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Pyrolysis of wood impregnated with phosphoric acid for the production of activated carbon: Kinetics and porosity development studies

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Abstract

The pyrolysis of impregnated wood for the production of activated carbon is investigated. Laboratory experiments are performed in a TG for heating rates of 10 $^{\circ}$ C/min and 20 $^{\circ}$ C/min and a mathematical model for the kinetics of the pyrolysis process is developed and validated. The effect of the temperature and of the time duration of the pyrolysis process on the specific surface of the activated carbon is examined on the basis of experiments conducted in a crossed bed reactor. Results indicate that the temperature and the residence time in the pyrolysis reactor may be optimised. Indeed, it is found that the maximum specific surface of the end product is obtained for pyrolysis processes conducted at a temperature of 400 $^{\circ}$ C for a time period of 1 h.

Keywords: Wood; Activated carbon; Phosphoric acid; Pyrolysis; Thermogravimetric analysis; Crossed bed reactor

1. Introduction

Activated carbons are used in many industrial applications, such as water treatment, separation of gases, refrigeration [1] and gas storage [2,3]. Activated carbons are usually produced from carbon-based substances, such as wood and crop residues. The substance is either processed physically or chemically. In the physical activation process, the carbon-based substance is first pyrolysed and then activated under water vapour or carbon dioxide atmosphere in order to increase its specific surface over $1000 \text{ m}^2/\text{g}$. On the other hand, for the chemical activation process, the precursor is first impregnated with a chemical agent before it is pyrolysed. The produced char must then be thoroughly washed in order to rid it from residual impurities.

In the present work, the pyrolysis of wood impregnated with phosphoric acid is examined. The objective of the study is twofold. First, a mathematical model for the pyrolysis process is proposed and validated with experimental data. Second, laboratory experiments are carried out in a crossed bed reactor in order to study the effect of the residence time and of the pyrolysis temperature on the specific surface area of the produced activated carbons.

2. Experimental procedure

Pine wood is the material under investigation here. Prior to their analysis, the wood samples are ground to particles less than 1 mm in diameter. Their content analysis is summarized in Table 1.

The moisture (air at $105 \,^{\circ}$ C), the volatiles (pyrolysis in nitrogen at 900 $\,^{\circ}$ C) and the ashes content (combustion at 815 $\,^{\circ}$ C) were determined in accordance with the NF-M03-002, NF-M03-003 and NF-M03-004 standard norms, respectively, while the ultimate analysis was carried out using a NA 2100 Carlo Erba analyser. To study the kinetics of pyrolysis, the wood samples were soaked in phosphoric acid (85%) for several days. The phosphoric acid to wood ratio, i.e., the ratio of the mass of acid to the mass of wood was maintained at 1.5. This ratio was retained as it ensures complete soaking of the precursor [5].

Next, thermogravimetric analyses were conducted to determine the kinetics parameters. Mass samples from

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Table 1 Wood analysis

Proximate analysis (w	rt.% basis)	Ultimate analysis (wt.%)		
Moisture	7.74	Carbon	46.18	
Ashes	0.45	Hydrogen	5.86	
Volatile matter	78.09	Nitrogen	0.44	
Fixed carbon ^a	13.72	Oxygen ^a	47.52	

^a Calculated by difference.

10 mg to 20 mg were pyrolysed in a nitrogen atmosphere and weighted with a TGA-DSC 111 SETARAM thermal balance.

The effect of the operating conditions on the porosity of the soaked wood was investigated using a crossed bed reactor (Fig. 1). Each sample, 24 mm in diameter and 22 mm in height, was encapsulated in a quartz container with sintered glass at the bottom. The reactor and the external quartz tube were preheated without the internal quartz tube. The sample was then inserted in the internal quartz tube and placed inside the external quartz tube. After a heating period varying from 6 min to 15 min, the pyrolysis was carried out at a constant temperature ranging between 250 °C and 600 °C. Afterwards, the sample was thoroughly washed in hot water for 72 h and dried at 105 °C for 24 additional hours. Finally, the porosity of the activated carbon was determined with a Micromeritics ASAP 2010 that uses liquid nitrogen.

3. Results and discussion

3.1. Experiments

Experiments were carried out for two different heating rates. In experiment #1, the heating rate was set at 10 $^{\circ}$ C/min while for experiment #2 it was set at 20 $^{\circ}$ C/min. In both cases, the final steady state temperature is 800 $^{\circ}$ C. Fig. 2 illustrates the



Fig. 1. Vertical quartz reactor with crossed bed. (1) Electrical furnace, (2) external quartz tube, (3) internal quartz tube, (4) sintered quartz and (5) sample.

time evolution of the samples for both experiments. Examination of these figures clearly indicates two main peaks in the mass loss. The temperature at which these peaks occur is dependent upon the heating rate. The first peak arises at a temperature between 150 °C and 200 °C. It results from the drying and the pyrolysis of the sample. Indeed, for wood impregnated with phosphoric acid, light gases, such as carbon monoxide, carbon dioxide and methane are released at a relatively low temperature (~100 °C) [5]. The second peak, which is observed at a much higher temperature (~700 °C), exemplifies the chemical conversion of phosphoric acid and of P₂O₅. This peak cannot be attributed to the pyrolysis of wood since the thermal degradation of pine wood is terminated at a temperature of 380 °C [6].

3.2. Modeling

Due to its complexity, the kinetics of the pyrolysis process of wood is often modeled as a series of simple chemical reactions [7]. For instance, Turner et al. [8] have developed a model that rests on three primary reactions for the char, the tar and the gas, respectively, and secondary reactions for the polymerization of tar into char and for the cracking of tar. On the other hand, Koufopanos et al. [9] have proposed to model the pyrolysis of wood as the sum of the pyrolysis of its main components, i.e., cellulose, hemicellulose and lignin. Their model could not, however, be easily transposed to the present case since the kinetics of reaction for the pyrolysis process of impregnated wood with phosphoric acid is not fully understood. In fact, to the authors' knowledge, only one study has been reported in the open literature on the modeling of the pyrolysis of lignocellulosic materials activated with phosphoric acid [4]. When applied to the pyrolysis of the wood impregnated with phosphoric acid, the model leads to the following reaction scheme:

$$Wood + H_3PO_4 \rightarrow WP + H_2O \tag{1}$$

$$H_2O(liquid) \rightarrow H_2O(gas)$$
 (2)

$$H_3PO_4 \rightarrow \frac{1}{2}(P_2O_5 + 3H_2O)$$
 (3)

$$P_2O_5(\text{liquid}) \to P_2O_5(\text{gas}) \tag{4}$$

$$WP \to \alpha char + (1 - \alpha) volatiles$$
(5)

$$Char \rightarrow gas$$
 (6)

Eq. (1) represents the reaction between wood and phosphoric acid. According to Montané et al. [4], this reaction occurs at room temperature and is completed within an hour. In fact, phosphoric acid reacts as soon as it is mixed with wood. The reaction does not lead however to a loss of mass. ¹³C NMR analyses of oak impregnated with phosphoric acid have shown that there are detectable changes in the composition of wood biopolymers and in the dimension of the wood matrix at a temperature of 50 °C [5].

Eq. (2) is the evaporation of water contained in the sample. Eq. (3) exemplifies the chemical transformation of phosphoric



Fig. 2. TG and DTG curves for experiments at 10 °C/min (a-b) and 20 °C/min (c-d).

acid into P_2O_5 via water desorption. As the temperature increases, phosphoric acid is converted to several species, such as pyrophosphoric acid ($H_4P_2O_7$) and polyphosphoric acid ($H_{n+2}P_nO_{3n+1}$) by condensation and dehydration and eventually P_2O_5 [4,10]. As a result, reaction (2) is a simplified formulation of a series of more complex chemical reactions.

Eq. (4) stands for the evaporation of P_2O_5 . This component vaporizes at a temperature between 580 °C and 585 °C (second peak observed near 700 °C in the DTG curves of Fig. 2) [11].

Eq. (5) illustrates the pyrolysis of the wood–phosphoric acid complex WP into char and volatiles. Finally, the release of light gases from char is taken into account by Eq. (6).

The first order rate equations for the pyrolysis of impregnated wood with phosphoric acid may then be stated as follows:

$$\frac{dy_{H_2O}}{dt} = -k_2 \times y_{H_2O} + \frac{3}{2} \times k_3 \frac{MW_{H_2O}}{MW_{H_3PO_4}} \times y_{H_3PO_4}$$
(7)

$$\frac{\mathrm{d}y_{\mathrm{H_3PO_4}}}{\mathrm{d}t} = -k_3 \times y_{\mathrm{H_3PO_4}} \tag{8}$$

$$\frac{\mathrm{d}y_{\mathrm{P}_{2}\mathrm{O}_{5}}}{\mathrm{d}t} = -k_{4} \times y_{\mathrm{P}_{2}\mathrm{O}_{5}} + \frac{1}{2} \times k_{3} \frac{\mathrm{MW}_{\mathrm{P}_{2}\mathrm{O}_{5}}}{\mathrm{MW}_{\mathrm{H}_{3}\mathrm{PO}_{4}}} \times y_{\mathrm{H}_{3}\mathrm{PO}_{4}} \tag{9}$$

$$\frac{\mathrm{d}y_{\mathrm{WP}}}{\mathrm{d}t} = -k_5 \times y_{\mathrm{WP}} \tag{10}$$

$$\frac{\mathrm{d}y_{\mathrm{char}}}{\mathrm{d}t} = \beta \times k_5 \times y_{\mathrm{WP}} - k_6 \times y_{\mathrm{char}} \tag{11}$$

$$y = y_{H_2O} + y_{H_3PO_4} + y_{P_2O_5} + y_{WP} + y_{char}$$
(12)

with

$$\beta = \alpha \frac{MW_{char}}{MW_{WP}}$$
(13)

and

$$k_i = A0_i \times \exp\left(-\frac{E_i}{\mathrm{RT}}\right) \tag{14}$$

 y_i is the normalized mass of species *i* and MW_i is its molar mass. The initial mass fractions for each species were estimated from the moisture content of the wood and the aqueous solution of phosphoric acid. When a wood sample is soaked into phosphoric acid, a fraction β' of phosphoric anhydrous binds with wood to form a wood-phosphoric acid complex WP. The remaining fraction $1 - \beta'$ represents the excess of phosphoric acid. The initial mass of the complex WP is then estimated by adding the mass of wood to the mass of bound acid that is $\beta' \times$ mass of anhydrous H₃PO₄. Moreover, the total mass of water is the sum of the moisture content of the wood to that of the water resulting from the chemical reaction with the acid. Therefore, the initial mass fractions for the rate Eqs. (7), (8) and (10) are, respectively,

$$y_{\rm H_2O,0} = \frac{\text{mass of water} + \text{mass of moisture}}{\text{total mass of the sample}}$$
(15)

$$y_{\rm H_3PO_4,0} = \frac{(1-\beta') \times \text{mass of anhydrous H}_3\rm{PO}_4}{\text{total mass of the sample}}$$
(16)

$$y_{WP,0} = \frac{\text{mass of dry wood} + \beta' \times \text{mass of anhydrous } H_3PO_4}{\text{total mass of the sample}}$$
(17)

Ten Arrhenius parameters ($A0_i$ and E_i) and two additional constants β and β' were estimated from a least square minimization procedure between the measurements and the predictions, i.e.,

$$OF = \sum_{i=1}^{p} \sum_{j=1}^{n} (y_{ij}^{cal} - y_{ij}^{exp})^{2}$$
(18)

p is the number of performed experiments and *n* is the number of data retained for the calculations. In the present study, p = 2 and n = 88.

As an example, Fig. 3 shows that the measured and the predicted time variation of the mass fractions for both heating rates are in excellent agreement. The corresponding optimal parameters are summarized in Table 2.

In these experiments, the activation energy for the drying process (Eq. (2)) was estimated at 30.8 kJ/mol, a value comparable to that found for the drying of wood, 26 kJ/mol [12] and for the drying of lignin, 24 kJ/mol [4].

The activation energy for the transformation of phosphoric acid into P_2O_5 (Eq. (3)) was measured at 71.5 kJ/mol. This value is similar to that reported in the kinetic modeling of lignin impregnated with phosphoric acid [4]. To the authors' knowledge, no other data for the activation energy of lignocellulosic materials impregnated with phosphoric acid are available in the open literature.

The activation energy for the evaporation of P_2O_5 (Eq. (4)) was determined at 102.5 kJ/mol and that for the pyrolysis of the complex WP at 32.8 kJ/mol (Eq. (5)). The latter is slightly less than that reported for the pyrolysis of non impregnated wood which, in general, ranges from 56 kJ/mol to 173 kJ/mol [6]. Finally, the activation energy found for the release of light gas (Eq. (6)) was 61.5 kJ/mol.

The numerical predictions reported in Fig. 3 also reveal the time evolution of the different chemical species during pyrolysis. It is seen that the drying of the wood sample is



Fig. 3. Comparison between experimental TG curve and predicted one.

completed at a temperature of roughly 230 °C while the pyrolysis of the complex WP is over when the temperature of the reactor reaches 400 °C. The pyrolysis of phosphoric acid starts at approximately 300 °C and continues for temperatures up to 700 °C. It is also observed that the effect of the release of light gases from char (Eq. (6)) on the evolution of the char mass fraction is insignificant.

3.3. Porosity and specific surface

Aside from the chemical transformations that take place during the pyrolysis process, the wood-phosphoric acid complex WP also undergoes morphological as well as dimensional changes. Two of the most influential textural parameters that characterize activated carbon are its porosity

Table 2 Optimal values for the parameters

Reaction	$A0_i (s^{-1})$	E_i (kJ/mol)	β	eta'	Minimum OF
(2)	236×10^{-1}	30.8	0.65	0.23	1.389×10^{-2}
(3)	$614 imes 10^{-1}$	71.5			
(4)	6673×10^{-1}	102.5			
(5)	553×10^{-2}	32.8			
(6)	824×10^{-3}	61.5			



Fig. 4. Specific surface area vs. temperature.



Fig. 5. Specific surface area vs. time.

and its specific surface [5]. These properties are dependent on the phosphoric acid to wood ratio, the activation temperature and the time duration of the pyrolysis process [5,10,13–17].

In the present study, the effect of the temperature and of the time duration of the pyrolysis process was examined.

Fig. 4 exemplifies the effect of the temperature on the specific surface of the activated carbon resulting from the pyrolysis of impregnated wood. In these experiments, the activation time period was fixed at 1 h. It is seen that a maximum is reached at a temperature of 400 °C. Other studies available in the literature reported maxima in the specific surface for operating temperatures ranging from 350 °C to 500 °C for lignocellulosic materials and bituminous coal [5,10,13–17].

The trend observed in Fig. 4 may be explained by the fact that phosphoric acid acts as a catalyst for breaking down large molecules, such as cellulose, hemicellulose and lignin in the wood. The acid also combines with organic matter yielding bridges between phosphates and polyphosphates [5,10]. As a result, the mechanical properties of the material are strengthened and contraction is hindered. For temperatures above 450 $^{\circ}$ C, however, these bindings break down and consequently the material contracts and its porosity diminishes [5].

The effect of the time duration of the pyrolysis process on the resulting porosity of the activated carbon was also examined. The results for the time evolution of the specific surface for three different process temperatures, i.e., $250 \,^{\circ}$ C, $450 \,^{\circ}$ C and $600 \,^{\circ}$ C, are depicted in Fig. 5. It is seen that the maximum porosity is obtained for a process temperature of $450 \,^{\circ}$ C and a residence time of 30 min. For time periods above 30 min, the results indicate that the porosity diminishes slightly. From an industrial point of view, these findings are of the utmost importance as they suggest that pyrolysis reactors may be operated in such a way as to simultaneously minimize their energy consumption and maximize the quality of the end product.

4. Conclusion

The kinetics for the pyrolysis of impregnated wood for the production of activated carbon was investigated. Based on laboratory experiments performed with a thermogravimetric apparatus, a mathematical model for the kinetics of the pyrolysis process was proposed and validated.

The effect of the temperature and of the time duration of the pyrolysis process on the specific surface of the activated carbon was then investigated experimentally, using a crossed bed reactor. Results indicate that the temperature and the residence time in the pyrolysis reactor may be optimised. It was found that the maximum specific surface of the produced activated carbon is obtained for pyrolysis processes conducted at a temperature of 400 °C and for a time period of 1 h.

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