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# Topological and metric properties of microscopic crack patterns: application to thermal fatigue of high temperature tool steels

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## Abstract

The topological properties of heat-checking patterns, produced on the oxidized surface of high temperature tool steels under thermal fatigue experiments, are investigated using image analysis methods. All crack networks are composed of polygonal cells with a mean number of sides close to 6. Whatever the thermal cycling conditions, the semi-empirical Aboav–Weaire’s and Lewis’ laws are quite well verified. The least-squares fit parameters of these laws are discussed and compared with values reported in the literature for other random cellular structures. It is shown that the heat-checking cells undergo a strong shrinkage and that the cellular organization is rather disordered at the beginning of the fragmentation process. The heat-checking networks evolve towards a more stable and ordered state upon cycling. Most disordered cellular networks are obtained at low maximal temperatures and low heating rates. The slope of Lewis’ law is mainly dependent on the maximum heat-flux density applied to the specimen during the heating period. Whatever the test conditions, the stabilized heat-checking networks obey a unique normalized Lewis’ law.

## 1. Introduction

When a brittle material (like an oxide film on a metallic substrate) is subjected to transient thermal gradients under thermal fatigue (TF), in-plane tensile stresses are generated during the cooling phase, due to thermal expansion mismatch between the layer and the substrate. According to their amplitude, these tensile stresses may be relieved by the formation of a multi-directional interconnected network of cracks on the surface [1]. Similar ‘cooling-induced’ or ‘shrinkage’ cracks patterns are produced in ceramics under thermal shock experiments [2, 3], in the glaze of ceramics [4], in solidified basaltic lava flows [5], or in thin layers of desiccating mud or gel [4, 6, 7]. These networks partition the free surface of the material in a two-dimensional random tessellation of cells, comparable to that formed by grains in planar sections of polycrystalline materials, or by bubbles in soap froths [8].

The topological properties of natural cellular patterns have been studied for a long time, in many scientific fields (e.g. biology, metallurgy, geology, geography) and at widely different size scales (from  $m^2$  to  $\mu m^2$ ) [8]. Most often, the universal Lantuejoul’s procedure [9], developed for polycrystalline ceramics and based on mathematical morphology, is used to determine the distribution of the number of first neighbours (or sides) of the cells. This method is applicable to all kind of networks, whatever the shape of polygons. However, the computation time can be very long for analysing a structure containing a large number of cells, due to the iterative nature of processing. Bandeira *et al* [10, 11] proposed a multi-layer approach to increase the processing speed of the algorithm, since the spatial resolution of their remotely acquired images was very high. This improved algorithm reduces the computation time significantly, but its application is restricted to tri- and tetravalent networks. Bohn *et al* [12] investigated the dynamic evolution of the

topological structure of ‘hierarchical’ crack patterns, using the ‘genealogical tree’ of cell division. However, such an approach requires that the cracking phenomenon is observed *in situ*.

Some semi-empirical statistical rules are commonly used to relate topological and geometrical properties of the cells. The Aboav–Weaire’s law [13, 14] states a linear relationship between the number of neighbours (or sides) of a cell,  $n$ , and the average number of neighbours (or sides) of its neighbouring cells,  $m(n)$ :

$$m(n) = \langle n \rangle - a + (\langle n \rangle a + \mu_2)/n, \quad (1)$$

which can otherwise be expressed as

$$nm(n) = (\langle n \rangle - a)n + \mu_2 + \langle n \rangle a, \quad (2)$$

where  $\langle n \rangle$  is the average number of sides (or neighbours) of the cells ( $\langle n \rangle = 6$  in infinite cellular structures),  $a$  is a structural constant and  $\mu_2$  is the second moment (or variance) of the probability distribution  $P(n)$  of cell sides ( $\mu_2 = \sum P(n)(n - \langle n \rangle)^2$ ).

This structural equation of state (called ‘nearest-neighbours correlation’) is a quantitative expression of the empirical fact that in planar space-filling cellular structures, many-sided cells tend to be surrounded by few-sided cells, and vice versa. It describes a statistical equilibrium, assuming that there is no correlation in cell shape beyond the nearest neighbours [8]. Since then, some authors [15–17] have shown that Aboav–Weaire’s law can be generalized to more distant neighbours.

Studying the cellular structure of vegetal tissues, Lewis [18] found that the average area of a  $n$ -sided cell,  $\langle A(n) \rangle$ , was linearly related to  $n$  as

$$\langle A(n) \rangle = \alpha(n - n_0), \quad (3)$$

where both  $\alpha$  (slope) and  $n_0$  (intercept) depend on the properties of the cellular structure.

This law reflects the tendency for many-sided cells to be larger, on average, than fewer-sided cells. Using the maximum-entropy principle, Rivier [8, 20, 21] showed that agreement to this equation of state means that the shaping of the network is governed only by mathematical constraints imposed by the need to completely fill the space without gaps. Furthermore, he defined  $\lambda$  (Lagrange multiplier related to the time) as an important structural parameter with a physical meaning, since it measures the topological ageing in a coarsening structure (like a soap froth or a polycrystalline aggregate). He demonstrated that  $\lambda$  is related both to the slope ( $\alpha = \lambda \langle A \rangle$ ) and the intercept ( $n_0 = 6 - 1/\lambda$ ) of Lewis’ law [20–22]. Equation (3) thus becomes:

$$\langle A(n) \rangle = \langle A \rangle [1 + \lambda(n - 6)], \quad (4)$$

where  $\langle A \rangle$  is the average area of all cells in the network.

The above-mentioned author has also suggested in [21] that the average area of a cell is linearly dependent on the time, in agreement to Von Neumann’s law [23].

Differentiating Lewis’ law (3) with respect to time, the rate of change of the average area of the cells,  $d\langle A(n) \rangle/dt$ ,

can be expressed as a function of their local topology by the following relationship:

$$d\langle A(n) \rangle/dt = \gamma(n - 6), \quad (5)$$

where  $\gamma$  is the diffusion constant of the system ( $\gamma > 0$ ).

Concretely, this equation implies that, in average, the cells with less than six sides grow, those which have more than six sides shrink, whereas the area of 6-sided cells does not evolve over time. This ‘topological growth’ correlation, established by Von Neumann for soap bubble froths [23], is in fact applicable to any evolving cellular mosaic, such as biological tissues, soap froths and metallurgical grain structures [21].

Both Aboav–Weaire’s and Lewis’ laws have been empirically validated for a wide variety of random cellular systems [8, 24], as biological and vegetable tissues [16, 18, 22, 25–27], soap froths [13, 28], polygonal convective structures [29], colloidal aggregations [30] and polygonal networks on the surface of stars [31, 32]. However, experiments reported in soap foams [26, 33] and polycrystalline materials [21, 34–36] have shown that Lewis’ law is not always obeyed. For these structures, it is the cell perimeter (or radius), rather than the area, which depends linearly on  $n$  (as expressed by Desch’s law [21, 37]). The failure of Lewis’ law has been attributed to particular constraints acting on the cellular network, other than strictly the mathematical and universal constraints of space-filling. These additional specific forces, which may be physical, biological or chemical, are linked to the energy carried by the cell interfaces (surface tension in soap froths, or grain boundary in metallurgical aggregates [22]), and associated with the mechanism driving the evolution towards statistical equilibrium [21, 30].

In this paper, the topological properties of microscopic crack patterns, produced by TF laboratory experiments on the oxidized surface of a X38CrMoV5 tool steel, are investigated using image analysis and Lantuejoul’s algorithm [1]. Based on many experimental data, topological and metric correlations (such as Aboav–Weaire’s and Lewis’ laws) are verified and compared with other natural cellular structures. The effects of the number of cycles and of the conditions of the TF test are shown and discussed.

## 2. Experimental procedure

### 2.1. TF tests

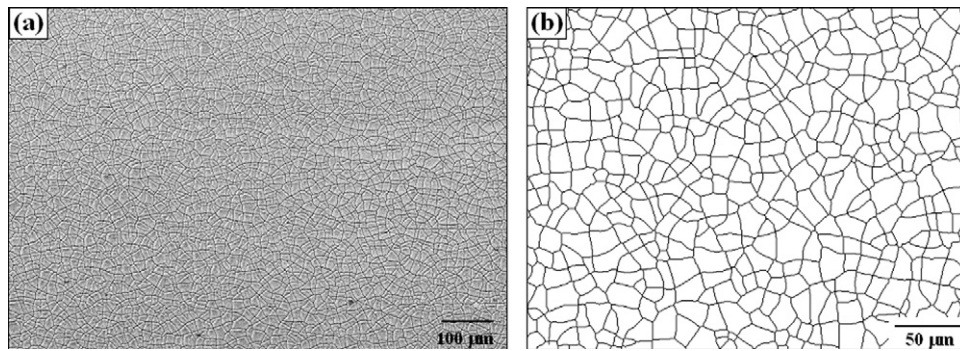
TF experiments were carried out on X38CrMoV5 tool steel, heat-treated to achieve either 42 or 47 HRC hardness. The tubular cylindrical-shaped specimens present an external diameter of 30 mm with a polished surface, and a wall thickness of 10 mm in the central gauge area [38]. During the test, the external surface of the specimen was alternatively fast-heated using a high-frequency induction system, and air-cooled by natural convection. The inner wall was continuously cooled by a flow of water circulating through the central hole of the specimen, thus generating a high thermal gradient.

Several thermal cycles were investigated, with a minimal temperature ( $T_{\min}$ ) always fixed to 100 °C, while the maximum

**Table 1.** Thermal fatigue test conditions performed on 42 and/or 47 HRC treated X38CrMoV5 steels.

TF test N°	Thermal cycle $T_{\min}-T_{\max}$ (°C)	Heating period		Maximum heat-flux density $\Phi_{\max}$ (MW m <sup>-2</sup> )	Cooling period		Cycling interruptions	
		Duration ht (s)	Mean rate hr (°C s <sup>-1</sup> )		Duration ct (s)	Mean rate cr (°C s <sup>-1</sup> )	Number of stops	First and last stops (number of cycles)
1	100–550	0.90	500	4.75	14.5	31	2	30 000–80 000 <sup>a</sup>
2	100–575	0.95	500	4.84	14.8	32	7	5000–50 000
3	100–600	1.0	500	4.85	15.0	33	9	2500–60 000
4	100–625	1.1	477	4.93	16.0	33	5	10 000–50 000 <sup>a</sup>
5	100–650	1.2	458	4.95	17.0	32	9	1000–20 000
6	100–650	2.0	275	3.93	20.0	28	9	1000–30 000
7	100–650	3.7	149	2.78	22.0	25	8	2000–30 000
8	100–650	6.5	85	2.13	30.0	18	7	3000–50 000
9	100–685	1.6	366	4.75	22.0	27	7	500–3000

<sup>a</sup> Tests non-interrupted in the early stages of crack initiation.

**Figure 1.** (a) Typical SEM cartography of the microscopic crack pattern observed on the surface of the specimen; (b) enlarged binary image of the skeletonised crack network (cracks in black and polygonal cells in white).

temperature ( $T_{\max}$ ) was varied from 550 to 685 °C. For the tests performed between 100 and 650 °C, various heating periods ( $1.2 < ht < 6.5$  s) were applied, leading to maximum heat-flux densities ( $\Phi_{\max}$ ) imposed on the specimen surface ranging from 2.13 to 4.95 MW m<sup>-2</sup> (table 1). The experiments were regularly stopped in order to investigate the crack pattern evolution, and determine the number of cycles to crack initiation and to achieve a stabilized crack density (see details in [38]). In table 1, for each TF test, the first interruption of cycling (corresponding to the number of cycles when the micro-cracks were detected first), and the last interruption are given (end of the test, when the crack density was fully stabilized).

## 2.2. Crack pattern analysis

After each cycling interruption, the surface of the TF specimen was observed with a scanning electron microscope and a back-scattered electron detector. By selecting a magnification of 250, an interconnected microscopic crack pattern (named ‘heat-checking’ [1]) was revealed on the superficial oxide layer covering the steel. A matrix of (3 × 3) images was acquired on a randomly chosen area of 0.825 mm<sup>2</sup> in the centre of the specimen. The nine SEM images were assembled to form a cartography sizing about (1740 × 1210) pixels<sup>2</sup>, with a spatial resolution of 0.5 μm/pixel (figure 1(a)). Using an image analysis algorithm [1] and the Aphelion<sup>®</sup> software, the micro-cracks were segmented and skeletonized

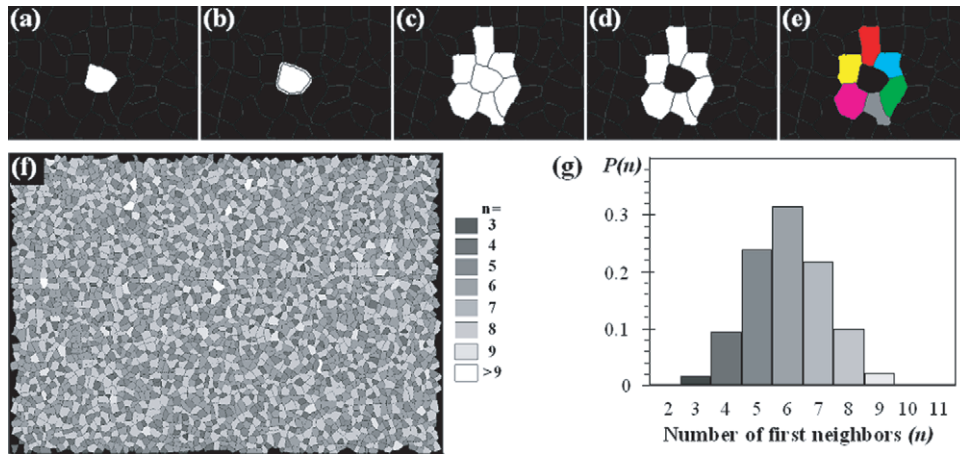
(i.e. thinned to one pixel). An example of the resulting two-dimensional cellular network is illustrated in figure 1(b). To analyse the topological features of the cellular structure, the cells touching the field border were eliminated, since their neighbourhood was incomplete. Within the ‘measuring mask’ consisting of the remaining cells, between 320 and 4750 cells ( $N_c$ ) were counted in the 70 heat-checking maps investigated for this study (table 2). Despite their high number, an exhaustive analysis of all cells was systematically carried out, leading to large computation time (typically several hours for most of cartographies). On the other hand, a statistical reliable description of the cellular networks was achieved. A previous study [1] has revealed that the crack-junctions were predominantly tri-, tetra- and pentavalent, excluding the possibility to apply the algorithm developed by Bandeira *et al* [11]. Therefore, the analysis was carried out following the procedure of Lantuéjoul [9], considering that two cells are neighbours if they share at least one side. This method consists of five steps, as illustrated in figure 2: individual extraction of each cell in the measuring mask (a); dilatation of size 2 of the selected cell using a square structuring element, which provides markers both in the selected cell and its first neighbours (b); geodesic reconstruction of the cell and its neighbourhood, using image b as a ‘marker’ in the initial cellular mosaic (c); logical subtraction of the central cell (d); labelling and counting of the first neighbours of the central cell (e). These operations were iteratively applied to each cell of the network, leading to a labelled image wherein the cells are



**Table 2.** Range of variation of topological properties (minimum and maximum values between the first and last cycle interruptions) calculated on the microscopic heat-checking cells produced under various TF test conditions on 47 HRC heat-treated specimens.

TF test N°	Measuring mask		Distribution of the number of cell neighbours (or sides) $n$					
	Total number of cells $N_c$	Cell density $d_c$ (mm <sup>-2</sup> )	$n_{\min}$	$n_{\max}$	$\langle n \rangle$	$\mu_2$	$P(6)$	$\sum_{n=5}^7 P(n)$
1	2812–3002	3705–4015	3	12–13	6.01–6.02	2.37–2.63	0.19–0.25	0.57–0.66
2	2495–3439	3311–4523	3	11–13	6.01–6.03	2.11–2.94	0.18–0.26	0.52–0.69
3	2256–3381	4109–4606	3	11–12	6.01–6.02	1.73–2.27	0.20–0.26	0.57–0.70
3 <sup>a</sup>	2798–4468	3693–5502	3	11–14	5.98–6.03	1.80–2.96	0.15–0.25	0.53–0.71
4	3645–4133	4746–5370	3	11–12	6.03	1.74–2.20	0.20–0.22	0.58–0.61
5	1855–3509	2487–4593	3	10–13	5.99–6.03	1.27–3.12	0.27–0.32	0.69–0.80
5 <sup>a</sup>	2038–3114	2726–4122	3	10–11	5.96–6.01	1.27–2.31	0.27–0.32	0.70–0.78
6	1567–2187	2322–2919	3	10–13	5.98–6.02	1.52–2.73	0.18–0.23	0.51–0.63
7	479–860	853–927	3	10–11	5.92–6.00	1.85–2.72	0.18–0.29	0.51–0.74
8	323–525	460–718	3	10–12	5.91–5.99	2.33–4.30	0.15–0.25	0.47–0.65
9	2820–3667	3755–4840	3	11–13	5.98–6.02	1.55–2.76	0.25–0.31	0.64–0.77
9 <sup>a</sup>	2651–4749	3952–5294	3	11–12	6.01–6.02	1.75–2.22	0.19–0.22	0.56–0.60

<sup>a</sup> Test performed on a 42 HRC heat-treated specimen.



**Figure 2.** Procedure to determine the number of first neighbours ( $n$ ) of the heat-checking cells [9]: (a) selection of a cell in the measuring mask; (b) dilatation of size 2 of the selected cell; (c) reconstruction of the cell and its neighbourhood; (d) subtraction of the central cell; (e) labelling and counting of its first neighbours; (f) cellular mosaic in which the cells are classified with a grey level related to their number of neighbours; (g) histogram of frequency distribution  $P(n)$  (probability of finding a cell with  $n$  neighbours or sides).

classified with a grey level related to their topological class  $n$  (figure 2(f)). The counting of the cells of each topological class  $n$  allowed determining the discrete probability function  $P(n)$ , as shown in figure 2(g). To compute the average number of neighbours of second order  $m(n)$  (i.e. the average number of neighbours of the cells that are adjacent to  $n$ -neighbour cells), the previous procedure was repeated for each adjacent cell of the selected  $n$ -sided cells. According to Lantuejoul's algorithm, in the particular case of two different cracks crossing at right angle, thus determining four adjacent cells, all these cells are considered as neighbours since they share a common point on their border (i.e. the intersection of the two cracks).

It should be emphasized that detailed investigations [39] have revealed that under the test conditions examined in this study, spallation of the oxide layer did not occur in the central useful area of the specimen (although some spalled areas may appear at geometrical singularities such as corners or free edges, due to growth effects leading to high strains of the oxide on highly curved surfaces). However, for maximum temperatures ( $T_{\max}$ ) of the thermal cycle lower than 550 °C, oxide scale spalling becomes a non-negligible damage

mechanism. The oxide layer then breaks preferentially by a buckling mechanism, and the heat-checking network is absent or very limited [39]. In such cases, the analysis procedure proposed here would not be appropriate.

### 3. Topological properties of the heat-checking networks

#### 3.1. Distribution of number of cell sides

Table 2 gives some topological descriptors, such as the density of cells in the heat-checking network ( $d_c$ , i.e. the number of cells  $N_c$  per mm<sup>2</sup>) and the statistical distribution of the number of cell sides  $n$  (minimum  $n_{\min}$ , maximum  $n_{\max}$ , average  $\langle n \rangle$ , variance  $\mu_2$ , fraction of 6-sided cells  $P(6)$  and cumulative fraction of 5–6–7-sided cells  $\sum_{n=5}^7 P(n)$ ). These results show that the investigated cellular patterns are composed of polygons whose number of sides lies in the range from 3 to between 10 and 14. The average number  $\langle n \rangle$  varies between 5.91 and 6.03, depending on the TF test. This is very close to the ergodic theoretical value of 6 expressed by Euler's theorem [8, 9, 14], indicating that the polygonal cells are predominantly 6-sided

**Table 3.** Least-squares fit parameters of Aboav-Weaire’s law (minimum and maximum values between the first and last cycle stops) calculated on the heat-checking networks produced under various TF test conditions on 47 HRC heat-treated specimens.

N° test	TF test conditions			Aboav-Weaire’s law (2) parameters		
	$T_{\max}$ (°C)	ht (s)	$\Phi_{\max}$ (MW m <sup>-2</sup> )	Slope of linear regression	System constant $a$	Determination coefficient $R_{AW}$
1	550	0.90	4.75	5.1–5.5	0.51–0.96	0.992–0.995
2	575	0.95	4.84	5.1–5.3	0.68–0.93	0.995–1.000
3	600	1.0	4.85	4.9–5.1	0.93–1.09	0.991–1.000
3 <sup>a</sup>	600	1.0	4.85	4.6–5.2	0.78–1.39	0.993–1.000
4	625	1.1	4.93	4.9–5.2	0.85–1.11	0.997–1.000
5	650	1.2	4.95	4.7–5.2	0.79–1.26	0.994–1.000
5 <sup>a</sup>	650	1.2	4.93	4.7–5.2	0.79–1.25	0.996–1.000
6	650	2.0	3.93	4.7–5.1	0.85–1.47	0.980–1.000
7	650	3.7	2.78	4.9–5.1	0.88–1.15	0.992–0.999
8	650	6.5	2.13	4.5–5.5	0.44–1.44	0.973–0.999
9	685	1.6	4.75	4.8–5.2	0.81–1.20	0.995–1.000
9 <sup>a</sup>	685	1.6	4.75	4.8–5.2	0.84–1.16	0.991–1.000

<sup>a</sup> Test performed on a 42 HRC heat-treated specimen.

(as in trivalent networks). In all heat-checking networks, the cells having 5, 6 or 7 sides represent 50–80% of the population. The contribution of 4-sided cells and 8-sided cells is minor, whereas cells with 3 sides and 9 sides or more are rarely observed. Rather comparable distributions of cell sides, mainly composed of a pentagonal–hexagonal–heptagonal mix, have also been reported for other cooling-induced crack networks (in thermal shocked ceramics [2] and basaltic lava flows [5]) as well as for many cellular systems (such as soap froths [8, 13], polycrystalline materials [9, 14, 34], Bénard-Marangoni convective structures [29] or polygonal terrains on Mars [32]). On the other hand, shrinkage-crack patterns generated by desiccation (such as in thin layers of dried slurries [6, 7] or in a ceramic glaze [4]) form an arrays of predominantly 4-sided polygons.

The variance  $\mu_2$ , which measures the spread in the probability distribution of cell sides  $P(n)$ , is a key indicator of the topological disorder which characterizes the deviation of the cellular structure with respect to the perfect hexagonal pattern [29]. The higher the  $\mu_2$ , the more the cells are randomly distributed in the network and the probability of finding 4-sided cell and/or 8-sided cells is high. Delannay and Le Caër [40] reported that  $\mu_2$  never exceeds 5 in natural cellular structures. The values determined on the heat-checking patterns fall in the interval 1.27–4.30 (table 2), with an average value close to 2.2. A rather comparable degree of disorder was measured in thermal shocked ceramics (where  $\mu_2 = 2.75 \pm 0.07$  [2]), Al metal grains ( $\mu_2 = 2.90 \pm 0.8$  [34]) and polygonal terrains on Mars ( $1.24 < \mu_2 < 3.46$  [32]), despite the very different size scales of these cellular networks (from  $\mu\text{m}^2$  to  $\text{m}^2$ ). However, lower values ( $\mu_2 \leq 1.5$ ) were reported, for example in biological cells, cork patterns and Bénard-Marangoni convective structures (see [41] and references therein).

### 3.2. Aboav–Weaire’s law

As indicated in table 3, all heat-checking networks satisfy the Aboav–Weaire’s law remarkably well. The slope of the regression line is close to 5, and the coefficient of determination

$R_{AW}$  is better than 0.99 in 97% of cases (the minimum  $R_{AW}$  is 0.97). The system-constant  $a$  (calculated from the slope ( $\langle n \rangle - a$ ) of equation (2)) ranges from 0.44 to 1.47. These values are in agreement with those reported in [41] for most cellular networks ( $0.5 < a < 1.5$ ). Different interpretations of this parameter are proposed in the literature. According to Zsoldos and Szasz [41],  $a$  is a numerical expression of the collectivity of the cellular pattern: the more the increase in  $a$ , the stronger the collectivity (with a maximum value of 2). A strong collectivity corresponds to the state of minimum energy for the system. It reflects the presence in the hexagonal structure of dipoles (or chains) of pentagonal and heptagonal cells, which can be regarded as ‘topological dislocations’ [8] (like the crystallographic defects or irregularities within the atomic structure of a crystalline material). These local ‘defects’ result from topological transformations (for example successive cell divisions) that change the number of sides of the cells involved. By considering the structure as an elastic solid, the topological dislocations constitute a local manifestation of plasticity [22]. In addition, Cerisier *et al* [29] have stated that  $a$  should be 1 when the cellular mosaic is evolutive, meaning that the cells can coalesce, divide or disappear (such as in polycrystallization processes [13], soap froths [28, 42] or biological tissues [25]). In our experiments, the mean value of  $a$  is slightly less than 1. We can therefore consider that our heat-checking networks are non-equilibrium structures in which the collectivity is not very strong (the results presented next in section 4.2 will confirm that the cell organization evolves effectively upon cycling).

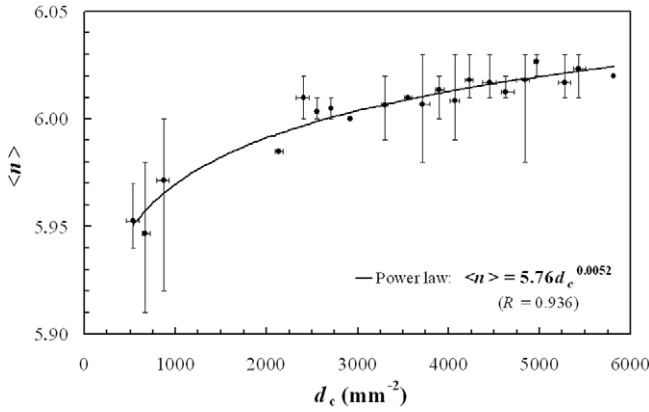
### 3.3. Lewis’ law

The linear Lewis’ law (3), relating the average area of the cells  $\langle A(n) \rangle$  to their number of sides  $n$ , is broadly verified by all heat-checking networks (table 4). Determination coefficients higher than 0.85 are found, except in four cases ( $0.635 < R_L < 0.998$ ). The slope  $\alpha$  of the linear regression shows a wide variation between 32 and 559, indicating that the mean size of the heat-checking cells may vary considerably from one test to another and during cycling. Parallely, the intercept  $n_0$  ranges

**Table 4.** Least-squares fit parameters of Lewis' law (minimum and maximum values between the first and last cycle stops) calculated on the heat-checking networks produced under various TF test conditions on 47 HRC heat-treated specimens.

N <sup>o</sup> test	TF test conditions			Lewis' law parameters in (3) and (4)			
	T <sub>max</sub> (°C)	ht (s)	Φ <sub>max</sub> (MW m <sup>-2</sup> )	Slope α (3)	Intercept n <sub>0</sub> (3)	Slope λ (4)	Determination coefficient R <sub>L</sub>
1	550	0.90	4.75	69–78	2.56–2.63	0.30–0.32	0.856–0.956
2	575	0.95	4.84	67–170	2.61–4.11	0.31–0.62	0.790–0.972
3	600	1.0	4.85	52–60	1.57–2.46	0.24–0.34	0.940–0.981
3 <sup>a</sup>	600	1.0	4.85	32–73	0.48–2.50	0.16–0.30	0.854–0.994
4	625	1.1	4.93	39–52	1.38–2.19	0.22–0.28	0.760–0.992
5	650	1.2	4.95	47–96	0.71–2.78	0.20–0.32	0.920–0.997
5 <sup>a</sup>	650	1.2	4.93	45–95	1.02–2.25	0.20–0.28	0.911–0.998
6	650	2.0	3.93	63–102	0.96–1.88	0.20–0.34	0.923–0.990
7	650	3.7	2.78	196–259	1.34–2.02	0.20–0.25	0.899–0.993
8	650	6.5	2.13	303–559	1.33–2.43	0.21–0.30	0.635–0.993
9	685	1.6	4.75	39–77	1.61–2.59	0.23–0.32	0.924–0.995
9 <sup>a</sup>	685	1.6	4.75	41–62	1.50–3.00	0.23–0.36	0.692–0.994

<sup>a</sup> Test performed on a 42 HRC heat-treated specimen.



**Figure 3.** Relation between the average number of sides  $\langle n \rangle$  of the cells and their density  $d_c$  in the stabilized heat-checking networks.

from about 0.5 to 4. In most cellular systems,  $n_0$  generally stand between 2 and 2.5 [24, 29], which is close to the average value found for the 70 heat-checking maps investigated here ( $n_0 = 2.06^{+2.05}_{-1.58}$ ). The parameter  $\lambda$  (calculated from (4), as the slope of the normalized curve  $\langle A(n) \rangle / A$  versus  $n$ ) lies in the interval from 0.16 to 0.62, with a mean value of 0.27. For comparison, values of the same order of magnitude were reported for Bénard–Marangoni convective structures (where  $\lambda = 0.23$  in the steady regime [29]), and polygonal networks on Mars ( $0.26 < \lambda < 0.51$  [32]).

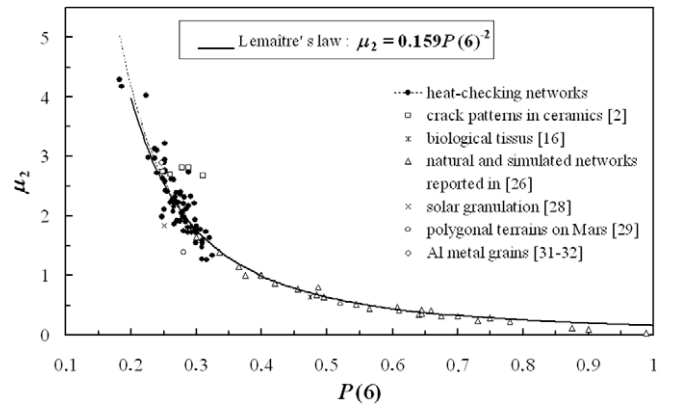
## 4. Discussion

### 4.1. Relations between topological quantities

For the stabilized crack networks, the average number of cell sides  $\langle n \rangle$  seems to be strongly linked to the cell density  $d_c$  (figure 3), according to a power law with a high coefficient of determination ( $R = 0.936$ ):

$$\langle n \rangle = 5.76 d_c^{0.0052}. \quad (6)$$

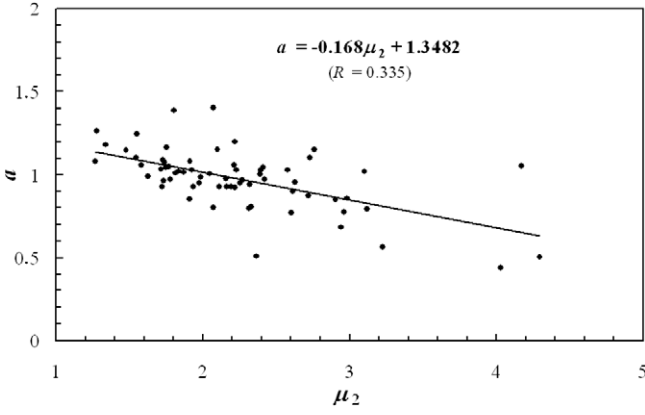
This relationship can be attributed to the fact that in finite cellular structure,  $\langle n \rangle$  increases as the number of cells increases



**Figure 4.** Universality of Lemaître's law: correlation between the variance  $\mu_2$  and  $P(6)$  for the heat-checking networks investigated in this work and other cellular structures reported in the literature.

(as stated by Euler's theorem:  $\langle n \rangle \leq 6 - 12/N_c$  [27, 30]). Such observation has also been reported in other cellular structures (two-dimensional soap froths [42], inflorescences of plants [27] and polygonal networks on Mars [32]). In our heat-checking networks,  $N_c$  varies from 323 to 4749, meaning that  $\langle n \rangle$  should theoretically vary between 5.96 and 6.00. In fact, the range of variation found experimentally is larger than expected ( $5.91 \leq \langle n \rangle \leq 6.03$ ), and values greater than 6.0 are even achieved, as also noted by Saraiva *et al.* Presumably, this could be explained by the large number of cells (much higher than in other studies) analysed in both cases.

Both the fraction of 6-sided cells  $P(6)$  and the topological variance  $\mu_2$  reflect the inhomogeneity of the cellular structure, the first inversely and the second directly since it measures the topological disorder [30]. Figure 4, plotting the variation of the topological variance  $\mu_2$  as a function of  $P(6)$ , confirms that these two thermodynamic variables are linked, despite the diversity of their origin. As can be seen, our data and those collected in the literature for others 2D cellular structures [2, 18, 29, 31, 32, 34, 35] lie on a single curve. This non-linear relationship between  $\mu_2$  and  $P(6)$  was first discovered empirically by Lemaître *et al* in two-dimensional foams [43, 44]. Lemaître's law has been expressed by Le Caër and



**Figure 5.** Linear relation between  $a$  (expressing the collectivity in Aboav-Weaire's law) and the variance  $\mu_2$ , for the heat-checking networks.

Delannay [45], and later by Rivier (based on maximum entropy analysis [46, 47]), as

$$\mu_2 \cdot P(6)^2 = 1/(2\pi) = 0.159 \text{ (for } 0.3 < P(6) < 0.7), \quad (7.1)$$

$$\text{and } \mu_2 = 1 - P(6) \text{ (for } P(6) > 0.7). \quad (7.2)$$

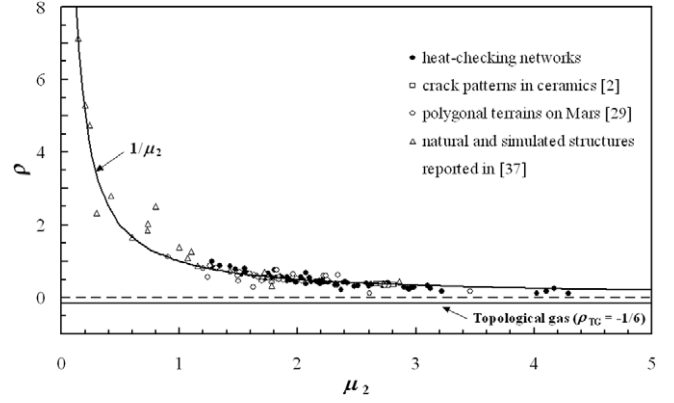
This structural equation of state, which is the equivalent of the virial equation of state in liquids and gases, is very robust for both experimental and simulated cellular systems [22, 30, 45]. The second expression (7.2) reflects an asymptotic behaviour for  $P(6) > 0.7$ . It corresponds to the case of a 'topological gas' (TG), which is an ideal model of uncorrelated arrangement of cells introduced by Fradkov [48]. Our experimental data obey (7.1) with good accuracy, confirming the universality of Lemaître's law for cellular mosaics as a consequence of maximum entropy inference [46]. Figure 4 further shows the reliability of this equation in the interval  $0.18 < P(6) < 0.3$  (hitherto not reported in the literature), indicating that Lemaître's law is also valid for highly disordered cellular networks with  $\mu_2 \geq 3$ .

It seems that the parameters of Aboav-Weaire's law ( $a$  and  $\mu_2$ ) are interdependent [40, 49]. Figure 5 shows that there is a tendency for the decrease of the system-constant  $a$  when the variance  $\mu_2$  becomes larger:

$$a = -0.168\mu_2 + 1.3482. \quad (8)$$

Even if the scattering is high ( $R = 0.335$ ), it can be noted that the slope of the linear regression curve calculated from our data ( $s = -0.168$ ) is very close to that reported by Vincze *et al* ( $s' = -1/6$ , with a coefficient of determination even lower,  $R' = 0.21$  [49]).

In figure 6 the variation of  $\rho$  (quotient  $a/\mu_2$ ) as a function of  $\mu_2$  (with  $\mu_2$  ranging from 0.14 to 4.3) is plotted, for various natural structures including our crack networks. As already established by Delannay and Le Caër [40], this figure reveals that  $\rho$  decreases quasi-universally according to a curve near  $1/\mu_2$ , and approaches an asymptotic value equivalent to that of a TG ( $\rho_{TG} = -1/6$ ) for cellular structures with a high disorder  $\mu_2$ .



**Figure 6.** Variation of  $\rho (= a/\mu_2)$  versus  $\mu_2$  for the heat-checking networks investigated in this work and other cellular structures reported in the literature.

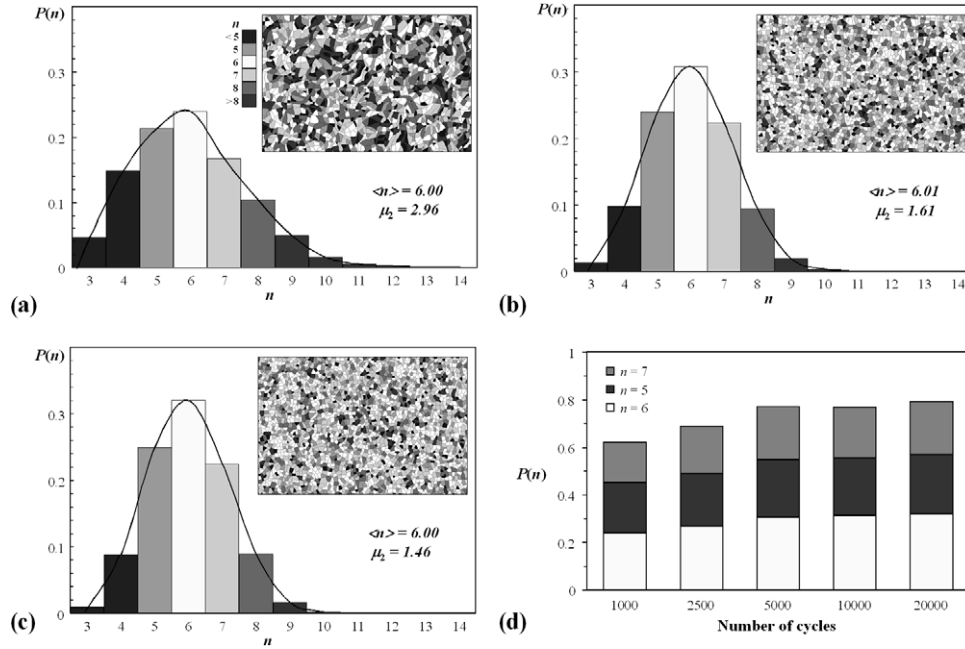
#### 4.2. Effect of the number of TF cycles

For most TF tests the topological properties of the heat-checking patterns were investigated in the early stages of cracking (for the first 500 or 1000 cycles, as indicated in table 1). Figure 7 shows that the frequency distributions of cell sides,  $P(n)$ , are quasi-normal and centred on 6. However, it should be emphasized that for a low number of cycles (i.e. when the heat-checking density is not fully stabilized or saturated [1]),  $P(n)$  is slightly asymmetric and flattened, with a smaller proportion of 6-sided cells (figure 7(a)) compared with larger numbers of cycles (figures 7(b) and (c)). Whatever the number of cycles  $N$ ,  $P(6)$  is always higher than  $P(5)$ , and  $P(5)$  higher than  $P(7)$ , as also reported for crack patterns formed in quenched ceramics [2] and basaltic lava flows [5], or for polygonal networks on Mars [32]. In addition, one can observe that the number of cells with 9 or more sides decreases or disappears with increasing  $N$  (figures 7(a)–(c)).

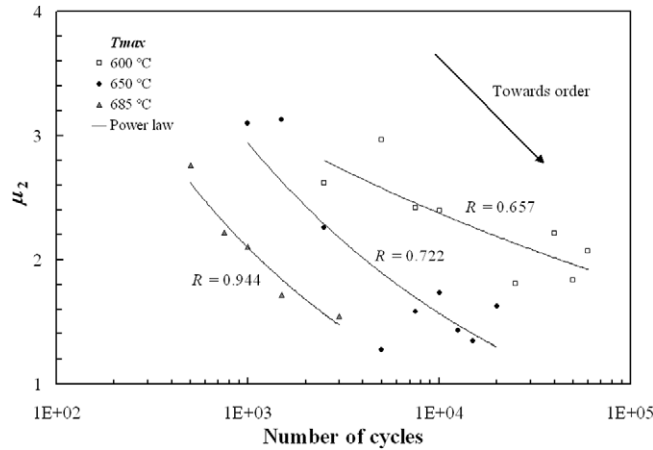
With rare exceptions, the variance  $\mu_2$  is less than 3 (table 2). According to Stavans and Glazier [8, 28, 42], such value means that the spatial disorder is 'long-lived in time' and characteristic of a non-asymptotic behaviour. This statement is confirmed by figure 8, plotting the evolution of  $\mu_2$  versus number of cycles  $N$ , which shows a decreasing trend and tends to a minimal value ( $\mu_2 < 2$ ) when  $N$  increases, regardless of  $T_{max}$ . This figure suggests that the heat-checking pattern evolves towards a more ordered geometry in the stabilized regime, without however achieving a markedly asymptotic behaviour. In soap froths, a somewhat different evolution was reported for  $\mu_2$  versus time [42]: the initially ordered cellular structure, composed mostly of hexagonal bubbles (with  $\mu_2 < 0.5$ ), widens to a maximum ( $\mu_2 = 2.65$ ) before narrowing to a steady intermediate value ( $\mu_2 = 1.5 \pm 0.2$ ) at longer times. In their experiments, Stavans and Glazier observed the evolution of the soap bubbles *in situ*, while our TF tests must be periodically interrupted to check the crack initiation. Therefore, we are not sure that the very early stages of fragmentation were observed, and a behaviour similar to soap froths cannot be completely excluded.

Both Aboav-Weaire's and Lewis' laws are satisfied throughout the whole TF cycling, as shown for test 5 in



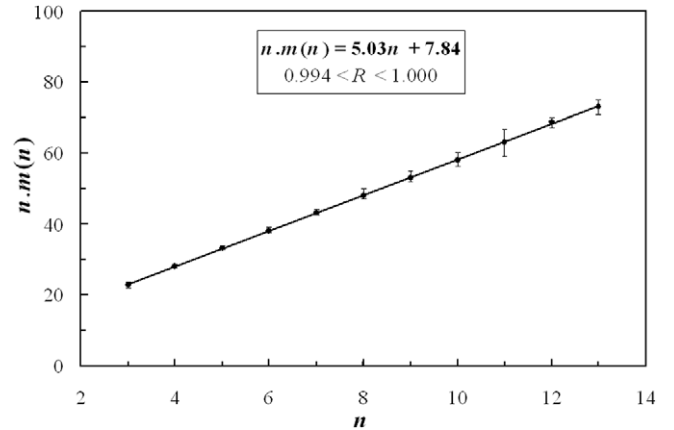


**Figure 7.** Frequency distributions  $P(n)$  of the number of cell sides at increasing number of cycles  $N$  (test 5): (a)  $N = 1000$  cycles; (b)  $N = 5000$  cycles; (c)  $N = 20000$  cycles; (d) evolution of  $P(n)$  versus  $N$ , for  $n = 5$  to  $7$ . ( $\langle n \rangle$  is the average number of sides of the cells, and  $\mu_2$  is the variance of  $P(n)$ ).



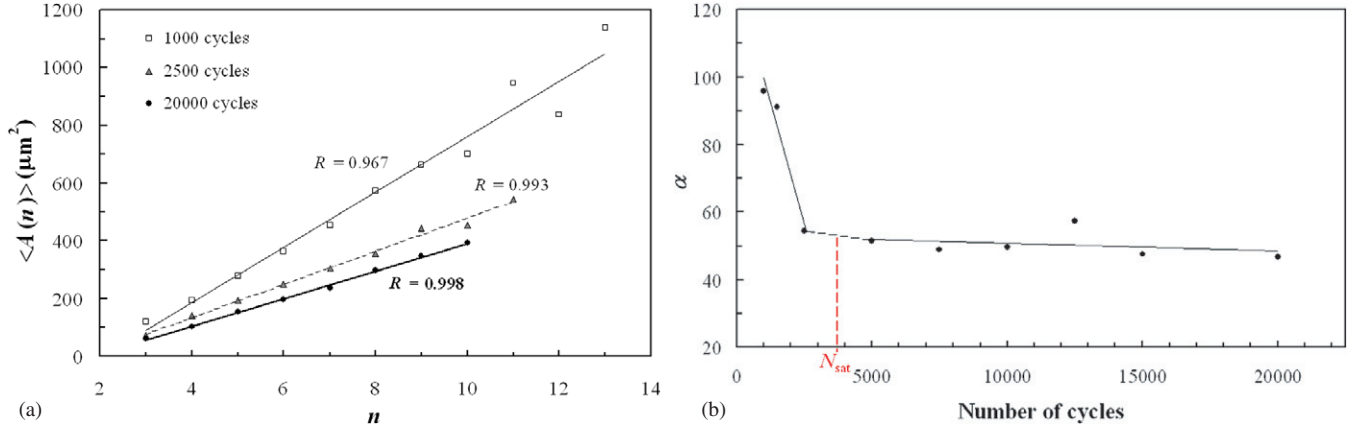
**Figure 8.** Evolution of the variance of  $\mu_2$  versus number of cycles, indicating a decreasing topological disorder in the heat-checking pattern.

figures 9 and 10(a), respectively. It should be emphasized that the coefficient of determination of both laws slightly increases with  $N$ . A higher deviation from the linear regression is, however, observed for many-sided cells (with  $n > 9$ ), that can be explained by a lower number of data for this population. This is particularly true for Lewis' law at low number of cycles, since the heat-checking cells have not yet completely reached their stabilized size [1]. Figure 10(b), showing the evolution of the slope of Lewis' law ( $\alpha$ ) as a function of the number of cycles  $N$ , indicates that  $\alpha$  decreases to an asymptotic minimal value. It was previously shown [1, 38] that the heat-checking density (which is inversely proportional to the mean cell size expressed here by  $\alpha$ ) follows a sigmoidal trend versus  $N$ , whatever the thermal cycling conditions. After an incubation period during which no crack is observed (since the oxide

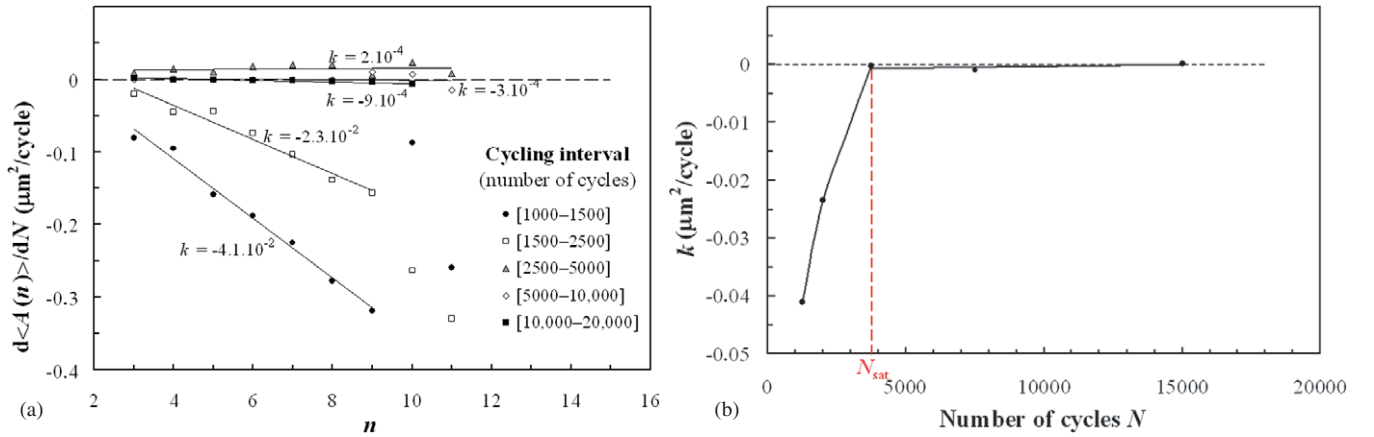


**Figure 9.** Applicability of the Aboav-Weaire's law (linear relation relating the average number of sides of cells surrounding a  $n$ -sided cell,  $m(n)$ , to  $(n)$ , for test 5. The data are the mean values of  $n \cdot m(n)$  calculated between the first (1000 cycles) and last (20000 cycles) interruption of the test, and the error bars represent their minimum and maximum values.

layer is too thin and has not achieved a critical thickness to rupture), the crack network initiates and stabilizes rapidly to a saturated density. Figure 10(b), which shows a bi-linear dependence of  $\alpha$  on  $N$ , reflects the same phenomenon. Thus,  $\alpha$  decreases strongly at the beginning of the cracking process (as shown by the first highly sloped linear portion of the curve), indicating that the heat-checking cells undergo rapidly a strong shrinking after successive cell divisions. Then, beyond a critical number of cycles ( $N_{sat}$ ) which may change depending on the test conditions [38],  $\alpha$  remains quasi-constant when  $N$  increases (corresponding to the second linear part with a near-zero slope), meaning that the cells have reached their stabilized (or saturated) size.



**Figure 10.** Applicability of Lewis' law (test 5): (a) linear relation relating the average area  $\langle A(n) \rangle$  of the cells to  $n$ , at different numbers of cycles; (b) evolution of the slope  $\alpha$  versus number of cycles.



**Figure 11.** Application of the 'modified' Von Neumann's law (9) to the heat-checking networks produced with test 5: (a) evolution of the rate of change of the average area of the cells,  $d\langle A(n) \rangle/dN$ , versus their topological class  $n$ , for various cycle intervals (the slope of the curve,  $k$ , expresses the shrinkage rate of the cells); (b) evolution of  $k$  versus number of cycles.

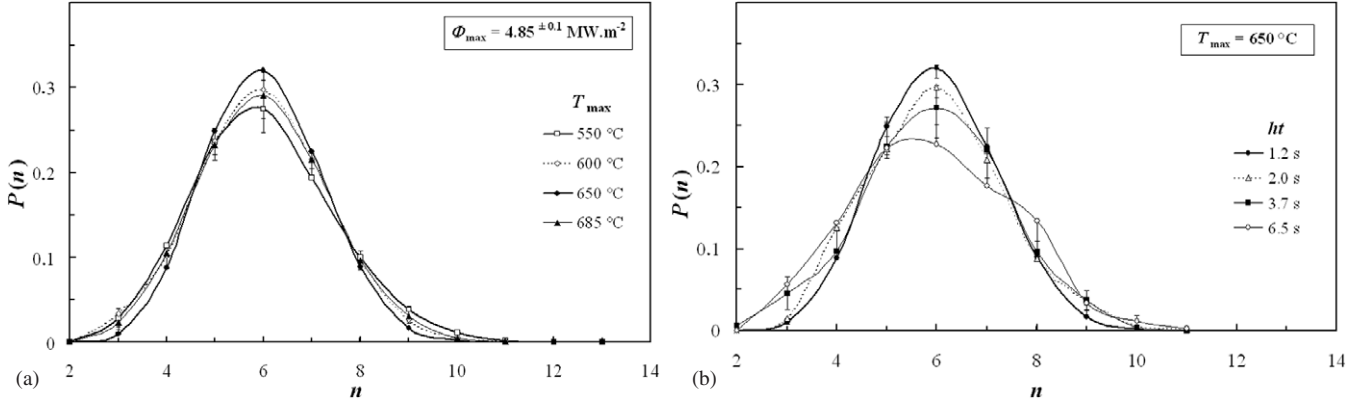
Thus, the heat-checking networks are non-equilibrium systems, whose topological and metric properties evolve with time. In figure 11(a), the rate of change of the average area of the cells,  $d\langle A(n) \rangle/dN$ , is plotted versus their topological class  $n$ , for different intervals of cycling (test 5). By excluding the cells with  $n > 9$  (which are very few in the heat-checking network), a linear evolution is observed as a function of  $n$ , for each interval between two successive cycling steps:

$$d\langle A(n) \rangle/dN = k(N) \cdot n + b, \quad (9)$$

where  $k(N)$  is called the 'rate constant', which depends on the TF cycling interval and indicates either a growth ( $k > 0$ ) or a shrinkage ( $k < 0$ ) of the cells, and  $b$  is a constant.

This expression can be considered as a 'modified' Von Neumann's law, by substituting the time  $t$  by the number of cycles  $N$  in (5) (it must be recalled that  $N$  is proportional to  $t$  for a given thermal cycle). At the beginning of the test (i.e. for low number of cycles, up to 2500 cycles in the case of test 5), a negative rate constant is observed ( $k < -2.10^{-2} \mu\text{m}^2/\text{cycle}$ ), meaning that the heat-checking cells shrink (due to their fragmentation). This behaviour is analogous to that of biological tissues (such as epidermis), where successive divisions occur under a microscopic process

called 'mitosis' [22]. It can be also noted that the linear regression curve predicts negative values of  $d\langle A(n) \rangle/dN$  even for values of  $n$  higher than 6, in contradiction with Von Neumann's law (which states a linear dependence of  $d\langle A(n) \rangle/dt$  with  $(n - 6)$ ). This is also in contradiction with experimental observations reported for bubbles in soap froths [28] and grains in polycrystalline aggregates [34, 35], which may shrink or expand in agreement with Von Neumann's law. However, even if the sign of  $d\langle A(n) \rangle/dN$  does not change according to the topological class of the cells, many-sided cells have a higher 'shrinkage rate' than few-sided cells (figure 11(a)). In addition, the cells with  $n > 10$  tend to disappear during the fragmentation process, as previously shown in the frequency distributions  $P(n)$  (figure 7(d)). Figure 11(b) indicates that the rate constant  $k$ , which expresses the rate constant of the cell size variation (slope of equation (8)), varies according to the number of cycles  $N$ . It may be noted that this curve follows the opposite trend to that of  $\alpha$  versus  $N$  (figure 10(b)). As explained above, the heat-checking cells globally shrink at the beginning of the fragmentation process, whatever their number of neighbours. Figure 11(b) better shows that the rate of shrinkage  $k$  decreases rapidly between the beginning of the fragmentation process and the number of cycles to saturation  $N_{\text{sat}}$  (as  $k$  varies from



**Figure 12.** Frequency distributions of the number of cell sides  $P(n)$  in the stabilized regime, for various maximum temperatures  $T_{\max}$  (a) and heating periods  $ht$  of the thermal cycle (b).

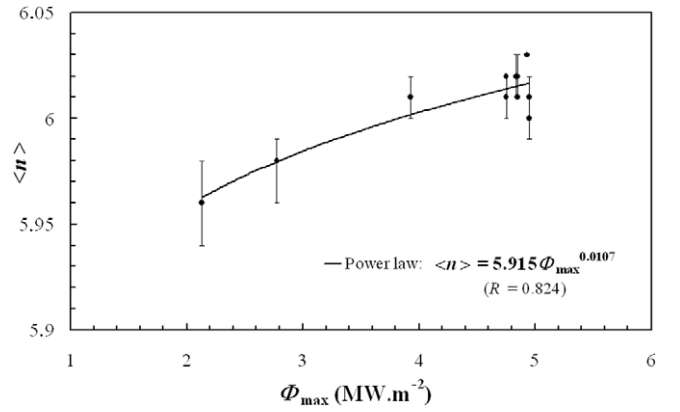
$-0.041$  to  $-0.0009 \mu\text{m}^2/\text{cycle}$ ). When the saturated regime is achieved (i.e. before 5000 cycles),  $k$  stabilizes to a constant value near zero, indicating that the cell size no longer evolves under further cycles. Thus, this curve reflects the fact that the fragmentation process is time dependent. Even if the stabilization of the crack network is rapidly achieved, this is not an instantaneous phenomenon since it takes a few thousand cycles before the cells reach their saturated size. This time dependence of  $k$  (which is equivalent to  $\gamma$  in original Von Neumann's law) was not observed in soap froths, where  $\gamma$  remains constant with time [28].

#### 4.3. Effect of TF test conditions

Focusing on the saturated heat-checking networks (when the crack density is stabilized at a high number of cycles), the effects of TF test conditions (maximal temperature  $T_{\max}$  and heating period  $ht$  of the thermal cycle) on the topological properties are investigated. Whatever  $T_{\max}$ , a Gaussian probability distribution of the number of cell sides  $P(n)$  is obtained, with a slightly more flattened shape when  $T_{\max} < 600^\circ\text{C}$  (figure 12(a)). In addition, figure 12(b) shows that the kurtosis of the distribution is lower when the heating rate  $hr$  decreases (i.e.  $ht$  increases), leading to a positively skewed distribution for the slowest thermal cycle ( $ht = 6.5$  s). The average number of cell sides does not drastically change with neither  $T_{\max}$  ( $\langle n \rangle = 6.01 \pm 0.2$ ), nor  $ht$  ( $\langle n \rangle = 5.99^{+0.03}_{-0.05}$ ). However, it seems that a relationship exists between  $\langle n \rangle$  and the maximum heat-flux density ( $\Phi_{\max}$ ) applied to the specimen during the heating period of the TF test (figure 13). It must be recalled that  $\Phi_{\max}$  depends on the test conditions and especially on the heating rate, as indicated in table 1 ( $2.13 < \Phi_{\max} < 4.95 \text{ MW m}^{-2}$  when  $85 < hr < 458^\circ\text{C s}^{-1}$  for the  $100\text{--}650^\circ\text{C}$  thermal cycle). In figure 13, data points are best-fitted by a power law (with  $R = 0.82$ ):

$$\langle n \rangle = 5.915 \Phi_{\max}^{0.0107}. \quad (10)$$

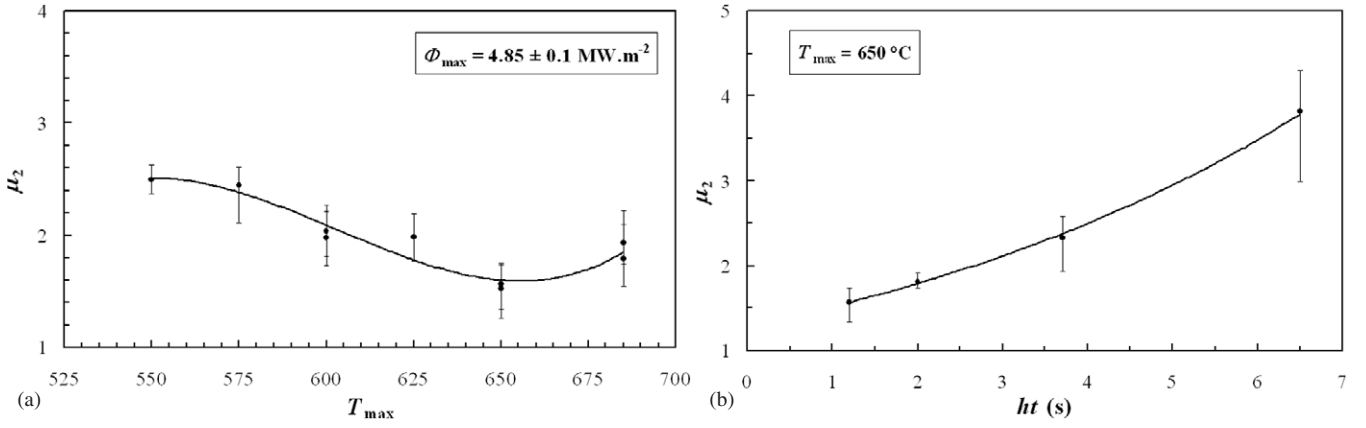
This relationship can be related to the tendency of  $\langle n \rangle$  to increase with the cell density  $d_c$ , as previously shown in figure 3. Indeed, the thermal cycles performed with a low  $\Phi_{\max}$  produce heat-checking networks with fewer cells than those performed with a high  $\Phi_{\max}$ , and vice versa (table 2).



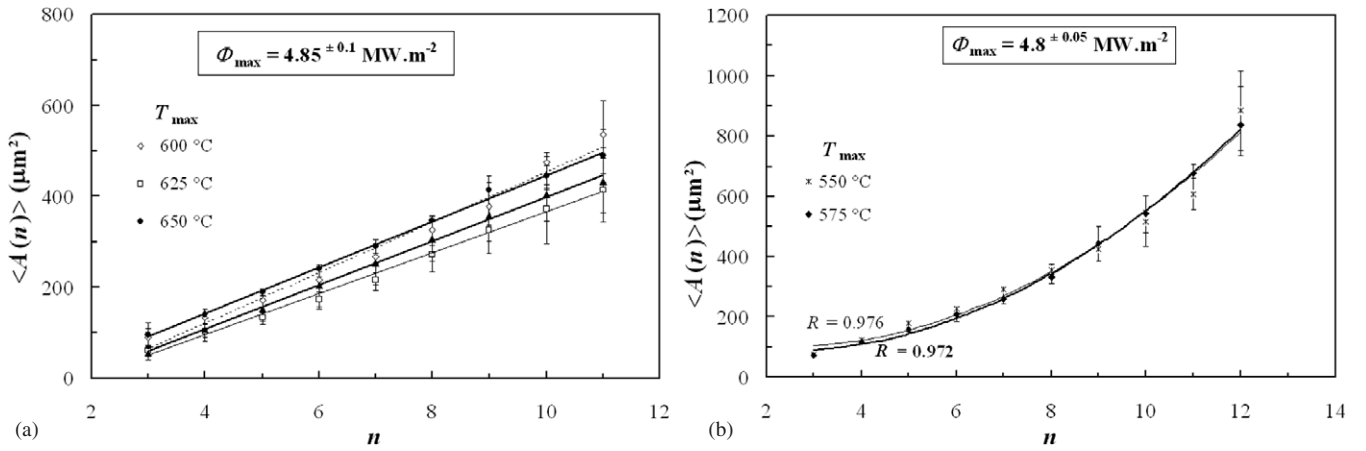
**Figure 13.** Effect of the maximum heat-flux density  $\Phi_{\max}$  on the average number of cell sides  $\langle n \rangle$ , for the saturated heat-checking networks.

No very significant effect of the steel hardness and the TF test conditions is observed on Aboav–Weaire's correlation, although the system-constant  $a$  appears to be lower when the test is performed at low  $T_{\max}$  ( $< 600^\circ\text{C}$ ) or at high  $ht$  (table 3). The topological disorder  $\mu_2$  exhibits greater variations. More disordered cellular networks (with  $\mu_2 > 2$ ) are obtained at low  $T_{\max}$ , while the most ordered organization seems to be reached at  $650^\circ\text{C}$  (figure 14(a)). On the other hand, figure 14(b) indicates that  $\mu_2$  increases by increasing  $ht$ , meaning that low heating rates tend to produce a greater deviation from geometric equilibrium, compared with fastest cycles.

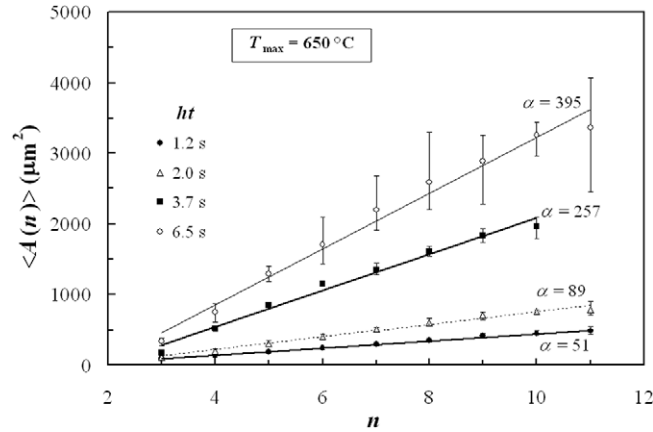
Figure 15(a) shows the effect of  $T_{\max}$  on Lewis' linear correlation, whose slope  $\alpha$  does not vary much in the saturated regime. However, it can be noted that when  $T_{\max} < 600^\circ\text{C}$  (tests 1 and 2), the dependence of  $\langle A(n) \rangle$  upon  $n$  seems rather quadratic than linear (figure 15(b)), thus improving the average correlation coefficient from 0.91 to 0.97. The failure of Lewis' law under these conditions would suggest that additional constraints to inescapable mathematical space-filling requirements are involved in shaping the heat-checking network [20–22]. In addition, figure 16 indicates that the slope of the linear regression,  $\alpha$ , is drastically increased by increasing  $ht$  (i.e. decreasing the mean heating rate  $hr$ ). The scattering from the linear regression is also larger by increasing  $ht$ , because the number of cells becomes lower (especially



**Figure 14.** Effect of the maximal temperature  $T_{\max}$  (a) and of the heating period  $ht$  of the thermal cycle (b) on the variance  $\mu_2$  in the stabilized regime ( $\mu_2$  is an indicator of the topological disorder in the cellular network).



**Figure 15.** Effect of  $T_{\max}$  on the applicability of Lewis' law in the stabilized regime: (a) classical linear variation of  $\langle A(n) \rangle$  versus  $n$ , for  $T_{\max} \geq 600 \text{ }^\circ\text{C}$ ; (b) quadratic variation of  $\langle A(n) \rangle$  versus  $n$ , for  $T_{\max} < 600 \text{ }^\circ\text{C}$ .

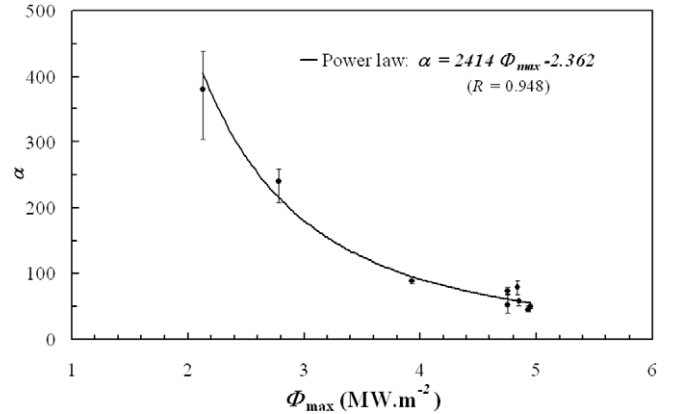


**Figure 16.** Effect of the heating period  $ht$  of the thermal cycle on Lewis' law in the stabilized regime (note that the slope  $\alpha$  increases with increasing  $ht$ ).

when  $ht \geq 3.7 \text{ s}$ . In fact, figure 17 reveals that  $\alpha$ , which is linked to the average cell area, decreases with  $\Phi_{\max}$  following a power law:

$$\alpha = 2414\Phi_{\max}^{-2.362}. \quad (11)$$

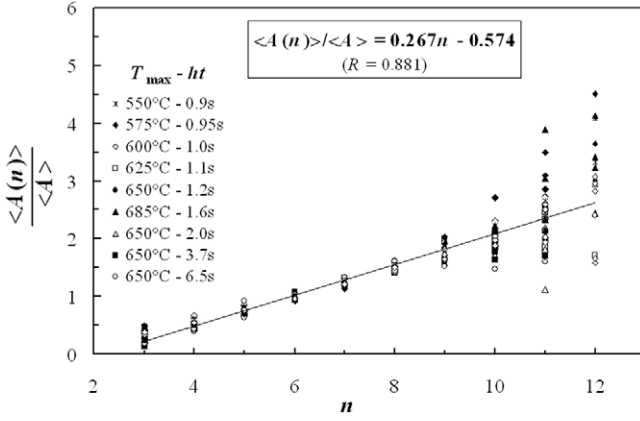
This curve, which fits our experimental points with a remarkably high coefficient of determination ( $R = 0.95$ ),



**Figure 17.** Effect of the maximum heat-flux density  $\Phi_{\max}$  on the slope of the Lewis' law  $\alpha$ , for the saturated heat-checking networks.

clearly shows that  $\alpha$  reaches an asymptotic minimum when  $\Phi_{\max}$  is greater than  $4 \text{ MW.m}^{-2}$ . It means that beyond this value, the saturated heat-checking cells would have achieved their minimum size, and could not be more fragmented. A previous study [38] revealed that the saturated crack density  $\rho_{\text{sat}}$  is dependent on the input energy (applied at the specimen surface during the heating period of the thermal cycle), which is itself linked to the maximum heat-flux density  $\Phi_{\max}$ . Thus,





**Figure 18.** ‘Universal’ normalized Lewis’ law ( $\langle A(n) \rangle / \langle A \rangle$ ) versus  $n$ ) applied to all the heat-checking networks produced with various test conditions (maximum temperature  $T_{\max}$  and heating period  $ht$ ).

$\rho_{\text{sat}}$  increases by increasing  $\Phi_{\text{max}}$ , and beyond a critical limit of the transmitted energy per unit-area,  $\rho_{\text{sat}}$  remains quasi-unchanged. Therefore, the stabilized size of the cells may vary in a wide range depending on the test conditions (and especially the heating rate of the thermal cycle). The higher the  $\Phi_{\text{max}}$  (and therefore the energy received by the specimen surface, i.e. the oxide layer), the smaller the resulting cell size. With our test facility, the maximum heat-flux density that can be achieved (by adjusting the power of the generator to 100%) does not exceed  $5 \text{ MW m}^{-2}$ , leading to heat-checking networks with a minimum cell size of about  $15\text{--}20 \mu\text{m}$  [38]. Once the heat-checking network is initiated and stabilized, increasing the number of thermal cycles leads to propagation of the micro-cracks of the oxide layer in the steel substrate. Under such conditions, the thermally induced mechanical energy is dissipated by the crack propagation inwards of the steel, rather than by subdividing the heat-checking cells [39]. The interaction between the thermal stresses and oxidation ahead of the crack tip modifies the oxidation diffusion paths. In fact, due to in-depth crack propagation, localized pit oxidation occurs preferentially to the formation of oxide on the surface of the specimen. Therefore, fewer driving forces are available to subdivide the existing cells.

By plotting the normalized area of the cells,  $\langle A(n) \rangle / \langle A \rangle$ , versus their topological class  $n$  (normalized Lewis’ law) for all test conditions (figure 18), all data points tend to cluster on a single curve, namely the linear law:

$$\langle A(n) \rangle / \langle A \rangle = 0.267n - 0.574. \quad (12)$$

Despite a higher scattering for the many-sided cells ( $n > 8$ ), a quite good coefficient of determination is obtained ( $R = 0.88$ ). This result indicates that irrespective of the TF test conditions, the heat-checking networks are similar apart from a size scaling factor, suggesting that the same rules govern the shaping of the cellular structure in the stabilized state. However, as previously shown, the cell organization could be affected, under some test conditions, by additional forces to the inescapable space-filling constraints. Actually, during our TF experiment, the maximum heat-flux density imposed on the specimen generates thermo-mechanical loading by self-constraining [38]. This thermo-

physical constraint contributes to the shaping of the heat-checking network, under certain conditions (low  $T_{\max}$  and low  $ht$ ).

The steel grade investigated in this study is commonly used as a tool material in hot-forming processes, such as die-casting or forging. In service, the tools suffer from thermal and mechanical solicitations, which can be reproduced at a lower scale by our TF test [1, 38]. In the run of industrial application, this work shows that by changing the test parameters (in particular the heat-flux density by modifying the heating rate of the thermal cycle), heat-checking networks with various cell sizes can be generated. It is well known that the TF life is considerably reduced when the superficial heat-checking network is denser, because these micro-cracks contribute to weakening the steel by accelerating the oxidation mechanisms and the initiation of macro-cracks that propagate through the tool material as a result of accumulated thermo-mechanical solicitations [39]. Therefore, better controlling the heat exchanges between the tool and the processed parts could be an interesting way to improve the life of hot-working tools in service [38].

## 5. Conclusions

This paper presents an experimental investigation on the topological properties of microscopic heat-checking patterns formed under thermal fatigue on the oxidized surface of a X38CrMoV5 steel specimen. 300 and 6000 cells were analysed in each polygonal crack network, leading to statistically relevant results. An average number of sides per cell very close to the ideal value expressed by Euler’s theorem is found ( $\langle n \rangle = 6.0_{-0.09}^{+0.03}$ ), indicating that the cellular networks are pseudo-hexagonal. The applicability of general topological laws (such as Aboav–Weaire’s and Lewis’) is verified, meaning that geometric correlations do not extend beyond adjacent cells in the polygonal network, and that the shaping of the network is governed by space-filling constraints [8]. The topological properties of the microscopic heat-checking networks are broadly consistent with those reported in the literature for crack patterns in thermal shocked ceramics or for polygonal terrains on Mars, which suggests that these random cellular systems are governed by the same rules despite their very different scale. The universality of Lemaître’s law is confirmed, and its domain of validity extended to highly disordered structures.

It is shown that the heat-checking networks are non-equilibrium systems, as their topological and geometrical properties change with the number of cycles. The topological disorder, estimated by the variance of  $P(n)$ , is rather high ( $\mu_2 = 2.22_{-0.95}^{+2.08}$ ). It decreases when increasing the number of cycles, and evolves towards a geometric equilibrium with  $\mu_2 < 2$ . A greater disorder is achieved for lower maximal temperatures ( $T_{\max} < 600 \text{ }^\circ\text{C}$ ) and lower heating rates. It is shown that the heat-checking cells undergo a strong shrinkage at the beginning of the thermal cycling. A modified version of Von Neumann’s law is established, relating the rate of change of the average area of the cells to their topological class.

Whatever the number of cycles and the TF test conditions, the linear Aboav–Weaire’s law is satisfied with a correlation

coefficient always greater than 0.97. The system-constant is near 1 on average ( $a = 0.96 \pm 0.52$ ). The Lewis' law, which states a linear relationship between the average area of the cells and their number of sides, is generally obeyed with a slope ( $32 < \alpha < 559$ ) mainly depending on the thermal cycling conditions (and especially the heating rate). However, better correlation coefficients are achieved when the heat-checking pattern is stabilized (for a high number of cycles), and at higher maximum temperatures ( $T_{\max} > 600^\circ\text{C}$ ). Below this  $T_{\max}$ , the best-fit correlation is quadratic rather than linear, suggesting that physical forces (related to the maximum heat-flux density applied to the specimen surface) are involved in the fragmentation process. Neither the intercept ( $n_0 = 2.06^{+2.05}_{-1.58}$ ) nor the 'ageing' parameter ( $\lambda = 0.27^{+0.35}_{-0.11}$ ) of Lewis' law appears related to the test conditions. It is shown that for stabilized cracks networks, the maximum heat-flux density ( $\Phi_{\max}$ ) influences both the average number of sides ( $\langle n \rangle$ ) and the average size of the heat-checking cells (i.e. the slope  $\alpha$  of Lewis' law). Whatever the test conditions, a unique normalized Lewis' law is found, indicating that the stabilized cellular networks are indistinguishable apart from a scale factor (the average cell size).

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