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Kinematic Modeling and Twist Feasibility of Mobile Cable-Driven Parallel Robots

Tahir Rasheed¹, Philip Long², David Marquez-Gamez³, and Stéphane Caro⁴

Abstract The kinematic performance of any robotic system can be analyzed from its first order kinematic model. Recently a novel concept of Mobile Cable-Driven Parallel Robots (MCDPRs) has been introduced to achieve an autonomous reconfiguration of Reconfigurable Cable-Driven Parallel Robots (RCDPRs). To analyze the kinematic performance of MCDPRs, this paper presents the first order kinematic model of the latter. Using the proposed kinematic model, the Available Twist Set (ATS) is determined that is required to analyze the twist capacities of MCDPRs. In contrast to ATS of classical CDPRs we show that the ATS of MCDPRs depends, not only on the cables velocities, but on the velocities of Mobile Bases (MBs) as well. As illustrative examples, the twist capacities of two and six Degree of Freedom (DoF) MCDPR is presented.

Key words: Cable-Driven Parallel Robots, Mobile Bases, Kinematic Modeling, Available Twist Set

1 Introduction

A Cable-Driven Parallel Robot (CDPR) is a type of parallel manipulator with limbs as cables, connecting the moving-platform with a fixed base frame. The platform is moved by appropriately controlling the cable lengths or tensions. CDPRs contains

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numerous advantages over conventional robots, *e.g.* high accelerations [6], large payload capabilities [1], and large workspace [7].

However, a major drawback in classical CDPRs having fixed cable layout, *i.e.*, fixed exit points and cable configuration, is the potential collisions between the cables and the surrounding environment which can significantly reduce the robot workspace. Better performances can be achieved with an appropriate CDPR architecture. Cable robots with a possibility of undergoing a change in their geometric structure are known as Reconfigurable Cable-Driven Parallel Robots (RCDPRs). Different strategies have been proposed for maximizing the robot workspace or increasing platform stiffness in the recent work on RCDPRs [3]. However, reconfigurability is typically performed manually for most existing RCDPRs.

To achieve autonomous reconfigurability of RCDPRs, a novel concept of Mobile Cable-Driven Parallel Robots (MCDPRs) was introduced in [10]. The first MCDPR prototype has been designed and built in the context of Echord++ FASTKIT project¹. The targeted application for such MCDPR prototype is logistics.

Some papers deal with the velocity analysis of parallel manipulators [9]. However, few focus on the twist analysis of CDPRs [8]. This paper deals with the kinematic modeling of MCDPRs that is required to analyze the kinematic performance of the robot. The paper is organized as follows. Section 2 presents the kinematic model of MCDPRs. Section 3 deals with the determination of the Available Twist Set (ATS) for MCDPRs using the kinematic modeling of the latter. The ATS can be used to obtain the twist capacities of the moving-platform. Section 4 presents the twist capacities of the moving-platform for the MCDPRs under study. Finally, conclusions are drawn and future work is presented in Section 5.

2 Kinematic modeling

A MCDPR is composed of a classical CDPR with m cables and a n degree-of-freedom (DoF) moving-platform mounted on p Mobile Bases (MBs). The j th mobile base is denoted as \mathcal{M}_j , $j = 1, \dots, p$. The i th cable mounted onto \mathcal{M}_j is named as \mathcal{C}_{ij} , $i = 1, \dots, m_j$, where m_j denotes the number of cables carried by \mathcal{M}_j . \mathbf{u}_{ij} denotes the unit vector along the cable \mathcal{C}_{ij} . Each j th mobile base along with its m_j number of cables is denoted as j th PD (pd_j) module. Each pd_j consists of a proximal ($prox_j$) and a distal ($dist_j$) module. $dist_j$ consists of m_j cables between \mathcal{M}_j and the moving-platform. In this paper, cables are assumed to be straight and massless, thus can be modeled as a Universal-Prismatic-Spherical (UPS) kinematic chain. Generally MBs are four-wheeled planar robots with two-DoF translational motions and one-DoF rotational motion, thus, $prox_j$ can be modeled as a virtual RPP kinematic chain between the base frame \mathcal{F}_0 and the frame \mathcal{F}_{bj} attached to \mathcal{M}_j . An illustrative example with $p = 4$ MBs and $m = 8$ cables is shown in Fig. 1a. A general kinematic architecture of a MCDPR is shown in Fig. 1b.

¹ <https://www.fastkit-project.eu/>

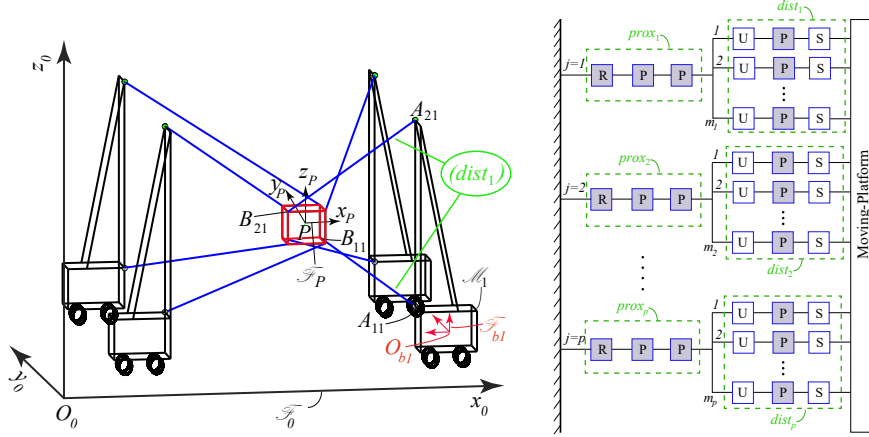


Fig. 1: (a) MCDPR Parameterization (b) Kinematic Architecture of MCDPRs, active joints are highlighted in gray, passive joints are highlighted in white

2.1 Kinematics of the Distal Module

A classical CDPR is referred as distal modules in MCDPR. The twist ${}^0\mathbf{t}_p^{dist}$ of the moving-platform due to the latter is expressed as [4, 11]:

$$\mathbf{A} {}^0\mathbf{t}_p^{dist} = \dot{\mathbf{i}}, \quad (1)$$

where \mathbf{A} is the $(m \times n)$ parallel Jacobian matrix, containing the actuation wrenches due to the cables on the mobile platform. The twist ${}^0\mathbf{t}_p = [\boldsymbol{\omega}, \dot{\mathbf{p}}]^T$ is composed of the platform angular velocity vector $\boldsymbol{\omega} = [\omega_x, \omega_y, \omega_z]^T$ and linear velocity vector $\dot{\mathbf{p}} = [\dot{p}_x, \dot{p}_y, \dot{p}_z]^T$, expressed in \mathcal{F}_0 . ${}^0\mathbf{t}_p^{dist}$ denotes the platform twist due to the distal module motion. $\dot{\mathbf{i}}$ is a m -dimensional cable velocity vector. Here, Eq. (1) can be expressed as:

$$\begin{bmatrix} \mathbf{A}_1 \\ \mathbf{A}_2 \\ \vdots \\ \mathbf{A}_j \\ \vdots \\ \mathbf{A}_p \end{bmatrix} {}^0\mathbf{t}_p^{dist} = \begin{bmatrix} \dot{\mathbf{i}}_1 \\ \dot{\mathbf{i}}_2 \\ \vdots \\ \dot{\mathbf{i}}_j \\ \vdots \\ \dot{\mathbf{i}}_p \end{bmatrix}, \quad (2)$$

where $\dot{\mathbf{i}}_j = [\dot{l}_{1j}, \dot{l}_{2j}, \dots, \dot{l}_{m_jj}]^T$. \mathbf{A}_j is expressed as:

$$\mathbf{A}_j = \begin{bmatrix} [({}^0\mathbf{b}_{1j} - {}^0\mathbf{p}) \times \mathbf{u}_{1j}]^T & \mathbf{u}_{1j}^T \\ [({}^0\mathbf{b}_{2j} - {}^0\mathbf{p}) \times \mathbf{u}_{2j}]^T & \mathbf{u}_{2j}^T \\ \vdots & \vdots \\ [({}^0\mathbf{b}_{m_{jj}} - {}^0\mathbf{p}) \times \mathbf{u}_{m_{jj}}]^T & \mathbf{u}_{m_{jj}}^T \end{bmatrix}, \quad (3)$$

where i th row of \mathbf{A}_j is associated with the actuation wrench of the i th cable mounted onto \mathcal{M}_j . ${}^0\mathbf{b}_{ij}$ denotes the Cartesian coordinate vector of the anchor points B_{ij} in \mathcal{F}_0 . ${}^0\mathbf{p}$ denotes the platform position in \mathcal{F}_0 .

2.2 Kinematic modeling of a MCDPR

The twist ${}^0\mathbf{t}_p^j$ of the moving-platform due to pd_j can be expressed in \mathcal{F}_0 as:

$${}^0\mathbf{t}_p^j = {}^0\mathbf{t}_p^{prox_j} + {}^0\mathbf{t}_p^{dist_j} \quad (4)$$

where ${}^0\mathbf{t}_p^{prox_j}$ (${}^0\mathbf{t}_p^{dist_j}$, resp.) is the twist of the moving-platform due to the motion of the proximal (distal, resp.) module of pd_j expressed in \mathcal{F}_0 . Equation (4) take the form:

$${}^0\mathbf{t}_p^j = {}^{bj}\mathbf{A}_{dp} {}^0\mathbf{t}_{bj}^{prox_j} + {}^0\overline{\mathbf{R}}_{bj} {}^{bj}\mathbf{t}_p^{dist_j} \quad (5)$$

where ${}^{bj}\mathbf{A}_{dp}$ is called the adjoint matrix, which represents the transformation matrix between twists expressed in \mathcal{F}_{bj} and twist expressed in \mathcal{F}_p ,

$${}^{bj}\mathbf{A}_{dp} = \begin{bmatrix} \mathbf{I}_3 & 0_3 \\ -{}^{bj}\hat{\mathbf{r}}_p & \mathbf{I}_3 \end{bmatrix} \quad (6)$$

where ${}^{bj}\hat{\mathbf{r}}_p$ is the cross-product matrix of vector $\overrightarrow{{}^0\mathbf{p}_{bj}}$ expressed in \mathcal{F}_0 . ${}^{bj}\mathbf{t}_p^{dist_j}$ is the moving-platform twist due to $dist_j$ expressed in \mathcal{F}_{bj} . The augmented rotation matrix (${}^0\overline{\mathbf{R}}_{bj}$) is used to express ${}^{bj}\mathbf{t}_p^{dist_j}$ in \mathcal{F}_0 :

$${}^0\overline{\mathbf{R}}_{bj} = \begin{bmatrix} {}^0\mathbf{R}_{bj} & 0_3 \\ 0_3 & {}^0\mathbf{R}_{bj} \end{bmatrix} \quad (7)$$

where ${}^0\mathbf{R}_{bj}$ is the rotation matrix between frames \mathcal{F}_{bj} and \mathcal{F}_0 . As the Proximal module is being modeled as a virtual RPP limb, ${}^0\mathbf{t}_{bj}^{prox_j}$ from Eq. (4) can be expressed as:

$${}^0\mathbf{t}_{bj}^{prox_j} = \mathbf{J}_{bj} \dot{\mathbf{q}}_{bj} \quad (8)$$

where \mathbf{J}_{bj} is a (6×3) serial Jacobian matrix of $prox_j$ and $\dot{\mathbf{q}}_{bj}$ is the virtual joint velocities of the latter, namely,

$${}^0\mathbf{t}_{bj}^{proxj} = \begin{bmatrix} \mathbf{k}_0 & \mathbf{0}_3 & \mathbf{0}_3 \\ \mathbf{k}_0 \times {}^0\mathbf{p} & {}^0\mathbf{R}_{bj}\mathbf{i}_0 & {}^0\mathbf{R}_{bj}\mathbf{j}_0 \end{bmatrix} \begin{bmatrix} \dot{\theta}_j \\ \dot{\rho}_{1j} \\ \dot{\rho}_{2j} \end{bmatrix} \quad (9)$$

where \mathbf{i}_0 , \mathbf{j}_0 and \mathbf{k}_0 denotes the unit vector along x_0 , y_0 and z_0 respectively. Upon multiplication of Eq. (5) with \mathbf{A}_j :

$$\mathbf{A}_j {}^0\mathbf{t}_p^j = \mathbf{A}_j {}^{bj}\mathbf{A}_{dP} \mathbf{J}_{bj} \dot{\mathbf{q}}_{bj} + \mathbf{A}_j {}^0\overline{\mathbf{R}}_{bj} {}^{bj}\mathbf{t}_p^{distj}. \quad (10)$$

As $\mathbf{A}_j {}^0\overline{\mathbf{R}}_{bj} {}^{bj}\mathbf{t}_p^{distj}$ represents the cable velocities of the $distj$ (see Eq. (2)), Eq. (10) can also be expressed as:

$$\mathbf{A}_j {}^0\mathbf{t}_p^j = \mathbf{A}_j {}^{bj}\mathbf{A}_{dP} \mathbf{J}_{bj} \dot{\mathbf{q}}_{bj} + \dot{\mathbf{i}}_j. \quad (11)$$

The twist of the moving-platform \mathbf{t}_p and the twists generated by the limbs are the same, namely,

$${}^0\mathbf{t}_p^1 = {}^0\mathbf{t}_p^2 = {}^0\mathbf{t}_p^3 \dots = {}^0\mathbf{t}_p^j \dots = {}^0\mathbf{t}_p^p = \mathbf{t}_p \quad (12)$$

Thus, the twist of the moving-platform in terms of all the p number of limbs can be expressed as:

$$\begin{bmatrix} \mathbf{A}_1 \\ \mathbf{A}_2 \\ \vdots \\ \mathbf{A}_p \end{bmatrix} \mathbf{t}_p = \begin{bmatrix} \mathbf{A}_1 {}^{b1}\mathbf{A}_{dP} \mathbf{J}_{b1} & \mathbf{0} & \mathbf{0} \dots & \mathbf{0} \\ \mathbf{0} & \mathbf{A}_2 {}^{b2}\mathbf{A}_{dP} \mathbf{J}_{b2} & \mathbf{0} \dots & \mathbf{0} \\ \vdots & \vdots & \vdots & \vdots \\ \mathbf{0} & \mathbf{0} & \mathbf{0} \dots & \mathbf{A}_p {}^{bp}\mathbf{A}_{dP} \mathbf{J}_{bp} \end{bmatrix} \dot{\mathbf{q}}_b + \dot{\mathbf{i}} \quad (13)$$

where $\dot{\mathbf{q}}_b = [\dot{\mathbf{q}}_{b1}, \dot{\mathbf{q}}_{b2}, \dots, \dot{\mathbf{q}}_{bp}]^T$ and $\dot{\mathbf{i}} = [\dot{\mathbf{i}}_1, \dot{\mathbf{i}}_2, \dots, \dot{\mathbf{i}}_p]^T$. Equation (13) can be expressed in the matrix form as:

$$\mathbf{A}\mathbf{t}_p = \mathbf{B}\dot{\mathbf{q}}_b + \dot{\mathbf{i}} \quad (14)$$

$$\mathbf{A}\mathbf{t}_p = \mathbf{B}\dot{\mathbf{q}} \quad (15)$$

where $\mathbf{B} = [\mathbf{B}_b \quad \mathbf{I}_m]$ is a $(m \times (3p + m))$ -matrix while $\dot{\mathbf{q}} = [\dot{\mathbf{q}}_b \quad \dot{\mathbf{i}}]^T$ is a $(3p + m)$ -dimensional vector containing all joint velocities. Equation (15) represents the first order kinematic model of MCDPRs.

3 Available Twist Set of MCDPRs

This section aims at determining the set of available twists for MCDPRs that can be generated by the platform. For a classical CDPR, the set of twist feasible poses of its moving platform are known as Available Twist Set (ATS). A CDPR posture is called twist-feasible if all the twists within a given set, can be produced at the platform, within given joint velocity limits [8].

According to [8], ATS of a CDPR corresponds to a convex polytope that can be represented as the intersection of the half-spaces bounded by its hyperplanes known as *Hyperplane-Shifting Method* (HSM) [2, 5]. Although HSM can be utilized to determine the ATS of MCDPRs, the approach in [8] is not directly applicable due to the difference in the kinematic models of CDPR (Eq. 1) and MCDPR (Eq. 15) as matrix $\mathbf{B} \neq \mathbf{I}$.

The kinematic model of the MCDPRs is used to determine the ATS of the moving-platform. In case $m = n$, \mathbf{A} is square, Eq. (15) can be expressed as:

$$\mathbf{t}_p = \mathbf{A}^{-1}\mathbf{B} \dot{\mathbf{q}} \implies \mathbf{t}_p = \mathbf{J} \dot{\mathbf{q}} \quad (16)$$

where \mathbf{J} is a Jacobian matrix mapping the joint velocities onto the platform twist. The ATS will correspond to a single convex polytope, constructed under the mapping of Jacobian \mathbf{J} .

In case $m \neq n$, matrix \mathbf{A} is not square, however there exist in total C_m^n ($n \times n$) square sub-matrices of matrix \mathbf{A} , denoted by \mathbf{A}^k , $k = 1, \dots, C_m^n$, obtained by removing $m - n$ rows from \mathbf{A} . For each sub-matrix we can write:

$$\hat{\mathbf{t}}_p^k = \mathbf{A}^{k-1}\mathbf{B}^k \implies \hat{\mathbf{t}}_p^k = \mathbf{J}^k \dot{\mathbf{q}}, \quad k = \{1, \dots, C_m^n\} \quad (17)$$

where $\hat{\mathbf{t}}_p^k$ is the twist generated by the k th sub-matrix \mathbf{A}^k out of C_m^n ($n \times n$) square sub-matrices of matrix \mathbf{A} . \mathbf{B}^k is a sub matrix of \mathbf{B} using corresponding rows that are chosen in \mathbf{A}^k from \mathbf{A} . HSM in [2, 5] is directly applicable to compute all the hyperplanes for C_m^n convex polytopes knowing the minimum and maximum joint velocity limits. Thus, the ATS of MCDPRs is the region bounded by all of the foregoing hyperplanes.

4 Results

This section deals with the twist feasibility analysis of two different case studies. From the ATS acquired using the kinematic model of a given MCDPR configuration, we aim to study the difference in the moving platform twist considering fixed and moving MBs.

4.1 Case study: $p = 2$, $m = 4$ and $n = 2$ DoF MCDPR

The first case study is a planar MCDPR with a point mass end-effector shown in Fig. 2a. The MBs have only one degree of freedom along \mathbf{i}_0 . The joint velocity limits are defined as:

$$-0.8 \text{ m.s}^{-1} \leq \dot{\rho}_{1j} \leq 0.8 \text{ m.s}^{-1}, -2 \text{ m.s}^{-1} \leq \dot{l}_{ij} \leq 2 \text{ m.s}^{-1}, i = \{1, 2\}, j = \{1, 2\}, \quad (18)$$

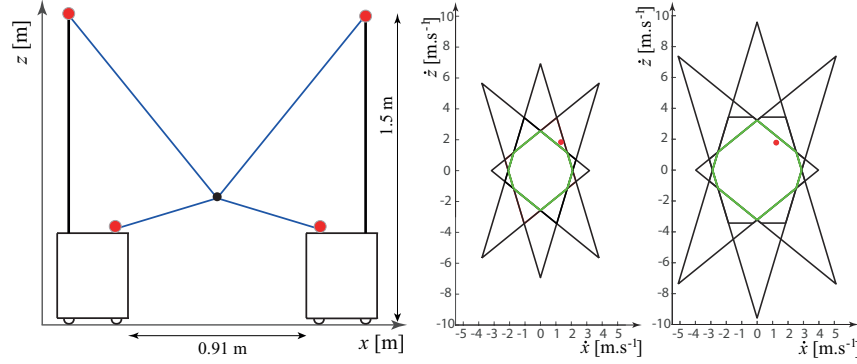


Fig. 2: (a) Configuration under study of $p = 2$, $m = 4$ and $n = 2$ MCDPR (b) ATS in green for fixed MBs (c) ATS in green for moving MBs

Matrix \mathbf{A} has six 2×2 sub-matrices. Thus, ATS is the region bounded by the hyperplanes formed by these six convex polytopes. The difference of ATS between fixed (correspond to a classical CDPR) and moving MBs can be observed in Figs. 2b and 2c. To illustrate the difference, a Required Twist Set (RTS) equal to $[1.15 \text{ m.s}^{-1}, 1.675 \text{ m.s}^{-1}]^T$ is considered, depicted by a red point in Figs. 2b and 2c. For fixed MBs, it should be noted that RTS is outside the ATS. By considering moving MBs, RTS is within the ATS.

4.2 Case study: $p = 2$, $m = 8$ and $n = 6$ DoF MCDPR

The same approach is adopted to determine the ATS for a given FASTKIT configuration in Fig. 3a. The joint velocity limits are defined as:

$$-0.2 \text{ m.s}^{-1} \leq \dot{\theta}_j, \dot{\rho}_{1j}, \dot{\rho}_{2j} \leq 0.2 \text{ m.s}^{-1}, \quad j = \{1, 2\}, \quad (19)$$

$$-2 \text{ m.s}^{-1} \leq \dot{l}_{ij} \leq 2 \text{ m.s}^{-1}, \quad j = \{1, 2\}, i = \{1, \dots, 4\}, \quad (20)$$

The maximum absolute twist that the platform can achieve in each Cartesian direction by considering fixed and moving MBs are illustrated in Figs. 3b and 3c. The maximum absolute wrench of the moving platform is illustrated in red where f_x, f_y, f_z and m_x, m_y, m_z represent the forces and the moments that can be generated by the cables onto the moving platform. For the analysis, the cable tensions are bounded between 0 and 20 N respectively. It can be observed the twist capacity of the moving-platform is increased when MBs are moving. On the contrary, high velocity capability of the moving-platform in certain directions also results in very less wrench capability in the respective directions. Thus, this velocity is unattainable outside certain dynamic conditions.

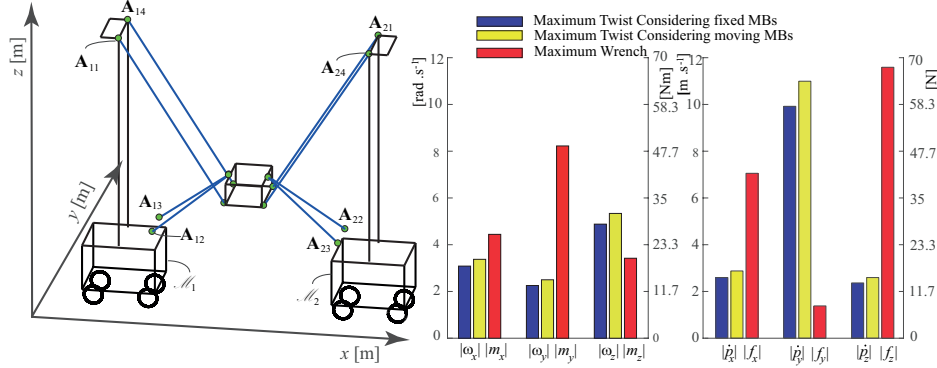


Fig. 3: (a) A FASTKIT configuration (b, c) Maximum absolute twist and wrenches that FASTKIT platform can generate about each Cartesian direction

5 Conclusion

This paper dealt with the kinematic modeling of Mobile Cable-Driven Parallel Robots (MCDPRs) that can be used to analyze its kinematic performance. The developed kinematic model was utilized to determine the Available Twist Set (ATS) of MCDPRs. It considers the joint velocity limits for cables and the Mobile Bases (MBs). Using ATS, the twist capacities of the moving-platform was determined. Two case studies have been used in order to illustrate the effect of the moving MBs onto the platform twist. Future work will focus the trajectory planning of of MCDPRs and experimental validations with FASTKIT prototype.

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