacks are investigated: a PEMFCAuto stack that is designed for automotive applications and a PEMFC_{μ CHP} stack, dedicated to stationary ones.

34 Singularity features extracted from the estimated VSS are 35 classified using Machine Learning approach, named k-Nearest 36 Neighbors (kNN).

- 1 The obtained classification results show that the proposed 51
- 2 PEMFC diagnosis tool allows identifying simple operating ⁵²
- 3 faults and more complicated situations that contain several $\frac{53}{2}$
- 4 fault types. The diagnosis are realized on two different test $\frac{54}{55}$
- 5 stands, for different stack sizes, powers and technologies, with 56

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- 6 different targeted environments of power application.
- 58 7 In this paper, we demonstrate that the singularity analysis of 59
- 8 voltage signal offers a generic diagnosis tool for the PEMFC 60
- 9 SoH monitoring. One key-point of the method is that the VSS 61
- 10 can be estimated from the "free" evolution of the stack voltage $\frac{62}{63}$
- 11 and without affecting in any way the FC operation: no external $_{64}$
- 12 additional solicitation is required to reveal the SoH patterns.
- 13

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 19 transition.
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