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A General Approach Based on Sampled-Current Voltammetry for Minimizing Electrode Fouling in Electroanalytical Detection

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Electrochemical analysis of species known to passivate electrode surfaces remains challenging. We previously proposed a new method dealing with sampled-current voltammetry performed on an electrode array to mimic polarography at a dropping mercury electrode for the detection of copper. In this work, we study the effectiveness of this method to circumvent electrode fouling with the analysis of phenol solutions at high concentrations (10^{-2} mol L⁻¹), known to polymerize on electrode surface during its oxidation. Electrode arrays well-adapted to the analysis with such system are prepared by photolithography and characterized by X-Ray photoelectron spectroscopy, X-ray diffraction and voltammetry. While analyses performed in conventional linear voltammetry or sampled-current voltammetry on a single electrode are considerably affected by electrode fouling, a linear calibration plot was achievable using our method. Modelling of the electrochemical signal showed that the current depends only on the applied potential and a parameter characteristic of the passivation phenomenon. It also underlined that sampled-current voltammetry on electrode array can circumvent the problem of passivation by a judicious choice of the sampling time.

Keywords: electroanalysis; electrode fouling; modelling; passivation; phenol

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1. Introduction

Electrochemical detection systems have been widely used for health, safety, and environmental assessments due to their unique characteristics, such as short analysis time, low-cost instruments, high sensitivity and compatibility with miniaturization and portability.^[1-3] However, the performance of solid electrodes may be drastically altered by fouling of their surface during the analysis, decreasing the electron transfer rate and so the electrochemical signal. Various processes could be responsible for this passivation phenomenon such as simple adsorption of species on the electrode surface, often occurring with biological macromolecules,^[4-5] and electrochemical reactions during the detection, leading to oligomerisation or larger polymeric structures^[6-10] or covalent bonding with the surface by radicals formed *in situ*.^[11-12] It is well known that these adsorption processes particularly affect biosensors but also the electrochemical analysis of many species that are particularly challenging to detect, such as the large family of phenolic compounds (bisphenol A, chloro phenols, serotonin, phenolic estrogenic compounds), dopamine, thiourea, ascorbic acid, NADH.

Several antifouling strategies have been proposed to decrease the effects of passivation. Some of them rely on the electrode material and its coating. Carbon-based electrodes^[13] with carbon nanotubes (CNTs),^[14-18] graphene or diamond such as boron-doped diamond electrodes^[19-25] and carbon black diamond composite electrodes^[26] have been widely used to minimize fouling. Their antifouling properties have been ascribed to different factors as their hydrophobic character.^[4] For example, a decrease of passivation reported with CNTs has been linked to the high density of edge plane sites on CNTs.^[27] Since the adsorption mainly occurs on edge plane sites, their high amount helps to delay electrode fouling. Nanographite impurities contained within CNTs have also been held responsible for the antifouling properties of CNTs.^[15] The adsorption could also be reduced by modifying the hydrophobic/hydrophilic character of the electrode surface, preventing the approach of species responsible for the passivation of the electrode. This has been achieved by electrode coating with, for example, conducting polymers^[28-32] and membranes^[33-36] or plasma treatments on the electrode surface.^[37-38] However, since these methods only delay the passivation process, it remains difficult to use the sensor in high concentrations of species known to foul the electrode or when fouling is fast and effective.

Minimizing electrode fouling during analyses on conventional electrodes using different procedures has also been reported. For example, adsorbed material has been removed by acid washing,^[39] photocatalysis^[40] and oxidation or reduction processes, such as the use of single anodic and/or cathodic potentials or a train of pulses to periodically clean the electrode surface.^[7, 19, 39, 41-42] However, since modified electrodes are often used to improve the performances of the electrochemical sensors taking advantage of a selective preconcentration of the analyte^[43-46] or of catalytic oxidation/reduction processes,^[47-48] these methods are inappropriate since they would inevitably damage the sensors surface.

We have previously developed a procedure based on sampled-current voltammetry performed on an electrode array prepared by techniques of printed circuit boards for the detection of copper in aqueous solutions.^[49] During the analysis, a single electrochemical measurement is performed independently and differently on each electrode of the array to draw a current-potential curve. The device is equivalent to a dropping Hg electrode where the electrode surface is periodically renewed and a fresh solution is available in the proximity of the electrode between each measurement. By this way, the current-potential curve presents a sigmoid shape like in polarography performed on a dropping mercury electrode. Furthermore, since the data acquisition, that does not require the use of a potential ramp, is simplified, the device can be easily portable.^[49]

In this work, we have evaluated the application of this method to minimize electrode fouling. Since the renewal of the electrode surface is assured during the analysis, passivation phenomenon due to electrochemical reactions during the detection can be circumvented. We used sampled-current voltammetry on an electrode array made by conventional photolithography methods to overcome the problem of passivation. As a challenging test system, we have considered the analysis of phenol that is well-known to form oligomers adsorbed on the electrode surface upon its electrochemical oxidation.^[6, 50] Results are supported by a theoretical approach that highlights the role of the main parameters involved in the analytical method.

2. Results and discussion

2.1 Characterization of the electrode array

The surface of gold electrodes was analyzed by X-ray photoelectron spectroscopy (Figure S1), revealing the photoelectron peaks characteristic of gold. It is worth noting that silicon was not present, underlining the effectiveness of the Si_3N_4 etching process.

The crystallinity and preferred orientation (texture) of the deposited polycrystalline gold films were studied by X-ray diffraction (Figure S2). The analyses revealed four peaks corresponding to (111), (200), (311) and (222) orientations in the polycrystalline film of gold. The existence of a preferred grain orientation was analyzed using the intensities of the peaks. A (111) preferred orientation (92.3%) was clearly highlighted from these analyses with only 5.6% of (222), 0.9% of (311) and 1.2% of (200).

To assure the reproducibility of the sensor fabrication, the electrochemical response of the gold electrodes of the array was first examined in a blank solution containing only the supporting electrolyte (0.5 mol L^{-1} phosphate buffer, $\text{pH}=7.2$). A cyclic voltammogram typical of gold, displayed in Figure 1a, was obtained with peaks corresponding to the formation of gold oxides as the potential was scanned from -1.0 to 1.5 V, and reduction of these oxides in the reverse scan.

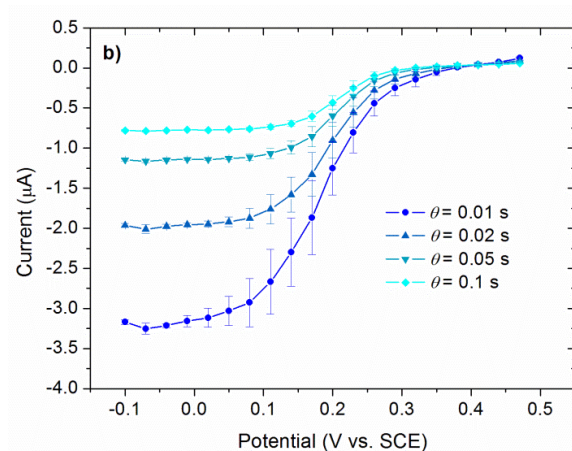
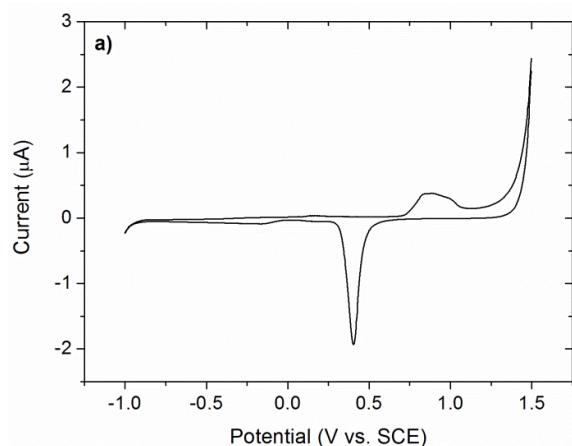


Figure 1. a) Typical cyclic voltammogram obtained on a gold electrode (0.002 cm^2) of the array in 0.5 mol L^{-1} phosphate buffer, $\text{pH}=7.2$ after stabilization of the signal. Scan rate 0.1 V s^{-1} b) Current-potential curves corresponding to the reduction of a $10^{-3} \text{ mol L}^{-1}$ solution of potassium ferricyanide in 0.5 mol L^{-1} phosphate buffer, $\text{pH}=7.2$ by EASCV for different sampling times θ . The potential was incremented by 0.02 V : $E_{n+1} = E_n + 0.0175 \text{ V}$. Error bars are based on measurements performed on 5 different electrode arrays (0.002 cm^2).

Then, to check the reproducibility of the electrochemical response obtained by sampled-current voltammetry on electrode array (EASCV, see Experimental Section), the reduction of potassium ferricyanide was examined on 5 different electrode arrays. The resulting current-potential curves for different sampling times are displayed in Figure 1b. Error bars increase for potentials close to the inflection point but are lower when the plateau current is reached, even for short sampling times. As the limiting current (I_l) is often used as a calibration parameter, its value was obtained based on a sigmoid fit (Table S1) and the variation of the electrochemical signal is estimated from the standard deviation of 5 independent measures. A variation ranging from 1.1 to 2.7% was calculated for the studied sampling times. These results underline the good performance of the electrode arrays prepared by photolithography for EASCV measurements.

2.2 Electrochemical analysis of phenol

Phenolic derivatives are electroactive and can be oxidized within the potential window of water, which makes electroanalysis a method of choice for their detection. Unfortunately, the oxidation of phenolic compounds leads to intermediate radicals that combine themselves and form dimeric products, which are readily oxidized giving rise to the formation of insulating oligomers and polymer chains.^[6, 50] It results that the formed oligomers and polymers rapidly passivate the electrode surface. This phenomenon is very efficient, as exemplified in Figure S5 with an electrochemical signal corresponding to phenol oxidation. One could notice the symmetric shape of electrochemical current and that the response is already lost in the second scan. The fast decrease of the current after reaching its maximum value strongly suggests that the peak current in the first scan was already affected by the passivation phenomenon. Indeed, the symmetric peak shape differs from those expected for a diffusion controlled process and is typical for an electrode process in which product adsorption occurs after the initial electron transfer reaction.^[51] The electrochemical behavior of phenol significantly complicates its analysis, making it a particularly interesting compound to evaluate the interest of EASCV as a

method to overcome the problem of electrode passivation. For comparison with EASCV, phenol oxidation was studied in sampled-current voltammetry performed on a same single electrode of the array (Figure S6a).

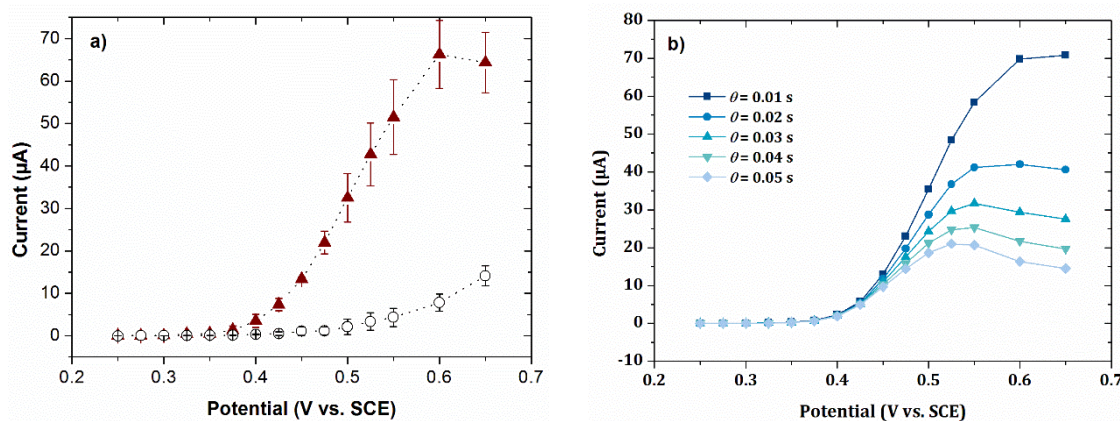


Figure 2. Current-potential curves (---▲---) of a solution of 10^{-2} mol L $^{-1}$ phenol in 0.1 mol L $^{-1}$ NaOH obtained by sampled-current voltammetry on the electrode array (EASCV) a) with a sampling time of 0.01 s and b) with sampling times ranging from 0.01 to 0.05 s. Blank (---○---) was performed in the same conditions in a 0.1 mol L $^{-1}$ NaOH aqueous solution. Error bars are based on three reproducibility measurements. Electrode surface area: 0.002 cm 2

To obtain the current-potential curve, chronoamperometry measurements were recorded at increasing potentials for 0.1 s and the values of current were read at 0.01 s. A symmetric peak shape is obtained indicating a gradual but incomplete covering of the electrode surface during the analysis since a same single electrode was used without cleaning of its surface. When the same experiment was performed with the stirring of the solution (Figure S6b), an increase of the electrochemical signal is observed since the stirring increases the transport of phenol to the electrode surface. Nevertheless the curve still displays a peak shape indicating the occurrence of the passivation process.

Finally, the same experiment performed on the electrode array (EASCV) led to a sigmoid current-potential curve (Figure 2a) recorded with a sampling time of 0.01 s. When increasing the sampling time (Figure 2b), the expected sigmoid curve tends to the peak shape curve as observed before indicating that the passivation process could be avoided by using EASCV at short sampling time. It is interesting to note that the passivation phenomenon did not lead to a simple decrease of the limiting current value corresponding to the plateau but changed the curve shape. In view of these results, a short sampling time (0.02 s) compatible with the response time of our potentiostat was chosen to construct the calibration plot. Shorter sampling times such as 0.01 s could obviously been chosen depending on the available potentiostat. Interestingly, the

electrochemical signal is significantly higher with this method than with sampled-current voltammetry carried out on a single electrode, underlining all the interest of the method that allows the renewal of the solution as well as the electrode surface during the analysis. Indeed, each electrode of the array is sufficiently far away from the others to ensure that the solution at the vicinity of their surface would not be affected by electrochemical oxidations performed on the other electrodes.

2.3 Calibration plot at relatively high concentration of phenols

The dependence of the current on the concentration in phenol was deliberately studied at relatively high concentrations of phenol (10^{-3} - 10^{-2} mol L⁻¹) to clearly observe the impact of the passivation phenomenon on the electrochemical response. A first study was performed by linear voltammetry on an electrode of the array, considering the current peak. The electrode was not cleaned between each analysis going from the lowest concentration in phenol to the highest one. The dependence of the current on the concentration of the analyzed solution is given in Figure 3a.

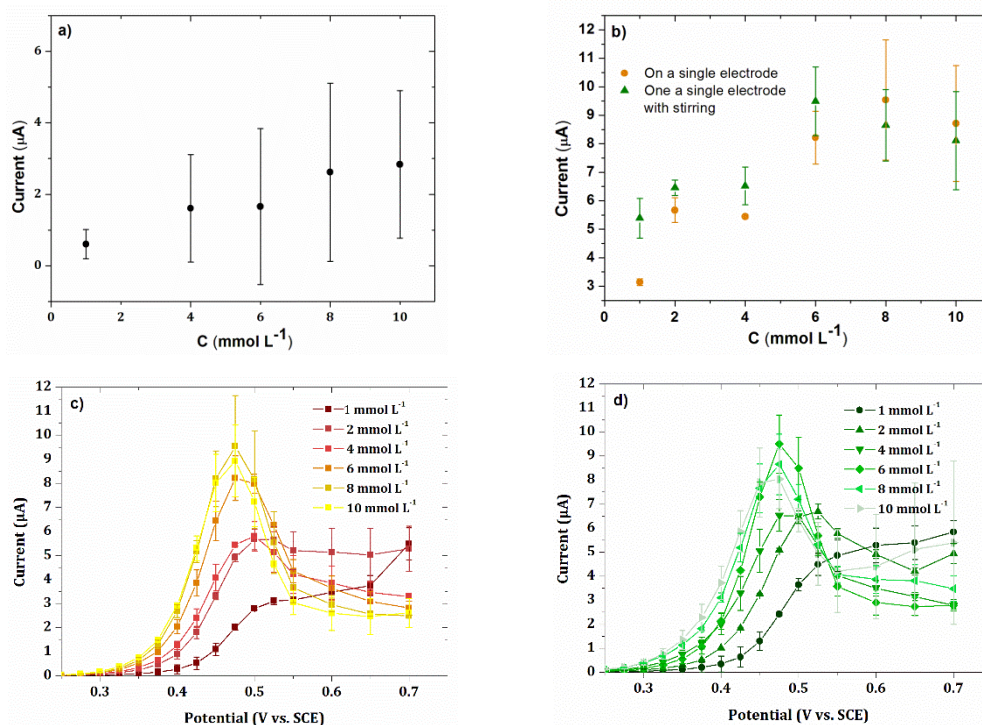


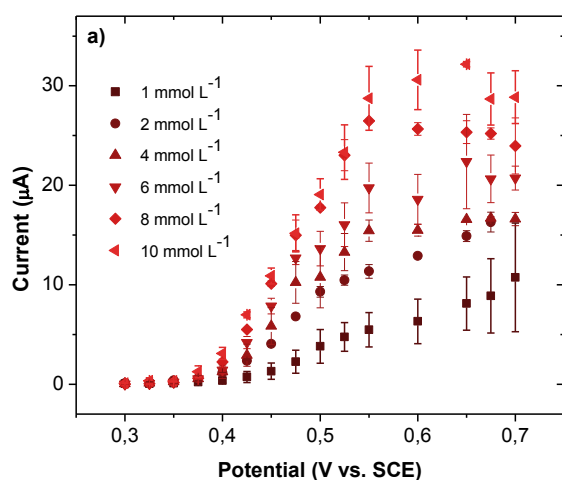
Figure 3. Calibration plot of current determined by a) linear voltammetry (0.1 V s^{-1}) and b) sampled-current voltammetry on a single electrode of the array with (\blacktriangle) and without (\bullet) stirring of the solution as a function of phenol concentration ranging from 10^{-3} - 10^{-2} mmol L⁻¹ in a 0.1 mol L^{-1} NaOH aqueous solution. Corresponding current-potential curves obtained by sampled-current voltammetry on a single electrode of the array c) without and d) with stirring

of the solution. Sampling time: 0.02 s. Error bars are based on measurements performed on two or three different arrays. Electrode surface area: 0.002 cm^2

The obtained variation is clearly nonlinear with high error bars. Indeed, the thickness of the peak corresponding to the oxidation of phenol differs from one analysis to another, owing to the complicated oxidation process of phenol. This behavior strongly affects the peak current.

For comparison with EASCV, similar experiments were carried out by sampled-current voltammetry on a single electrode with and without stirring of the solution (Figure 3b). The curves were also nonlinear with the loss of linearity for phenol concentrations between 2 and $4 \times 10^{-3} \text{ mmol L}^{-1}$, due to a competition between electrode fouling and the oxidation of phenol on free electrode surface. A decrease of the current is also observed for concentrations higher than $6 \times 10^{-3} \text{ mol L}^{-1}$, showing a considerable influence of the passivation phenomenon on the measurement. Stirring of the solution at the vicinity of the electrode led to a similar behavior, whereas higher currents are obtained until $6 \times 10^{-3} \text{ mol L}^{-1}$ due to the increase of the transport of phenol to the electrode surface. The current-potential curve shapes depicted in Figure 3c and 3d are clearly dependent on the concentration of phenol. Whereas a plateau is obtained at $10^{-3} \text{ mol L}^{-1}$, higher concentrations of phenol led to the formation of a peak with decreasing width. This phenomenon is due to electrode fouling that already affects the electrochemical signal at a concentration of $2 \times 10^{-3} \text{ mol L}^{-1}$ in phenol. The current measured at the plateau or at the peak to construct a calibration plot is clearly affected by electrode fouling.

Figure 4a shows the current-potential curves obtained by sampled-current voltammetry on an electrode array (EASCV) for different concentrations of phenol.



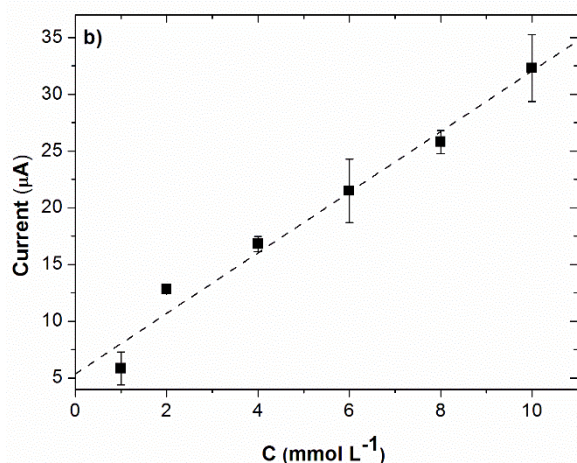


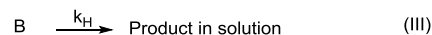
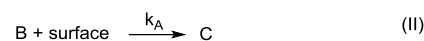
Figure 4. a) Current-potential curves of a solution of phenol with a concentration ranging from 10^{-3} to 10^{-2} mol L⁻¹ in a 0.1 mol L⁻¹ NaOH aqueous solution obtained by EASCV for a sampling time of 0.02 s b) corresponding calibration plot. Error bars are based on measurements performed on two or three different arrays.

For all considered concentrations, current-potential curves that could be easily overlapped by sigmoid functions are obtained. An increase of the current is visible for the lowest concentrations of phenol (10^{-3} and 2×10^{-3} mol L⁻¹) for potentials higher than 0.6 V/SCE, corresponding to the formation of oxides on gold. The value of the limiting current estimated by a sigmoid fit (Table S2) vs the concentration of phenol is given in Figure 4b, showing the interest of EASCV to minimize the passivation phenomenon. A linear relationship is obtained with a regression coefficient of 0.989.

2.4 Modelling of sampled-current voltammetry on an electrode array with passivation

As seen in Figure 2b, when higher sampling times were used, the current-potential curves exhibit a peak instead of the expected plateau with decreasing values of limiting current in EASCV. For a better understanding of the role of the sampling time in EASCV, a modelling of the current was performed. A model for passivation, previously proposed by Savéant et al.,^[52] is adopted here. In this model, we will consider a redox system consisting of a one-electron irreversible reaction between the reactant A and the product B (represented by Equation (I) below) that is characterized by an apparent charge transfer standard rate constant k_s . Butler-Volmer law was considered for the electron-transfer kinetics and semi-infinite linear diffusion conditions are assumed to prevail. The passivation is treated as a competition between the adsorption of species on the electrode surface with a rate constant k_A (Equation II) and their

reaction when diffusing in the bulk solution with a corresponding rate constant, k_H (Equation III).



Some other assumptions are made i) the surface area covered by C totally inhibits the reduction of A, ii) the reaction (equation III) is fast compared with diffusion (“pure kinetic” conditions). Normalized variables, functions and parameters giving rise to dimensionless formulation are introduced by following the definition in Savéant et al.’s work:^[52]

- Time : $\tau = \frac{t}{\theta}$ with θ the time characteristic of the experiment.

- Potential: $\xi = \frac{-F}{RT} (E - E^0)$ with E the applied potential, E^0 the standard potential of the couple A/B, T the temperature, R the gas constant, F the Faraday constant.

- Space: $y = \frac{x}{\sqrt{\theta D}}$ with D the diffusion coefficient of A.

- Current without passivation: $\psi = \frac{i}{FSC_A^0 \sqrt{\frac{D}{\theta}}}$ with S the initial electrode surface and C_A^0 the initial concentration of A.

- Concentration : $a = \frac{C_A}{C_A^0}$

The fractional coverage Ω of the electrode is defined as:

$\Omega = \frac{n_C}{n_C^0} = \frac{\Gamma}{\Gamma^0} = 1 - \frac{S}{S^0}$ with n_C the number of moles of C on the surface and n_C^0 the maximum number of moles of C for a total coverage of the surface S^0 , Γ the surface concentration of C and Γ^0 its maximum value.

Taking into account the current resulting from sampled-current voltammetry ψ and the passivation phenomenon characterized by Ω , the current ψ_f obtained in sampled-current voltammetry with passivation of the electrode is:^[52]

$$\psi_f = (1 - \Omega)\psi \quad (1)$$

The resolution of the following system (the details for the calculations are provided in the Supporting Information) provides the value of the dimensionless current ψ :

$$\frac{\psi e^{-\alpha\xi}}{\Lambda} = 1 - \frac{1}{\sqrt{\pi}} \int_0^\tau \frac{\psi(\eta)}{\sqrt{\tau-\eta}} d\eta \quad (2)$$

$$\Omega = p \int_0^{\tau} (1 - \Omega) \psi d\tau \quad (3)$$

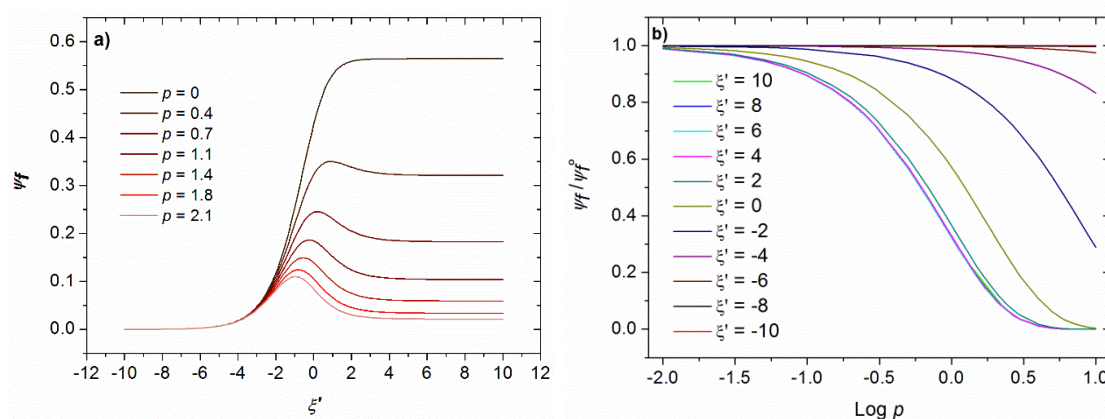
$$\psi_f = (1 - \Omega) \psi$$

ψ only depends on two independent parameters Λ and p :

$$\Lambda = k_s \sqrt{\frac{\theta}{D}} = \Lambda^\circ \sqrt{\theta}$$

$$p = \frac{k_A}{k_A + \sqrt{D}k_H} \frac{C^\circ \sqrt{D\theta}}{r^\circ} = p^\circ \sqrt{\theta}$$

Thus, p is a parameter characteristic of the passivation phenomenon. Indeed, it depends on the two rate constants k_H and k_A of the reactions (II) and (III), respectively. A low value of p is obtained when the reaction of B is prominent ($k_A \ll k_H$) and a high value is due to a high passivation phenomenon ($k_A \gg k_H$). To observe the effect of p on the electrochemical response, the calculated dimensionless current-potential curves are displayed for different values of p in Figure 5a. It is noticeable that a peak is predicted by calculations as observed in the experimental curves (Figure 2b). When p is low, a sigmoid curve is obtained and conversely, when p is high, the current-potential curve has a peak shape. These results underline that the appearance of a peak is directly linked to the adsorption of species on the electrode surface.



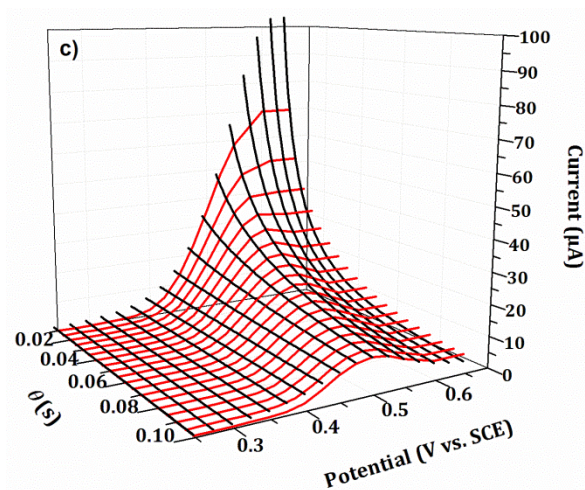


Figure 5. a) Modelled current-potential curves in adimensional parameters ($\psi_f = f(\xi')$, ξ' see definition in Supporting Information) for different values of p b) Effect of the parameter p on ψ_f/ψ_f° for ψ_f° the value of ψ_f when $p=0$ c) Comparison of modelled and experimental data obtained by EASCV. (—) Experimental I-E curves obtained for a 10^{-3} mol L $^{-1}$ phenol aqueous solution in 0.1 mol L $^{-1}$ NaOH for different sampling times, (—) modelled I- θ curves for different potentials.

Similarly, curves relating the ratio ψ_f/ψ_f° (ψ_f° the current for $p = 0$) with $\log p$ for different values of ξ' are given in Figure 5b. For low values of p , ψ_f tends to ψ_f° , as expected when no passivation phenomenon occurs. When p increases, the current decreases owing to a higher blockage of the electrode. For values of ξ' lower than -6, the ratio ψ_f/ψ_f° tends to 1, even for high values of p , but the current is too low to be used. As seen in Figure 5a, when ξ' increases, the effect of the passivation becomes more pronounced but a maximum is observed. Because the influence of the passivation depends on both the parameter p and ξ' , it is possible to optimize the sensitivity of the detection by a judicious choice of the sampling time and applied potential. For example, for $p = 2.1$, if a potential is chosen as $\xi' = -1$, i.e. close to the maximum values of current (see Figure 5a), ψ_f is increased by approximately 5 compared with the value of ψ_f for $\xi' > 2$. Similarly, in terms of sampling time, for $\xi' = 0$ and $\log p = 0$ (Figure 5b), a decrease of θ by a factor of 100 leads to a ratio ψ_f/ψ_f° close to one, i.e. almost without attenuation of the current. The effect of the sampling time on the current is even more pronounced when $\log p$ is higher than 0.

Calculated curves were adjusted to fit the experimental data performed with a 10^{-2} mol L $^{-1}$ solution of phenol in 0.1 mol L $^{-1}$ NaOH (Figure 5c). Experimental currents are derived from the dimensionless currents for different experimental time θ using the following relation: $I =$

$\psi_f(\tau = 1)FSC^\circ\sqrt{(D/\theta)}$ that provides the current *versus* time curve $I=f(\theta)$ at a constant potential. A good agreement is obtained between the model and the experimental data for all experimental times using a single set of parameters ($\xi^\circ = 9.5$ and $p^\circ = 5.7$). As seen experimentally, the plateau corresponding to the limiting current is observed for short experimental sampling times and a peak appears when increasing θ . According to Figure 2, a sampling time lower than 0.02 s is necessary to significantly minimize the attenuation of the current by the passivation of the electrode. Such value of the experimental time is compatible with the time response of the commercially available potentiostats, meaning that even if strong electrode fouling occurs as in the example of phenol considered in our work, EASCV is an efficient way to minimize the effect.

3. Conclusions

Sampled-current voltammetry on an electrode array (EASCV) is an efficient method to minimize electrode passivation. It allows reproducible detection and quantification of species that leads to electrode fouling, as illustrated in this work with phenol, a compound that leads to a fast and efficient passivation of the electrode surface during its analysis. Electrode arrays with good surface area reproducibility were prepared by conventional photolithography that is a simple and mass-production method. Modelling of EASCV allows a deeper understanding of the passivation phenomenon occurring during the analysis. Curves relating the electrochemical signal to a parameter p characteristic of the passivation phenomenon were achieved, underlining the importance of the choice of the sampling time and the potential that would strongly minimize the passivation of the electrode. A sampling time of 0.02 s is enough to prevent the attenuation of the current by the passivation of the electrode and allows the establishment of a linear calibration plot. Such a value of the experimental time is compatible with the time response of the commercially available potentiostats. The method can be generalized to all species that leads to electrode fouling and bring an alternative to destructive methods for their analysis in relatively high concentrations.

Experimental Section

Microfabrication

Standard microfabrication methods and equipment were used to satisfy the strict purity requirements for sensitive electrochemical detection and to maintain a strict reproducible response of the final sensor. A cleanroom microfabrication process is described in four steps. The first step involves patterning gold on an electrode array (Figure 6a) on 0.8 mm thick glass substrates.

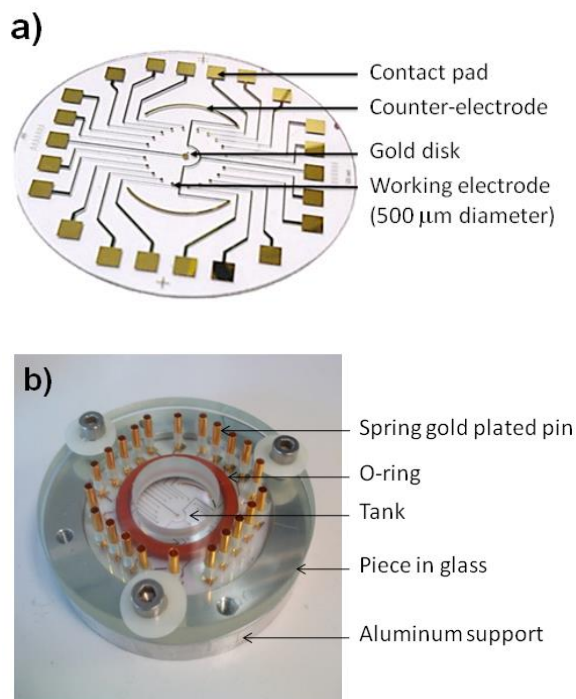


Figure 6. a) Electrode array prepared by photolithography b) Electrochemical two-part cell adapted to the electrode array.

To ensure high purity, the substrates were cleaned using 1% (v/v) Hellmanex[®] solution in deionized water for one hour in an ultrasound bath at 40°C and then rinsed abundantly in deionized water followed by 13 min of plasma cleaning. Titanium and gold were sequentially deposited by thermal evaporation (Plassys ME300) under high vacuum ($P < 5 \times 10^{-5}$ mbar) on the cleaned substrates. A thin layer of titanium (30 nm) was first deposited on a glass wafer by thermal vapor deposition, to ensure adhesion of the gold layer on the glass substrate.^[53] The thickness of the gold layer was chosen to be 200 nm, to assure a good quality of gold for electrochemical analyses. All metals used for the photolithography process were 99.99% quality, supplied by Neyco, SA. In the second step, the electrode array was patterned by photolithography using Shipley S1818 positive tone photoresist deposited by spin coating (Figure S3). After 50 s in a developer bath to wash out the resin, the metal was chemically

etched using titanium and gold etchants (Very Large Scale Integration quality). This second step ends with the removal of the polymerized resin. The wafer was dried under argon and cleaned for 13 min using a plasma cleaner. In the third step, the patterns were electrically insulated (Figure S4) using coating by a silicon nitride film deposited by Plasma Enhanced Chemical Vapor Deposition using a SiH_4 and N_2 mixture (280°C, 30 W). Another thin layer of titanium (30 nm) was added before the insulating layer of Si_3N_4 (600 nm) to protect gold from oxidation in air and improve the adherence of Si_3N_4 ^[54-56] and to facilitate the patterning of the Si_3N_4 layer by the plasma treatment. Finally, the Si_3N_4 insulator was patterned by photolithography (the same process as that described with the Shipley S1818 positive tone photoresist was followed) and etched by a SF_6 Reactive Ion Etching process to achieve the electrode array, using 60 sccm SF_6 at 2×10^{-2} mbar and 150 W radiofrequency power for 25 min and 100 W radiofrequency power for 5 min. The titanium layer was also etched by the SF_6 reacting ion etching process, avoiding the introduction of an additional step in the process to remove it. The nature of the insulating layer has been chosen to support both organic and aqueous media. Thus, the electrode array including twenty working electrodes (500 μm diameter), the counter electrode (two circular arcs with a width of 500 μm and a length of 2 cm) and the reference electrode (1000 μm diameter) was defined, as well as the pads for connection to the external potentiostat. The substrate was positioned in a two-part cell (Figure 6b), the lower aluminum part of which accommodates the electrode array and the upper glass part provides electrical contacts through pogo pins. At the end of this process the residual resin was removed and the electrode array was cleaned for 13 min using a plasma cleaner.

Cleaning step

The working electrodes of the array prepared by photolithography were cleaned in acetone with soft stirring (50 rpm) for 5 min and rinsed with ultrapure water. After drying with argon, they were exposed for 25 min under ozone/UV. The electrodes were then rinsed twice with acetone, acetonitrile for 5 min and ethanol for 5 min, followed by copious ultrapure water. The electrodes were then dried with argon. Finally, all the working electrodes were connected together and cyclic voltammetry was performed from 1.5 to -1 V against a saturated calomel electrode (SCE) until a stable electrochemical signal was obtained in a 0.5 mol L⁻¹ phosphate buffer, pH 7.2. After the analysis of phenol, the electrode array was regenerated by dipping it in concentrated HNO_3 for 20 min and then carefully washed with ultrapure water.

Electrochemical analyses

Electrochemical experiments were performed in a homemade cell (Figure 6b). After positioning the electrode array on an aluminum support, it was covered by a piece of glass containing 22 spring gold plated pins for electrical contacts and a 15 mm diameter tank as an analyte reservoir. The tank was sealed using an O-ring that was clamped between the aluminum support and the piece in glass. The electrochemical analyses were performed in a standard three-electrode configuration, with a platinum wire counter electrode and a saturated calomel reference electrode. These counter and reference electrodes were used in this first work to avoid any complication due to contamination of the integrated counter and reference electrodes of the array. The 20 gold electrodes (0.2 mm^2) of the array were used as working electrodes. All electrochemical experiments were performed at room temperature (25°C) without any degassing. Cyclic voltammetry and chronoamperometry experiments were carried out using a VersaSTAT3 AMETEK[®] Model potentiostat/galvanostat with a VersaSTAT LC Low Current Interface (Princeton Applied Research) and the versaStudio Software. I vs. E curves were obtained by applying sampled-current voltammetry on the electrode array by the following procedure (Figure 7): a potential E_n ($n = 1$ up to a maximum of 20, corresponding to the number of electrodes on the array) was applied sequentially to the n^{th} electrode of the array.^[49] The value of the current response I_n was measured after a sampling time θ ranging from 0.01 to 0.1 s. The resulting current-potential curve (I_n - E_n) was drawn. To simplify, this method is called sampled-current voltammetry on an electrode array (EASCV).

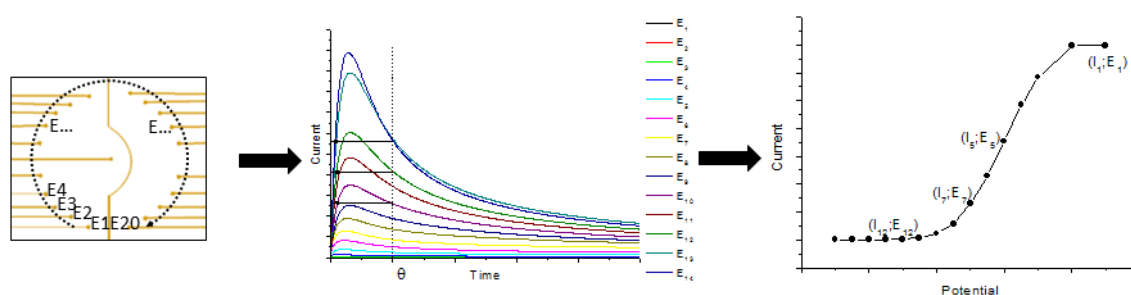


Figure 7. Principle of sampled-current voltammetry on an electrode array (EASCV)

Supporting information

Preparation and characterization of the electrode array, data corresponding to the overlapping of the experimental curves by sigmoid functions and details of the calculations for the modelling of EASCV, Figures S1, S2, S3, S4, S5, S6 and Tables S1, S2.

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