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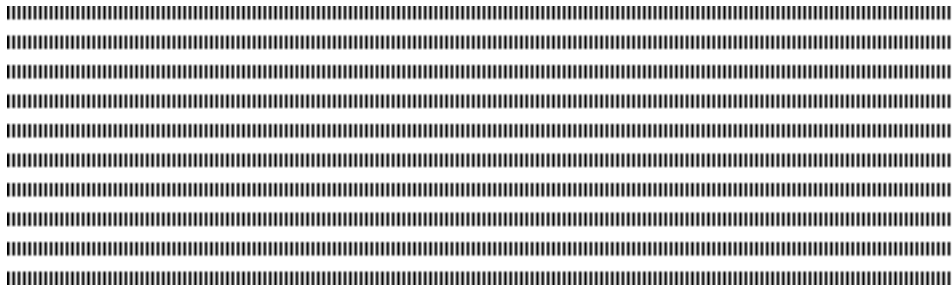
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Optimal control of a parabolic solar collector

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ABSTRACT. The aim of this paper is to study an optimal control problem for a parabolic solar collector. We consider a bilinear distributed model, where the control models the velocity of the heat-transfer fluid. We prove the existence of an optimal control, and we derive a necessary optimality condition. Then we give an algorithm for the computation of the optimal control. The obtained results are illustrated by simulations of the simplified model, using data of Ain Beni Mathar solar plant in Morocco.

RÉSUMÉ. L'objet de cet article est d'étudier un problème de contrôle optimal d'un collecteur solaire parabolique. On considère un modèle bilinéaire distribué, où le contrôle modélise la vitesse du fluide caloporteur. On démontre l'existence d'un contrôle optimal, et on établit une condition nécessaire d'optimalité. Ensuite, on donne un algorithme pour l'implémentation numérique du contrôle optimal. Les résultats obtenus sont illustrés à travers des simulations numériques, en utilisant les données de la station solaire Ain Beni Mathar au Maroc.

KEYWORDS : Bilinear systems, Semigroups, Optimal control, Solar collector, Parabolic trough reflector.

MOTS-CLÉS : Systèmes bilinéaires, Semi-groupes, Contrôle optimal, Collecteur solaire, Réflecteur parabolique.



1. Introduction

Renewable energy is a clean and sustainable alternative to fossil energy. It is a promising technology to face the increasingly global demand for energy and the fluctuating prices of fossil fuels. Particularly, solar thermal energy (STE) is an abundant energy resource, which consists in collecting sunlight to generate thermal or electric energy. The efficiency of solar energy is affected by the position of the sun and by the weather. In this context, the geographic position of Morocco enables the exploitation of solar thermal energy with highly efficient power stations, which significantly reduces electricity production costs. Land availability is also an important factor that gives Morocco a tremendous potential to successfully invest in solar energy.

In this work, we are interested in the optimization of a parabolic power plant performance. Power plants usually use parabolic mirrors to concentrate sunlight onto a receiver tube, containing a heat-transfer fluid, which is often a synthetic oil. The mirrors (or reflectors) change their position along the day from east to west to collect a maximum of sunlight. The receiver tube is enclosed in a vacuum glass envelope. The vacuum significantly reduces the heat losses. Once the fluid is heated by solar irradiation, it is carried to a heat engine, where the heat energy is converted to electricity via steam turbines. For a maximal efficiency of the heat engine, the fluid temperature has to be close to a required level $T_d \simeq 673.15\text{K}$ ($\simeq 400^\circ\text{C}$). The fluid temperature depends on the intensity of solar irradiation, on the optical properties of the reflectors, and on the fluid velocity. To drive the fluid temperature close to the required level, it is imperative to determine the optimal fluid velocity, which can be achieved via minimizing a given functional.

This is the aim of this paper. We consider an optimal control problem, where the control stands for the velocity of the heat-transfer fluid. The optimal control to be searched is the minimizer of a quadratic cost functional. The heat balance within the collector is modeled by a distributed bilinear system, written as $\dot{y}(t) = Ay(t) + u(t)By(t) + b(t)$. A rich literature is devoted to the optimal control of such systems (see for instance [1, 3, 5, 9, 11, 12]). However, in previous works, the control operator B is usually assumed to be relatively bounded with respect to the dynamics operator A . By contrast, the model studied here is a bilinear system whose operator A is bounded, while the control operator B is unbounded, and is the generator of a strongly continuous semigroup. Thereby, the optimal control problem will be studied using a new method, based on the tools of semigroup theory.

The paper is organized as follows. Section 2 is devoted to the description of the distributed bilinear system, modeling the evolution of the fluid temperature. In section 3, we prove the existence of optimal controls, and we derive a necessary optimality condition. In section 4, we provide simulations of the solar collector model, using data of Ain Beni Mathar solar plant in Morocco.

2. The bilinear model

We consider a parabolic solar collector, as depicted in Fig. 1. The heat-transfer fluid flows through a metallic receiver tube of length L , which is enclosed in a concentric glass envelope. Both tubes are located in the focal line of a parabolic mirror, which concentrates sunlight towards the tubes.

The following assumptions are made on the basis of empirical estimations :

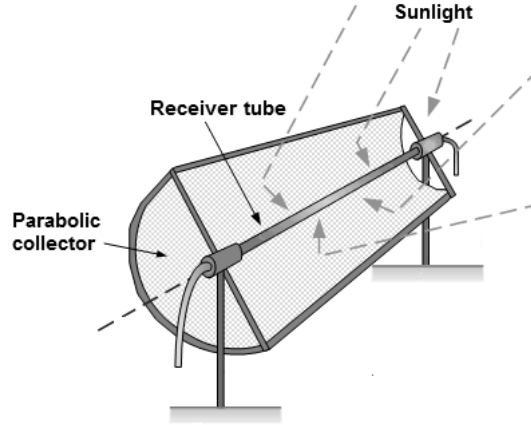


Figure 1. Cylindro-parabolic solar collector [2]

1) The fluid is incompressible, and the fluid flow is laminar, then the fluid velocity is space-independent, and depends only on time.

2) The fluid velocity and temperature are uniformly distributed over the tube section, hence the receiver tube may be modeled by a one-dimensional domain $]0, L[$.

3) There is perfect vacuum separating the receiver tube and the glass envelope, then the heat loss caused by the glass tube is negligible.

Upon the above assumptions, it has been proved, in subsection 3.3.b of [4], that the heat balance within the solar collector may be modeled by a system of two partial differential equations on $]0, L[$, describing the temperature of the fluid T_f (K) and that of the receiver tube T_m (K), and given by :

$$\begin{cases} \frac{\partial T_f}{\partial t}(x, t) = aT_f(x, t) + a_1T_m(x, t) - u(t)\frac{\partial T_f}{\partial x}(x, t) &]0, L[\times]0, T[\\ \frac{\partial T_m}{\partial t}(x, t) = b_1T_f(x, t) + b_2T_m(x, t) + b_3 &]0, L[\times]0, T[\\ T_f(0, t) = T_{f,0} &]0, T[\\ (T_f(x, 0), T_m(x, 0)) = (T_{f,0}, T_{m,0}) &]0, L[\end{cases} \quad (1)$$

where a, a_1, b_1, b_2 and b_3 are empirically estimated coefficients, depending on the weather and the optical properties of the collectors, and assumed to be constant in our application due to the choice of a small time interval.

$u(t)$ (m s^{-1}) is the velocity of the heat-transfer fluid. In what follows $u(t)$ stands for the control.

In [6], El Jai and Chalqi provide simulations of the original model (1), where it is shown that, for a relatively small fluid velocity, the temperature of the receiver tube reaches rapidly a given value $T_{max} \simeq 873 \text{ K}$ ($\simeq 600^\circ\text{C}$), due to the quick metal heat absorption. They deduce that the temperature of the receiver tube $T_m(.,.)$ can be assumed to be time-independent and close to T_{max} , while the simulated fluid temperature remains very close to the one in the original model (1). Therefore, El Jai and Chalqi con-

clude in [6] that the collector model (1) may be simplified into a system of one partial differential equation, given by

$$\begin{cases} \frac{\partial T_f}{\partial t}(x, t) = aT_f(x, t) + a_1T_m(x) - u(t)\frac{\partial T_f}{\partial x}(x, t) \\ T_f(0, t) = T_{f,0} \\ T_f(x, 0) = T_{f,0} \end{cases} \quad (2)$$

where the metallic tube temperature T_m is approximated by a smooth function, satisfying $T_m(0) = -\frac{a}{a_1}T_{f,0}$, as depicted in Fig. 2.

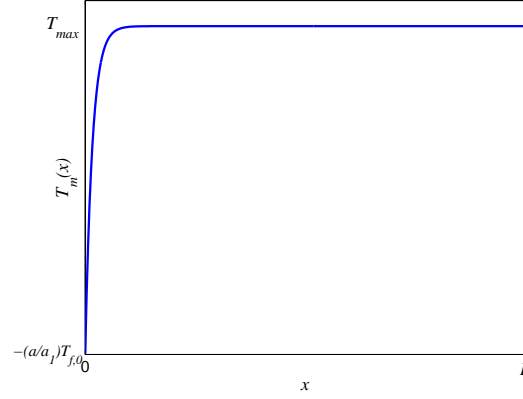


Figure 2. Temperature profile of the metallic tube T_m

We consider the state space $H = L^2(0, L)$, and we define the state $y(t) \in H$ by

$$[y(t)](x) = T_f(x, t) - T_{f,0}$$

Denote $B = -\frac{\partial}{\partial x}$, and $b = aT_{f,0} + a_1T_m \in H$, then equation (2) takes the form of the following bilinear system

$$\begin{cases} \dot{y}(t) = ay(t) + u(t)By(t) + b \\ y(0) = 0 \end{cases} \quad (3)$$

The domain of B is $\mathcal{D}(B) = \{z \in H^1(0, L) : z(0) = 0\}$, hence $y(0), b \in \mathcal{D}(B)$. Moreover, B is the infinitesimal generator of the following C_0 semigroup

$$[S(t)y](x) = \begin{cases} y(x-t) & \text{if } x-t > 0 \\ 0 & \text{if } x-t < 0 \end{cases}$$

For a maximal performance, the fluid temperature T_f has to be close to a given value $T_d = 673.15\text{K}$ (400°C) along the tube. To this end, we will search the optimal fluid velocity $u(\cdot)$ that drives $y(t)$ close to $y_d = T_d - T_{f,0}$ by minimizing a quadratic cost functional. This is the purpose of the next section.

3. Optimal control problem

We consider the following system

$$\begin{cases} \dot{y}(t) = ay(t) + u(t)By(t) + b(t) \\ y(0) = y_0 \end{cases} \quad (4)$$

where B is the infinitesimal generator of a C_0 semigroup $(S(t))_{t \geq 0}$ on a separable Hilbert space H , with a dense domain $\mathcal{D}(B)$. $u \in L^\infty(0, T)$ is the control, such that $u(t) \geq 0$ almost everywhere (a.e.). $a \in \mathbb{R}$, $b \in L^2(0, T; \mathcal{D}(B))$, and $y_0 \in \mathcal{D}(B)$.

Our purpose is to minimize the following cost functional

$$J(u) = \frac{\alpha}{2} \|y(T) - y_d\|^2 + \frac{\beta}{2} \int_0^T \|y(s) - y_d\|^2 ds + \frac{r}{2} \int_0^T u(s)^2 ds \quad (5)$$

over the set of admissible controls

$$U_{ad} = \{u \in L^\infty(0, T) : u_{min} \leq u(t) \leq u_{max} \text{ a.e. } \} \quad (6)$$

where $y_d \in H$, $\alpha, \beta \geq 0$, $r > 0$, and $0 \leq u_{min} < u_{max}$.

If r is small compared to $\frac{\alpha}{Tu_{max}^2}$ or $\frac{\beta}{u_{max}^2}$, then the minimization of the cost functional (5) allows to drive the state $y(t)$ close to y_d .

Thus, the optimal control problem is stated as :

$$\begin{cases} \min J(u) \\ u \in U_{ad} \end{cases} \quad (7)$$

We first give the expression of the unique mild solution of system (4).

Lemma 3.1. *System (4) has a unique mild solution, written as*

$$y(t) = S\left(\int_0^t u(\tau) d\tau\right) y_0 + \int_0^t S\left(\int_s^t u(\tau) d\tau\right) [ay(s) + b(s)] ds \quad (8)$$

where $(S(t))_{t \geq 0}$ is the C_0 semigroup generated by B .

Moreover, since $y_0 \in \mathcal{D}(B)$, then $y(t) \in \mathcal{D}(B)$, $\forall t \geq 0$.

Proof. For $u \in L^\infty(0, T)$ such that $u(t) \geq 0$ a.e., denote $U(t, s) = S\left(\int_s^t u(\tau) d\tau\right)$.

The family of operators $(U(t, s))_{t \geq s}$ satisfies definition 9.2, chapter VI in [7], then $U(t, s)$ is a strongly continuous evolution family. Besides, there exist constants $M \geq 1$ and $\omega \in \mathbb{R}$ such that $\|U(t, s)\| \leq Me^{|\omega|(t-s)}$, then $U(t, s)$ is exponentially bounded. Additionally, a simple calculus yields

$$\frac{d}{dt} U(t, s)z = u(t)BU(t, s)z, \quad \forall t \geq s, \forall z \in \mathcal{D}(B)$$

Then $(U(t, s))_{t \geq s}$ is generated by the family of operators $B(t) = u(t)B$.

By virtue of corollary 9.20, chapter VI in [7], it follows that the family of operators $(u(t)B + aI)_{t \geq 0}$ generates an exponentially bounded evolution family $(\Gamma(t, s))_{t \geq s \geq 0}$, given by

$$\Gamma(t, s)z = U(t, s)z + \int_s^t U(t, \tau)a\Gamma(\tau, s)z d\tau, \quad \forall z \in H$$

Then system (4) has a unique mild solution, written as

$$y(t) = \Gamma(t, 0)y_0 + \int_0^t \Gamma(t, s)b(s)ds$$

Replacing $\Gamma(t, 0)$ and $\Gamma(t, s)$ by their respective expressions, and applying Fubini's theorem yield

$$y(t) = U(t, 0)y_0 + \int_0^t U(t, s) [ay(s) + b(s)] ds$$

Hence we obtain (8). Finally, since $y_0 \in \mathcal{D}(B)$ then, by proposition 9.3, chapter VI in [7], $y(t) \in \mathcal{D}(B)$, $\forall t \geq 0$. \square

In the next proposition we prove the existence of an optimal control.

Proposition 3.2. *There exists $u^* \in U_{ad}$ such that*

$$J(u^*) = \inf_{u \in U_{ad}} J(u)$$

Proof. The functional J is nonnegative, and the set U_{ad} is nonempty, then there exists $J^* \geq 0$ such that $J^* = \inf\{J(u) \mid u \in U_{ad}\}$. Let $(u_n)_{n \in \mathbb{N}}$ be a sequence in U_{ad} , such that $\lim_{n \rightarrow \infty} J(u_n) = J^*$. By the boundedness of U_{ad} , the sequence $(u_n)_{n \in \mathbb{N}}$ is bounded, then $(u_n)_{n \in \mathbb{N}}$ has a subsequence, still denoted $(u_n)_{n \in \mathbb{N}}$, converging weakly to u^* in $L^2(0, T)$. U_{ad} is convex and closed in $L^2(0, T)$, hence weakly closed in $L^2(0, T)$, which yields $u^* \in U_{ad}$.

Let y_n and y^* be the respective mild solutions of system (4), relatively to u_n and u^* . Then

$$\begin{aligned} y_n(t) - y^*(t) &= S\left(\int_0^t u_n(\tau)d\tau\right)y_0 - S\left(\int_0^t u^*(\tau)d\tau\right)y_0 \\ &\quad + \int_0^t S\left(\int_s^t u_n(\tau)d\tau\right)a[y_n(s) - y^*(s)]ds \\ &\quad + \int_0^t \left[S\left(\int_s^t u_n(\tau)d\tau\right)y^*(s) - S\left(\int_s^t u^*(\tau)d\tau\right)y^*(s) \right] ds \\ &\quad + \int_0^t \left[S\left(\int_s^t u_n(\tau)d\tau\right)b(s) - S\left(\int_s^t u^*(\tau)d\tau\right)b(s) \right] ds \end{aligned}$$

Denote $\mu = \sup_{n \in \mathbb{N}} \|u_n\|_{L^\infty(0, T)}$, and let $M \geq 1$ and $\omega \in \mathbb{R}$ such that $\|S(t)\| \leq Me^{\omega t}$, $\forall t \geq 0$. Let $\widehat{M} = Me^{|\omega a|T\mu}$. Then applying Gronwall's lemma to the above equality yields

$$\begin{aligned} \|y_n(t) - y^*(t)\| &\leq \widehat{M} \left\| S\left(\int_0^t u_n(\tau)d\tau\right)y_0 - S\left(\int_0^t u^*(\tau)d\tau\right)y_0 \right\| \\ &\quad + \widehat{M} \left\| \int_0^t \left[S\left(\int_s^t u_n(\tau)d\tau\right)y^*(s) - S\left(\int_s^t u^*(\tau)d\tau\right)y^*(s) \right] ds \right\| \\ &\quad + \widehat{M} \left\| \int_0^t \left[S\left(\int_s^t u_n(\tau)d\tau\right)b(s) - S\left(\int_s^t u^*(\tau)d\tau\right)b(s) \right] ds \right\| \end{aligned}$$

The weak convergence $u_n \rightharpoonup u^*$ gives $\lim_{n \rightarrow \infty} \int_s^t u_n(\tau) d\tau = \int_s^t u^*(\tau) d\tau$, $\forall s, t \in [0, T]$.

It follows that

$$\begin{aligned} \lim_{n \rightarrow \infty} \left\| S \left(\int_0^t u_n(\tau) d\tau \right) y_0 - S \left(\int_0^t u^*(\tau) d\tau \right) y_0 \right\| &= 0 \\ \lim_{n \rightarrow \infty} \left\| S \left(\int_s^t u_n(\tau) d\tau \right) y^*(s) - S \left(\int_s^t u^*(\tau) d\tau \right) y^*(s) \right\| &= 0 \quad \text{a.e. on } [0, t] \\ \lim_{n \rightarrow \infty} \left\| S \left(\int_s^t u_n(\tau) d\tau \right) b(s) - S \left(\int_s^t u^*(\tau) d\tau \right) b(s) \right\| &= 0 \quad \text{a.e. on } [0, t] \end{aligned}$$

Then, by applying Lebesgue's dominated convergence theorem, we obtain

$$\begin{aligned} \lim_{n \rightarrow \infty} \left\| \int_0^t \left[S \left(\int_s^t u_n(\tau) d\tau \right) y^*(s) - S \left(\int_s^t u^*(\tau) d\tau \right) y^*(s) \right] ds \right\| &= 0 \\ \lim_{n \rightarrow \infty} \left\| \int_0^t \left[S \left(\int_s^t u_n(\tau) d\tau \right) b(s) - S \left(\int_s^t u^*(\tau) d\tau \right) b(s) \right] ds \right\| &= 0 \end{aligned}$$

Therefore $y_n(t) \rightarrow y^*(t)$ strongly in H , for every $t \in [0, T]$.

By Fatou's lemma, we obtain

$$\int_0^T \|y^*(t) - y_d\|^2 dt \leq \liminf_{n \rightarrow \infty} \int_0^T \|y_n(t) - y_d\|^2 dt$$

and by the lower semi-continuity of norms, we have

$$\int_0^T u^*(t)^2 dt \leq \liminf_{n \rightarrow \infty} \int_0^T u_n(t)^2 dt$$

Hence $J(u^*) \leq \liminf_{n \rightarrow \infty} J(u_n) = J^*$, which yields $J(u^*) = J^*$. \square

Hereafter we prove some technical results, that will be useful to formulate an optimality condition.

Proposition 3.3. *Let $u, h \in L^\infty(0, T)$ such that $u(t), h(t) \geq 0$ a.e., then*

$$\lim_{\varepsilon \rightarrow 0^+} \frac{y_{u+\varepsilon h}(t) - y_u(t)}{\varepsilon} = z_h(t) \quad (9)$$

where z_h is the mild solution of the following equation :

$$\begin{cases} \dot{z}_h(t) = az_h(t) + u(t)Bz_h(t) + h(t)By_u(t) \\ z_h(0) = 0 \end{cases} \quad (10)$$

and is written as :

$$z_h(t) = \int_0^t S \left(\int_s^t u(\tau) d\tau \right) [az_h(s) + h(s)By_u(s)] ds \quad (11)$$

Proof. Let $u, h \in L^\infty(0, T)$, such that $u(t), h(t) \geq 0$ a.e. on $[0, T]$. Let $\varepsilon > 0$. Without loss of generality, we can assume that $\varepsilon \|h\| \leq 1$.

Let y_u and $y_{u+\varepsilon h}$ be the respective mild solutions of system (4), relatively to u and $u+\varepsilon h$, and let z_h be the mild solution of equation (10). Denote $U(t, s) = S\left(\int_s^t u(\tau)d\tau\right)$. By replacing $y_u(s)$ in equation (11) by its expression, we obtain

$$\begin{aligned} z_h(t) &= \int_0^t U(t, s)az_h(s)ds + \int_0^t h(s)BU(t, 0)y_0ds \\ &\quad + \int_0^t \int_0^s h(s)BU(t, \theta)[ay_u(\theta) + b(\theta)]d\theta ds \end{aligned}$$

Applying Fubini's theorem to the above expression yields

$$\begin{aligned} z_h(t) &= \int_0^t U(t, s)az_h(s)ds + \left(\int_0^t h(\tau)d\tau\right) BU(t, 0)y_0 \\ &\quad + \int_0^t \left(\int_s^t h(\theta)d\theta\right) BU(t, s)[ay_u(s) + b(s)]ds \end{aligned} \quad (12)$$

For $0 \leq s \leq t \leq T$, we denote

$$\begin{cases} Y_0(t) = U(t, 0)y_0 \\ Y(s) = U(t, s)ay_u(s) \\ Z(s) = U(t, s)b(s) \\ H_\varepsilon(t, s) = S\left(\varepsilon \int_s^t h(\tau)d\tau\right) \end{cases}$$

Then

$$\begin{aligned} y_u(t) &= Y_0(t) + \int_0^t [Y(s) + Z(s)]ds \\ y_{u+\varepsilon h}(t) &= H_\varepsilon(t, 0)Y_0(t) + \int_0^t H_\varepsilon(t, s)U(t, s)ay_{u+\varepsilon h}(s)ds + \int_0^t H_\varepsilon(t, s)Z(s)ds \end{aligned}$$

and, by expression (12), we have

$$z_h(t) = \int_0^t U(t, s)az_h(s)ds + \left(\int_0^t h(\tau)d\tau\right) BY_0(t) + \int_0^t \left(\int_s^t h(\tau)d\tau\right) B[Y(s) + Z(s)]ds$$

which yields

$$\begin{aligned} \frac{y_{u+\varepsilon h}(t) - y_u(t)}{\varepsilon} - z_h(t) &= \frac{H_\varepsilon(t, 0)Y_0(t) - Y_0(t)}{\varepsilon} - \int_0^t h(\tau)d\tau BY_0(t) \\ &\quad + \int_0^t \left[\frac{H_\varepsilon(t, s)Y(s) - Y(s)}{\varepsilon} - \int_s^t h(\tau)d\tau BY(s) \right] ds \\ &\quad + \int_0^t \left[\frac{H_\varepsilon(t, s)Z(s) - Z(s)}{\varepsilon} - \int_s^t h(\tau)d\tau BZ(s) \right] ds \\ &\quad + \int_0^t H_\varepsilon(t, s)U(t, s)a \left[\frac{y_{u+\varepsilon h}(s) - y_u(s)}{\varepsilon} - z_h(s) \right] ds \\ &\quad + \int_0^t [H_\varepsilon(t, s)az_h(s) - az_h(s)] ds \end{aligned}$$

There exist $M \geq 1$ and $\omega \in \mathbb{R}$ such that $\|S(t)\| \leq Me^{\omega t}$, $\forall t \geq 0$. Then applying Gronwall's lemma to the above equality yields

$$\begin{aligned} \left\| \frac{y_{u+\varepsilon h}(t) - y_u(t)}{\varepsilon} - z_h(t) \right\| &\leq \widehat{M} \left\| \frac{H_\varepsilon(t, 0)Y_0(t) - Y_0(t)}{\varepsilon} - \int_0^t h(\tau) d\tau BY_0(t) \right\| \\ &+ \widehat{M} \left\| \int_0^t \left[\frac{H_\varepsilon(t, s)Y(s) - Y(s)}{\varepsilon} - \int_s^t h(\tau) d\tau BY(s) \right] ds \right\| \\ &+ \widehat{M} \left\| \int_0^t \left[\frac{H_\varepsilon(t, s)Z(s) - Z(s)}{\varepsilon} - \int_s^t h(\tau) d\tau BZ(s) \right] ds \right\| \\ &+ \widehat{M} \left\| \int_0^t [H_\varepsilon(t, s)az_h(s) - az_h(s)] ds \right\| \end{aligned}$$

where $\widehat{M} = Me^{|\omega a|T(\|u\|+1)}$. By passing to the limit, we have

$$\lim_{\varepsilon \rightarrow 0} \|H_\varepsilon(t, s)az_h(s) - az_h(s)\| = 0 \quad \text{a.e. on } [0, t]$$

Since $Y_0(t)$, $Y(s)$ and $Z(s)$ belong to $\mathcal{D}(B)$ then, by using the semigroup property

$\lim_{\tau \rightarrow 0^+} \frac{S(\tau)z - z}{\tau} = Bz$, $\forall z \in \mathcal{D}(B)$, we obtain

$$\begin{aligned} \lim_{\varepsilon \rightarrow 0^+} \left\| \frac{H_\varepsilon(t, 0)Y_0(t) - Y_0(t)}{\varepsilon} - \int_0^t h(\tau) d\tau BY_0(t) \right\| &= 0 \\ \lim_{\varepsilon \rightarrow 0^+} \left\| \frac{H_\varepsilon(t, s)Y(s) - Y(s)}{\varepsilon} - \int_s^t h(\tau) d\tau BY(s) \right\| &= 0 \quad \text{a.e. on } [0, t] \\ \lim_{\varepsilon \rightarrow 0^+} \left\| \frac{H_\varepsilon(t, s)Z(s) - Z(s)}{\varepsilon} - \int_s^t h(\tau) d\tau BZ(s) \right\| &= 0 \quad \text{a.e. on } [0, t] \end{aligned}$$

By using appropriate bounds, and applying the dominated convergence theorem, we have

$$\begin{aligned} \lim_{\varepsilon \rightarrow 0^+} \left\| \int_0^t [H_\varepsilon(t, s)az_h(s) - az_h(s)] ds \right\| &= 0 \\ \lim_{\varepsilon \rightarrow 0^+} \left\| \int_0^t \left[\frac{H_\varepsilon(t, s)Y(s) - Y(s)}{\varepsilon} - \int_s^t h(\tau) d\tau BY(s) \right] ds \right\| &= 0 \\ \lim_{\varepsilon \rightarrow 0^+} \left\| \int_0^t \left[\frac{H_\varepsilon(t, s)Z(s) - Z(s)}{\varepsilon} - \int_s^t h(\tau) d\tau BZ(s) \right] ds \right\| &= 0 \end{aligned}$$

Therefore

$$\lim_{\varepsilon \rightarrow 0^+} \left\| \frac{y_{u+\varepsilon h}(t) - y_u(t)}{\varepsilon} - z_h(t) \right\| = 0$$

□

Corollary 3.4. *Let $u \in L^\infty(0, T)$ such that $u(t) \geq 0$ a.e.*

For any $h \in L^\infty(0, T)$ satisfying $h(t) \leq 0$ and $h(t) + u(t) \geq 0$ a.e., we have

$$\lim_{\varepsilon \rightarrow 0^+} \frac{y_{u+\varepsilon h}(t) - y_u(t)}{\varepsilon} = z_h(t) \quad (13)$$

where z_h is the mild solution of (10), and satisfies expression (11).

Proof. Let $h \in L^\infty(0, T)$ such that $h(t) \leq 0$ and $u(t) + h(t) \geq 0$ a.e. Let $0 < \varepsilon \leq 1$, and denote $v = u + \varepsilon h$. Then

$$\frac{y_{u+\varepsilon h}(t) - y_u(t)}{\varepsilon} = -\frac{y_{v+\varepsilon(-h)}(t) - y_v(t)}{\varepsilon}$$

By proposition 3.2, we have

$$\frac{y_{v+\varepsilon(-h)}(t) - y_v(t)}{\varepsilon} = z_{(-h)}^\varepsilon(t) + \theta(\varepsilon)$$

where $\lim_{\varepsilon \rightarrow 0} \theta(\varepsilon) = 0$, and $z_{(-h)}^\varepsilon$ is the solution of equation (10), with v and $-h$ instead of u and h , respectively. A standard calculus leads to

$$\lim_{\varepsilon \rightarrow 0^+} z_{(-h)}^\varepsilon(t) = -z_h(t)$$

Hence

$$\lim_{\varepsilon \rightarrow 0^+} \frac{y_{v+\varepsilon(-h)}(t) - y_v(t)}{\varepsilon} = -z_h(t)$$

which yields the limit (13). \square

Proposition 3.5. Let $u \in L^\infty(0, T)$ such that $u(t) \geq 0$ a.e.

For any $h \in L^\infty(0, T)$ of constant sign, satisfying $u(t) + h(t) \geq 0$ a.e., we have

$$\lim_{\varepsilon \rightarrow 0^+} \frac{J(u + \varepsilon h) - J(u)}{\varepsilon} = \int_0^T J'_u(t) h(t) dt$$

where

$$J'_u(t) = \langle \varphi(t), B y(t) \rangle_H + r u(t) \quad (14)$$

such that y is the mild solution of system (4), associated to u , and φ is the mild solution of the following adjoint equation

$$\begin{cases} \dot{\varphi}(t) = -a\varphi(t) - u(t)B^*\varphi(t) - \beta(y(t) - y_d) \\ \varphi(T) = \alpha(y(T) - y_d) \end{cases} \quad (15)$$

B^* denotes the adjoint operator of B .

Proof. Let $h \in L^\infty(0, T)$ have a constant sign, and such that $u(t) + h(t) \geq 0$ a.e. Using the limits (9) and (13), we have

$$\begin{aligned} \lim_{\varepsilon \rightarrow 0^+} \frac{J(u + \varepsilon h) - J(u)}{\varepsilon} &= \langle \alpha(y_u(T) - y_d), z_h(T) \rangle_H + \int_0^T \langle \beta(y_u(t) - y_d), z_h(t) \rangle_H dt \\ &\quad + \int_0^T r u(t) h(t) dt \end{aligned}$$

For $n \in \rho(B)$, the resolvent set of B , let $B_n = nB(nI - B)^{-1}$ be the Yosida approximation of B . Let z_n and φ_n be the respective mild solutions of the following equations

$$\begin{cases} \dot{z}_n(t) = a z_n(t) + u(t) B_n z_n(t) + h(t) B y_u(t) \\ z_n(0) = 0 \end{cases}$$

$$\begin{cases} \dot{\varphi}_n(t) = -a \varphi_n(t) - u(t) B_n^* \varphi_n(t) - \beta(y_u(t) - y_d) \\ \varphi_n(T) = \alpha(y_u(T) - y_d) \end{cases}$$

B_n^* is bounded, then $\mathcal{D}(B_n^*) = H$, leading to $B_n^*\varphi_n(t) \in H$ a.e. on $[0, T]$. Therefore

$$\begin{aligned} \int_0^T \langle \beta(y_u(t) - y_d), z_n(t) \rangle_H dt &= - \int_0^T \langle \dot{\varphi}_n(t) + u(t)B_n^*\varphi_n(t) + a\varphi_n(t), z_n(t) \rangle_H dt \\ &= - \int_0^T \langle \dot{\varphi}_n(t), z_n(t) \rangle_H dt - \int_0^T \langle \varphi_n(t), u(t)B_n z_n(t) + a z_n(t) \rangle_H dt \\ &= - \int_0^T \langle \dot{\varphi}_n(t), z_n(t) \rangle_H dt - \int_0^T \langle \varphi_n(t), \dot{z}_n(t) \rangle_H dt + \int_0^T \langle \varphi_n(t), h(t)B y_u(t) \rangle_H dt \end{aligned}$$

Since $\dot{z}_n, \dot{\varphi}_n \in L^2(0, T; H)$, then

$$\begin{aligned} \int_0^T \langle \dot{\varphi}_n(t), z_n(t) \rangle_H dt + \int_0^T \langle \varphi_n(t), \dot{z}_n(t) \rangle_H dt &= \langle \varphi_n(T), z_n(T) \rangle_H - \langle \varphi_n(0), z_n(0) \rangle_H \\ &= \langle \alpha(y_u(T) - y_d), z_n(T) \rangle_H \end{aligned}$$

It follows that

$$\int_0^T \langle \beta(y_u(t) - y_d), z_n(t) \rangle_H dt = - \langle \alpha(y_u(T) - y_d), z_n(T) \rangle_H + \int_0^T \langle \varphi_n(t), h(t)B y_u(t) \rangle_H dt$$

By virtue of proposition 5.4, chapter 2 of [10], we have

$$\lim_{n \rightarrow +\infty} \|z_n - z_h\|_{C([0, T]; H)} = 0 \quad \text{and} \quad \lim_{n \rightarrow +\infty} \|\varphi_n - \varphi\|_{C([0, T]; H)} = 0$$

where z_h and φ are the respective mild solutions of (10) and (15). Then the above equality yields

$$\int_0^T \langle \beta(y_u(t) - y_d), z_h(t) \rangle_H dt + \langle \alpha(y_u(T) - y_d), z_h(T) \rangle_H = \int_0^T \langle \varphi(t), B y_u(t) \rangle_H h(t) dt$$

Therefore

$$\lim_{\varepsilon \rightarrow 0^+} \frac{J(u + \varepsilon h) - J(u)}{\varepsilon} = \int_0^T [\langle \varphi(t), B y_u(t) \rangle_H + r u(t)] h(t) dt$$

□

In the next proposition we formulate a necessary optimality condition.

Proposition 3.6. *Let u^* be an optimal control, then u^* satisfies :*

$$u^*(t) = \max \left(u_{min}; \min \left(u_{max}; -\frac{1}{r} \langle \varphi(t), B y(t) \rangle_H \right) \right) \quad (16)$$

where y and φ are respectively the mild solutions of (4) and (15), associated to u^* .

Proof. Let u^* be an optimal control, and let $h \in L^\infty(0, T)$ have a constant sign, and such that $u^* + h \in U_{ad}$, where U_{ad} is given by (6). The convexity of U_{ad} yields $u^* + \varepsilon h \in U_{ad}$, $\forall \varepsilon \in]0, 1]$. Hence

$$J(u^* + \varepsilon h) \geq J(u^*), \quad \forall \varepsilon \in]0, 1]$$

Using proposition 3.5, we obtain

$$\int_0^T J'_{u^*}(t) h(t) dt = \lim_{\varepsilon \rightarrow 0^+} \frac{J(u^* + \varepsilon h) - J(u^*)}{\varepsilon} \geq 0 \quad (17)$$

– If $u_{min} < u^*(t) < u_{max}$ over a nonempty open set $I \subset]0, T[$:
Let $h \in \mathcal{D}(I)$ (the space of smooth functions, compactly supported) of constant sign. If $\|h\|_{L^\infty(I)}$ is sufficiently small, then $u^* + h, u^* - h \in U_{ad}$. It follows from inequality (17), applied to h and $-h$, that

$$\int_I J'_{u^*}(t)h(t)dt = 0, \quad \forall h \in \mathcal{D}(I) \text{ of constant sign,}$$

which yields $J'_{u^*}(t) = 0$ a.e. on I . Then by expression (14) we have

$$u^*(t) = -\frac{1}{r} \langle \varphi(t), By(t) \rangle \text{ a.e. on } I$$

– If $u^*(t) = u_{min}$ over a nonempty open set $I \subset]0, T[$:
Let $h \in \mathcal{D}(I)$ such that $h(t) \geq 0, \forall t \in I$. Then for $\|h\|_{L^\infty(I)}$ sufficiently small we have $u^* + h \in U_{ad}$. Hence inequality (17) yields $\int_I J'_{u^*}(t)h(t)dt \geq 0$.
It follows that $J'_{u^*}(t) \geq 0$ a.e. on I . Thus

$$-\frac{1}{r} \langle \varphi(t), By(t) \rangle_H \leq u_{min} = u^*(t) \text{ a.e. on } I$$

– Similarly to the above case, if $u^*(t) = u_{max}$ over a nonempty open set $I \subset]0, T[$, then

$$-\frac{1}{r} \langle \varphi(t), By(t) \rangle_H \geq u_{max} \text{ a.e. on } I$$

Therefore, $u^*(t) = \max \left(u_{min}; \min \left(u_{max}; -\frac{1}{r} \langle \varphi(t), By(t) \rangle_H \right) \right)$ a.e. on $[0, T]$. \square

Remark 3.7. Going back to the collector model (2), Proposition 3.6 shows that the optimal fluid velocity is written as

$$u^*(t) = \max \left(u_{min}; \min \left(u_{max}; \frac{1}{r} \int_0^L \varphi(x, t) \frac{\partial T_f}{\partial x}(x, t) dx \right) \right) \quad (18)$$

where T_f is the temperature of the heat-transfer fluid, and φ is the solution of the following adjoint equation

$$\begin{cases} \frac{\partial \varphi}{\partial t}(x, t) = -a\varphi(x, t) - u^*(t) \frac{\partial \varphi}{\partial x}(x, t) - \beta(T_f(x, t) - T_d) \\ \varphi(L, t) = 0 \\ \varphi(x, T) = \alpha(T_f(x, T) - T_d) \end{cases}$$

Expression (18) shows that the optimal fluid velocity u^* is function of the spatial derivative of the temperature, and of the desired temperature T_d , which appears implicitly in the equation governing φ . Moreover, u^* increases proportionately with α , β , and $\frac{1}{r}$.

The optimality condition (16) shows that the optimal control u^* is function of y and φ , which themselves are function of u^* . Then the control cannot be directly computed by (16). For this reason, we introduce the following algorithm, to implement numerically the optimal control.

Algorithm

- Step 1 : Choose an initial control $u_0 \in U_{ad}$, a threshold accuracy $\varepsilon > 0$, and a step length λ . Initialize with $k = 0$.
- Step 2 : Compute y_k , solution of (4), and φ_k , solution of (15), relatively to u_k .
- Step 3 : Compute

$$J'_{u_k}(t) = \langle \varphi_k(t), By_k(t) \rangle + ru_k(t)$$

$$u_{k+1}(t) = \max(u_{min}; \min(u_{max}; u_k(t) - \lambda J'_{u_k}(t)))$$

- Step 4 : If $\|u_{k+1} - u_k\| > \varepsilon$, $k = k + 1$, go to step 2. Otherwise $u^* = u_k$.

4. Simulations

We consider the collector model (2) with data of Ain Beni Mathar solar plant, in Northeast Morocco (see [4]) :

$$L = 618m , a = -0.030 , a_1 = 0.024 , T_{f,0} = 423.15K \text{ (150}^\circ\text{C)}$$

To determine the optimal fluid velocity, we consider system (3), and the optimal control problem (7) with the cost functional (5), where

$$T = 3600s , \alpha = 3 , \beta = 0.1 , r = 5 \times 10^4 , y_d = T_d - T_{f,0} = 250$$

We assume that $0 \leq u(t) \leq 10^{-2}$. Then the set of admissible controls is

$$U_{ad} = \{u \in L^\infty(0, T) \mid 0 \leq u(t) \leq 10^{-2} \text{ a.e.}\}$$

Using the previous algorithm, with $u_0 = 0$, $\lambda = 10^{-6}$, and $\varepsilon = 10^{-5}$, simulations lead to the following figures :

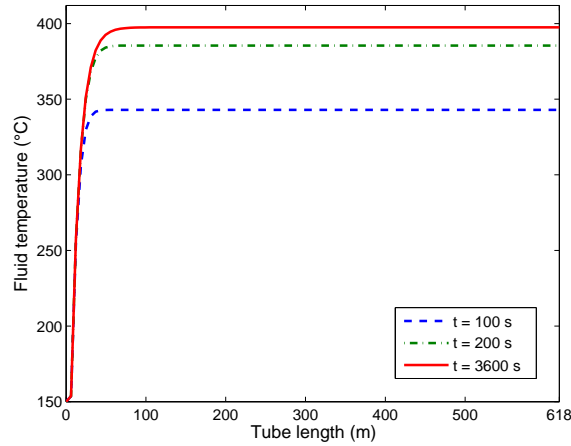


Figure 3. Fluid temperature at times $t = 100s$, $t = 200s$, and $t = 3600s$

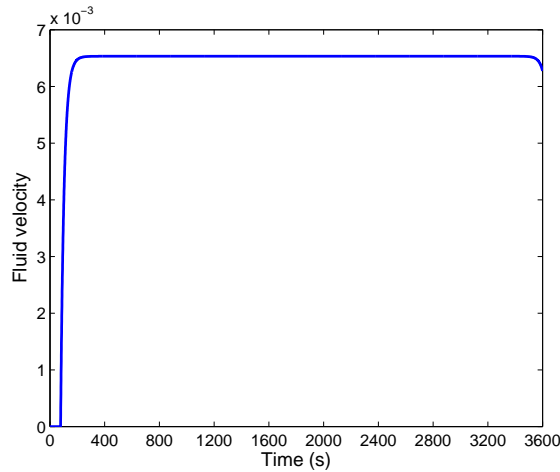


Figure 4. *Optimal fluid velocity*

Fig. 3 depicts the fluid temperature ($^{\circ}\text{C}$) at times $t = 100\text{s}$, $t = 200\text{s}$, and $t = T = 3600\text{s}$, while the corresponding optimal fluid velocity is plotted in Fig. 4. Fig. 3 shows that the fluid temperature gets close to the desired level $T_d = 400^{\circ}\text{C}$ within a short time interval. At the final time $T = 3600\text{s}$, the average fluid temperature is about $\bar{T} \simeq 390^{\circ}\text{C}$. As shown by the above simulations, the optimal fluid velocity, obtained with our approach, drives the system close to the desired temperature profile. This is crucial for the performance of the solar plant.

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