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A methodology and new criteria to quantify the adhesive and abrasive wear damage on a die radius using white light profilometry

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A B S T R A C T

A methodology is developed in this article to assess the wear damage occurring on a die radius in a deep-drawing process. Profilometric and topographic measurements were performed with a white-light-source confocal microscope on the rubbed part of the die radius, using a repeatable procedure. Four new quantitative damage criteria were defined from 2D profiles, to quantify and determine the degree of regularity of both adhesive and abrasive damage. This method allows different tool steels to be classified in terms of their adhesive and abrasive wear behavior, with fairly good repeatability and reliability.

Keywords:

Surface damage criteria
Adhesive and abrasive wear
White-light profilometry
Hot stamping process

1. Introduction

In tribology, the quantification of wear damage is not usually easy to achieve, whatever the field of application may be. Wear quantification techniques are based on mass or geometric measurements. One widely used technique is gravimetric wear measurement which calculates the wear volume loss [1–4], but this method is not pertinent when the specimen mass loss or addition is lower than the accuracy of the weight balance (typically 0.01 mg). Neither is it useful when the wear damage involves both adhesive and abrasive mechanisms. Another technique consists in weighing the wear particles ejected from the contact area. In this case, adhesive particles cannot be measured accurately. Many studies involve microscopic observations of the test samples after the wear test, with optical or scanning electron microscopes (sometimes coupled with energy dispersive spectrometry), to study the wear morphologies (craters, cracking, spallation, transfer layer, plastic deformation, fatigue, shear fracture, etc.). Although these investigations are useful to understand the wear mechanisms better [3,5], they remain qualitative and do not allow measurement of wear damage quantities.

Approaches using 2D or 3D profilometry measurements with standard stylus or optical devices could be good alternatives. These techniques are powerful tools, which can not only quantify the wear volume or depth, but also assess the local development

of the wear damage on the sample surface. The normal standardized roughness parameters calculated from profiles or topographies make them possible to follow wear development [6], but do not provide a direct quantification of the wear damage. Several authors evaluate the wear volume from functional surface parameters calculated from the probability distribution (called the Abbott–Firestone or bearing ratio curve). Las Casas et al. [7] analyzed the surface texture parameters (skewness Sk , roughness probability parameters Spk and Svk , and texture aspect ratio Str) to characterize the wear damage on dental enamel specimens. Gara et al. [8] performed wear measurements at different locations on the liner surface of a diesel-engine cylinder, using a replication technique. They developed wear-volume equations based on bearing-ratio parameters (Rk , Rpk , Rvk , $Mr1$ and $Mr2$), calculated from 2D profiles measured with an optical profilometer. The bearing-ratio curve is divided into three approximate areas, related respectively to the peaks, the core and the valleys of the surface profile, and the related volume of the material is calculated with a simplified pyramidal model. Then, the wear volume is calculated by subtracting the volumes before and after the wear test. But these calculations constitute an approximation of the real wear volumes, as no reference is taken between two bearing ratio curves. Moreover, this method does not allow discrimination between transferred and material loss damage, as the global wear volume includes both the elements. Kumar et al. [9] developed a procedure to measure the engine-liner wear volume and depth, based on bearing-length curves. This method consists in estimating the difference between the bearing-area curves calculated from roughness profiles, measured on the

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cylinder before and after the test. Nevertheless, this method requires that the zone of wear is less than the valley depth, in order to keep a lower reference line equivalent for both profiles. Theocharopoulos et al. [10] processed the surface topographies measured on dental enamel and glass ceramic disk samples, using the profilometer dedicated software. They assessed the worn volume by subtracting the topographies scanned before and after the wear test. However, this tool is difficult to apply on samples with irregular shapes, as the mathematical processing can generate distorted surfaces, making wear quantification complicated.

The global aim of this study is to investigate the adhesive and abrasive wear generated by the sliding at high temperature of a High Strength Steel strip on different tool steels, using a deep-drawing simulator. Because of the cylindrical shape of the tools (die radii), the quantification of wear loss and material transfer is not particularly easy. A method and new criteria, based on profilometric and topographic measurements, are developed here in order to locate and quantify the wear damage. The relative amount and degree of regularity of the adhesive and abrasive wear are determined on the die radius surface, allowing us to classify the tool steels investigated.

2. Wear test

2.1. Materials

The strip was a high-strength 22MnB5 boron–manganese steel with an Al–Si coating (*Usibor 1500P*[®], ArcelorMittal). The width of the sheet was 50 mm and its thickness was 1 mm.

Three different steel grades were studied for the die radius: an X50CrMoV5 alloyed nitrided steel (called SG1), a 60CrMoTiV16 alloyed steel (SG2), and a Mo alloyed steel (SG3). These three tool steels present a martensitic microstructure with good wear resistance, and are currently used as mold materials. For SG2 and SG3 steel grades, the bulk and surface hardness is about 550HV_{0.2}. The SG1 steel grade presents a bulk hardness of about 650HV_{0.2}, and because of the nitrided surface, its superficial hardness reaches 980HV_{0.2}.

2.2. Test procedure

In order to reproduce tribological interactions between the strip and the tool in the hot stamping process, an experimental high-temperature friction simulator was developed in the laboratory (Fig. 1) [11,12]. The pre-alloyed strip was heated to 875 °C, and maintained at this temperature before being slid onto the die radius. Two campaigns were undertaken, the first up to 5000 cycles with cycling interruptions at each 1000 cycles, and the second up to 2000 cycles with shorter interruption cycles at 200, 500 and 1000 cycles. The test parameters (sliding distance and speed, strip temperature, strip exit angle, die radius geometry and materials) were strictly identical for the two campaigns [13]. The test interruptions were used to carry out non-destructive investigations on the die radius, in order to monitor its surface degradation.

3. Wear measurement methodology

3.1. White-light profilometer

Profilometric and topographic measurements were performed using an extended field confocal microscope (AltiSurf520 from Altimet), based on the principle of chromatic coding (Fig. 2). A white-light-source (W) is focused onto the sample surface (O), where it is reflected. The beam of this polychromatic light source

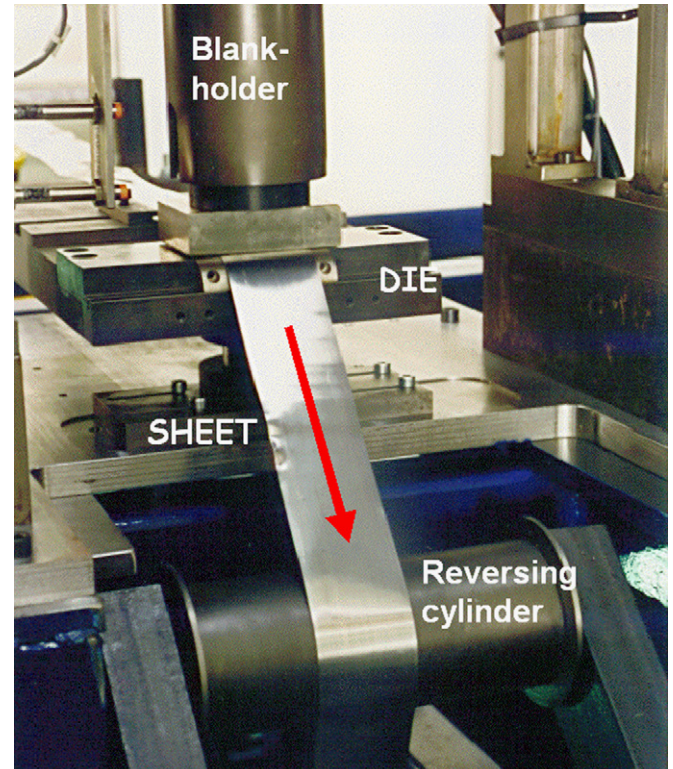


Fig. 1. Detailed view of the working system of the DDPS (Deep Drawing Process Simulator).

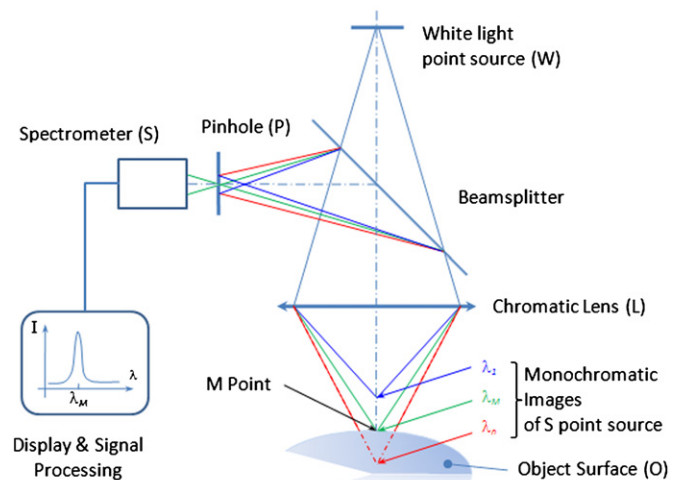


Fig. 2. Principle of white light profilometry.
Source: Stil S.A., Aix-en-Provence, France.

is split into its constituent wavelengths by an accurate distance-measuring sensor which incorporates special chromatic lenses (L). Each wavelength can only be sharply focused on a point lying at a specific distance from the sensor, thus creating a continuum of monochromatic imaging points (M). The distance-sensing ability of the sensor is enabled by matching the central wavelength of the reflected beam to the exact height of the focused point, via a spectrometer (S). A microtopographic image is then constituted by raster scanning across the desired specimen surface. This optical surface profilometer can provide analysis of shape and texture, micro-topography as well as roughness measurements [10]. Compared to a standard mechanical measuring device, it performs a non-contact measurement, leaving sample surfaces intact.

Two chromatic sensors, with a measuring range of 350 μm and 3 mm, were available in the laboratory. Their measurement performances are given in Table 1. For this type of sensors, the axial resolution and the reflection limit angle increase as the working range decreases. The reflection limit angle implies that when the angle between the sample surface and the optical ray is greater than the limit, measurement becomes impossible. This means that at the roughness scale, the sharper the asperity angle, the more difficult it is to recover the optical information.

The scanning was carried out through a CHR-150 controller (Stil S.A.) connected to the profilometer. In order to improve the sensitivity of the sensor to reflected light, dark background measurement was systematically performed before the scanning measurement was taken.

3.2. Measuring requirements on die radius

The sample geometry is a right square prism of 70 mm length and 20 mm height, with one edge machined with a die radius (R_m) of 6 mm (Fig. 3). The active part of the sample is focused on the die radius. The arithmetic roughness (R_a) of the polished surface is $0.2 \pm 0.05 \mu\text{m}$, ranging from 0.14 to 0.25 μm depending on the steel grade and the location on the die-radius. This high surface quality combined with a reflective material (steel) may lead to the saturation of the optical sensor. Consequently, the high sensor amplitude (3 mm) is required to assess the spread of the wear damage on the whole active die-radius surface (from 0° to 65° , Fig. 4). However, considering the technical specifications of each chromatic sensor at the shape sample scale, especially the reflection limit angle, the die-radius must be divided into four sub-sections to be measured completely, from the entry to the exit of the die-radius (Fig. 4). Thus, four different cradles were adjusted to the required angular position corresponding to the minimum angle between the sample surface and the optical ray during the measurements. The die radius was fixed on a sample holder, where four flats were machined in order to locate the four sub-sections to investigate on the die-radius. The set was then placed in a swiveling cradle, which was positioned according to the die radius sub-section to be measured (Fig. 5a). Stop screws, fixed on the power-driven table of the profilometer, ensured that the die radius was always in the same position under the optical sensor (Fig. 5b).

Table 1
Measuring performances of the chromatic sensors used with the extended field confocal microscope.

Measuring range	Working distance (mm)	Axial (Z) resolution (nm)	Lateral resolution (μm)	Precision (μm)	Reflection limit angle ($^\circ$)
350 μm	12	10	4	0.1	30
3 mm	28	100	10	1	15

3.3. Topographic and profilometric measurement procedure

Topographic measurements were performed with the chromatic sensor with the largest measuring range (3 mm), on the four die radius sub-sections. The scanning areas were 80 mm in length and 3 mm wide, in order to cover respectively a part of the sample holder (which constitutes a reference position) and an overlapping area between the maps of two adjacent sub-sections. In order to optimize the scanning duration, a lateral resolution of 25 μm , a scanning speed of 1 mm/s, and a high sampling frequency (1000 Hz) were selected. The raw surface topographies were analyzed using a dedicated software (AltiMap). The first step was to extract the area of interest corresponding only to the die-radius (excluding the sample holder parts), in order to reduce the surface maps to 65 mm \times 1.8 mm to 2.2 mm (the width depending on the sub-section under consideration). The unmeasured points corresponding to sensor saturation were interpolated by

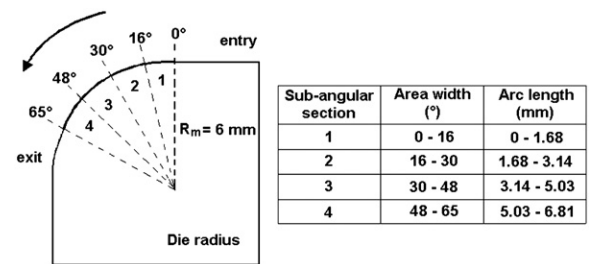


Fig. 4. Definition of four sub-sections on the die radius cross-section for non-destructive investigations.

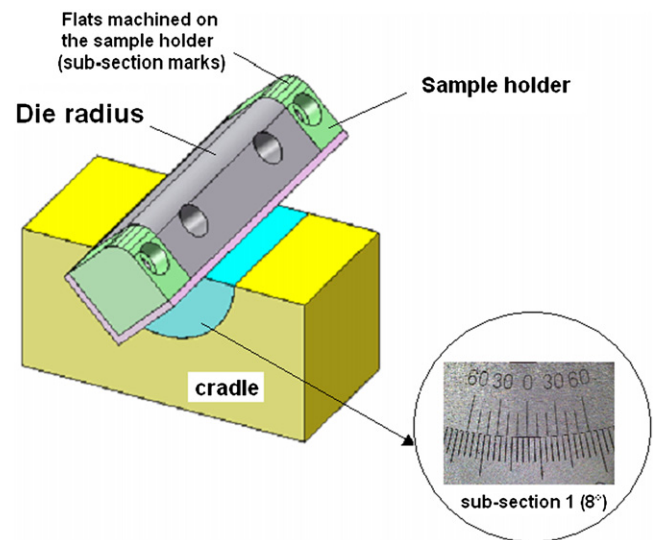


Fig. 5. Positioning of the die radius in the sample holder and the swiveling cradle.

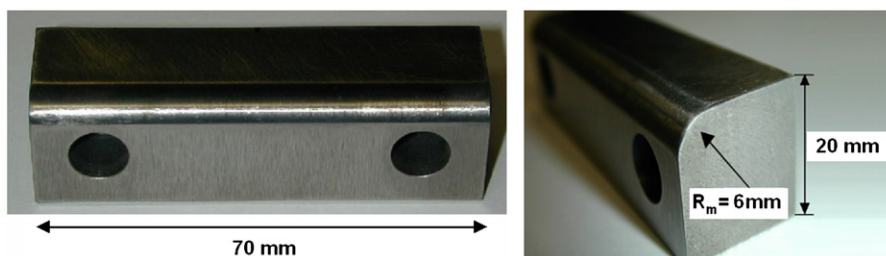


Fig. 3. Geometry and dimensions of the DDPS die radius sample.

considering their neighboring points, and the cylindrical shape of the die-radius was suppressed by a polynomial function (degree 5). The standard 3D parameters (Sa , Sq , St , etc.) were calculated on the “flattened” topographies. The polar graph of textural directions was calculated, in order to assess the spatial isotropy or directionality of the die-radius surface texture, measured through the Str spatial parameter. This texture aspect ratio, theoretically ranging between 0 and 1, indicated a strong uniform texture aspect in all directions when $Str > 0.5$, and a strong directional structure when $Str < 0.3$. The 3D topographies also provided information on the spread of the damage on the die radius, and made it possible to locate the most worn areas.

In order to access precise quantitative damage measurements, profilometric measurements were performed on the die radius perpendicular to the strip sliding direction, using the 350 μm chromatic sensor and a fairly low sampling frequency (100 Hz). Three profiles of 72.5 mm length, crossing the die radius in the longitudinal direction from the sample-holder parts and spaced 0.5 mm from each other, were recorded for each sub-section of the die radius (Fig. 6). The profiles used were much longer than the sliding part on the die radius (which is around 60 mm), in order to retrieve an unworn reference surface on the die radius after the cycle. The lateral resolution (X) of the profiles was 1 μm , for a measuring speed of 1 mm/s. Each raw profile was analyzed to extract the region of interest corresponding to the die radius solely, and then the profile was straightened using the least-

squares method. The reference line, from where the adhesion and ploughing areas were measured, is the mean plane of the unworn zone (Fig. 7).

3.4. Wear criteria definitions

The standard roughness parameters calculated by the dedicated software did not provide enough precise information about the abrasive and adhesive damage on the die radius surface. For this reason, we defined four new quantitative wear criteria, calculated from the straightened raw profiles measured on the die radius.

3.4.1. Transfer wear area (St_m) and regularity (Tr_m) criteria

In order to quantify the adhesive wear on the die radius, the total area (St_t) and maximal height (Ht_{max}) of the transfer layer were determined on each profile (Fig. 8).

The transfer wear area criterion St_m , expressed in $\mu\text{m}^2/\text{mm}$, is defined as the mean value of the total transferred area (St_t) of the n profiles p acquired on the die radius, related to the length (L_p) of the worn part of the straighten profile:

$$St_m = \sum_{p=1}^n St_{tsp} / (nL_p) \quad (1)$$

For each profile, the regularity of the transfer layer (Tr) is calculated as the ratio of the total area of the transfer layer (St_t) to the product of the maximal height (Ht_{max}) of the transfer layer by the length (L_p) of the worn part of the straighten profile (Fig. 8):

$$Tr = St_t / (Ht_{max} L_p) \quad (2)$$

Tr is a dimensionless value ranging from 0 to 1, and is independent of the mean thickness of the transfer layer. The more the transferred layer is homogeneous and continuous, the higher is the Tr (the maximal theoretical value 1 can never be reached, because of the roughness of the transfer layer). Conversely, a heterogeneous and scattered transferred layer gives a low value (near zero).

The transfer wear regularity criterion (Tr_m) is then calculated as the mean value of the transfer regularity of the n profiles p

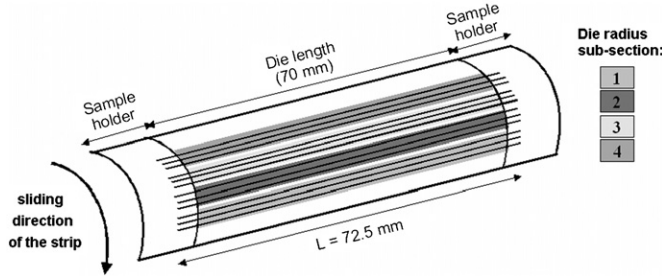


Fig. 6. Location of the profile measurements on the die radius (three profiles per sub-section).

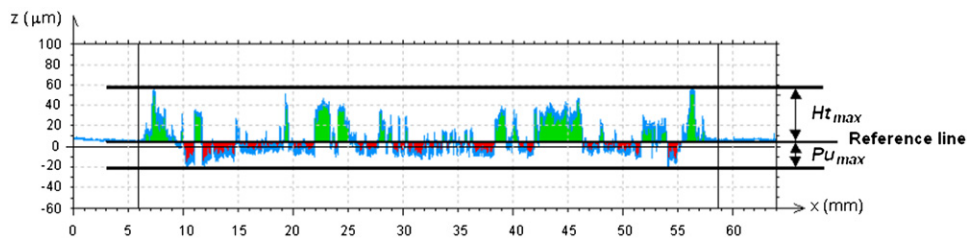


Fig. 7. Definition of the reference line as the mean plane of the unworn zone on the profile, to quantify the adhesive and abrasive wear areas (transfer layer is green and material loss is red). (For interpretation of the references to color in this figure legend, the reader is referred to the web version of this article.)

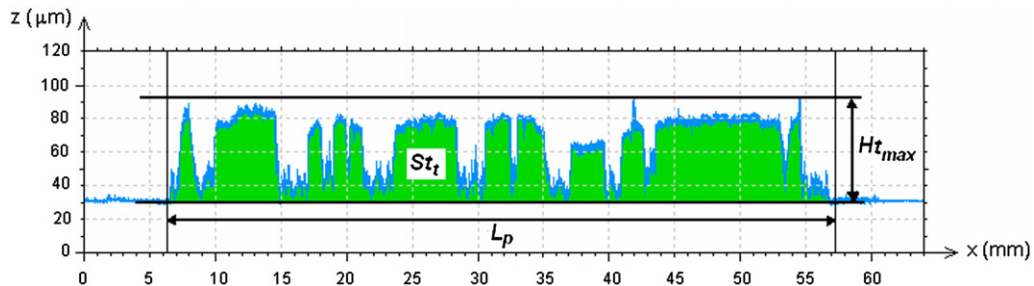


Fig. 8. Determination of the regularity of the transfer layer on the straightened profile: $Tr = St_t / (L_p Ht_{max}) = 0.521$.

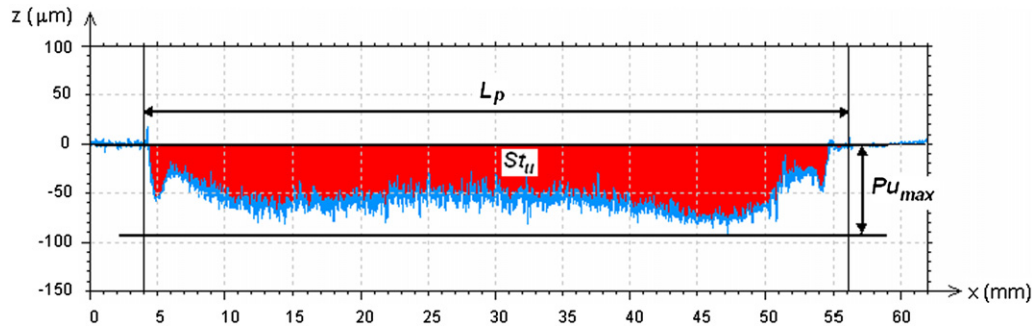


Fig. 9. Determination of the regularity of the material loss on the straightened profile: $Ur = St_u / (L_p Pu_{max}) = 0.580$.

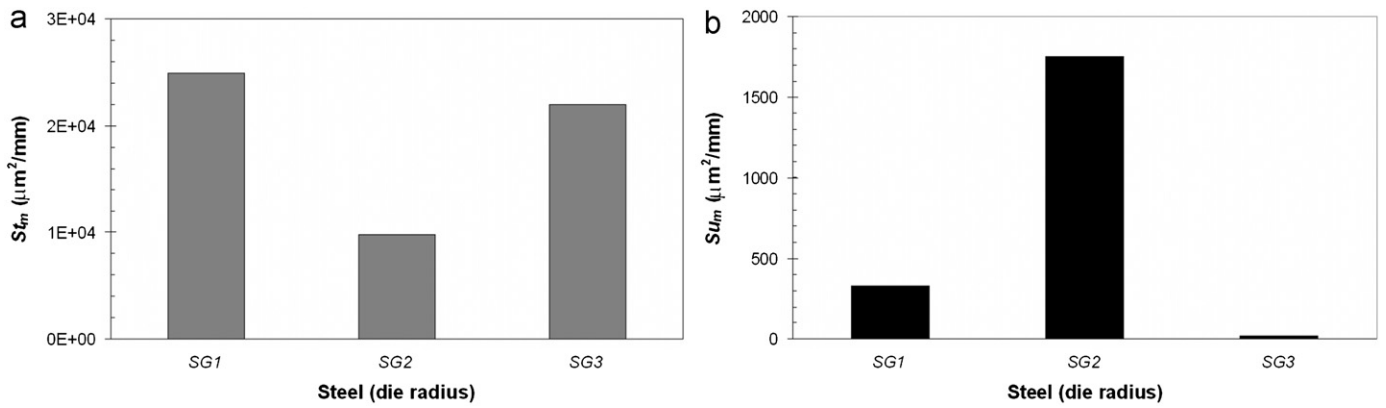


Fig. 10. Classification of die radius steel grades vs. adhesive and abrasive wear damage after of the 5000 cycles: transfer area St_m (a) and material loss area Su_m (b) criteria.

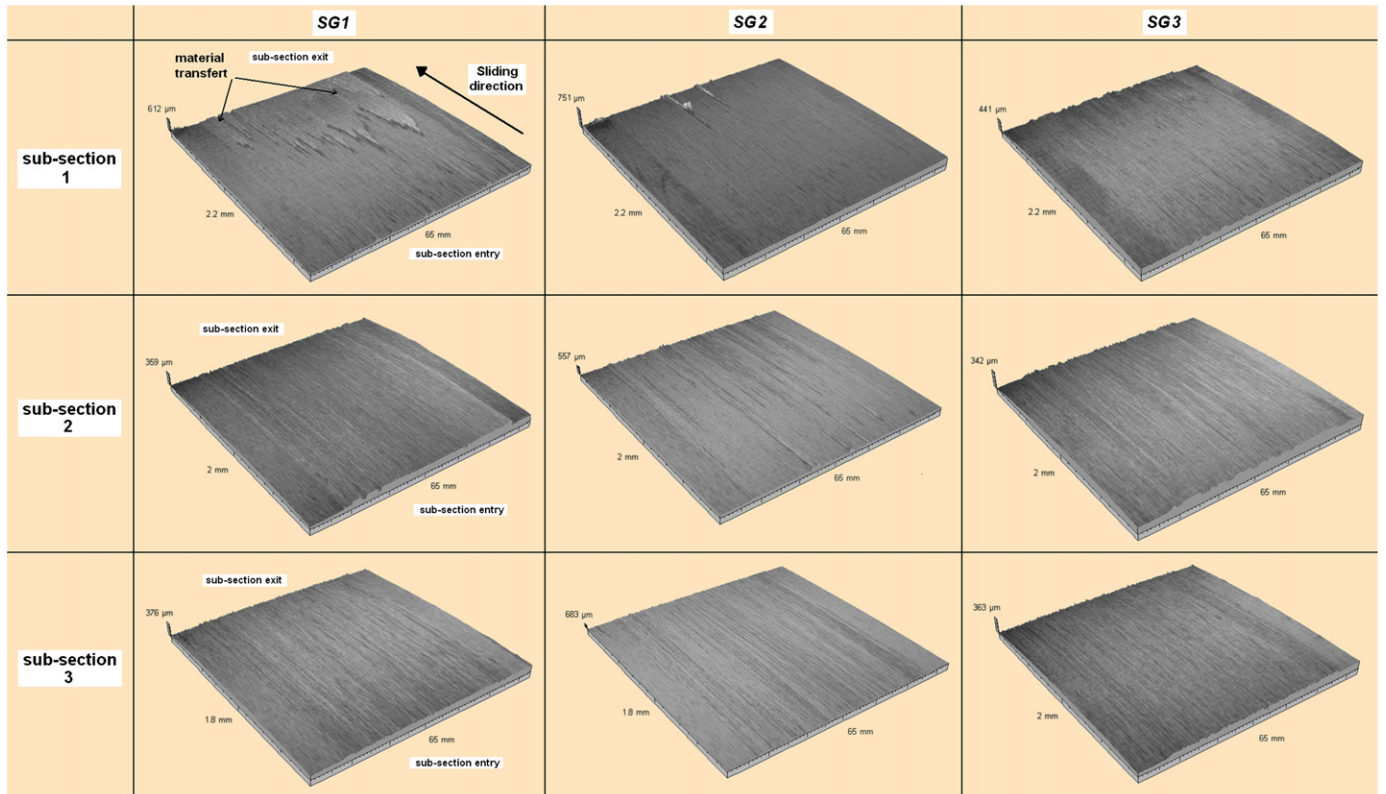


Fig. 11. Topographies of the three steel-grade tools at the die radius entry, after 5000 cycles (the sliding direction is identical for all the topographies).

acquired on the die radius:

$$Tr_m = \sum_{p=1}^n Th_p/n \quad (3)$$

3.4.2. Material loss area (Su_m) and regularity (Ur_m) criteria

In order to quantify the abrasive wear on the die radius, the total area (Su_t) and maximal depth (Pu_{max}) of the material loss were determined on each profile (Fig. 9).

The material loss area criterion Su_m , expressed in $\mu\text{m}^2/\text{mm}$, is defined as the mean value of the total area of material loss (Su_t) of the n profiles p acquired on the die radius, related to the length (L_p) of the worn part of the straighten profile:

$$Su_m = \sum_{p=1}^n Su_{tp}/(nL_p) \quad (4)$$

For each profile, the dimensionless regularity of the material loss (Ur) is defined as the ratio of the total area of the material loss (Su_t) to the product of the maximal depth (Pu_{max}) of the material loss by the length (L_p) of the worn part of the straighten profile (Fig. 9):

$$Ur = Su_t/(Pu_{max}L_p) \quad (5)$$

The material loss regularity criterion (Ur_m) is then calculated as the mean value of the material loss regularity of the n profiles p acquired on the die radius:

$$Ur_m = \sum_{p=1}^n Uhp/n. \quad (6)$$

4. Results and discussion

4.1. Tool classification based on wear criteria

The transfer and material-loss wear criteria St_m and Su_m were used to quantify the wear at the die radius surface, and to classify the tools in terms of adhesive and abrasive wear damage. In Fig. 10, the three steel grades are compared after 5000 cycles. At the end of the first cycling campaign, SG1 and SG3 die radii present approximately the same level of adhesive wear at their surface, whereas SG2 is less damaged (Fig. 10a). In contrast, Fig. 10b shows that SG2 presents the highest propensity to abrasive wear, and SG3 is the lowest. St_m and Su_m were calculated on the three first sub-sections 1–3, excluding sub-section 4 on which no significant damage was observed. Although St_m and Su_m criteria are average values calculated from nine profiles, the standard deviations are not indicated in Fig. 10. This is because the adhesive wear is highly localized at the entry of the contact on the die radius (at the boundary between sub-sections 1 and 2), as illustrated in the topographies (Fig. 11). Therefore, St_t and Su_t values are scattered, and the standard deviations are not representative of the main results. In the next paragraph, a study of the reproducibility of these criteria will be presented and discussed.

Table 2

Statistical dispersion calculated from five series of measurements of the wear criteria St_m , Su_m and Tr_m , for the three steel die radii.

Damage criterion	Transfer wear area St_m ($\mu\text{m}^2/\text{mm}$)			Material loss area Su_m ($\mu\text{m}^2/\text{mm}$)			Transfer regularity, Tr_m		
	SG1	SG2	SG3	SG1	SG2	SG3	SG1	SG2	SG3
Mean value	20,286	14,332	26,443	26.6	276.4	207.2	0.376	0.269	0.300
Standard deviation	236	1247	381	9.1	41.5	33.3	0.014	0.006	0.011
Coefficient of variation (%)	1.2	8.7	1.4	34.1	15.0	16.1	3.7	2.2	3.7

A more detailed analysis of the tribological behavior and wear damage mechanisms is reported in [13].

4.2. Repeatability of wear damage criterion measurements

The repeatability of the wear-damage criterion measurements was evaluated on the three die radii after 2000 cycles (at the end of the second campaign). Five series of profilometric measurements, spaced in time, were performed by the same operator using the same measurement device with the same optical sensor (intra-laboratory reproducibility). Before each series of measurements, the profilometer was reinitialized, and the power-driven table and the positioning system of the sample-holder refitted.

The statistical dispersion results of St_m , Su_m and Tr_m criteria are given in Table 2, for the three steel die radii. The coefficient of variation (CV) of the mean values characterizes the relative dispersion of a statistical series:

$$CV = \frac{\sigma}{\bar{X}} \times 100 \quad (7)$$

It is generally considered that when $CV < 10\%$, there is little scattering of the population and the sample can be considered homogeneous; otherwise, the population is dispersed. For St_m and Tr_m criteria, CV ranges between 0.9% and 8%, and between 2.1% and 3.7%, respectively. These particularly low values attest to the good repeatability of the transfer wear area and regularity measurements. For the material loss area Su_m , CV ranges from 14.5% to 34.2%. Fig. 12 indicates that the coefficient of variation calculated from our St_m and Su_m criteria measurements is strongly dependent on the quantity of wear loss or transfer (expressed here by equivalent thickness e_{eq}): the lower the e_{eq} , the higher the CV. On this curve, the minimal equivalent thickness from which the measurements are statistically reliable (i.e. for $CV \leq 10\%$) is $3 \mu\text{m}$. The higher variability for the Su_m criterion can thus be explained by the relatively small amount of material loss (maximal depth of a few micrometers) generated on the tools in the applied test conditions, which, in addition, is highly localized on

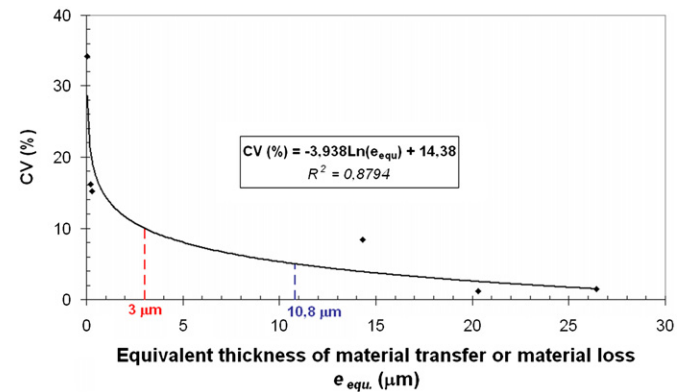


Fig. 12. Relationship between the coefficient of variation CV and the equivalent thickness of material transfer or material loss e_{eq} .

the die radii, as shown in Fig. 13. Therefore, given the low abrasive wear observed on the tool surface under the applied wear-test conditions, the material loss regularity (Ur) was not investigated in this study.

It can thus be concluded that our measurement methodology is reliable when the wear damage (material transfer or material loss) is consistent enough, i.e. when the equivalent thickness of material transfer or loss is higher than 3 μm .

4.3. Reliability of the wear test

The two test campaigns, performed in the same operating conditions, contained interruptions at two identical numbers of

cycles (1000 and 2000 cycles). This allowed the reliability of the wear test and measurement to be verified.

As previously concluded from the repeatability study of the profilometric measurement and processing (Section 4.2), the reproducibility of the test is better for the transfer criterion (St_m) compared to the material loss criterion (St_u). In Fig. 14, one can see that the St_m values exhibit a particularly strong reproducibility, except for the test on the SG1 tool at 1000 cycles. A mean difference of 37.5% and 6%, respectively, is obtained at 1000 cycles and 2000 cycles. The reproducibility of the transfer regularity criterion (Tr_m) is also very strong, with a mean difference of 12% and 19%, respectively, at 1000 cycles and 2000 cycles (Fig. 15). The maximal difference reaches 33% for the SG2 tool, on which the transfer layer is smaller than that for SG1 and SG2 steels.

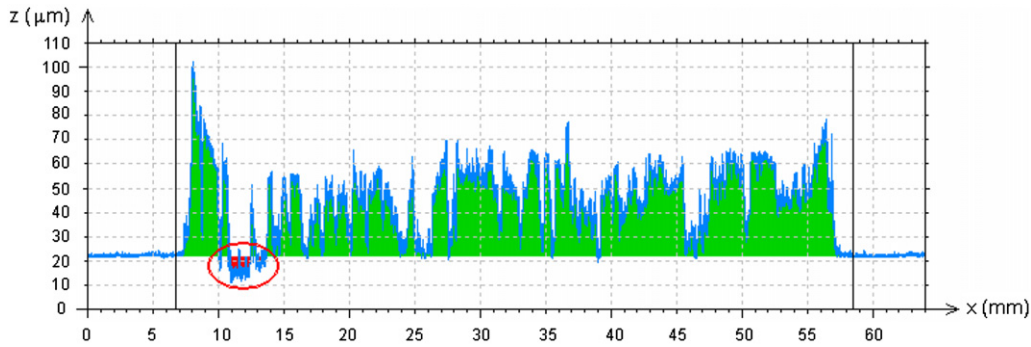


Fig. 13. Profile showing the small depth and localized spread of material loss on the SG1 die radius after 2000 cycles.

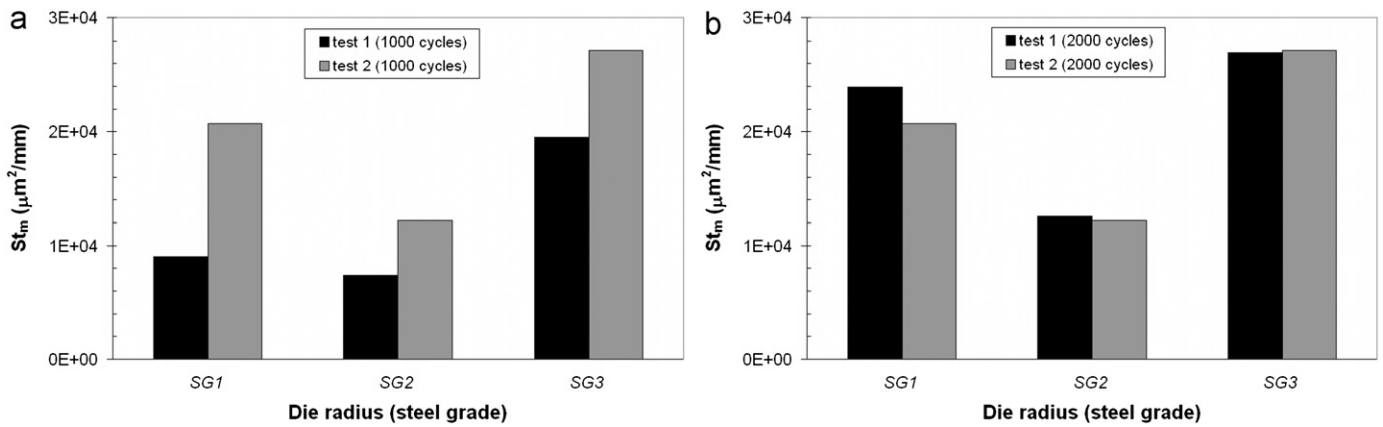


Fig. 14. Reproducibility of the transfer area criterion (St_m) for both cycling tests, after 1000 cycles (a) and 2000 cycles (b).

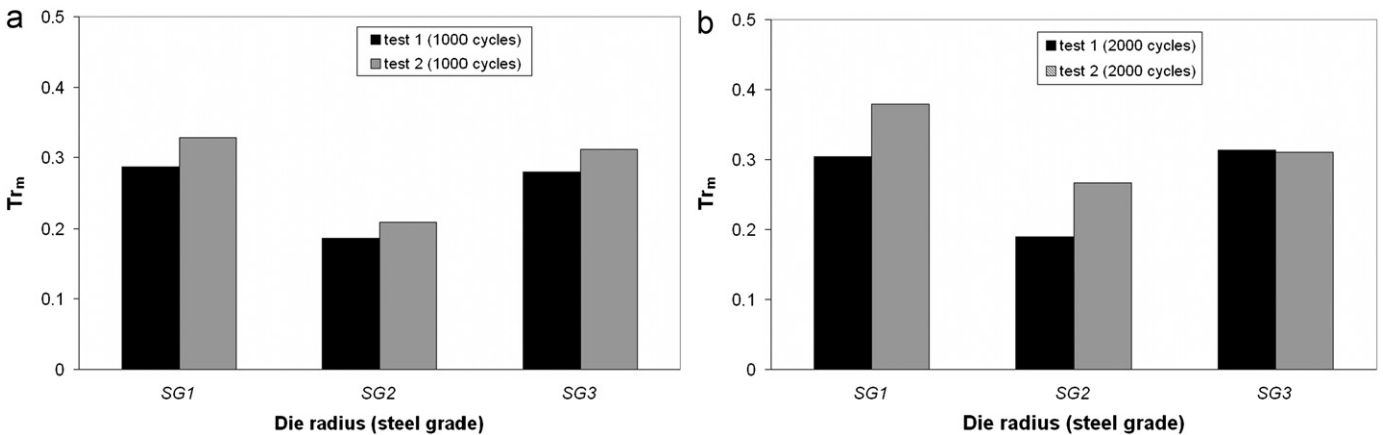


Fig. 15. Reproducibility of the transfer regularity criterion (Tr_m) for both cycling tests, after 1000 cycles (a) and 2000 cycles (b).

As shown in Fig. 16, the St_u criterion exhibits a higher difference between the two tests. It should mostly be attributed to the negligible amount of material loss (compared to material transfer) measured on the investigated tools, as explained in the previous paragraph. Moreover, the thermo-mechanical history of

the tools was not exactly identical during the two campaigns. Indeed, the second test campaign was interrupted more often before 1000 cycles, which does not allow the tool to reach a stable thermal regime. This could explain the higher differences observed in Figs. 14a and 16a.

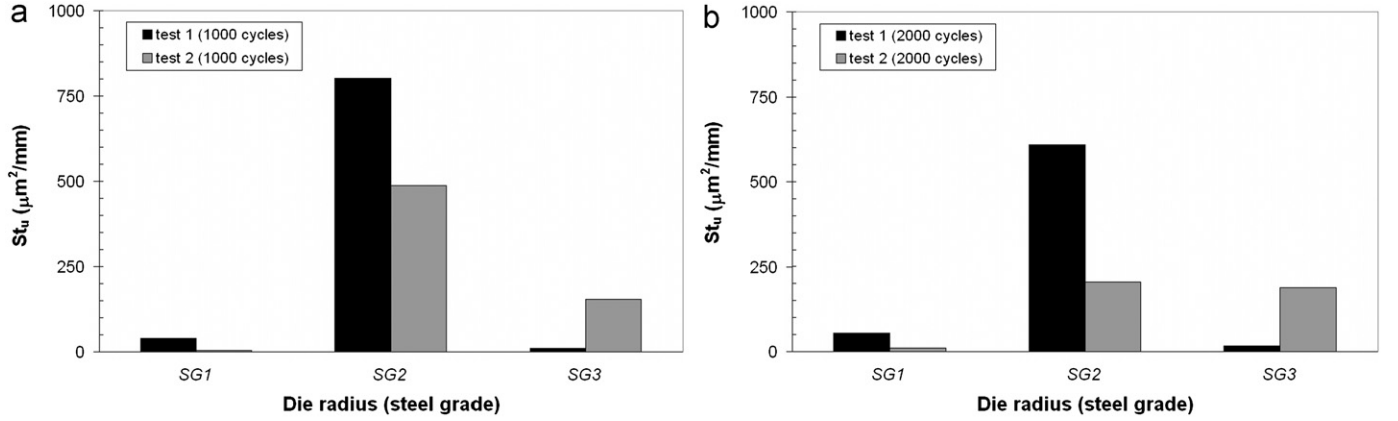


Fig. 16. Reproducibility of the material-loss area criterion (St_u) for both cycling tests, after 1000 cycles (a) and 2000 cycles (b).

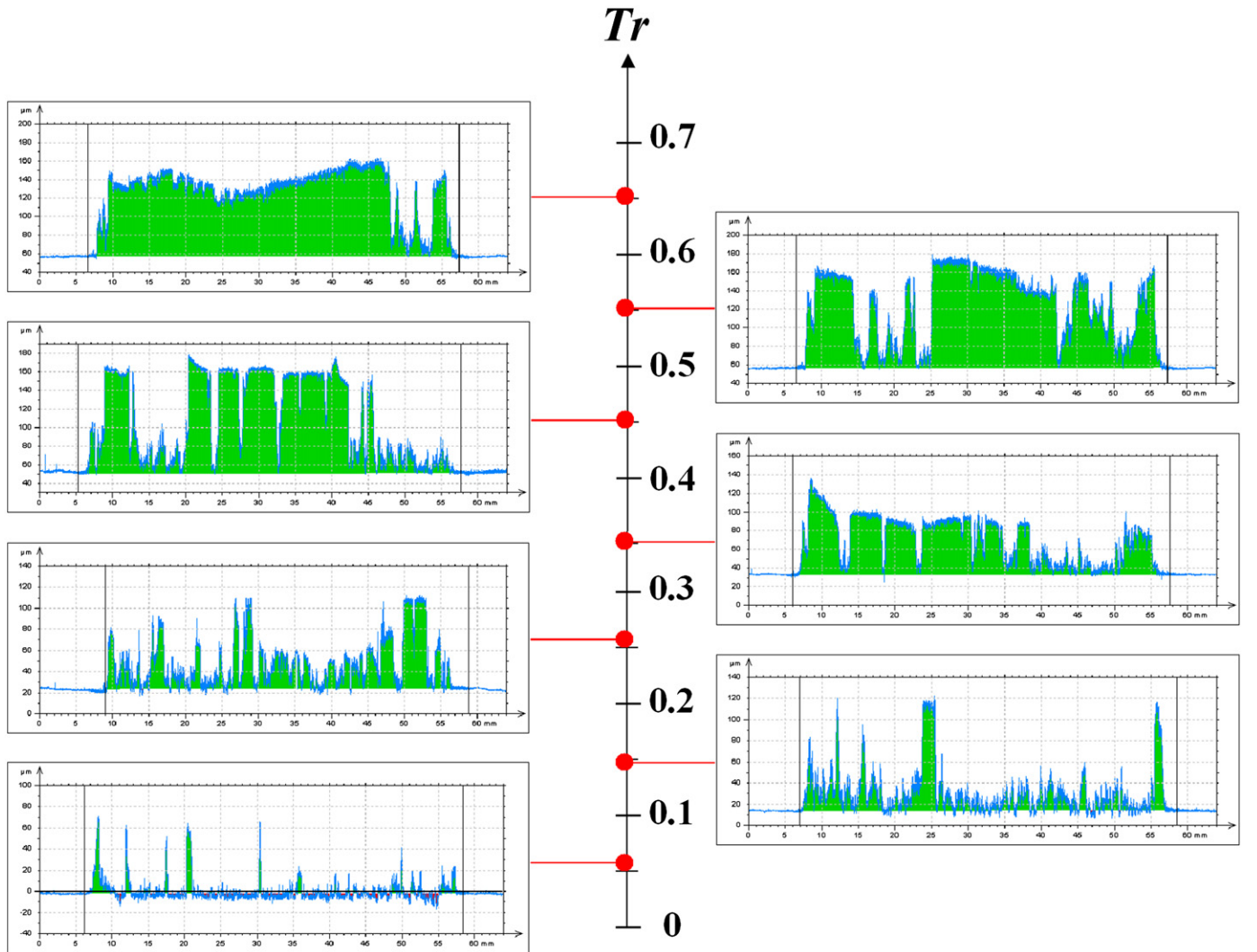


Fig. 17. Ability of the regularity criterion to discriminate between various morphologies of the transfer layer, from a homogeneous and continuous layer ($Tr=0.65$) to a heterogeneous and scattered layer ($Tr=0.056$).

Given the mechanical complexity of the DDPS device, the consistency of the wear damage criteria between the two test campaigns attests to the very high reliability of our wear-test simulator. In addition, the reproducibility of the wear damage criteria calculated from profilometric measurements demonstrates the strength of our measurement methodology.

4.4. Representativeness of regularity criterion

The degree of regularity of the transfer layer (Tr) measured on our specimens varies from 0.05 to almost 0.7. As shown in Fig. 17, this parameter allows fine differentiation of the morphology of the transfer layer, from a compact and homogeneous layer to a scattered and heterogeneous one. It must be remembered, however, that Tr is calculated on the straightened raw profiles, which contain both long wavelength (shape) and short wavelength (roughness) information. So, Tr reflects not only the compactness of the layer, but also its scattered aspect. Therefore, the Tr value is affected by the presence of sharp peaks, which most probably represent local heterogeneity or, more rarely, measurement noise. Although this phenomenon was not very pronounced in our samples, a sensitivity study was carried out to

assess its effects on the Tr value. For this purpose, the raw profiles were filtered with the appropriate cut-off length, to eliminate the micro-roughness information. On the resulting waviness profiles, the maximal height of the transfer layer is lower, therefore increasing the calculated Tr value (Fig. 18). The results indicate that Tr values calculated from waviness profiles are 5–30% higher than that with the first method (Fig. 19a), and that this difference decreases when Tr increases (Fig. 19b). However, this does not change the classification of the transfer layers illustrated in Fig. 17.

5. Conclusion

In this work, a methodology has been developed to quantify the adhesive and abrasive wear damage generated by the sliding at high temperature of a pre-alloyed Al–Si coated High Strength Steel strip on a die radius. Wear tests were carried out with a deep drawing simulator device, to characterize the wear behavior of three different steel grades used for the tool (die radius). Profilometric and topographic measurements, using a white-light confocal microscope, were performed after each test interruption. Because of the complexity of the die radius shape and the lack of

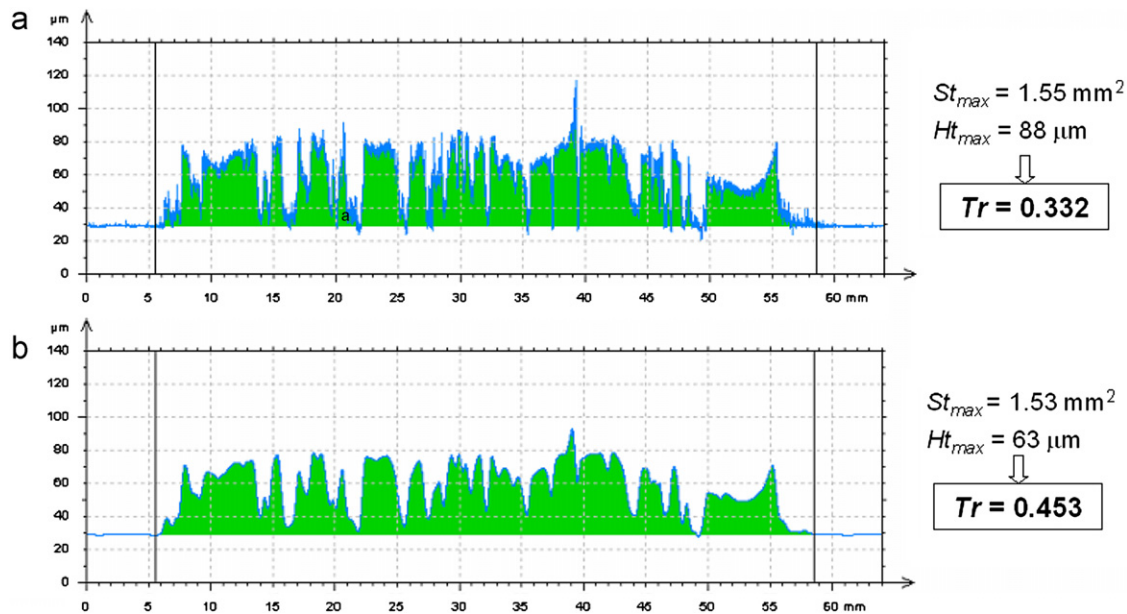


Fig. 18. Sensitivity to noise of the transfer regularity: (a) Tr calculated on the raw profile of the transfer layer and (b) variant of calculation of Tr on the waviness profile (on which the micro-roughness parts have been filtered).

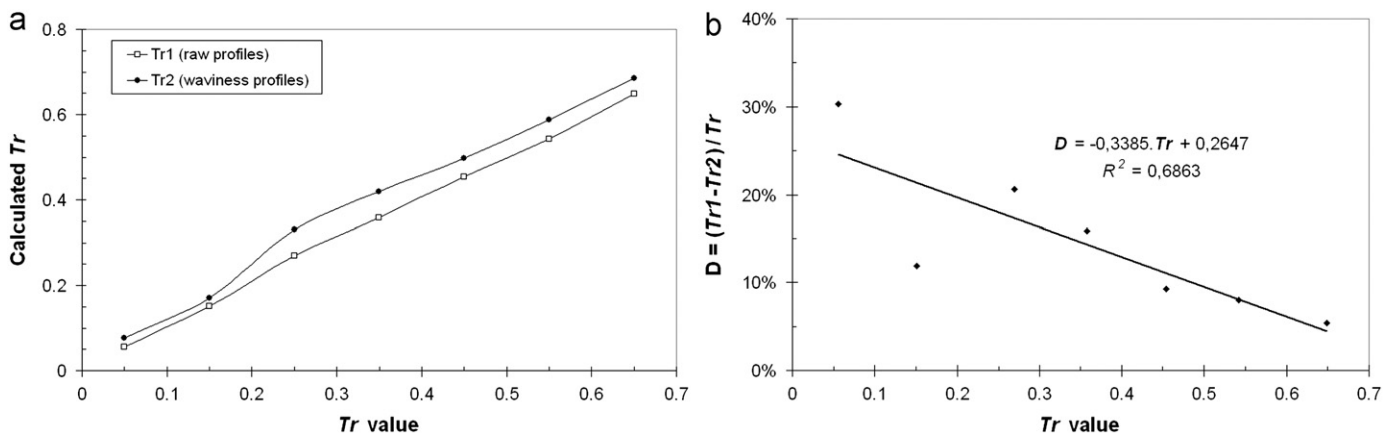


Fig. 19. Comparison of the transfer regularity values calculated from raw profiles ($Tr1$) and waviness profiles ($Tr2$) on the transfer layers shown in Fig. 17(a), and evolution of $D = (Tr2 - Tr1)/Tr$ vs. Tr value (b).

pertinent normalized parameters to quantify adhesive and abrasive wear damage, new criteria have been defined and used to classify the wear behavior of the steel grades. The results show that both the wear test and the measurement methodology are reproducible, and reliable enough to classify the tool samples investigated in this study.

The measurement procedure and the associated wear criteria could be used in other applications dealing with revolution samples. For example, transfer criteria could be appropriated to characterize oxide scales or surface coatings, and material loss criteria to assess corroded or damaged surfaces.

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