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Performance Optimization of a Solar-Driven Multi-Step Irreversible Brayton Cycle Based on a Multi-Objective Genetic Algorithm

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Abstract — An applicable approach for a multi-step regenerative irreversible Brayton cycle on the basis of thermodynamics and optimization of thermal efficiency and normalized output power is presented in this work. In the present study, thermodynamic analysis and a NSGA II algorithm are coupled to determine the optimum values of thermal efficiency and normalized power output for a Brayton cycle system. Moreover, three well-known decision-making methods are employed to indicate definite answers from the outputs gained from the aforementioned approach. Finally, with the aim of error analysis, the values of the average and maximum error of the results are also calculated.

Résumé — Optimisation des performances d'un cycle de Brayton irréversible solarisé à compressions et détente multiples sur la base d'un algorithme génétique multi-objectif — Une approche applicable à un cycle de Brayton irréversible régénératif à compressions et détente multiples, sur la base de la thermodynamique, de l'optimisation du rendement thermique et de la puissance de sortie normalisée, est présentée dans cet article. Dans la présente étude, l'analyse thermodynamique et un algorithme NSGA II sont couplés, afin de déterminer les valeurs optimales de rendement thermique et de puissance de sortie normalisée pour un système à cycle de Brayton. En outre, trois méthodes de prise de décision bien connues sont utilisées pour indiquer des réponses définies à partir des résultats obtenus à partir de l'approche mentionnée ci-dessus. Enfin, afin d'analyser les éventuelles erreurs, les valeurs de la moyenne et de l'erreur maximale des résultats sont également calculées.

NOMENCLATURE

A_a	Aperture area
A_r	Absorber area
a_c	Isentropic compressor pressure ratio
C_w	Constant heat capacity rate of the working fluid
C	Concentration ratio
C_i	Internal conductance of the power plant
C_v	Constant volume specific heat
Cl_i	Decision index in TOPSIS approach
d	Deviation index
d_{i+}	Deviation or distance of i th outcome from ideal outcome
d_{i-}	Deviation or distance of i th outcome from non-ideal outcome
G	The solar irradiance (W/m^2)
P'	The net output power of the cycle
p	Pressure
Δp	Pressure loss
P	Normalized power
\dot{Q}	Heat transfer rate
N_t	Number of turbines
N_c	Number of compressors
r_p	Overall compression ratio
T	Temperature
U_L	Overall effective coefficient
i	i th objective
j	j th solution
X	Vector of decision parameters

Greek letter

ε	Irreversibilities
ε_r	Effectiveness of the regenerator
ε_c	Isentropic efficiency of the compressors
ε_L	Isentropic efficiency of the turbines
ε_H	Irreversibilities bring in the mixing of the working fluid with the heat reservoir at temperature T_H
ε_L	Irreversibilities bring in the mixing of the working fluid with the heat reservoir at temperature T_L
η	Efficiency
γ	Adiabatic coefficient
μ	Fuzzy membership function
ξ	Heat leakage throughout the plant to the surroundings
τ	Heat source temperature ratio

Subscripts

H	Heat source
L	Heat sink
$1-4$	The process states

INTRODUCTION

Nowadays, due to strategies minimizing the environmental difficulties and energy savings, solar-driven heat engines have attracted high attentions. Also, different heat engine cycles coupled with solar collectors have been investigated. In these researches, solar driven Carnot, Stirling, Ericsson and Braysson cycles were studied [1-16]. Academically, to enhance the performance of simple Brayton cycles, many modifications have been carried out to develop the system performance which consist of regeneration, isothermal heat addition, intercooler compression and reheat expansion [17-28]. Among the various objective functions that have been investigated for Brayton-based heat engines are power, efficiency [29-32], power density [33, 34], different ecological criteria [35, 36], thermoeconomic functions [37, 38] and other functions which have a compromise with output power and energy consumption [39]. In any case, as discussed by Chen [40] and Arias-Hernandez *et al.* [41] and Dong *et al.* [42], the optimal effectiveness of a heat engine is located between the maximum output power conditions and the maximum efficiency situation. As a special case, we ought to analyze the maximum efficiency regimes and maximum power of the given multi-step gas turbine.

The traditional single objective optimizations suffer from defect, since these optimize the systems based on only one criterion expressed by the objective functions. However, other aspects of design for perfect system planning are missed and those criteria might become worse than the previous optimizations. Therefore, attention to multi-objective optimizations has been paid by the majority of researchers in designing of thermal systems [43-55]. Firstly, Evolutionary Algorithms (EA) were evolved and employed in the previous decades to unravel random issues of this generic type [43]. A rational further step to a multi-objective issue is to assay a set of routes, which assures the objectives at a nice degree without being prevailed by any other routes [44]. Multi-objective optimization issues represent a great number of routes, and thus should be named as a Pareto frontier, whose assessed vectors illustrate the prior trade-offs' outcomes.

In the current work, a multi-step solar-driven Brayton engine was optimized using an evolutionary algorithm,

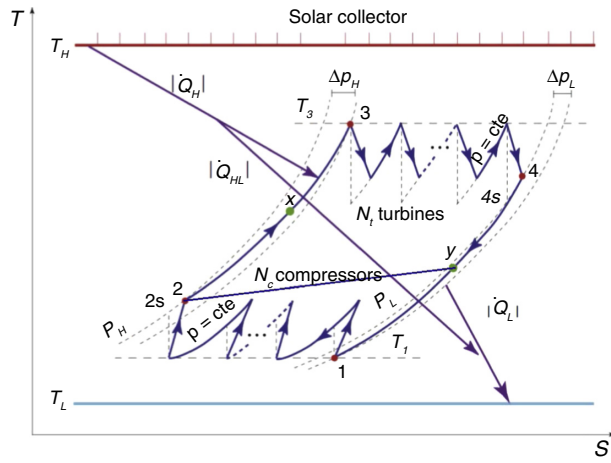


Figure 1
T-S diagram of the thermodynamic cycle [56].

while thermal efficiency and the normalized output power in non-dimensional forms are presumed as the objectives of the optimization. For this solution, the operating parameters of thermal engine which includes the engine temperature ratio, irreversibilities (from coupling the working fluid with the heat source and heat sink), and regenerator effectiveness were considered as the decision variables.

1 THEORETICAL MODEL

The T-S diagram of the suggested approach and the layout carton for a Brayton heat engine with irreversible solar-driven multi-step are demonstrated in Figure 1, and the scheme of the plant which under studied here is depicted in Figure 2, [56]. Throughout the Brayton heat engine, from the solar collector at temperature T_H it receives a net heat rate \dot{Q}_H and asserts at temperature T_L a net heat rate \dot{Q}_L to the surroundings. Moreover, the linear behavior of heat leakage \dot{Q}_{HL} regarding the heat source at T_H to the heat sink at T_L is presumed in the current study [6].

According to Duffie and Beckman [57] and Zhang *et al.* [58], a concentrating collector is considered where heat losses at intermediate and low temperatures are mainly affiliated with convection and conduction; however, at high sufficient temperatures, heat losses due to radiation are prevailing. Thanks to this consideration, in our approach, the effective energy attributed to the heat engine, \dot{Q}_H , and the solar collector's efficiency, η_s , can be formulated as following as [56, 58, 59]:

$$\dot{Q}_H = \eta_0 G A_a - U_L A_r T_L (\tau - 1) \quad (1)$$

$$\eta_s = \frac{\dot{Q}_H}{G A_a} = \eta_0 (1 - (\tau - 1) M) \quad (2)$$

In the aforementioned formulas, $\tau = T_H/T_L$ stands for the temperature ratio of the heat reservoirs; G denotes the solar irradiance; A_r and A_a represent the absorber and aperture areas, correspondingly; $C = A_a/A_r$ denotes the concentration ratio; η_0 represents optical efficiency (the efficient transmittance absorptance product); and M is formulated as $M = U_L T_L / (\eta_0 G C)$, where U_L stands for an accounted overall effective coefficient for losses due to radiation in terms of linear heat loss [57, 58]. The fundamental formulations of the approach are as follows [30, 56, 58, 59]:

$$\begin{aligned} \dot{Q}_H = C_w T_L \left(\varepsilon_H \left(\tau - Z_c (1 - \varepsilon_r) \frac{T_1}{T_L} - \varepsilon_r Z_t \frac{T_3}{T_L} \right) \right. \\ \left. + \varepsilon_t (N_t - 1) \left(1 - a_t^{\frac{1}{N_t}} \right) \frac{T_3}{T_L} + \xi (\tau - 1) \right) \quad (3) \end{aligned}$$

$$\begin{aligned} \dot{Q}_L = C_w T_L \left(\varepsilon_L \left(-1 - Z_t (1 - \varepsilon_r) \frac{T_3}{T_L} + \varepsilon_r Z_c \frac{T_1}{T_L} \right) \right. \\ \left. + \frac{1}{\varepsilon_c} (N_c - 1) \left(a_c^{\frac{1}{N_c}} - 1 \right) \frac{T_1}{T_L} + \xi (\tau - 1) \right) \quad (4) \end{aligned}$$

$$Z_c = 1 + \frac{a_c^{\frac{1}{N_c}} - 1}{\varepsilon_c} \quad (5)$$

$$Z_t = 1 - \varepsilon_t \left(1 - a_t^{\frac{1}{N_t}} \right) \quad (6)$$

$$a_t = a_c \rho_H \rho_L \quad (7)$$

$$\frac{T_1}{T_L} = \frac{\varepsilon_L + (1 - \varepsilon_L)(1 - \varepsilon_r) Z_t \frac{T_3}{T_L}}{1 - (1 - \varepsilon_L) \varepsilon_r Z_c} \quad (8)$$

$$\rho_H = \left(\frac{p_3}{p_2} \right)^{\frac{\gamma-1}{\gamma}} = \left(\frac{p_H - \Delta p_H}{p_H} \right)^{\frac{\gamma-1}{\gamma}} \quad (9)$$

$$\rho_L = \left(\frac{p_1}{p_4} \right)^{\frac{\gamma-1}{\gamma}} = \left(\frac{p_L - \Delta p_L}{p_L} \right)^{\frac{\gamma-1}{\gamma}} \quad (10)$$

$$\begin{aligned} \frac{T_3}{T_L} = \\ \frac{\tau \varepsilon_H (1 - (1 - \varepsilon_L) \varepsilon_r Z_c) + \varepsilon_L (1 - \varepsilon_H) (1 - \varepsilon_r) Z_c}{(1 - (1 - \varepsilon_L) \varepsilon_r Z_c) (1 - (1 - \varepsilon_H) \varepsilon_r Z_t) - (1 - \varepsilon_H) (1 - \varepsilon_L) (1 - \varepsilon_r)^2 Z_t Z_c} \quad (11) \end{aligned}$$

where:

C_w is the working fluid's constant heat capacity rate,

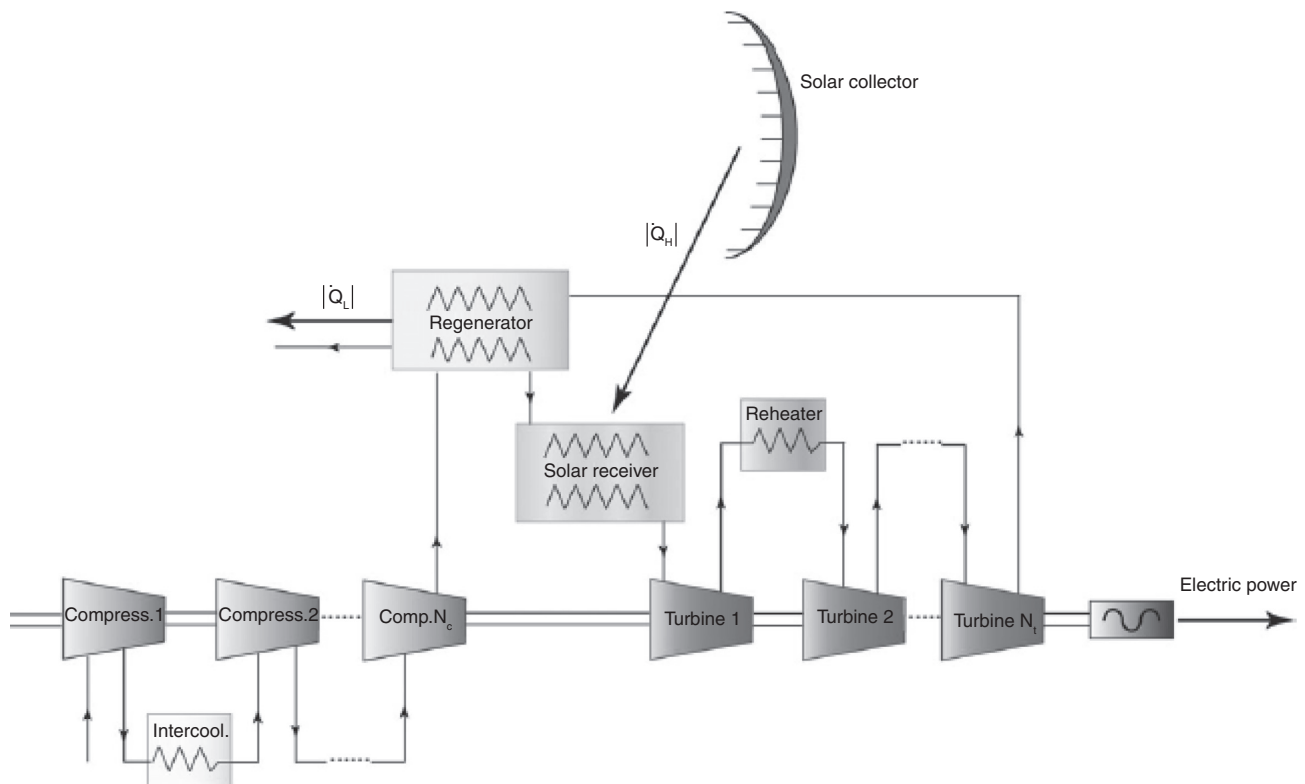


Figure 2

Scheme of the considered solar-driven Brayton plant [56].

$$a_c = \frac{T_{2s}}{T_1} = r_p^{\frac{\gamma-1}{\gamma}}$$

is the pressure ratio of the isentropic compressor and $r_p = p_2/p_1$ represents the overall compression ratio. $\dot{Q}_{HL} = C_i(T_H - T_L) = C_i T_L(\tau - 1)$ represents the leakage of heat during the heat reservoirs throughout the system. Furthermore, it can be formulated as $\xi(\tau - 1)$, in which $\xi = C_i/C_w$ stands for the internal conductance ratio of the plant in terms of the working fluid and C_i represents the power plant internal conductance [6, 35, 56, 59]. Equations (3) and (4) express the Brayton heat engine efficiency for heat release and heat input, correspondingly

$$\eta_h = \frac{P'}{\dot{Q}_H} = \frac{\dot{Q}_H - \dot{Q}_L}{\dot{Q}_H} = 1 - \frac{\dot{Q}_L}{\dot{Q}_H} \quad (12)$$

in which P' denotes the net output power of the cycle.

The overall solar-driven plant efficiency:

$$\eta = \frac{P'}{GA_a}$$

can be formulated as the product of the effectiveness of the Brayton heat engine with multi-step and of the solar collector [30, 56, 59]:

$$\eta = \frac{P'}{GA_a} = \frac{P'}{\dot{Q}_H} \frac{\dot{Q}_H}{GA_a} = \eta_s \eta_h \quad (13)$$

The normalized power is obtained by [30]:

$$P = \frac{P'}{C_w T_L} \quad (14)$$

2 MULTI-OBJECTIVE OPTIMIZATION WITH EVOLUTIONARY ALGORITHMS

2.1 Evolutionary Algorithms

John Holland was a scientist who evolved and proposed a Genetic Algorithm (GA) in the 1960s inspired by natural adaption from Darwin's theory and imported it into a computer program for a stochastic optimization process [43]. Fundamentally, genetic algorithms employ

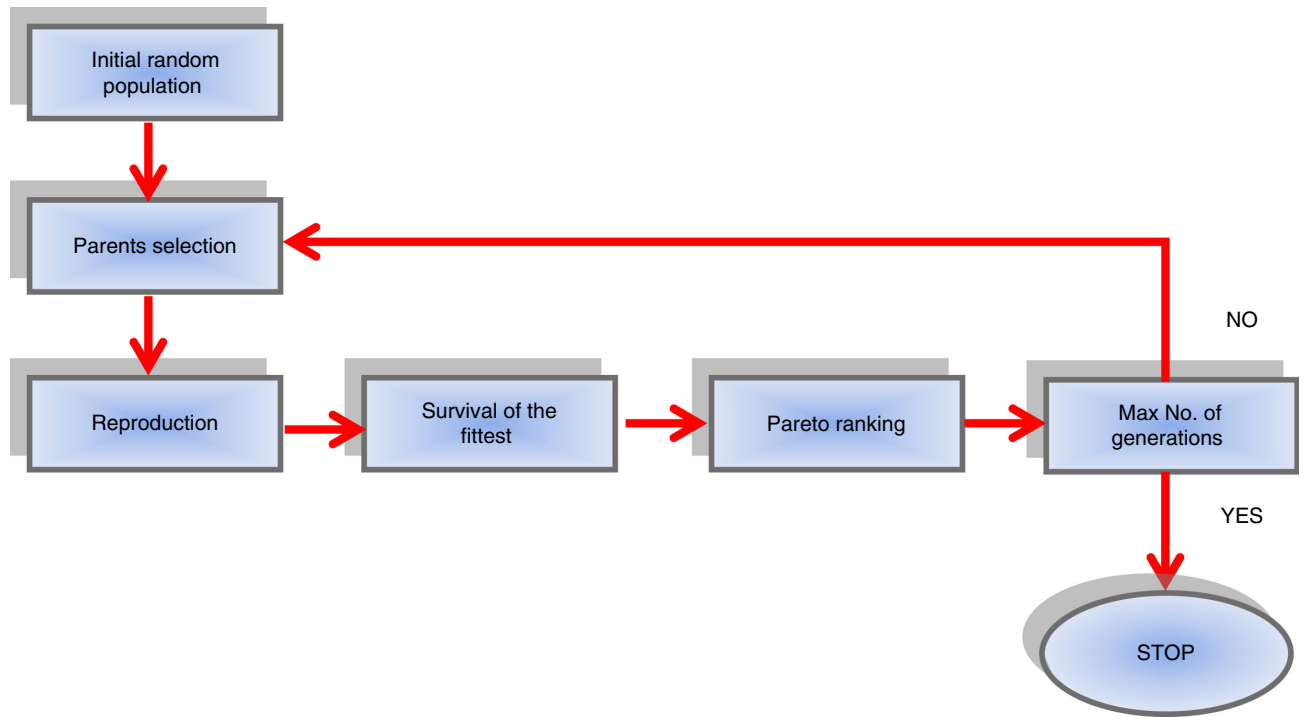


Figure 3

Scheme for the multi-objective evolutionary algorithm used in the present study [46, 47, 60].

stochastic and iterative search strategy to determine an optimum route and mimic a reduced maximum of biological evolution (Fig. 3). In the current research, a GA as a split of evolutionary algorithm is utilized to determine the Pareto frontier. As noted previously, GA is a robust and effective tool for optimization of nonlinear issues [44, 45]. The optimality of Pareto is an important sense to specify a ranking between the routes of a multi-objective optimization issue, in order to indicate which solution is prior to other possible solutions [45]. In this communication, a NSGA-II approach is executed as a multi-objective optimization algorithm to figure out the Pareto frontier by utilizing a GA [45, 48, 60-62].

2.2 Objective Functions, Decision Variables and Constraints

Two objective functions for the current research are thermal efficiency (η) and the normalized power output (P), which are denoted by Equations (13, 14), correspondingly.

Throughout this research, four decision variables including temperature ratio ($x = T_3/T_L$), engine temperature ratio (τ), irreversibilities (ε) and regenerator

effectiveness (ε_r) were considered. The objective functions are optimized regard to the below restrictions on the decision variables:

$$2.25 \leq \frac{T_3}{T_L} \leq 3 \quad (15)$$

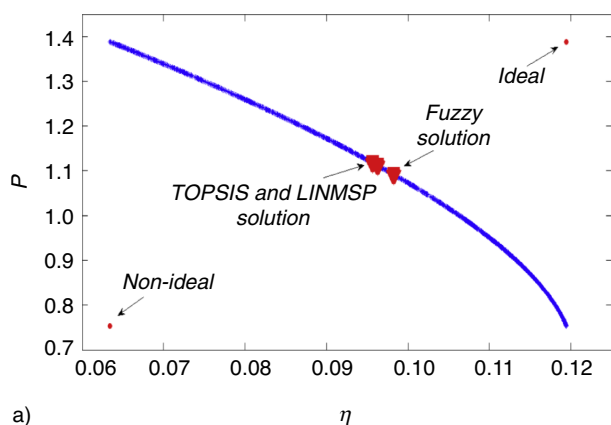
$$3 \leq \tau \leq 4 \quad (16)$$

$$0.7 \leq \varepsilon \leq 0.9 \quad (17)$$

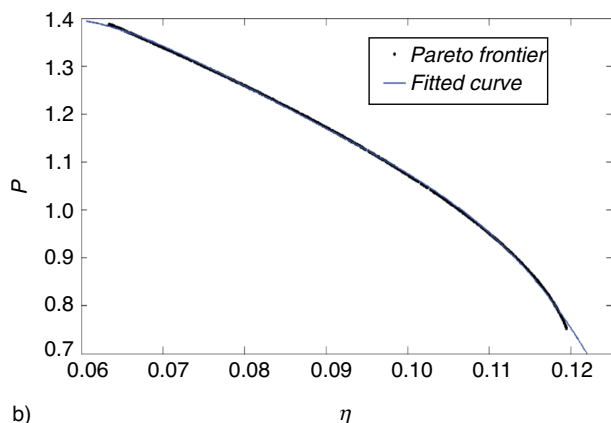
$$0.8 \leq \varepsilon_r \leq 1 \quad (18)$$

3 DECISION-MAKING IN THE MULTI-OBJECTIVE OPTIMIZATION

Throughout multi-objective subjects, the algorithm of decision-making to elect the best route from among other possible outcomes is needed. Many procedures can be applied to make decision for taking the ultimate route from the Pareto frontier. In the first step, the scales and dimensions of the objective region have to be incorporated thanks to the eventuality of various dimensions that may exist in the multi-objective optimization



a)



b)

Figure 4

a) The original Pareto optimal curve; b) the optimal curve with curve fit.

process. In fact, the objective vectors have to be dimensionless prior to the decision-making algorithm. Different approaches to dimensionless utilization in decision-making include linear, Euclidean and fuzzy. Detailed descriptions regarding these methods of non-dimensioning were reported in [48]. In addition, more details of the decision-making approaches addressed are found in the literature, such as [46-49, 60].

4 RESULTS AND DISCUSSION

The thermal efficiency and the normalized output power of an irreversible Brayton regenerative cycle were maximized. These objectives are optimized concurrently executing a type of multi-objective evolutionary algorithms called NSGA-II. The process of optimization is performed by executing the objective functions expressed by Equations (13, 14) beside the limitations which are stated in Equations (15-18). Figure 4a depicts the Pareto frontier in the presumed objectives' region

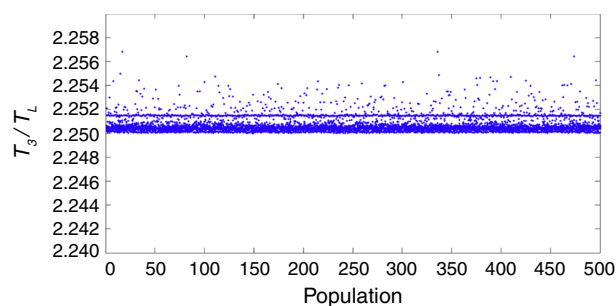


Figure 5

Scatter distribution of T_3/T_L with population in Pareto frontier.

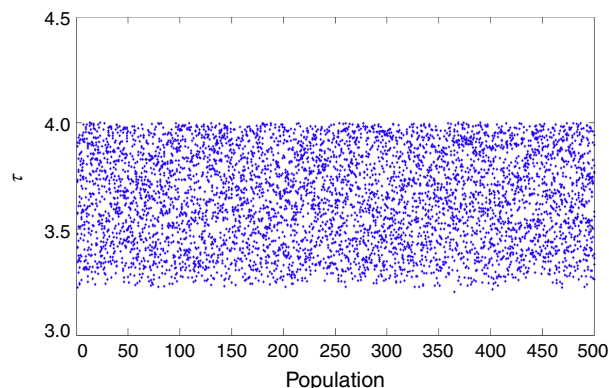


Figure 6

Scatter distribution of τ with population in Pareto frontier.

that gained from the scenario. Moreover, optimum solutions which are gained by performing LINMAP, Fuzzy Bellman-Zadeh, and TOPSIS decision-makers are demonstrated in the aforementioned figure. According to Figure 4a, the points obtained by LINMAP and TOPSIS have an approaching trend. Also it is shown that the optimal value of P varies from 0.75 to 1.4 and the optimal value of η is 0.0625 to 0.12. Based on the curve fit obtained depicted in Figure 4b, Equation (19) was developed:

$$P = p_1\eta^4 + p_2\eta^3 + p_3\eta^2 + p_4\eta + p_5 \quad (19)$$

Where η is normalized by mean 0.09689 and std 0.01717 coefficients (with 95% confidence bounds):

$$p_1 = -0.008249$$

$$p_2 = -0.02302$$

$$p_3 = -0.026$$

$$p_4 = -0.166$$

$$p_5 = 1.106$$

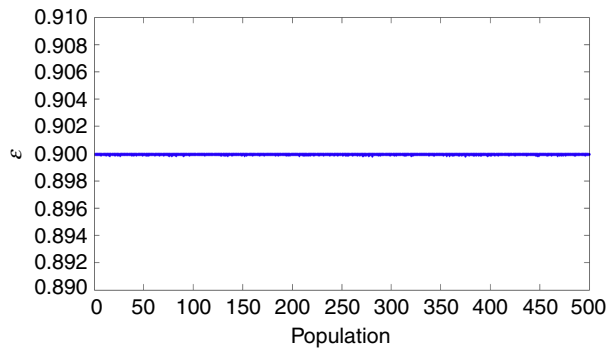


Figure 7
Scatter distribution of ε with population in Pareto frontier.

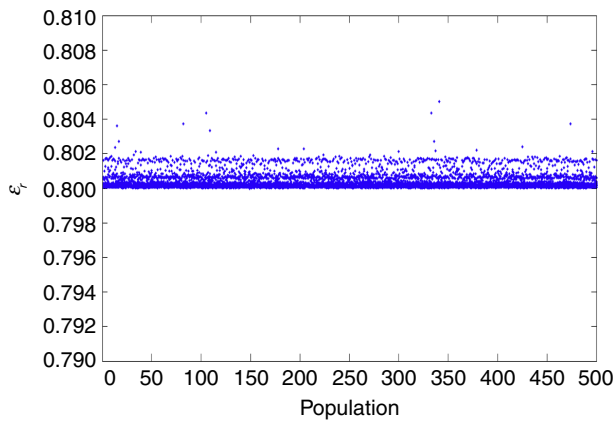


Figure 8
Scatter distribution of ε_r with population in Pareto frontier.

Goodness of fit:

SSE: 0.007218

R^2 : 0.9997

RMSE: 0.003013

Figures 5-8 demonstrate the scattered distribution of the design variables *versus* the population. These figures can provide a better vision of the variation of the decision variables from the Pareto frontier. According to this distribution, it is found that the irreversibilities bring in the mixing of the working fluid with the heat sink and the heat source meets their maximum magnitudes. It displays that increasing the design parameters results in enhancement in both objective functions. Figure 5 depicts the range of variation of $x = T_3/T_L$ for an optimal Pareto front. The distribution of variables for the optimum points on the Pareto front for τ over the population are exhibited in Figure 6 and the range of

τ varied from 3.25 to 4. It can be seen from Figure 7 that the magnitude of ε for an optimal Pareto front is equal to 0.9. As shown in Figure 8, the changes in ε_r for an optimal Pareto front varied from 0.8 to 0.802.

The optimum outcomes for decision variables and objective functions executing TOPSIS, LINMAP and Bellman-Zadeh decision-making approaches are explained in Table 1. Table 1 demonstrates results gained from the aforementioned decision-makers for the solar-driven multi-step irreversible Brayton cycle and outcomes described by Sánchez-Orgaz *et al.* [56, 59]. For better grasp regarding the situation of different outcomes gained here in contrast with the outcome of the single objective-single variable approach [56, 59], a deviation index which determines the deviation of each outcome from the ideal outcome is introduced here:

$$d_+ = \sqrt{(p_n - p_{n,ideal})^2 + (\eta - \eta_{n,ideal})^2} \quad (20)$$

$$d_- = \sqrt{(p_n - p_{n,non-ideal})^2 + (\eta - \eta_{n,non-ideal})^2} \quad (21)$$

$$d = \frac{d_+}{(d_+) + (d_-)} \quad (22)$$

p_n and η_n stand for Euclidian non-dimensionalized normalized output power and thermal efficiency (the indices *ideal* and *non-ideal* denote the relevant amounts of objective functions at the ideal and non-ideal data points, correspondingly). The last column of Table 1 denotes the deviation index (d) for the outcomes gained from each decision-makers. As illustrated in Table 1, the deviation indices of the multi-objective optimization method throughout the current study are 0.4159, 0.4253 and 0.4562 for outcomes that were gained by utilizing the FUZZY, LINMAP and TOPSIS decision-makers, correspondingly. These values are analogous with the relevant value gained previously by performing the single objective-single variable optimization approach [56, 59] where the deviation index is 0.4785. This indicates that the deviation indices of the single objective-single variable optimization are greater than the multi-objective-multi-variable optimization for all decision-makers while the ideal deviation index is zero.

Further, the last column of Table 1 indicates that the FUZZY decision-maker leads to a lower value for deviation index; therefore, throughout the current study, the outcome that is chosen by executing the FUZZY decision-maker is presumed to be an ultimate optimum outcome of the multi-objective-multi-parameter optimization process for the solar-driven multi-step irreversible

TABLE 1
Decision-making of multi-objective optimal solutions

Decision-making method	Decision variables				Objective functions		Deviation index from the ideal solution (d)
	τ	$\frac{T_3}{T_L}$	ε_r	ε	η	P	
Fuzzy	3.695164	2.250287	0.8	0.9	0.095673	1.11791522	0.4159
LINMAP	3.68845	2.250166	0.8	0.9	0.096280	1.11194254	0.4253
TOPSIS	3.666383	2.250066	0.8	0.9	0.098223	1.09212691	0.4562
References [56, 59]	3.6	-	0.8	0.9	0.100000	0.80000000	0.4785
Ideal point	-	-	-	-	0.118000	1.38000000	0.0000
Non-ideal point	-	-	-	-	0.063000	0.75000000	∞

TABLE 2
Error analysis based on the Mean Absolute Percent Error (MAPE) method

Decision-making method	LINMAP		TOPSIS		Fuzzy	
	η	P	η	P	η	P
Max error (%)	1.28	1.16	2.26	2.06	3.18	2.94
Average error (%)	0.55	0.46	1.03	0.90	1.46	1.35

Brayton cycle. It is worth bearing in mind that this is not a universal approach for other cases, so other decision-makers might have superior outcomes.

5 ERROR ANALYSIS

To compare each of the decision-makers and select the most robust one, the Mean Absolute Percentage Error (MAPE) is utilized to indicate the amount of error for the aforementioned decision-makers. To this end, each approach was executed 30 times to gain the ultimate outcome by LINMAP, Bellman-Zadeh and TOPSIS decision-makers. The first rank throughout Table 2 exhibits the Maximum Absolute Average Error (MAAE) of each decision-maker. Besides, the second row of Table 2 reports the MAPE of the decision-makers executed in our study.

CONCLUSIONS

In this study, an analytical model for an irreversible regenerative multi-step Brayton cycle was applied to

determine the normalized power output (P) and the thermal efficiency (η) of the cycle. The thermal efficiency (η) and the normalized power output (P) of the multi-step irreversible Brayton cycle are spotted in parallel throughout the multi-objective optimization process. The heat source to heat sink and regenerator effectiveness (ε_r), temperature ratio (x), engine temperature ratio (τ), and irreversibilities (ε) are presumed to be the design variables. NSGA-II is exploited throughout the multi-criteria optimization process and further, the Pareto optimal frontier throughout the objective space is determined. By performing three rigorous decision-making methods, three different optimum solutions are gained, regarding which the decision making approach was executed. By taking plots of previous works into account, the optimum results gained by the aforementioned decision-making approaches TOPSIS, LINMAP and Fuzzy were compared with a relevant actual one on the basis of the deviations from the ideal state. As can clearly be seen, the lowest deviation in the results refers to the Fuzzy method, which is superior in contrast to the ideal; conversely, greater deviation from the ideal state refers to previous research. These comparisons prove that the results of this optimization are acceptable.

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APPENDIX: DECISION-MAKING IN THE MULTI-OBJECTIVE OPTIMIZATION

To obtain the optimum value of the design parameters during multi-objective optimization in regard to satisfying the termination conditions, decision-making is used. Put another way, decision-making is executed to determine the best solution among all of the other possible solutions. Owing to this fact, different methods and algorithms can be used to make a decision whose solution from the Pareto frontier is better or not. Before tackling the methods of decision-making that was utilized in our study in detail, the scales and dimensions of the objective region have to be incorporated thanks to the eventuality of various dimensions that may exist in the multi-objective optimization process. Meanwhile, the vectors of objectives have to be non-dimensionalized prior to making a decision. For this end, approaches such as fuzzy, Euclidean and linear non-dimensionalization can be carried out throughout the process of decision-making. More explanation is given in the work performed by Ahmadi *et al.* [10].

• Linear non-dimensionalization

F_{ij} represents the matrix of objectives at different data points of the Pareto frontier in which i stands for the index of each aforementioned point on the Pareto frontier and j denotes the index of each objective throughout the space of objectives. Accordingly, a non-dimensionalized objective, F_{ij}^n , can be expressed as follows:

$$F_{ij}^n = \frac{F_{ij}}{\max(F_{ij})} \text{ Maximizing orientation} \quad (\text{A-1a})$$

$$F_{ij}^n = \frac{F_{ij}}{\max(1/F_{ij})} \text{ Minimalizing orientation} \quad (\text{A-1b})$$

• Euclidian non-dimensionalization

Throughout this approach, a non-dimensionalized objective, F_{ij}^n , is formulated as below:

$$F_{ij}^n = \frac{F_{ij}}{\sqrt{\sum_{i=1}^m (F_{ij})^2}} \text{ Minimizing and maximizing orientations} \quad (\text{A-2})$$

• Fuzzy non-dimensionalization

Throughout this approach, a non-dimensionalized objective, F_{ij}^n , is formulated as below [10-12]:

$$F_{ij}^n = \frac{F_{ij} - \min(F_{ij})}{\max(F_{ij}) - \min(F_{ij})} \text{ Maximizing orientations} \quad (\text{A-3a})$$

$$F_{ij}^n = \frac{\max(F_{ij}) - F_{ij}}{\max(F_{ij}) - \min(F_{ij})} \text{ Minimizing orientation} \quad (\text{A-3b})$$

In the current research, the rigorous and efficient types of decision-making algorithms that include TOPSIS, LINMAP and the fuzzy Bellman-Zadeh approach are utilized in order to compare their robustness toward obtaining the most reliable solutions. It is worth bearing in mind that determining the optimum solution from the final optimum solutions which were gained by the aforementioned decision-making methods are on the basis of engineering experience and criteria suggested previously. The Bellman-Zadeh approach carries out fuzzy non-dimensionalization, whereas the LINMAP and TOPSIS approaches utilize Euclidian non-dimensionalization. The next sections demonstrate the details of the above-mentioned algorithms for making decisions through the optimization process.

A.1. Bellman-Zadeh's Decision-Making Method

According to an approach evolved by Bellman and Zadeh (1970), the fuzzy set or fuzzy objective function should be replaced by $F_j(x)$:

$$A_j = \{X, \mu_{A_j}(X)\} \quad X \in L, j = 1, 2, \dots, k \quad (\text{A-4})$$

In which $\mu_{A_j}(X)$ denotes A_j 's membership function [10].

The junction between all of the fuzzy criteria and restrictions in the Bellman and Zadeh approach represents the final decision; meanwhile, it is presented by means of membership function. A fuzzy route D establishing the fuzzy assortments (Eq. 5) is procreated as an outcome of the conjunction $D = \cap_{j=1}^k A_j$ with a membership function:

$$\mu_D(X) = \cap_{j=1}^k \mu_{A_j}(X) = \min_{j=1, \dots, k} \mu_{A_j}(x), \quad X \in L \quad (\text{A-5})$$

By utilizing Equation (3a), it is feasible to gain the outcome verifying the maximum level as follows:

$$\max \mu_D(X) = \max_{X \in L} \min_{j=1, \dots, k} \mu_{A_j}(x) \quad (\text{A-6})$$

$$X^0 = \arg \max_{X \in L} \min_{j=1, \dots, k} \mu_{A_j}(x) \quad (\text{A-7})$$

To gain (Eq. 6), it is necessary to create membership functions $\mu_{A_j(X)}$; $j = 1, \dots, k$, reverberating a level of meeting its “own” optimum by the relevant $F_j(X)$, $X \in L$; $j = 1, \dots, k$. This is contented by the executing of the membership functions [62]. The context of the issue plays an important role in choosing the membership function of objectives and restrictions, whether linear or nonlinear limitation exists. Thanks to this point, one of the feasible fuzzy convolution themes is illustrated as follows [62].

The primary estimation for the X -vector is selected. With the aim of scalar minimization/maximization, the minimum/maximum values for each standard $F_j(X)$ are formed. Outcomes stand for “ideal” data points $\{X_j^0, j = 1, \dots, m\}$.

Consequently, the matrix table $\{T\}$, where the diagonal components are “ideal” data points, is constructed as below:

$$\{T\} = \begin{bmatrix} F_1(X_1^0) & F_2(X_1^0) & \dots & F_n(X_1^0) \\ F_1(X_2^0) & F_2(X_2^0) & \dots & F_n(X_2^0) \\ & & \cdot & \\ & & \cdot & \\ & & \cdot & \\ F_1(X_n^0) & F_2(X_n^0) & \dots & F_n(X_n^0) \end{bmatrix} \quad (\text{A-8})$$

Minimum and maximum limitations for the norms are expressed

$$F_i^{\min} = \min_j F_j(X_j^0), \quad i = 1, \dots, n \quad (\text{A-9a})$$

$$F_i^{\max} = \max_j F_j(X_j^0), \quad i = 1, \dots, n \quad (\text{A-9b})$$

Following membership functions are presumed throughout applying fuzzy technique on the generated results For minimized objective functions:

$$\mu_{F_i}(X) = \begin{cases} 0 & \text{if } F_i(x) > F_i^{\max}, \\ \frac{F_i^{\max} - F_i}{F_i^{\max} - F_i^{\min}} & \text{if } F_i^{\min} < F_i \leq F_i^{\max}, \\ 1 & \text{if } F_i(x) \leq F_i^{\min} \end{cases} \quad (\text{A-10a})$$

For maximized objective functions:

$$\mu_{F_i}(X) = \begin{cases} 1 & \text{if } F_i(x) > F_i^{\max}, \\ \frac{F_i - F_i^{\min}}{F_i^{\max} - F_i^{\min}} & \text{if } F_i^{\min} < F_i \leq F_i^{\max}, \\ 0 & \text{if } F_i(x) \leq F_i^{\min} \end{cases} \quad (\text{A-10b})$$

Limitations of fuzzy are expressed as:

$$G_j(X) \leq G_j^{\max} + d_j, \quad j = 1, 2, \dots, k \quad (\text{A-11})$$

In which d_j stands for a subjective variable that represents an interval between the accessible shift for the bound G_j^{\max} of the j th limitation. Relevant membership functions are formulated as below [10, 11]:

$$\mu_{G_i}(X) = \begin{cases} 0 & \text{if } G_i(x) > G_i^{\max} \\ 1 - \frac{G_i(x) - G_j^{\max}}{d_j} & \text{if } G_i^{\max} < G_i(X) \leq G_i^{\max} + d_j \\ 1 & \text{if } G_i(x) \leq G_i^{\max} \end{cases} \quad (\text{A-12})$$

As noted previously, the junction between all of fuzzy criteria and restrictions represents the final decision, whereas it is illustrated with the aim of membership function. This issue is lessened to the standard nonlinear programming issues: to determine such values of X and k which maximize k regarding:

$$\begin{aligned} \lambda &\leq \mu_{F_i}, \quad i = 1, 2, \dots, n \\ \lambda &\leq \mu_{G_j}, \quad j = 1, 2, \dots, k \end{aligned} \quad (\text{A-13})$$

The route of the multi-index issue reveals the sense of the optimality factor and its affinity on the decision-makers' expertise and grasp of the issue.

A.2. LINMAP Decision-Making Method

An ideal point on the Pareto frontier defined as the point where each objective is optimized irrespective of assuring of other objectives. Obviously, each objective in the multi-criteria optimization does not have the same value as gained by single-objective optimization. Hence, the ideal point is not posited on the Pareto frontier. Throughout the LINMAP approach, with Euclidian non-dimensionalization of all objectives, the interval of each route on the Pareto frontier from the ideal point represented by d_{i+} is calculated as follows:

$$d_{i+} = \sqrt{\sum_{j=1}^n F_{ij} - F_j^{\text{Ideal}}} \quad (\text{A-14})$$

In which n represents the number of objectives, whereas i represents each route on the Pareto frontier ($i = 1, 2, \dots, m$). In Equation (14), F_j^{Ideal} denotes the ideal value for the j th objective gained by a single-objective optimization. Throughout the LINMAP approach, the outcome with a minimum interval from ideal point is chosen as an ultimate optimum route; meanwhile, i_{final} represents the i index of an ultimate route:

$$i_{\text{final}} = i \in \min(d_{i+}) \quad i = 1, 2, \dots, m \quad (\text{A-15})$$

A.3. TOPSIS Decision-Making Method

In addition to the definition of the ideal point, throughout the TOPSIS approach, a non-ideal point should be described and specified. Thanks to this fact, the non-ideal point is defined as the latitude in the objectives region where

each objective has its arrant amount. Thus, alongside the distance between the outcome and ideal point, d_{i+} , the distance from the non-ideal point which represented by d_{i-} is executed as another screening parameter for choosing the ultimate route. Therefore [10, 11]:

$$d_{i-} = \sqrt{\sum (F_{ij} - F_j^{non-ideal})^2} \quad (\text{A-16})$$

Furthering the TOPSIS approach, the Cl_i variable is formulated as follows:

$$Cl_i = \frac{d_{i-}}{d_{i+} + d_{i-}} \quad (\text{A-17})$$

Consequently, the final optimum solution is chosen on the basis of minimum Cl_i , so, if i_{final} denotes the index for the ultimate chosen route, the following expression is true:

$$i_{final} = i \in \max(Cl_i); \quad i = 1, 2, \dots, m \quad (\text{A-18})$$