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Imelda Elizabeth Ortiz-Cerda, Phahath Thammavong, Vincent Caqueret, Catherine Porte, Isabelle Mabille, et al.. Synthesis of Prebiotic Caramels Catalyzed by Ion-Exchange Resin Particles: Kinetic Model for the Formation of Di- d -fructose Dianhydrides. Journal of Agricultural and Food Chemistry, 2018, 66 (7), pp.1693-1700. 10.1021/acs.jafc.7b04868 . hal-01757786

HAL Id: hal-01757786 https://hal.science/hal-01757786v1

Submitted on 26 Sep 2024

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AGRICULTURAL AND FOOD CHEMISTRY

Article

Synthesis of prebiotic caramels catalyzed by ion exchange resin particles: kinetic model for the formation of di-D-fructose dianhydrides

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for the formation of di-D-fructose dianhydrides Imelda-Elizabeth Ortiz Cerda ¹ , Phahath Thammavong ¹ , Vincent Caqueret ¹ , Catherine Porte ¹ ,
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Keywords
Prebiotic caramel, difructose dianhydride, kinetic law, fructose, heterogeneous catalysis.

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- 21

22 ABSTRACT

23 Caramel enriched in di-D-fructose dianhydrides (DFAs, a family of prebiotic cyclic 24 fructodisaccharides) is a functional food with beneficial properties for health. The aim of this 25 work was to study the conversion of fructose into DFAs catalyzed by acid ion-exchange resin, 26 in order to establish a simplified mechanism of the caramelization reaction and a kinetic 27 model for DFA formation. Batch reactor experiments were carried out in a 250 mL spherical 28 glass flask and afforded up to 50% DFA yields. The mechanism proposed entails order 2 29 reactions that describe fructose conversion on DFAs or formation of by-products such as 30 HMF or melanoidins. A third order 1 reaction defines DFA transformation into fructosyl-31 DFAs or fructo-oligosaccharides. The influence of fructose concentration, resin loading and 32 temperature was studied to calculate the kinetic parameters necessary to scale up the process. 33

35 **INTRODUCTION**

36 The current increase in the frequency of some chronic diseases such as cardiovascular 37 diseases, obesity, diabetes and certain types of cancer, in particular colon cancer, is linked to 38 environmental issues among which nutrition plays a prominent role. Indeed, nutrition is 39 becoming a major public health issue. The food industry therefore offers innovative solutions 40 to improve the quality of products by adding beneficial health substances such as 41 antioxidants, vitamins and prebiotics. In this context, di-D-fructose dianhydrides (DFAs), a complex family of cyclic fructodisaccharides with prebiotic activity present in caramel^{1,2} 42 43 provide an innovative option. A prebiotic is defined as "a non-digestible food ingredient that 44 beneficially affects the host by selectively stimulating the growth and/or activity of one or a 45 limited number of bacteria in the colon, thus improving the host health". New processes have 46 been proposed to enhance the proportion of DFAs in caramel, among which caramelization of 47 fructose at relatively low temperature (80-100 °C) catalyzed by ion exchange resin particles is particularly attractive in view of industrial development.^{3–5} Fructose is one of the most 48 abundant monosaccharides and is known to be the sweetest natural sugar.⁶ 49

50 Formation of DFAs under caramelization conditions competes with unspecific dehydration 51 reactions of the starting sugar, which is essentially related to the formation of 5-(hydroxymethyl)furfural.⁷⁻¹⁰ The kinetics of DFA formation have been investigated under 52 various conditions. Thus, Chu and Berglund¹¹ determined the rate of DFA formation during 53 fructose crystallization and Idri et al.¹² studied the synthesis of prebiotic DFA-enriched 54 55 caramels assisted by microwave. Caramelization is a complex phenomenon in which many 56 reactions occur, involving several reactional intermediaries (Figure 1). As a result, obtaining 57 an average rate of DFA production is not straightforward. Two approaches have been used to 58 caramelize a sugar: heating at temperatures about the melting point, often in the presence of an homogeneous acid promotor^{11,13} or using a heterogeneous solid catalyst as caramelization 59

60 promotor, which allows lowering the temperature¹⁴. The second approach has proven 61 preferable in order to obtain DFA-enriched caramels for which prebiotic properties have been evidenced in several animal models ¹⁵⁻¹⁹. Although the heterogeneous conditions further 62 63 complicate a kinetics analysis of DFA formation, several studies indicate that homogeneous models generally provide satisfactory results. For instance, Shan et al.²⁰ studied the hydration 64 65 of cyclohexene in the presence of an ion exchange resin and zeolites and found that a model representing a homogeneous system best fitted their experimental data. Other authors^{21,22} 66 67 proposed a pseudo-homogeneous model to describe the esterification and transesterification 68 kinetics catalyzed by an Amberlite® or Lewatit® ion exchange resin. As attested by several studies which compared the reaction kinetics in heterogeneous and homogeneous media^{23,24} 69 70 the reaction kinetics of certain species resulting from a heterogeneous mixture can be modeled 71 by equations generally applied to reactions used in a homogeneous medium. In line with those 72 antecedents, the objectives of the present study are twofold: to propose a simplified 73 mechanism to describe in a general way the production of DFAs, and to calculate the kinetic 74 parameters of the caramelization reaction catalyzed by resin particles in order to obtain kinetic 75 laws, which can be used in the modelling, design and operational conditions of a reactor.

76

77 MATERIALS AND METHODS

78 **Products**

Anhydrous D-fructose (99% purity) was purchased from Danisco Sweeteners (Paris, France).
The ion-exchange resin Lewatit® S2328, designed for food-products, was purchased from
Lanxess (La Wantzenau, France). It is a strongly acidic, macroporous resin exposing sulfonic
acid groups that has proven very efficient to promote caramelization processes. The average
particle size is between 0.4 and 0.5 mm. Phenyl-β-D-glucopyranoside (Internal standard, I.S.),
pyridine, hydroxylamine, hexamethyldisilazane and trimethylchlorosilane were purchased

from Sigma–Aldrich. Di- α -D-fructofuranose 1,2':2,3'-dianhydride (DFA 1), α -Dfructofuranose β -D-fructopyranose 1,2':2,1'-dianhydride (DFA 9) and α -D-fructofuranose β -D-fructofuranose 1,2':2,1'-dianhydride (DFA 10) were synthesized and purified at Instituto de Investigaciones Químicas (CSIC – Universidad de Sevilla) following previously reported procedures ^{25–27}.

90

91 Reaction and experimental setup

The Lewatit® S2328 ion-exchange resin (250 g) was stacked in a glass column and subsequently eluted (3 - 4 mL min⁻¹) with deionized water (1 L), 1 M aqueous HCl (1 L) and deionized water (2 L). Drying was first carried out under air current at room temperature and then in an oven at 90 °C for 16 h.

The resin exchange capacity was studied in the laboratory²⁸ and showed that i) after use for a 96 97 two-hour experiment, the resin was almost completely inactivated, ii) its reactivation is only 98 partial with the method used, and an identical conversion of fructose during the second use is 99 not obtained nor a production of similar DAF, which is reduced by one third. Table 1 shows 100 that the fructose conversion is similar for the second use of the resin but is very weak for the 101 third use (even if resin is regenerated after each new use). Moreover, kinetics of DFAs 102 formation is becoming slower and the yield of these compounds decreases. These various 103 tests have shown that the resin loses its exchange efficiency and is exhausted during the 104 reaction. In order to be able to reuse it, it is necessary to regenerate it by methods other than 105 simple washing followed by an activation acid.

Batch reactor experiments were carried out in a 250 mL spherical glass flask equipped with a coil condenser to prevent any loss of product and heated by a silicon oil bath controlled by a thermal sensor Pt 100 connected to a hotplate. The mixture was mechanically stirred at 150 rpm. The reference conditions were based on the study of Suárez-Pereira et al.¹⁴: fructose mass fraction of 0.9, water mass fraction of 0.1, temperature of 90 °C and resin quantity of 0.18 w/w_{mixture}. The effect of fructose mass fraction (0.9, 0.8, 0.7), temperature (70, 80, 90 °C) and resin fraction (0.09, 0.18, 0.27 w/w_{mixture}) were studied. Kinetic monitoring was performed by collecting aliquots at different times (0, 5, 15, 30, 60, 120 min) in 2 mL Eppendorf tubes. The caramelization reaction was stopped by a thermal shock (T < 50 °C). The caramel samples were stocked in a 0 °C bath before their derivatization and gas chromatography (GC) analysis.

117

118 Analysis

119 GC analyses were carried out using an Agilent 7820A series gas chromatograph equipped 120 with an FID detector (Agilent Technologies). A crosslinked 5% phenyl-dimethylsiloxane 121 column (HP-5; 30 m \times 320 μ m \times 0.25 μ m) was used. Operating conditions were: injection 122 port temperature: 310 °C; splitting ratio 25:1; injection volume 1 µL of derivatized samples; column oven temperature programmed from 180 to 310 °C at 5 °C min⁻¹, with a 25 min hold 123 124 at 310 °C; carrier gas helium (constant flow at 1.2 mL min⁻¹); detector port temperature 310 125 °C. Total acquisition time was 31 min. Caramel samples, as well as the reference samples 126 used for identification, were converted into their corresponding per-O-trimethylsilyl (TMS; 127 non-reducing sugars) or per-O-trimethylsilvlated oxime (TMS-oximes; reducing sugars) derivatives following the method described by Sweeley et al.²⁸ Samples were diluted with 128 129 deionized water (1 mL), the resin (in caramel cases) was separated by centrifugation (6,000 130 rpm, 10 min) and the aqueous solutions were freeze-dried. The dried sugar or caramel was diluted in deionized water to a concentration of 16 mg mL⁻¹. 100 mL of this solution were 131 collected and 100 mL of a solution of phenyl-β-D-glucopyranoside (4 mg mL⁻¹ in acetone-132 133 water, 1:9; v/v) were added. This solution was freeze-dried at -60 °C. The residue was then oximated by treatment with 1 mL of a solution of hydroxylamine in pyridine (20 mg mL⁻¹) at 134

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135 60 °C for 50 min. The cooled sample was then trimethylsilylated by reaction with a mixture 136 of hexamethyldisilazane (200 mL) and trimethylchlorosilane (100 mL) at 60 °C for a further 137 40 min period. Formation of a white precipitate was observed during this operation, which 138 was separated by centrifugation (6,000 rpm, 5 min) before injection in the GC apparatus. It is 139 worth noting that following oximation-trimethylsilylation derivatization, reducing compounds 140 (e.g., residual D-fructose and HMF) provide two peaks in the GC chromatograms, 141 corresponding to the syn- and anti-TMS-oximes, while non-reducing derivatives (e.g., DFAs and the I.S.) provide a single peak.¹⁴ Calibration lines were established from pure fructose and 142 143 DFAs 1, 9 and 10. Injections were repeated three times. Quantification was done by the 144 internal standard method. Response factors (RF) for fructose (RF = 1.26) and four individual 145 DFAs were determined and used for quantification of their relative proportions in caramels. The results compare well with those previously reported by Idri et al.⁴ As the various RF 146 147 values for different DFA samples were very similar, an average RF value of the different 148 isomers was calculated and used for quantitative estimation of the ensemble of DFAs (RF =0.88), following the method developed by Suárez-Pereira et al.¹⁴ 149

Figure 1 presents the chemical structure of DFAs. Numbering follows the order previously used in the literature and is consistent with the elution profile in gas chromatography.¹⁴ Number 8 skipped because it denotes a fructose-glucose mixed dianhydride present only in sucrose caramel, which is not the object of the present study.

To compare the caramel produced under different conditions, the remaining amount of fructose and DFA yield in the sample was normalized. In Figures 3 to 5, mass fructose proportion and DFA proportion of each aliquot were respectively calculate by %Fructose = $m_{Fructose}/m_{Fructose 0}$ and %DFAs = $m_{DFAs}/(m_{Fructose syrup})$.

158

159 **RESULTS AND DISCUSSION**

160 A complete mechanism to describe fructose transformation under caramelization conditions implies about one hundred reactions.²⁹ Considering that under the caramelization conditions 161 162 used in this study DFA formation is strongly favored over unspecific dehydration, a 163 simplified mechanism is proposed to describe the degradation of fructose, leading to DFA 164 products (path A) and by-products such as HMF and melanoidins (path B). In path C, DFAs 165 are consumed to give fructosyl-DFAs or fructo-oligosaccharides through glycosylation 166 (reversion) reactions. The simplified mechanism of the reaction is shown in Figure 2. This 167 simplified mechanism was used to evaluate the kinetic reaction profile and to calculate the 168 kinetic coefficients of fructose consumption and the production of DFAs.

169

170 **Reaction orders**

171 Christian et al.²⁹ studied independently the kinetics of degradation of each DFA formed from 172 inulin. The DFA diastereomers 2, 3, 5, 6, 7, 9, 11, 13 and 14 (group 1) are degraded according 173 to first order kinetics, whereas the other five DFAs (1, 4, 8, 10 and 12) follow a different path 174 imposed by second-order kinetics (group 2). This difference is related to the chemical 175 structure and thermal stability of the compounds.

176 The DFAs present in the synthesized caramels studied here belong mostly to group 1 (about 177 70%). Consequently, a first-order kinetic was considered for the consumption of the set of 178 DFAs (path C). Four different configurations (Configurations I-IV) are proposed here to 179 determine the reaction orders of pathways A and B. In fact, several authors who have studied the degradation of fructose in an acid medium observed first order kinetics for the formation 180 of HMF³⁰ and second order kinetics for the formation of acids.³¹ In the present study, the 181 182 reaction order and kinetic parameters were determined using the Polymath software to solve 183 the system equations 1 and 2, in which α is the partial reaction order of path A and β the 184 partial reaction order of path B. All the configurations were tested for the values of α and β .

185	$v_{Fructose} = -k_a [Fructose]^{\alpha} - k_b [Fructose]^{\beta} $ Equation 1
186	$v_{DFAs} = k_a [Fructose]^{\alpha} - k_c [DFAs] $ Equation 2
187	The configurations were evaluated by imposing values of k_a , k_b and k_c in order to adapt the
188	model to the experimental data of the reference test. The coefficients k_a , k_b and k_c were
189	determined by a two-step iterative method. The first step was to dichotomize the values of the
190	pair (k_a, k_b) to monitor the consumption of fructose. The value of k_c remained constant and
191	was set to 10^{-10} s ⁻¹ such that path C could be neglected in a first instance. In the second step,
192	the glycosylation reaction of DFAs (path C) was considered, changing the value of k_c . The
193	Polymath software represents the results in a graphical form (Figure 3).
194	The mechanism proposed by Configuration I fit the experimental data for the formation and
195	degradation of DFAs. In the case of fructose consumption, however, some divergences
196	between experimental and modeled results were observed. Up to 40 minutes, the model
197	followed the experimental points. However, after 60 min, a discrepancy was observed
198	between the experimental data and the model.
199	Whatever the k_c value, the results of Configuration II were inappropriate because the
200	theoretical amount of DFAs remained close to zero. In this configuration, the pathway B is
201	predominant; consequently the model does not generate enough DFAs to fit the experimental

202 points.

Modeling by III and IV configurations showed that fructose is primarily consumed to form DFAs. The representation of the two configurations is therefore close at this temperature as shown in Figure 3. Under these conditions, in both configurations the mechanism can be limited by the DFA formation (pathway A) and consequently by the DFA consumption (pathway C). The pathway B has a minimal influence on the fructose consumption. At this stage, the reaction order of pathway B cannot be defined. Consequently, these two models were applied to a new test carried out at 80 °C with a fructose ratio of 0.9 and a resin quantity

Equation 4

210 of 0.18 w/w_{mixture} to measure pathway B. Figure 4 shows that the best correlation coefficient

211 was obtained with configuration IV ($R^2 = 0.96$ for DFAs). This configuration proposes a

212 second order fructose consumption kinetics and a second order DFA consumption.

213 The kinetic parameter values for all the configurations are reported in Table 2. Therefore, the

214 kinetic equations are:

215
$$v_{Fructose} = -k_a [Fructose]^2 - k_b [Fructose]^2$$
 Equation 3

216
$$v_{DFAs} = k_a [Fructose]^2 - k_c [DFAs]$$

217 with v in g mL⁻¹ s⁻¹; k_a and k_b in mL g⁻¹ s⁻¹; k_c in s⁻¹ and concentration in g mL⁻¹. Each kinetic

218 coefficient is dependent on temperature and resin concentration.

219 It should be noted that the predominant pathway is pathway A, which corresponds to the

220 formation of DFAs. For the reference experiment, the latter is even the only pathway.

221

222 Effect of operational parameters on fructose consumption and DFA production

The next aim was to study the effects of the operational parameters, including the initial fructose mass fraction, the temperature and the resin catalyst loading, on the caramelization reaction outcome and to obtain the kinetic parameters in order to characterize an optimal process for the synthesis of prebiotic caramels (Figure 5).

227

228 Fructose mass fraction effect

A first set of experiments show the influence of the fructose mass fraction on the rate of fructose consumption and DFA production. At the same temperature (90°C) and for different fructose mass fractions (0.9, 0.8, 0.7), the kinetic coefficients are approximately constant. For k_a , average of (4.5×10⁻⁴; 4.7×10⁻⁴; 4.7×10⁻⁴) = 4.6×10⁻⁴ ± 0.12×10⁻⁵. For k_b , the three values are 1×10⁻⁴. For k_c , average of (0.007; 0.014; 0.017) = 0.013 ± 0.005. The results for k_c have been found to be acceptable. 235 The experiment at 0.7 mass fraction shows that fructose conversion is lower than in the other 236 two cases (67% versus 80%). In addition, this experiment does not show an adequate fit to the 237 model (Figure 5a). Transfer phenomena could be modified with the fructose mass fraction. 238 The viscosity measurements show a significant decline which could explain this change in 239 kinetic behavior (337 mPa s for 0.7 and 3920 mPa s for 0.9 at 70 °C). Figure 5b shows that 240 the optimum DFA production is higher for the 0.9 mass fraction compared to the other 241 proportions (48% for the mass fraction of 0.9, 43% for the mass fraction of 0.8 and 38% for 242 mass fraction of 0.7). A fructose-rich medium promotes the production of DFAs.

243

244 **Temperature effect**

245 An increase in temperature favors the rate of fructose consumption (Figure 5c). Moreover, 246 Table 3 shows that kinetic coefficient decreases when the temperature decreases. At a 247 temperature of 90 °C, fructose consumption is controlled by the pathway that favors the production of DFAs (Table 3). At 70 and 80 °C, the influence of pathway B is no longer 248 249 insignificant, since half of the fructose is consumed by the formation of HMF and 250 melanoidins. The DFA content is therefore much lower. Pathway C is favored with an 251 increasing temperature. DFA formation (Figure 5d) and reaction times are shorter as the 252 temperature increases (maximum DFA production: 32% at 120 min, 44% at 60 min and 48% 253 at 45 min at 70, 80 and 90 °C). In fact, at higher temperatures molecular agitation is promoted 254 and the viscosity of the mixture decreases. These two phenomena allowed a better transfer 255 between the solid phase and the liquid phase.

The rate constants of DFA formation (k_a) , HMF and other products' formation (k_b) and DFA consumption (k_c) , at different temperatures, were applied to the Arrhenius plot. The resulting equations are:

259
$$k_a = k_{a,0} \times \exp(-96381/RT)$$

Equation 5

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260	$k_b = k_{b,0} \times \exp(-29021/RT) $ Equation
261	$k_c = k_{c,0} \times \exp(-340485/RT)$ Equation
262	where R is the ideal gas constant (8.3144598 J mol ⁻¹ K ⁻¹), T is the temperature (K) and $k_{a,c}$
263	$k_{b,0}$ et $k_{c,0}$ are the Arrhenius pre-exponential factors ($k_{a,0} = 3.27 \times 10^{10}$ mL g ⁻¹ s ⁻¹ , $k_{b,0} = 2.11$ mL
264	$g^{-1} s^{-1}$ et $k_{c,0} = 9.69 \times 10^{46} s^{-1}$).
265	An activation energy value of 96 kJ mol ⁻¹ is obtained for the formation of DFA (pathway A)
266	This value was higher to the one given by Chu and Berglund ¹¹ (52 kJ mol ⁻¹). On the other
267	hand, this value is in agreement with those obtained by Pazur ³³ , ranging from 85 to 165 k
268	mol ⁻¹ .
269	For HMF and other products formation (pathway B), the activation energy value is 29 kJ mo
270	¹ and is comparable to those obtained by Zhang et al. ³⁴ (from 15 to 29 kJ mol ⁻¹). However
271	other authors ^{35,36} talk about higher activation energies values between 120 and 150 kJ mol ⁻¹ .
272	Concerning DFA degradation into oligosaccharides (pathway C), an activation energy valu
273	of 340 kJ mol ⁻¹ is obtained but comparison with other authors is difficult due to a lack of
274	publication of this subject.
275	
276	Resin quantity effect
277	The total rate of fructose consumption is decreased by a factor of two when comparing th

results obtained for 0.09 w/w_{mixture} and 0.27 w/w_{mixture} (Figure 5e). These values take into consideration of fructose consumed by the pathway A and consumed by the pathway B. The calculated coefficients $k_a + k_b$ are 6.3 10⁻⁴ mL g⁻¹ s⁻¹ and 3.0 10⁻⁴ mL g⁻¹ s⁻¹ respectively for 0.09 w/w_{mixture} and 0.27 w/w_{mixture} (Table 3). The results of Figure 5f show that the production of DFAs is also variable when the percentage of resin increases. This trend can be attributed to the decrease in pH in the medium, linked to a higher presence of acid catalyst. According to the study by Chu and Berglund ¹¹, an increase in pH decreases DFA production. 285 Nevertheless, DFA decrease can be also explained by a transfer problem. The ion exchange 286 resin effectively reduces the reaction time by progressively releasing the cation for activation 287 of the caramelization as determined by Suarez-Pereira (2010). However, as the percentage of 288 resin increases, viscosity increases causing diffusion problems and consequently decreased 289 reactivity. The medium becomes doughy and more difficult to agitate and homogenize in 290 relation of resin content. A viscosity study was conducted and shows, for example, that in 291 90% fructose syrup at 90°C, the viscosity is equal to 760 mPa s for 0.18 g resin/g mixture and reach to 1030 mPa s for 0.27. Lastly, the high viscosity reduces the production of fructosyl-292 DFAs and fructo-oligosaccharides. The k_c values are 0.015 s⁻¹, 0.007 s⁻¹ and 0.006 s⁻¹ for resin 293 294 proportions of 0.09, 0.18 and 0.27 w/w_{mixture}, respectively.

295

296 CONCLUSION

297 The model proposed to describe fructose consumption is based on a second-order global 298 kinetic model: a pathway for the generation of by-products such as HMF, formic acid, and 299 lactic acid and a pathway for the production of DFAs. The evolution of DFAs is modeled by 300 two successive reactions: DFA production (second order reaction) and DFA consumption 301 (first order reaction). The second reaction was determined from the DFAs generated during 302 kinetics. This model provides a qualitative understanding of the phenomena that occur and a 303 quantitative description of these processes. This set was evaluated by calculating the kinetic 304 coefficients. Although it cannot provide a complete quantitative description, this model gives 305 reliable information on the simplified caramelization process operating under the investigated 306 heterogeneous conditions. In this work, the by-product pathway may be insignificant 307 compared to DFA production. Finally, favorable conditions for obtaining caramel enriched in 308 di-D-fructose dianhydride (about 50%) were identified, namely a high fructose proportion 309 (0.9), high temperature (90 °C) and a resin proportion of 0.18 w/w_{mixture}.

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413 **TABLES**

- 414
- 415 Table 1: Fructose conversion and DFA production for caramels prepared with new resin, resin

416 regenerate one time and resin regenerate two time.

		Fructose conversion ratio (%)	DFA maximum production (%)
		at 120 min	(at different time)
new resin		88	30 (55 min)
resin regenerate time	one	86	20 (120 min)
resin regenerate time	two	39	15 (120 min)

420 Table 2. Kinetic coefficients calculate by Polymath.

tions	Parameters	Configurations			
Condi		$a = 1; \beta = 1$	$\prod_{\alpha=1; \beta=2}^{II}$	$\underset{\alpha = 2; \beta = 1}{\text{III}}$	$IV \\ \alpha = 2; \beta = 2$
0.9 w/w	<i>k</i> _a	3×10 ⁻³ s ⁻¹	3×10 ⁻³ s ⁻¹	$4.5 \times 10^{-4} \text{ mL g}^{-1} \text{ s}^{-1}$	$4.5 \times 10^{-4} \text{ mL g}^{-1} \text{ s}^{-1}$
tose: : 0.18 : 90 °C	k_b	1×10 ⁻⁶ s ⁻¹	$0.4 \times 10^{-3} \text{ mL g}^{-1} \text{ s}^{-1}$	1×10 ⁻¹⁰ s ⁻¹	$1.4 \times 10^{-4} \text{ mL g}^{-1} \text{ s}^{-1}$
fruc resin T	k_c	0.015 s ⁻¹	-	0.012 s ⁻¹	0.007 s ⁻¹
0.9 w/w	<i>k</i> _a	-	-	$3 \times 10^{-4} \mathrm{mL g^{-1} s^{-1}}$	$1.8 \times 10^{-4} \text{ mL g}^{-1} \text{ s}^{-1}$
ttose: (0.18 : 80 °C	k_b	-	-	$7 \times 10^{-10} \text{ s}^{-1}$	$1.1 \times 10^{-4} \text{ mL g}^{-1} \text{ s}^{-1}$
fruc resin T	k _c	-	-	0.009 s ⁻¹	9×10 ⁻⁴ s ⁻¹

421

Conditions			$k_a [\mathrm{mL} \mathrm{g}^{-1} \mathrm{s}^{-1}]$	$k_b [\mathrm{mL g}^{-1} \mathrm{s}^{-1}]$	$k_c [\mathrm{s}^{-1}]$
nass Tect	w/w	0.9	4.5×10 ⁻⁴	1.4×10 ⁻⁴	0.007
tose n tion ef	: 90 °(: 0.18	0.8	4.7×10 ⁻⁴	1×10 ⁻⁴	0.014
fruc frac	T resin	0.7	4.7×10 ⁻⁴	1×10 ⁻⁴	0.017
ure	0.9 w/w	90 °C	4.5×10 ⁻⁴	1.4×10 ⁻⁴	0.007
nperat effect	ctose: I: 0.18	80 °C	1.8×10 ⁻⁴	1.1×10 ⁻⁴	0.0009
ten	fruo resin	70 °C	0.7×10 ⁻⁴	0.8×10 ⁻⁴	0.00001
ntity	0.9 C	0.09 w/w _{mixture}	5×10 ⁻⁴	1.3×10 ⁻⁴	0.015
n quar effect	ctose: 1: 90 °	0.18 w/w _{mixture}	4.5×10 ⁻⁴	1.4×10 ⁻⁴	0.007
resi	fru. T	0.27 w/w _{mixture}	2.3×10 ⁻⁴	0.7×10^{-4}	0.006

423 Table 3. Effect of operational parameters on kinetic coefficients.

424

426 FIGURE GRAPHICS

427



428

Figure 1. Main transformations occurring during the caramelization of D-fructose and chemical structure of the di-D-fructose dianhydrides with indication of the intersaccharide glycosidic bonds, the anomeric configuration (α or β) and the cyclic form of the fructose units (*f*, furanose; *p*, pyranose).



435 Figure 2. Simplified mechanism of fructose transformation.



438

439 Figure 3. Modeling of the reference experiment (fructose mass fraction of 0.9, water mass

440 fraction of 0.1, temperature of 90 °C and resin quantity of 0.18 w/w_{mixture}).





Figure 4. Evolution of the amounts of fructose and DFAs as a function of time (fructose mass
fraction of 0.9, water mass fraction of 0.1, temperature of 80 °C and resin quantity of 0.18

 $446 \qquad \text{w/w}_{mixture}\text{)}.$

447





450 Figure 5. Effect of operational parameters on fructose consumption and DFA production
451 (reference conditions: fructose mass fraction of 0.9, water mass fraction of 0.1, temperature of
452 90 °C and resin quantity of 0.18 w/w_{mixture}).

454 **TOC graphic**



456