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# Remarkable enhancement of the Selective Catalytic Reduction of NO at low temperature by collaborative effect of ethanol and NH<sub>3</sub> over Silver supported catalyst.

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**Abstract:** The NO<sub>x</sub> selective catalytic reduction (SCR) is extensively studied as an effective process for air pollutants abatement from lean burn and Diesel vehicles. In the implemented Urea-SCR technology, the NO<sub>2</sub>/NO<sub>x</sub> ratio is a key parameter that limits the deNO<sub>x</sub> efficiency at low temperature (175-250°C). We demonstrate that co-feeding of ammonia and ethanol on a Ag/Al<sub>2</sub>O<sub>3</sub> catalyst enables a drastic enhancement of the NO<sub>x</sub> conversion at temperatures below 200°C using only NO as NO<sub>x</sub> (standard SCR condition). Even if NO<sub>2</sub> is provided at low temperature by the NO oxidation over Ag/Al<sub>2</sub>O<sub>3</sub> in presence of EtOH, the NO<sub>x</sub> conversion improvement is not only due to a direct reaction between NH<sub>3</sub> and NO<sub>x</sub>, but mainly attributed to the availability of hydrogen H\* species resulting from EtOH oxidation (similar to a H<sub>2</sub> assisted NH<sub>3</sub>-SCR process). Due to the presence of remaining NH<sub>3</sub> and NO<sub>2</sub> (formed over Ag/Al<sub>2</sub>O<sub>3</sub> catalyst), further deNO<sub>x</sub> efficiency improvement was obtained at low temperature by addition of a NH<sub>3</sub>-SCR catalyst (WO<sub>3</sub>/Ce-Zr). The critical dependence of the SCR process on the Diesel Oxidation Catalyst (DOC) efficiency at low temperature is thus avoided.

#### 1. Introduction

Air pollution is responsible of direct harmful effects on human health with hundred thousand deaths per year throughout the world [1]. Consequently, stringent standards regulate pollutants emissions such as for nitrogen monoxide (NO) and nitrogen dioxide (NO<sub>2</sub>) from stationary and mobile sources.

Worldwide, the introduction of three way catalyst (TWC) converters for gasoline spark ignition engines noticeably contributed to increasing the air quality [2-4]. However, for internal combustion engines operated in excess of air, such as Diesel engines, TWC converter is unable to efficiently reduce NO<sub>x</sub> into N<sub>2</sub> and the implementation of selective catalytic reduction (SCR) technology, with a large choice of reductants, is described as one of the most promising way to control NO<sub>x</sub> emissions in lean media.

Among the various possible reductants, ammonia (or urea used as NH<sub>3</sub> provider), hydrocarbons (propene, propane, decane...), ethanol (EtOH) were widely studied. Interestingly, whatever the considered reductant, the mechanistic studies generally suggest that N<sub>2</sub> is obtained *via* the formation of species like –CN and –NCO, which are known to be involved in ammonia formation. Indeed, such species were identified during the lean NO<sub>x</sub> reduction by propene over LaFe<sub>1-x</sub>(Cu, Pd)xO<sub>3-6</sub> perovskites [5], supported transition metals like Cu/Ti<sub>0.7</sub>Zr<sub>0.3</sub>O<sub>2</sub> [6], or supported noble metals like Rh/TiO<sub>2</sub> [7]. NH<sub>3</sub> intermediate species was also clearly identified over Cu-ZSM-5 exchanged zeolite when propane [8] or decane [9] are used, as well as during the NO<sub>x</sub> reduction process by ethanol over Ag/Al<sub>2</sub>O<sub>3</sub> catalyst [10]. These examples point out the key role of the ammonia-like intermediate species in the deNO<sub>x</sub> pathway, whatever the considered reductant and the type of catalyst (noble metal, oxide, zeolite...).

To meet the current environmental standards limiting the NO<sub>x</sub> emission from Diesel vehicles, the automotive industry has commonly adopted the Urea-SCR technology. The use of an aqueous urea solution as ammonia precursor is a safe and operational adaptation of the NH<sub>3</sub>-SCR technology initially developed for stationary sources. Urea (NH<sub>2</sub>-CO-NH<sub>2</sub>) is theoretically decomposed in ammonia via two consecutives reactions: urea thermal decomposition and HNCO hydrolysis reactions. Thereafter, NO<sub>x</sub> reduction is assumed to be correlated with NH<sub>3</sub> yield and supposed to follow similar pathways than those demonstrated with ammonia reductant:

$$NO + NO_2 + 2NH_3 \rightarrow 2N_2 + 3H_2O \tag{1}$$

More precisely, the fast-SCR reaction (Eq. 1) results from sequences involving ammonium nitrate or related surface species as intermediates (Eq. 2, Eq. 3):

$$2NO_2 + 2NH_3 \rightarrow N_2 + NH_4NO_3 + H_2O \tag{2}$$

$$NO + NH_4NO_3 \rightarrow N_2 + NO_2 + 2H_2O \tag{3}$$

Firstly, ammonium nitrate formation (Eq. 2) involves NO<sub>2</sub> reactivity by dimerization (Eq. 4), disproportionation (Eq. 5), and successive reaction to form N<sub>2</sub> (Eq. 6) and ammonium nitrate (Eq. 7). The second step of the fast-SCR chemistry (Eq. 3) implies the NO reactivity with ammonium nitrate which proceeds via the NO oxidation by nitric acid (Eq. 8) followed by reaction of NH<sub>3</sub> with nitrous acid to form N<sub>2</sub> (Eq. 6). As a result, conversion of nitrogen oxides is optimized when NO, NO<sub>2</sub> and NH<sub>3</sub> respect a 1:1:2 ratio, enabling the stoichiometric reaction of fast SCR and is intimately related to HONO/HNO<sub>3</sub> reactional pathway [11-15]. Finally, N<sub>2</sub> is obtained by decomposition of ammonium nitrite (Eq. 6). With many practical catalysts and regardless the used reductant, this reaction is commonly suggested to be the final step of deNO<sub>x</sub> chemistry [16-19].

$$2 \text{ NO}_2 \rightleftarrows \text{N}_2\text{O}_4 \tag{4}$$

$$N_2O_4 + H_2O \rightleftharpoons HONO + HNO_3$$
(5)

$$NH_3 + HONO \rightleftharpoons NH_4^+ + NO_2^- \rightleftharpoons NH_4NO_2 \rightarrow N_2 + 2H_2O$$
(6)

$$NH_3 + HNO_3 \rightleftarrows NH_4^+ + NO_3^- \rightleftarrows NH_4NO_3$$
(7)

$$NO + HNO_3 \rightleftharpoons NO_2 + HONO$$
 (8)

Unfortunately, the on-board Urea-SCR technology suffers from a poor activity at low temperatures (200°C) due to an insufficient  $NO_2/NO_x$  ratio to promote the fast SCR stoichiometry (Eq. 1) [20].  $NO_2$  yield can be adjusted by the Diesel oxidation catalyst (DOC) upstream of the SCR converters, but the oxidation activity is also strongly dependent on both temperature and operating conditions. Recently an over-injection of aqueous solution of ammonium nitrate (Eq. 9) was reported to enhance the de $NO_x$  efficiency while avoiding NO pre-oxidation [11].

$$2NO + 2NH_3 + NH_4NO_3 \rightarrow 3N_2 + 5H_2O \tag{9}$$

EtOH-SCR process was also described as an attractive way to reduce NO<sub>x</sub>, especially due to the practicality/availability of ethanol and its relative safety. Silver-based materials were found to be the most active and selective for the NO<sub>x</sub> reduction by oxygenates reductant compounds [19,21]. With ethanol as reductant, the NO conversion is assumed to be strongly dependant of the nitromethane route, based on the ethanol oxidation to acetaldehyde via a variety of intermediates which are subsequently adsorbed, such as surface acetate and ethoxide ions leading to the global reaction (Eq. 10):

$$C_2H_5OH + 6NO \rightarrow 3N_2 + 2CO_2 + 3H_2O$$
 (10)

N-containing compounds as HNCO and ammonia are also eventually produced [10,22-26] as surface organic intermediate. A detailed surface mechanism for the SCR of NO<sub>x</sub> with ethanol on silver alumina catalyst was proposed by Tham *et al.* [24]. In summary, the first step of the reaction framework results in  $C_2H_5OH$  dissociative adsorption into surface ethoxide  $C_2H_5O^*$  and surface hydrogen H<sup>\*</sup> ad-species (Eq. 11) [26]. Thereafter, ethoxide can be consumed either by the oxidation pathway to yield acetaldehyde (Eq. 12) or by the NO<sub>x</sub> reduction pathway via nitromethane route (Eq. 13-16).

$$C_2H_5OH \rightarrow C_2H_5O^*_{(ad)} + H^*_{(ad)}$$
(11)

$$C_{2}H_{5}O^{*}_{(ad)} \rightarrow CH_{3}CHO^{*}_{(ad)} + H^{*}_{(ad)} \rightarrow CH_{3}CHO$$
(12)

$$CH_{3}CHO^{*}_{(ad)} + O^{*}_{(ad)} \rightarrow CH_{3}COO^{*}_{(ad)} + H^{*}_{(ad)} \rightarrow CH_{3}COOH$$
(13)

 $CH_{3}COO^{*}_{(ad)} + NO_{2} \rightarrow CH_{3}NO_{2} + CO_{2}$ (14)

$$CH_3NO_2 \rightarrow HNCO + H_2O \tag{15}$$

$$HNCO + H_2O \rightarrow NH_3 + CO_2$$
(16)

Interestingly, the formation of ammonia *via* the isocyanate hydrolysis route (Eq. 9) takes place in this reaction pathway. It is assumed that the reaction pathway then follows very similar routes to those reported for the  $NH_3$ -SCR reaction, with  $N_2$  formation from ammonium nitrite decomposition (Eq. 6).

Unfortunately, the deNO<sub>x</sub> activity of the EtOH-SCR technology at low temperatures appears not sufficient for a practical application to the next generation of the energy-efficient Diesel vehicles, especially due to the rate limiting step of  $CH_3NO_2$  formation at T<250-300°C. However, some studies reported that an improvement of NO<sub>x</sub> reduction efficiency of EtOH-SCR technology at low temperature is possible. For instance, addition of hydrogen into the reaction mixture allows an enhancement of the deNO<sub>x</sub> efficiency. It was advanced that H<sub>2</sub> addition promotes the partial oxidation of C<sub>2</sub>H<sub>5</sub>OH to form enolic species which mainly contribute to accelerate NO<sub>x</sub> reduction [27-29]. Note that Ag/Al<sub>2</sub>O<sub>3</sub> catalysts were reported to exhibit a poor activity in NH<sub>3</sub>-SCR but they become very active in case of H<sub>2</sub> addition [30-32]. An improvement of the N<sub>2</sub> yield can also be obtained modifying the alumina support to form surface zinc aluminates [21]. Indeed, an activation of the ethanol conversion in acetaldehyde was observed, but mainly from 250-300°C.

Interestingly, the ethanol dehydrogenation leading to acetaldehyde appears concomitant with a high proportion of NO<sub>2</sub> emission from NO oxidation, as previously reported by Flura *et al.* [23]. This NO<sub>2</sub> formation at relatively low temperature (from 150°C) may also favourably interfere in the SCR process, favouring the fast SCR reaction (Eq. 1). Moreover, the formation of ammonia by the isocyanate hydrolysis route (Eq. 9) appears in the EtOH-SCR reaction pathway. Ammonia was detected for

temperature higher than 250°C, when  $NO_x$  reach a high conversion level [23]. It could indicates that ammonia is a key intermediate species, but with a too low production rate at low temperature.

Obviously, N<sub>2</sub> yield of EtOH-SCR process seems to appear strongly dependant to subsequent ammonia route formation. Thus, in the present work, we studied the role of ammonia as co-reactant species for assisted EtOH-SCR process in NO rich media for future application in a coupled Urea/Ethanol-SCR process. Particular attention was paid to increasing the efficiency of EtOH-SCR system at low temperatures (T=175-250°C) while overcoming the NO<sub>2</sub> yield of the DOC.

#### 2. Experimental part

#### 2.1 Materials

Silver supported catalyst was selected to conduct EtOH-SCR experiments due to their high reactivity toward oxygenated compounds [33-35]. Alumina support was provided by Axens and exhibited a specific surface area of  $170 \text{ m}^2 \text{ g}^{-1}$  after calcination 4 hours under air at 700°C. Silver (2.0 <sub>wt.</sub>%, which is commonly described as the optimal loading [36]) was added by impregnation of AgNO<sub>3</sub> dissolved in ethanol [21,23,37]. Sample was finally calcined under synthetic air with 10 % H<sub>2</sub>O at 700°C for 4 h and is noted Ag/Al.

 $WO_3/Ce_xZr_{1-x}O_2$  catalyst was selected as NH<sub>3</sub>-SCR material [38-40]. Ceria-zirconia support (40 <sub>wt</sub>% of CeO<sub>2</sub>) was provided by Solvay. This solid solution, was first calcined 4 hours under air at 700°C before use and exhibited a specific surface area of 73 m<sup>2</sup> g<sup>-1</sup>. Tungsten (6 <sub>wt</sub>% WO<sub>3</sub>) was added by impregnation at 60°C under continuous agitation using an aqueous solution of ammonium metatungstate. After drying at 80°C, the preparation was placed in an oven at 120°C during a night. Finally, the solid was calcined under synthetic wet air (10 % H<sub>2</sub>O) during 4h at 700°C. The obtained catalyst is noted WO<sub>3</sub>/Ce-Zr.

#### 2.2 Characterization

Specific surface areas were determined by BET method (Tristar 3000, Micromeritics) using nitrogen adsorption at 77 K. Prior to the  $N_2$  physisorption, the samples were degassed under vacuum 2 h at 250°C. The Ag/Al and WO<sub>3</sub>/Ce-Zr catalysts exhibited specific surface areas of 160 and 52 m<sup>2</sup> g<sup>-1</sup>, respectively.

The powder XRD patterns of Ag/Al was collected using an Empyrean (PANalytical) diffractometer. Data acquisition was recorded from 20° to 120° (20) with a scanning step of 0.1°. X-ray diffraction pattern

evidenced the  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> phase [ICDD PDF n° 00-050-0741(I)] with no visible reflection assigned to silver species (Ag<sup>0</sup>, Ag<sub>2</sub>O, AgO, Ag<sub>2</sub>Al<sub>2</sub>O<sub>4</sub>...).

Temperature programmed reduction (TPR) experiments were performed on a Micromeritics Autochem 2920 apparatus equipped with a thermal conductivity detector (TCD). Sample of about 100 mg was placed in a U-shape quartz reactor. Prior to the TPR measurements, the sample was calcined at 500°C for 60 min under O<sub>2</sub> flow (heating rate: 5°C min<sup>-1</sup>). The sample was cooled down to room temperature, and it was purged under Ar flow for 45 min. The reduction was carried out under 1 vol.% H<sub>2</sub> in Ar flow up to 500 °C (heating rate: 5°C min<sup>-1</sup>). TCD signal being sensible to water, an H<sub>2</sub>O-trap was added downstream of the reactor, allowing the quantification of the H<sub>2</sub> consumption during the TPR experiment. H<sub>2</sub>-TPR experiment of Ag/Al showed a broad H<sub>2</sub> consumption peak, with a maximum at around 260°C. Hydrogen consumption indicated that 33 % of the deposited silver was in metallic state, according to results previously reported by Musi *et al* [41].

Transmission Electron Microscopy (TEM) micrographs were recorded on JEOL 2100 instrument (operated at 200 kV with a LaB<sub>6</sub> source and equipped with a Gatan Ultra scan camera). TEM experiments showed that  $Ag/Al_2O_3$  presents small silver particles, most of the particles ranging below 3 nm (Supplementary information (SI) file, Figure S1).

Infrared characterization was carried out with a Nicolet 6700 infrared spectrometer equipped with a MCT detector and a KBr beamsplitter using a resolution of 4 cm<sup>-1</sup> and 126 scans. A home-made designed cell (SI file, Figure S2) that allows *in situ* treatment and high temperature adsorption of probe molecule was used. The cell was connected to a vacuum manifold system which could supply nitric oxide, ethanol, ammonia and oxygen. Silver supported catalyst was pressed as self-supported wafer (disc of about 20 mg, 2 cm<sup>2</sup>) and was firstly treated *in situ* at 400°C under vacuum (residual pressure of about 5.10<sup>-5</sup> hPa). The calibrated doses of desired gas mixture were successively added at 200°C up to equilibrium pressure. Three gas mixtures (EtOH-O<sub>2</sub>, NO-O<sub>2</sub> and NH<sub>3</sub>) and combinations of co-adsorption (EtOH-O<sub>2</sub>+NH<sub>3</sub>, NO-O<sub>2</sub>+NH<sub>3</sub>, EtOH-O<sub>2</sub>+NH<sub>3</sub>) were particularly studied. For EtOH-O<sub>2</sub> and NO-O<sub>2</sub> mixtures, the O<sub>2</sub>/reductant pressure ratio was fixed at 5. The spectra presented in this paper were normalized to a disc of 10 mg cm<sup>-2</sup> and the reference spectra (recorded at 200°C after calcination) was systematically subtracted to highlight the adsorbed species.

#### 2.3 Catalytic tests

Catalytic tests were performed in a quartz tubular micro-reactor under a synthetic flow simulating a realistic Diesel engine exhaust. The total flow rate was fixed at 333 mL.min<sup>-1</sup> for 100 mg of powdered catalyst diluted in 100 mg SiC, both sieved between 100  $\mu$ m and 250  $\mu$ m, corresponding to a GHSV of

130 000 h<sup>-1</sup> toward the catalyst (200 L h<sup>-1</sup>  $g_{cata}$ <sup>-1</sup>; 100 L h<sup>-1</sup>  $g_{powder}$ <sup>-1</sup>). For the dual-bed configuration, 100 mg of WO<sub>3</sub>/Ce-Zr were placed downstream 100 mg of Ag/Al catalyst (no SiC for these experiments).

Three reductants were evaluated, namely ethanol (EtOH), NH<sub>3</sub>, and a blend (EtOH+NH<sub>3</sub>). The compositions of the gas mixtures for the various catalytic tests are reported in Table 1. Gaseous NO/NO<sub>2</sub>/NH<sub>3</sub>/O<sub>2</sub>/N<sub>2</sub> gas flows were adjusted by mass-flow controllers (Bronkhorst). Ethanol aqueous solution (8.02 10<sup>-1</sup> mol L<sup>-1</sup>) was vaporized and mixed upstream the SCR catalyst by means of a micro-nozzles provided by The Lee Company ( $Ø_{nozzle}$ = 50 µm) connected to a HPLC pump (Jasco, PU-2085, 22 µL min<sup>-1</sup>,  $\Delta$ P=10 Bar). The compositions of the feed gas and effluent stream were monitored continuously using online MKS 2030 Multigas infrared analyser for NO, NO<sub>2</sub>, N<sub>2</sub>O, HNCO, NH<sub>3</sub>, CH<sub>3</sub>CH<sub>2</sub>OH, CH<sub>3</sub>CHO, CH<sub>3</sub>OH, CH<sub>2</sub>O, C<sub>2</sub>H<sub>4</sub>, CH<sub>4</sub>, CO, CO<sub>2</sub> and H<sub>2</sub>O.

**Table 1.** Composition of the Gas mixtures of the SCR tests (total rate: 333 mL min<sup>-1</sup> for 100 mg of powdered catalyst).

Catalytic test	NO (ppm)	NO2 (ppm)	NH₃ (ppm)	C₂H₅OH (ppm)	H₂ (ppm)	O2 (%)	CO2 (%)	H₂O (%)	N <sub>2</sub>
Standard-NH <sub>3</sub> -SCR	400		400			10	10	8	
Fast-NH <sub>3</sub> -SCR	200	200	400			10	10	8	
EtOH-SCR	400			1200		10	10	8	balance
(EtOH+NH₃)-SCR	400		400	1200		10	10	8	
H <sub>2</sub> -SCR	400				400	10	10	8	

#### 3. Results and discussion

The NO reduction by ethanol (EtOH-SCR condition, Table 1) over Ag/Al catalyst is the reference test in this study. EtOH and NO concentrations were fixed at 1200 ppm and 400 ppm respectively, corresponding to a usual C/N ratio of 6 [10,21,23]. First, note that N<sub>2</sub>O emissions were limited at a very low level whatever the involved catalytic system. More precisely, N<sub>2</sub>O was detected with a maximum concentration of 6 ppm from 250 to 500°C in EtOH-SCR condition. The maximum N<sub>2</sub>O concentration (11 ppm) was recorded at 450°C over Ag/Al catalyst in (EtOH+NH<sub>3</sub>)-SCR condition.

#### 3.1 Highlight of the (EtOH+NH<sub>3</sub>) collaborative effect on NO SCR

To highlight the beneficial effect of  $(EtOH+NH_3)$  co-feeding on the NO reduction rate over Ag/Al, Figure 1 reports the evolution of outlet gas feed composition *versus* time on stream for NO, NO<sub>2</sub>, C<sub>2</sub>H<sub>5</sub>OH, and NH<sub>3</sub> over Ag/Al catalyst at 200°C, before and after NH<sub>3</sub> co-addition.



**Figure 1.** Effect of NH<sub>3</sub> co-feeding (400 ppm) at 200°C on NO<sub>x</sub> (NO, NO<sub>2</sub>), C<sub>2</sub>H<sub>5</sub>OH, and NH<sub>3</sub> outlet concentrations over Ag/Al in EtOH-SCR (400 ppm NO, 1200 ppm C<sub>2</sub>H<sub>5</sub>OH, 8 % H<sub>2</sub>O, 10 % CO<sub>2</sub>, 10 % O<sub>2</sub> balanced in N<sub>2</sub>).



**Figure 2.** Comparison of EtOH-SCR (blue) and (EtOH+NH<sub>3</sub>)-SCR (red) behaviour in NO<sub>x</sub> conversion (full line) and EtOH conversion (dotted line) over Ag/Al catalyst.

With only ethanol as reductant (EtOH-SCR condition), NO<sub>x</sub> conversion reached 9 % and a significant NO<sub>2</sub> outlet concentration was recorded at 225 ppm, which corresponds to a NO<sub>2</sub>/NO<sub>x</sub> outlet ratio of 0.6. In the same time, the C<sub>2</sub>H<sub>5</sub>OH conversion reached at 35 %.

At t=200 s, 400 ppm NH<sub>3</sub> was added to the reaction mixture ((EtOH+NH<sub>3</sub>)-SCR, Table1). Outlet profiles of NO and NO<sub>2</sub> dropped rapidly to quadrupled the NO<sub>x</sub> conversion (up to 38 %), together with NH<sub>3</sub> consumption. In parallel, ethanol and acetaldehyde outlet concentrations remained unchanged after few oscillations associated with gas feed stabilization. Obviously,  $NH_3$  addition to EtOH-SCR system showed a dramatic benefit for the  $NO_x$  conversion at low temperature and in NO rich media.

This significant deNO<sub>x</sub> enhancement is also reflected in a wider temperature range. Conversions of EtOH and NO<sub>x</sub> for EtOH-SCR and (EtOH+NH<sub>3</sub>)-SCR over Ag/Al catalyst are reported in Figure 2. First, note that addition of NH<sub>3</sub> as co-reductant did not significantly affect the ethanol conversion profile (blue and red dotted lines). On the contrary, the NO<sub>x</sub> conversion was remarkably enhanced, from 9 % and 38 % at 200°C and 250°C , respectively (blue full line), to 38 % and 74 % (red full line) when EtOH and NH<sub>3</sub> were co-fed. Above 350°C, full NO<sub>x</sub> conversion was achieved with or without NH<sub>3</sub> addition.

Interestingly, the NO<sub>x</sub> conversion obtained with the (EtOH+NH<sub>3</sub>)-SCR condition then fitted with the EtOH conversion, suggesting a beneficial effect of ethanol in the activation of ammonia to reduce NO<sub>x</sub> over the Ag/Al<sub>2</sub>O<sub>3</sub> material. This point is especially discussed section 3.2 focussed on C-compounds distribution in EtOH-SCR and (EtOH+NH<sub>3</sub>)-SCR conditions.

However, to put in evidence the collaborative effect of ethanol and NH<sub>3</sub> over Ag/Al, the NH<sub>3</sub>-SCR behaviour was also examined on Ag/Al sample (experimental feed composition reported in Table 1). Results depicted in Figure 3 indicate that when only NO was introduced as NO<sub>x</sub> (orange line), the Ag/Al catalyst exhibited nearly no activity to reduce NO<sub>x</sub> by NH<sub>3</sub>. The NO<sub>x</sub> conversion remained very low at 1-3 % whatever the studied temperature. The ammonia conversion (not shown) followed the same trend, with a maximum NH<sub>3</sub> conversion of 4 % at 500°C. Note that the ammonia conversion was also close to zero without NO<sub>x</sub> in the inlet mixture. These tests showed that this catalyst is unsuitable to activate neither the direct NO reduction by  $NH_3$  nor the ammonia oxidation by  $O_2$ . Considering that EtOH-SCR led to high NO<sub>2</sub> formation which may be favourable to the NO<sub>x</sub> reduction allowing the "fast-SCR" process, the Ag/Al catalyst was also evaluated in NH<sub>3</sub>-SCR using a NO<sub>2</sub>/NO<sub>x</sub> inlet ratio of 0.5 (blue line, Figure 3). Compared with the "standard NH<sub>3</sub>-SCR" condition, the NO<sub>x</sub> conversion by NH<sub>3</sub> was just a little improved and reached between 7 % and 15 % in the 200-500°C temperature range. Again, the ammonia conversion remained close to that of NO<sub>x</sub>, except for the higher temperatures. This poor activity of Ag/Al catalyst in NH<sub>3</sub>-SCR is consistent with previously reported results [30-32] and demonstrates that the enhancement of the deNO<sub>x</sub> efficiency in (EtOH+NH<sub>3</sub>)-SCR conditions is not directly attributable to the NO<sub>x</sub> reduction by NH<sub>3</sub>.



**Figure 3.** NO<sub>x</sub> conversion in NH<sub>3</sub>-SCR over Ag/Al catalyst for standard-SCR condition (—: 400 ppm NO, 400 ppm NH<sub>3</sub>, 8 % H<sub>2</sub>O, 10 % CO<sub>2</sub>, 10 % O<sub>2</sub> balanced in N<sub>2</sub>,) and fast-SCR condition (—: 200 ppm NO, 200 ppm NO<sub>2</sub>, 400 ppm NH<sub>3</sub>, 8 % H<sub>2</sub>O, 10 % CO<sub>2</sub>, 10 % O<sub>2</sub> balanced in N<sub>2</sub>).

3.2 Mechanistic study of the (EtOH+NH<sub>3</sub>)-SCR process

#### 3.2.1 C-compounds distribution in EtOH-SCR and (EtOH+NH<sub>3</sub>)-SCR conditions

In order to obtain information about the reaction pathway involved in the (EtOH+NH<sub>3</sub>)-SCR chemistry, the carbon compound distribution was examined depending on the presence of NH<sub>3</sub>. Results are depicted in Figure 4. As previously reported [10], ethanol was mainly converted into acetaldehyde at low temperature (T<300°C). Formaldehyde, ethylene were also detected, as well as traces of methanol (not shown).



**Figure 4.** Ethanol conversion (—, ---) and C-compounds distribution (acetaldehyde (—, ---); ethylene (—, ---); formaldehyde (—, ---)) over Ag/Al catalyst in EtOH-SCR (full lines) and (EtOH+NH<sub>3</sub>)-SCR (dotted lines) conditions.

(1200 ppm EtOH, with or without 400 ppm NH<sub>3</sub>, 400 ppm NO, 8 % H<sub>2</sub>O, 10 % CO<sub>2</sub>, 10 % O<sub>2</sub> balanced in N<sub>2</sub>).

In reaction mixture including NH<sub>3</sub> ((EtOH+NH<sub>3</sub>)-SCR), no apparent alteration in both ethanol conversion and C-compounds selectivity was denoted. Consequently, there is no evidence for a reactivity between ammonia and organic species.

However, the possible formation of an organo-nitrogen intermediate species, obtained by reaction of ethanol with ammonia was supplementary checked by mass spectrometry analysis. In fact, ammonia condensation with aldehydes is well known to lead to imine compounds. The first step is a nucleophilic addition of primary amine like NH<sub>3</sub>, to the carbonyl group of acetaldehyde, followed by a rapid proton transfer, as reported in Scheme 1 for ethanimine synthesis. In accordance with Vinogradoff *et al.* [42], the corresponding m:z=28 value is expected as the main peak corresponding to the loss of CH<sub>3</sub> fragment from an alpha fragmentation of the ethanimine (CH=NH<sup>+</sup>). The m:z=42 and m:z=43 value of CH<sub>3</sub>C=NH<sup>+</sup> and CH<sub>3</sub>CH=NH<sup>+</sup> respectively are also expected. Finally, none of these fragments were observed, giving no evidence of an organo-nitrogen compound formation and confirming that a direct reaction pathway between organic species and ammonia to enhance the NO<sub>x</sub> reduction is invalidated.

$$\begin{array}{c} O \\ H_{3}C \xrightarrow{C} H \end{array} + H_{2}N - H \longleftrightarrow \begin{bmatrix} H_{N} \xrightarrow{H} \\ H_{3}C \xrightarrow{C} H \\ H_{3}C \xrightarrow{C} H \end{bmatrix} \longleftrightarrow \begin{array}{c} N \xrightarrow{H} \\ H_{3}C \xrightarrow{C} H \\ H_{3}C \xrightarrow{C} H \end{array} + H_{2}O$$

Scheme 1. Ethanimine formation mechanism.

#### 3.2.2 NO<sub>2</sub> reactivity in (EtOH+NH<sub>3</sub>)-SCR

As previously reported in Figure 1, EtOH-SCR over Ag/Al sample revealed NO<sub>2</sub> emission of approximately 225 ppm at 200°C. More precisely, the NO<sub>2</sub> emission reported in Figure 5 depended on the temperature and varied together with the CH<sub>3</sub>CHO profile (Figure 4). As already reported in ref. [10], the EtOH reaction pathway at low temperature (T<300°C) firstly involves a reaction between ethanol, NO and O<sub>2</sub> to produce acetaldehyde and NO<sub>2</sub> (Eq. 17).

$$C_2H_5OH + NO + O_2 \rightarrow CH_3CHO + NO_2 + H_2O$$
(17)

Figure 1 also showed that addition of NH<sub>3</sub> in the reaction mixture induced a decrease in NO<sub>2</sub> outlet concentration. Figure 5 confirms that (EtOH+NH<sub>3</sub>) co-injection (red curve, (EtOH+NH<sub>3</sub>)-SCR) led to a significant decreases in NO<sub>2</sub> emission for all the studied temperature. This result suggests a reactivity between NH<sub>3</sub> and the *in situ* NO<sub>2</sub> formed from EtOH-SCR chemistry. Nevertheless, as previously discussed, the Ag/Al catalyst presented a poor activity in NH<sub>3</sub>-SCR, even under the most favourable fast-SCR stoichiometry (Figure 3), showing that NO<sub>2</sub> did not preferentially react with NH<sub>3</sub> over Ag/Al sample.



**Figure 5.** NO<sub>2</sub> outlet emission over Ag/Al catalyst: Reaction mixture: (—) EtOH-SCR (400 ppm NO, 1200 ppm C<sub>2</sub>H<sub>5</sub>OH, 8 % H<sub>2</sub>O, 10 % CO<sub>2</sub>, 10 % O<sub>2</sub> balanced in N<sub>2</sub>); (—) (EtOH+NH<sub>3</sub>)-SCR (400 ppm NO, 1200 ppm C<sub>2</sub>H<sub>5</sub>OH, 400 ppm NH<sub>3</sub>, 8 % H<sub>2</sub>O, 10 % CO<sub>2</sub>, 10 % O<sub>2</sub> balanced in N<sub>2</sub>).

Subsequently, the influence of the inlet NH<sub>3</sub> concentration was studied in the low temperature range (175°C-250°C). The ammonia concentration was adjusted from 0 to 750 ppm in addition to the gas mixture corresponding to EtOH-SCR condition (Table 1). Results are presented in Figure 6. As expected, the NO<sub>x</sub> conversion increased with temperature, and it clearly appears that the gain in NO<sub>x</sub> conversion in regard on the amount of added ammonia is strongly temperature dependant, even in a rather small temperature range (175-250°C). Interestingly, Figure 6 clearly shows that NO<sub>2</sub> is the main compound affected by the NH<sub>3</sub> addition, especially with the increase of the temperature. It indicates that ammonia reacted preferentially with NO<sub>2</sub> in ethanol media, even if the Fast-NH<sub>3</sub>-SCR test previously depicted in Figure 3 showed a limited activity. In line with this observation, the calculated ratio between the amount of converted ammonia and the amount of supplementary converted NO<sub>x</sub> also increased with the temperature. It was close to 1 at 175°C (with a quite large uncertainty because ammonia and NO<sub>x</sub> variations were then limited), increased to 1.1-1.2 at 200°C and reached 1.3-1.4 at 250°C, without clear evidence of the ammonia inlet concentration. Then, the apparent NH<sub>3</sub>-NO<sub>x</sub> stoichiometry appeared to vary from a fast/standard-SCR stoichiometry at 200°C to an additional contribution of a NH<sub>3</sub>-NO<sub>2</sub> reaction with the increase of temperature.

Lastly, whatever the temperature between 175°C and 250°C, the ethanol outlet concentration (not shown) appears unaffected by the amount of added ammonia.

To further study the interactions between ammonia, ethanol and NO<sub>x</sub> on Ag/Al catalyst, adsorption of these molecules was monitored by Infrared Spectroscopy.



**Figure 6.** Effect of  $NH_3$  inlet concentration in NO (—) and  $NO_2$  (—) outlet emissions at 175, 200 and 250°C for (EtOH+NH<sub>3</sub>)-SCR process over Ag/Al catalyst.

#### 3.2.3 Infrared Spectroscopy study

 $NH_3$  adsorption. NH<sub>3</sub> adsorption over Ag/Al sample was firstly studied. Spectra (not shown) are remarkable by low intensive bands due to the weak acidity of alumina to adsorb ammonia at 200°C. Nevertheless, ammonia is apparently adsorbed on both Lewis and Brønsted acid sites. The bands at 1228 and 1288 cm<sup>-1</sup> are attributed to the symmetric deformation of NH<sub>3</sub> ( $\delta_s(NH_3)$ ) coordinatively bound to Lewis acid sites on Ag/Al<sub>2</sub>O<sub>3</sub>. Note that the symmetric deformation vibration is the more sensitive mode to the strength of the Lewis acid-base interaction. The two components observed at 1228 and 1288 cm<sup>-1</sup> probably reveal ammonia coordination onto tetrahedral Al<sup>3+</sup> and octahedral Al<sup>3+</sup> Lewis acid sites of different strength. The band at 1579 cm<sup>-1</sup> is due to the asymmetric deformation of NH<sub>3</sub> ( $\delta_{as}(NH_3)$ ) adsorbed on Lewis acid sites on the catalyst surface. Two bands at 1684 and 1628 cm<sup>-1</sup> are attributed to  $\delta_s(NH_4^+)$  and  $\delta_{as}(NH_4^+)$  bound onto Brønsted acid sites respectively. The peak at 1395 cm<sup>-1</sup> is assigned to NH<sub>4</sub><sup>+</sup> species on Al<sub>2</sub>O<sub>3</sub> support ( $\delta_{as}(NH_4^+)$  [43-46]. The corresponding assignments are reported Table 2.

*EtOH-O*<sub>2</sub> *co-adsorption*. IR spectra of (EtOH-O<sub>2</sub>) adsorption at equilibrium (Figure 7A black full line) results in the appearance of several bands at 1629, 1588, 1463, 1391 and 1333 cm<sup>-1</sup>. Assignments are reported in Table 2. In accordance with results reported in previous study for acetic acid adsorption, the bands at 1588 and 1463 cm<sup>-1</sup> are assigned to adsorbed acetate ( $v_{as(OCO)}$  and  $v_{s(OCO)}$  respectively) [47]. In addition, bands at 1629, 1391 and 1333 cm<sup>-1</sup> are clearly observed. The band at 1629 cm<sup>-1</sup> is assigned to asymmetric stretching vibration mode ( $v_{as(CCO)}$ ) and peaks at 1391 and 1333 cm<sup>-1</sup> is attributed to a symmetric stretching vibration ( $v_{s(CCO)}$ ) mode and to a C-H deformation mode ( $\delta_{(CH)}$ ) of enolic species (CH<sub>2</sub>-CH-O)<sup>--</sup>, respectively. Several bands are observed around 1800-1700 cm<sup>-1</sup> and 1300-1200 cm<sup>-1</sup> which are assigned to acetaldehyde gas species. These bands disappear after evacuation.

*NH*<sub>3</sub> adsorption over (*EtOH-O*<sub>2</sub>) ad-species As shown in Figure 7A, the adsorption of ammonia (10 hPa at equilibrium) on ethanol-covered Ag/Al<sub>2</sub>O<sub>3</sub> surface leads to decrease the intensity of the bands at 1629, 1391 and 1333 cm<sup>-1</sup> previously attributed to enolic species. It means that, without NO<sub>x</sub> compounds, ammonia reacts preferentially with ethoxy species than with acetate. This is highlighted by subtracting spectra obtained after adsorption of ethanol and ammonia (shown in bold gray line). The negative absorption bands show the consumption of the enolic species by ammonia. Note that the IR vibration mode of ammonia is not observed.

Gas mixture	Surface species		Assignment	Wavenumber (cm <sup>-1</sup> )
	Type Ib (Alvı)OH	н-с	<i>V</i> (он)	3800-3785
	Type Ia (Al <sub>IV</sub> )OH	M	<i>V</i> (он)	3780-3760
	Type IIb (Alvı)2OH	H L	<i>V</i> (он)	3745-3740
	Type IIa (Al <sub>IV</sub> Al <sub>VI</sub> )OH	MM	<i>V</i> (он)	3735-3720
	Type III (Alvı)₃OH	H M M M	<i>V</i> (он)	3710-3680
	Enolic	(CH <sub>2</sub> -CH-O) <sup></sup>	Vas(CCO)	1629
	Acetate	(CH₃-(C=O)-O) <sup>—</sup>	Vas(OCO)	1588
(EtOH-O <sub>2</sub> )	Acetate	(CH <sub>3</sub> -(C=O)-O) <sup></sup>	V <sub>s(OCO)</sub>	1463
	Enolic	(CH <sub>2</sub> -CH-O) <sup></sup>	V <sub>s</sub> (cco)	1391
	Enolic	(CH <sub>2</sub> -CH-O) <sup></sup>	$\delta_{(CH)}$	1333
	Monodontato Nitrato	0 N 0	V3	1547-1562
		о М	<i>V</i> 3 <sup>'''</sup>	1299-1289
	Bidentate Nitrate	O N	Assignment         Wave (r           H $V_{(OH)}$ 3800           M $V_{(OH)}$ 3780           H $V_{(OH)}$ 3745           M $V_{(OH)}$ 3745           H $V_{(OH)}$ 3735           H $V_{(OH)}$ 3710           (CH2-CH-O) <sup>-</sup> $V_{as(CCO)}$ 1629           (CH3-(C=O)-O) <sup>-</sup> $V_{as(OCO)}$ 1588           (CH2-CH-O) <sup>-</sup> $V_{as(OCO)}$ 1463           (CH2-CH-O) <sup>-</sup> $V_{as(OCO)}$ 1391           (CH2-CH-O) <sup>-</sup> $V_{as(CCO)}$ 1299 <td>1587-1583</td>	1587-1583
$(NO_{2}O_{2})$		¢ v	<i>V</i> 3 <sup>''</sup>	1254-1244
(100-02)	Bridged Nitrate	0-N 0-M M	<i>V</i> 3 <sup>'</sup>	1612
	Manadantata Nitrita	0 N 0	<i>V</i> 1	1313
	Monodentate Nitrite	мм	V <sub>3</sub>	1229
	Ammonium ion (Brønsted AS)		$\delta_{ m s(NH4+)}$	1684
	Coordinated ammonia (Lewis AS)		$\delta_{ m as(NH3)}$	1628
(NUL)	Coordinated ammonia (Lewis AS)	AssignmentH $V_{(OH)}$ H $V_{(OH)}$ H $V_{(OH)}$ H $V_{(OH)}$ H $V_{(OH)}$ Image: Constraint of the state	1579	
(INH3)	Ammonium ion (Brønsted AS)		$\delta_{as(NH4+)}$	1395
	Coordinated ammonia (Lewis AS)		Assignment         Wavent (cm $\mathcal{V}_{(OH)}$ 3800-3 $\mathcal{V}_{(OH)}$ 3780-3 $\mathcal{V}_{(OH)}$ 3745-3 $\mathcal{M}$ $\mathcal{V}_{(OH)}$ 3735-3 $\mathcal{M}$ $\mathcal{V}_{(OH)}$ 3710-3 $\mathcal{M}$ $\mathcal{V}_{(OCO)}$ 1629 $\mathcal{O}$ $\mathcal{V}_{s(OCO)}$ 1588 $\mathcal{O}$ $\mathcal{V}_{s(OCO)}$ 1463 $\mathcal{V}^{-1}$ 1333 $\mathcal{O}$ $\mathcal{V}^{-1}$ 1333 $\mathcal{O}$ $\mathcal{V}^{-1}$ 1333 $\mathcal{V}_{s'}$ $\mathcal{V}_{3}^{-1}$ 1547-11 $\mathcal{V}_{3}^{-1}$ 1587-11 $\mathcal{V}_{3}^{-1}$ 1587-11 $\mathcal{V}_{3}^{-1}$ 1587-11 $\mathcal{V}_{3}^{-1}$ 1517 $\mathcal{V}_{3}^{-1}$ 1229 $$	1288
	Coordinated ammonia (Lewis AS)		$\delta_{ m s(NH3)}$	1228

Table 2. Infrared bands attribution for adsorbed species and free OH groups on Ag/Al<sub>2</sub>O<sub>3</sub>



**Figure 7.** Transmission IR spectra of co-reactive compounds adsorption at 200°C over Ag/Al catalyst. (A): (EtOH-O<sub>2</sub>)+(NH<sub>3</sub>); (B): (NO-O<sub>2</sub>)+(NH<sub>3</sub>); (C): (EtOH-O<sub>2</sub>)+(NO-O<sub>2</sub>)+(NH<sub>3</sub>). (10 hPa at equilibrium).

(*NO*-*O*<sub>2</sub>) adsorption. It is well-known that NO<sub>2</sub> and NO can react on metal oxide surfaces to yield a number of different surface species that in principle can be differentiated by infrared spectroscopy and results in different absorption frequencies in the spectral range from 1200 to 1700 cm<sup>-1</sup>. Nitrogen dioxide adsorption can result in the formation of both adsorbed nitrate (NO<sub>3</sub><sup>-</sup>) and nitrite (NO<sub>2</sub><sup>-</sup>). The coordination of nitrate, nitrite, and nitric oxide in inorganic complexes has been discussed in the literature in detail and provides a useful guide for the interpretation of the infrared absorption bands of adsorbed species [48-50]. It is reported that the planar nitrate ion belongs to the point group D<sub>3h</sub> and has four fundamental vibrations: v<sub>1</sub> (symmetric stretch), v<sub>2</sub> (out-of-plane bend), v<sub>3</sub> (asymmetric stretch), and v<sub>4</sub> (in-plane bend). The last three are infrared active. The surface interaction with NO<sub>2</sub> or (NO+O<sub>2</sub>) leads to the reduction of the nitrate ion symmetry from D<sub>3h</sub> to C<sub>2v</sub> and causes the degenerated v<sub>3</sub> mode to split into four modes, of which two are IR active (v<sub>3</sub>' and v<sub>3</sub>'' for the high and low-frequency component respectively).

IR spectra of adsorbed N-containing species after an exposure of Ag/Al<sub>2</sub>O<sub>3</sub> to (NO-O<sub>2</sub>) are reported in Figure 7B (black dotted line). After the first adsorption dose (spectra not shown), spectrum is remarkable by bands at 1313 and 1229 cm<sup>-1</sup>. The band observed at 1229 cm<sup>-1</sup> is assigned to the asymmetric stretch vibration (v<sub>3</sub>) of the nitrite ion; the band at 1313 cm<sup>-1</sup> to the symmetric stretching vibration (v<sub>1</sub>). For higher (NO-O<sub>2</sub>) coverage, several absorption bands are observed, unanimous assigned to nitrates species by many authors despite some inconsistencies. For instance, Venkov *et al.* [48] assigned the band at 1627 (v<sub>3</sub>') and 1261 cm-1 (v<sub>3</sub>'') to bridged nitrates while the bands at 1593 (v<sub>3</sub>') and 1296 cm<sup>-1</sup> (v<sub>3</sub>'') are due to bidentate nitrate. The bands at 1562 cm<sup>-1</sup> associated with one component around 1300 cm<sup>-1</sup> corresponds to monodentate nitrate. Note that a similar coincidence between the v<sub>3</sub>'' vibrations of mono- and bidentate nitrates was reported in this work. Yu *et al.* [51] observed monodentate (1560, 1250 cm<sup>-1</sup>), bidentate (1583, 1302 cm<sup>-1</sup>), and bridging (1612 cm<sup>-1</sup>) nitrates after an exposure of the Ag/Al<sub>2</sub>O<sub>3</sub> to NO+O<sub>2</sub>. Tamm *et al.* [52] assigned the high-frequency component (v<sub>3</sub>') at 1611, 1586 and 1546 cm<sup>-1</sup> to bridge-bound, bidentate and monodentate nitrates species respectively associated to the low-frequency component at 1250 cm<sup>-1</sup> (bidentate) and 1304 cm<sup>-1</sup> (monodentate).

Finally, in this work, the assignments reported in Table 2 are proposed. The bands at 1254 and 1587  $cm^{-1}$  and the bands at 1299 and 1547  $cm^{-1}$  growth simultaneously, which indicates that they either correspond to two surface species. With (NO+O<sub>2</sub>) coverage increase, these bands are shifted to 1244/1583  $cm^{-1}$  and 1289/1562  $cm^{-1}$  (black full line). In agreement with data from the literature, the bands with maxima at 1562 and 1289  $cm^{-1}$  are attributed to monodentate nitrate, and the doublet at 1583 and 1244  $cm^{-1}$  to bidentate nitrates. The bands at 1612  $cm^{-1}$  is assigned to bridging nitrates.

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*NH*<sub>3</sub> adsorption over (*NO-O*<sub>2</sub>) ad-species. After adsorption of (*NO-O*<sub>2</sub>) at equilibrium (10 hPa, bold black line, Figure 7B), the co-adsorption of ammonia (10 hPa, gray line) was performed. It induced a decrease of the intensity of the high-frequency component (v<sub>3</sub>') of bridged (1612 cm<sup>-1</sup>) and bidentate (1583 cm<sup>-1</sup>) nitrates, but without a full consumption of adsorbed NO<sub>x</sub> compounds after two hours at 200°C. The v<sub>3</sub>" band at 1289 cm<sup>-1</sup> is shifted to higher frequency of about 1300 cm<sup>-1</sup>. Note that the  $\delta_{s(NH3)}$  vibration mode of coordinated ammonia can be superimposed to the degenerated v<sub>3</sub>" mode of adsorbed monodentate nitrate.

More precisely, the negative bands near 1612, 1583 and 1280 cm<sup>-1</sup> illustrates that bridged and bidentate nitrates are preferentially consumed by ammonia co-adsorption. The higher stability of the monodentate nitrate is in accordance with previous literature data [52]. This result shows a direct interaction between nitrates (preferentially bidentate and bridged) and NH<sub>3</sub> on the catalyst surface.

*Effect of*  $NH_3$  *adsorption over* (*EtOH-O<sub>2</sub>*)+(*NO-O<sub>2</sub>*) *ad-species*. Resulting IR spectra for (EtOH-O<sub>2</sub>)+(NO-O<sub>2</sub>)+NH<sub>3</sub> are presented in Figure 7C. The black full line (spectrum a) corresponds to the spectrum recorded after EtOH-O<sub>2</sub> adsorption that is consistent with results already discussed in Figure 7A. After evacuation and co-adsorption of NO-O<sub>2</sub>, the spectrum in black dotted line (b) exhibited a new band at 1299 cm<sup>-1</sup>which is attributed to v<sub>3</sub>" of monodentate nitrate. The corresponding v<sub>3</sub>' overlaps in the  $v_{as(OCO)}$  of adsorbed acetate species (1588 cm<sup>-1</sup>). To highlight adsorbed species resulting of the co-adsorption of (EtOH-O<sub>2</sub>) and (NO-O<sub>2</sub>), these two spectra were subtracted (b-a). Nitrates species are then clearly distinguished by bands at 1612 cm<sup>-1</sup> (v<sub>3</sub>' bridged nitrates) and 1562 cm<sup>-1</sup> (v<sub>3</sub>' monodentate nitrates). Co-adsorption of NH<sub>3</sub> (spectra c, c-a and c-b), results in a strong decrease of all the bands assigned to the nitrate species. Unlike co-adsorption (NO-O<sub>2</sub>)+(NH<sub>3</sub>), the presence of enolic and acetates species are different, monodentate nitrates were almost fully consumed by NH<sub>3</sub> in presence of EtOH.

*OH and NH stretching modes.* In Figure 8 is presented IR spectra recorded in the 3900-3000 cm<sup>-1</sup> spectral range ( $\nu_{(OH)}$  and  $\nu_{(NH)}$ ) for the following gas mixture co-adsorption: NO-O<sub>2</sub>, NO-O<sub>2</sub>+NH<sub>3</sub>, EtOH-O<sub>2</sub>+NH<sub>3</sub> and EtOH-O<sub>2</sub>+NO-O<sub>2</sub>+NH<sub>3</sub>. IR spectra are remarkable by NH stretching bands at 3390 and 3290 cm<sup>-1</sup> assigned to coordinated ammonia. These bands are not observed when ammonia is adsorbed alone (without NO<sub>x</sub> pre-adsorption; spectra not shown). Thus, it is proposed that when nitrates are formed, due to their negative induction effect, they withdraw electron density from nearby Al<sup>3+</sup> cation. As a result, the Lewis acidity of the latter increases and nitrosyl complexes/ammonia adsorption is probably formed.



**Figure 8.** IR spectra at 200°C in  $v_{(OH)}$  and  $v_{(NH)}$  stretching region over Ag/Al catalyst. ---: reference spectrum after calcination (400°C under vacuum); —: (NO-O<sub>2</sub>) adsorbed species; ---: (NO-O<sub>2</sub>)+(NH<sub>3</sub>) adsorbed species ...: (EtOH-O<sub>2</sub>)+(NO-O<sub>2</sub>)+(NH<sub>3</sub>) adsorbed species ...: (EtOH-O<sub>2</sub>)+(NH<sub>3</sub>) adsorbed species.

Additionally, OH groups of alumina are characterized by complex O-H stretching band in the 3900-3500 cm<sup>-1</sup> zone. The assignment of these bands was largely studied in the literature but is still controversial. Among the various proposed models, the most used was proposed by Tsyganenko *et al.* [53,54] and completed by Knözinger *et al.* [55]. Five types of OH species were identified on the surface of alumina layers, depending firstly on the number of Al<sup>3+</sup> bonding to the OH group and secondly on the coordination number of the Al<sup>3+</sup> ion. This model was used in this work to study the free OH group of silver supported alumina catalyst. IR spectra reported Figure 8 are consistent with those reported in the literature, showing the different types of OH groups of alumina that display bands at 3758, 3728 and 3680 cm<sup>-1</sup>. Assignments are reported in the Table 2.

In addition, Figure 8 indicates that adsorption of reactive species (NO-O<sub>2</sub>, EtOH-O<sub>2</sub>) led to the decrease of peaks at 3758 cm<sup>-1</sup> and 3728 cm<sup>-1</sup> attributed to a loss of OH surface species. These absorption bands have been described before [56] and correspond to the O-H stretching vibration of OH groups coordinated with one aluminum atom in coordination states IV (Type Ia), and with two aluminum atoms in coordination IV and VI (type IIa), respectively.

Interestingly, new OH bands at 3598-3577, 3528, and 3470 cm<sup>-1</sup> are observed. These bands can be assigned to the O-H vibration of hydrogen-bonded OH groups of acids, such as HNO<sub>3</sub> or HONO [50]. The observed acidic OH vibrations (3600-3400 cm<sup>-1</sup>) are caused by adsorbed HNO<sub>3</sub> or HONO, which are in equilibrium with nitrate and nitrite ions and surface-adsorbed water observed at 3559 cm<sup>-1</sup>. These

new intermediate species are especially observed after EtOH adsorption (gray dotted line). It suggests that resulting ethanol ad-species enhance the reactivity of NO<sub>x</sub> compounds.

To conclude, IR characterization reveals that ammonia is highly reactive towards enolic ad-species. In addition, bridged and bidentate nitrates are preferentially consumed by ammonia co-adsorption, but are still observed in absence of ethanol. Finally, over surface pre-exposed to ethanol, the reactivity of NH<sub>3</sub> with nitrates compounds is enhanced and intermediates HONO or HNO<sub>3</sub>, commonly reported as intermediates in NO<sub>x</sub> SCR pathway, are observed.

#### 3.2.4 Role of H<sup>\*</sup> Intermediate species

IR characterization showed that ethanol ad-species are involved in the reduction of NO<sub>x</sub> compounds by NH<sub>3</sub> in the (EtOH+NH<sub>3</sub>)-SCR process. As mentioned in the introduction part, the first step of the EtOH-SCR framework results in  $C_2H_5OH$  dissociative adsorption into surface ethoxide  $C_2H_5O^*$  and surface hydrogen H<sup>\*</sup> species (Eq. 11) [10,24,26,57]. Thereafter, ethoxide is converted into acetaldehyde (Eq. 12) providing a second surface-bound hydrogen ad-atoms. Figure 4 shows that acetaldehyde emission started from 175 °C (lowest tested temperature) and reached a maximum at 250°C, indicating that hydrogen ad-atoms should be available at low temperature. Addition of hydrogen into the reaction mixture was reported to enhance the deNO<sub>x</sub> efficiency in EtOH-SCR process. It was advanced that H<sub>2</sub> addition promotes the partial oxidation of C<sub>2</sub>H<sub>5</sub>OH to form enolic species which mainly contribute to accelerate NO<sub>x</sub> reduction [29,58,59]. Additionally, Flura et al. [10] observed that NO oxidation into NO<sub>2</sub> was enhanced in presence of small amounts of H<sub>2</sub> (167 ppm) over silver supported catalyst. It was proposed that hydrogen is able to reduce silver particles, leading to higher oxidation performances. It is also likely that hydrogen favours the nitrates species desorption. The promotion effect of  $H_2$  co-feeding was also evidenced in hydrocarbon-SCR, with an enhancement of the deNO<sub>x</sub> activity at low temperature [60]. However, the most significant impact of  $H_2$  addition is observed on the H<sub>2</sub>-assisted NH<sub>3</sub>-SCR process over Ag/Al<sub>2</sub>O<sub>3</sub> catalysts [24,32,61,62]. Consequently, the H<sub>2</sub> behaviour in NO reduction was examined and compared to the previously studied reductant mixture.

First, the deNO<sub>x</sub> efficiency of Ag/Al catalyst was evaluated in H<sub>2</sub>-SCR. Figure 9 reports the NO<sub>x</sub> conversion (full line) and the NO<sub>2</sub> emission (dotted line) for H<sub>2</sub>-SCR, EtOH-SCR and EtOH+NH<sub>3</sub>-SCR. As expected, no deNO<sub>x</sub> activity was observed in H<sub>2</sub>-SCR condition (brown curve). Formation of NO<sub>2</sub> was observed, but in a lower extent than in EtOH-SCR condition, with maximum concentrations of 130 ppm for H<sub>2</sub>-SCR (at 300°C, brown dotted line), compared with 250 ppm for EtOH-SCR (at 200°C blue dotted line). These results support the high reactivity of ethanol to oxide NO and provide NO<sub>2</sub> at low

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temperature (Eq. 17). More interestingly, these experiments demonstrates that the hydrogen  $H^*$  species provided by the ethanol dehydrogenation do not directly act as NO<sub>x</sub> reductant over Ag/Al but would rather be involved during the (EtOH+NH<sub>3</sub>)-SCR process (red curve).

To highlight the reactivity of hydrogen in the NO<sub>x</sub> reduction process by NH<sub>3</sub>, the reactivity of Ag/Al sample was investigated in H<sub>2</sub>-assisted NH<sub>3</sub>-SCR and compared with both EtOH-SCR and (EtOH+NH<sub>3</sub>)-SCR (Table 3). The H<sub>2</sub> concentration was fixed in regard on the activity of ethanol dehydrogenation, *i.e.* at 100 ppm and 270 ppm for temperature test of 175°C and 200°C, respectively. Compared with EtOH-SCR, NH<sub>3</sub> addition induced an enhancement of the NO<sub>x</sub> conversion of 8 % and 25 % at 175°C and 200°C, respectively. Interestingly, similar deNO<sub>x</sub> improvement was obtained in H<sub>2</sub>-assisted NH<sub>3</sub>-SCR despite the low H<sub>2</sub> concentration used. It clearly indicates that the deNO<sub>x</sub> enhancement supplied by the NH<sub>3</sub> addition to EtOH-SCR is related to the H<sup>\*</sup> species formed during ethanol oxidation.

**Table 3.** NO<sub>x</sub> conversions at 175 and 200°C in EtOH-SCR (1200 ppm  $C_2H_5OH$ ), in NH<sub>3</sub>-assisted EtOH-SCR (1200 ppm  $C_2H_5OH$  + 400 ppm NH<sub>3</sub>) and in H<sub>2</sub>-assisted NH<sub>3</sub>-SCR (400 ppm NH<sub>3</sub> + 100-270 ppm H<sub>2</sub>) processes blended in 400 ppm NO, 8 % H<sub>2</sub>O, 10 % CO<sub>2</sub>, 10 % O<sub>2</sub>

Temperature (°C)	NO <sub>x</sub> conv.	NO <sub>x</sub> conv.	NO <sub>x</sub> conv.	NO <sub>x</sub> conv.	
	EtOH-SCR (%)	EtOH/NH₃-SCR (%)	gain by NH₃ add. in EtOH-SCR <sup>[a]</sup> (%)	$H_2$ -assisted $NH_3$ - SCR <sup>[b]</sup> (%)	
175	7	15	8	9	
200	9	38	29	27	

[a] difference between NO<sub>x</sub> conv. in EtOH-SCR with or without NH<sub>3</sub> addition [b] H<sub>2</sub> amount corresponds to the quantity potentially produced by EtOH oxidation to CH<sub>3</sub>CHO during EtOH-SCR process (100 ppm H<sub>2</sub> at 175°C; 270 ppm H<sub>2</sub> at 200°C).



**Figure 9.**  $NO_x$  conversion (full line) and  $NO_2$  emission (dotted line) over Ag/Al catalyst for H<sub>2</sub>-SCR (—), EtOH-SCR (—) and EtOH+NH<sub>3</sub>-SCR (—).

#### 3.2.5 Proposed reaction pathways

The enhancement of NO<sub>x</sub> conversion by NH<sub>3</sub> co-feeding in EtOH-SCR over Ag/Al catalyst is clearly evidenced (Figure 2). However, no reactivity of ammonia with carbon-based by-products was observed. It means that NH<sub>3</sub> did not react to produce organo-nitrogen reactive intermediate. In addition, Ag/Al sample was not significantly active to reduce NO<sub>x</sub> by NH<sub>3</sub>. Obviously, NH<sub>3</sub> is activated over Ag/Al catalysts only in the presence of ethanol. Moreover, the highly beneficial effect of H<sub>2</sub> addition on the NH<sub>3</sub>-SCR process over Ag/Al<sub>2</sub>O<sub>3</sub> catalysts is well documented and the observed improvement in (EtOH+NH<sub>3</sub>)-SCR over Ag/Al is consistent with the amount of H<sup>\*</sup> species obtained from ethanol dehydrogenation into acetaldehyde (see section 3.2.4). Besides, IR results evidence the formation of HONO/HNO<sub>3</sub> intermediates when ethanol and NO are co-adsorbed.

Consequently, taking into account all the data presented in this work, it is proposed that the hydrogen  $H^*$  species provided by the ethanol dehydrogenation are the main responsible for the high deNO<sub>x</sub> efficiency at low temperature observed in the (EtOH+NH<sub>3</sub>)-SCR experiments. Based on the mechanism presented in the introduction part, it is assumed that the HONO/HNO<sub>3</sub> route formation is a determining step to the NO<sub>x</sub> reduction by NH<sub>3</sub>. The effect of H<sup>\*</sup> species are tentatively attributed to an activation of the NO oxidation into reactive intermediate N-containing species, such as HONO and/or HNO<sub>3</sub>, evidenced by FTIR experiments (Figure 7). Ammonium nitrite formation (Eq. 6), which is described as the penultimate step of deNO<sub>x</sub> chemistry with many practical catalysts, can subsequently be formed by reaction of NH<sub>3</sub> with nitrous acid [63].

Finally, the proposed (EtOH+NH<sub>3</sub>)-SCR process avoids the rate-limiting step of nitromethane formation by three different routes (Scheme 2). The N<sub>2</sub> route formation originated from EtOH-SCR (blue route in scheme 2) is limited at low temperature by the CH<sub>3</sub>NO<sub>2</sub> rate-determining step. Ammonia formation is obtained only for T > 250°C [23]. Gaseous NH<sub>3</sub> addition helps to avoid this problem. Actually, the deNO<sub>x</sub> efficiency improvement in the (EtOH+NH<sub>3</sub>)-SCR process is not determined by the efficiency of Ag/Al sample to directly reduce NO<sub>x</sub> by NH<sub>3</sub>. In fact, the NH<sub>3</sub>-SCR route (green dotted route in scheme 2), only active when NO<sub>2</sub> is formed during EtOH-SCR, has only few influence on the overall efficiency of the system. Finally, the remarkable NO<sub>x</sub> conversion achieved with the NH<sub>3</sub> co-feeding is assigned to the formation of HNO<sub>x</sub> species, obtained by the generation of H<sup>\*</sup> compound from the dehydrogenation of ethanol. Ethanol can therefore be seen as a hydrogen provider, in addition to induce the oxidation of NO into NO<sub>2</sub>. The added ammonia can then follow the conventional mechanism of H<sub>2</sub>-assisted NH<sub>3</sub>-SCR exposed in the literature. This system allows the *in situ* generation at low temperature of the key intermediates of the deNO<sub>x</sub> chemistry over Ag/Al sample (red route in scheme 2).



Scheme 2. Proposal of reaction pathway in EtOH+NH<sub>3</sub>-SCR over Ag/Al catalyst.

With a conversion ranging from 15 to 75% in the 175-250°C region, this system is efficient for  $NO_x$  removal using only NO as  $NO_x$ . However, this system can be further optimized by means of a dual-bed configuration, exposed in the next section.

#### 3.2.6 DeNO<sub>x</sub> efficiency Improvement of the (EtOH+NH<sub>3</sub>)-SCR process: dual-bed configuration

In this section, the (EtOH+NH<sub>3</sub>)-SCR process is extended to a more complex catalytic system to obtain a supplementary enhancement of the NO<sub>x</sub> conversion at low temperature (175-300°C) using the same ethanol-NH<sub>3</sub> mixture. In fact, in (EtOH+NH<sub>3</sub>)-SCR process over Ag/Al, the outlet exhaust gas still contained some NH<sub>3</sub> and NO<sub>x</sub> (especially including NO<sub>2</sub>) in this low temperature range. Consequently, a dedicated SCR catalyst placed downstream the Ag/Al<sub>2</sub>O<sub>3</sub> catalyst was supposed to allow both a supplementary NO<sub>x</sub> abatement together with an ammonia slip restraint. Supported transition metal, ceria based oxides such as Fe<sub>2</sub>O<sub>3</sub>/WO<sub>3</sub>/ZrO<sub>2</sub> [38], MnO<sub>x</sub>-CeO<sub>2</sub> [39] or WO<sub>3</sub>/Ce<sub>x</sub>Zr<sub>1-x</sub>O<sub>2</sub> [40] or metal exchanged zeolite [20] are active materials for this purpose. WO<sub>3</sub>/Ce<sub>x</sub>Zr<sub>1-x</sub>O<sub>2</sub> catalyst was selected in this work as NH<sub>3</sub>-SCR material, since it appeared to be active with various NO<sub>2</sub>/NO<sub>x</sub> inlet ratio including the standard-SCR stoichiometry. Moreover, this catalyst may also act as an ammonia slip catalyst since it was reported to be active in NH<sub>3</sub> oxidation by O<sub>2</sub>, with a full selectivity into N<sub>2</sub> [40].

First, single WO<sub>3</sub>/Ce-Zr catalyst was evaluated in EtOH-SCR and (EtOH+NH<sub>3</sub>)-SCR with only NO as injected NO<sub>x</sub> (SI file, Figure S3). The NO<sub>x</sub> conversion obtained with only ethanol as reductant was very limited, with a maximum of only 7 % recorded at 300°C. This WO<sub>3</sub>/Ce-Zr catalyst is then poorly active in NO<sub>x</sub> reduction by ethanol. To the opposite, the NO<sub>x</sub> conversion was significant in (EtOH+NH<sub>3</sub>)-SCR condition, from 13 to 70 % in the 175-450°C temperature range. Interestingly, this catalyst is very active in Fast-NH<sub>3</sub>-SCR condition, with NO<sub>x</sub> conversion of 53% and 90 % at 170°C and 200°C, respectively.



**Figure 10.** NO<sub>x</sub> conversion (full line) and NH<sub>3</sub> oulet concentration (dotted line) in EtOH-SCR (—) and (EtOH+NH<sub>3</sub>)-SCR (—) over Ag/Al sample ( $\bigcirc$ ), and in (EtOH+NH<sub>3</sub>)-SCR condition over Ag/Al+WO<sub>3</sub>/Ce-Zr ( $\Box$ ) dual bed system (—).

Figure 10 reports the NO<sub>x</sub> conversion obtained in (EtOH+NH<sub>3</sub>)-SCR over the the Ag/Al+WO<sub>3</sub>/Ce-Zr dual bed system. Compared with Ag/Al alone, a remarkable supplementary NO<sub>x</sub> conversion was obtained at low temperature. The NO<sub>x</sub> conversion was then ranked between 46 and 95% in the 175-250°C temperature range, while only NO was initially injected. As expected, supplementary ammonia consumption was also observed in the dual bed system. At 200°C, the overall NH<sub>3</sub>-NO<sub>x</sub> stoichiometry respected a ratio close to 1-1. Consequently, the low temperature ammonia slip was limited, at only 115 ppm and 125 ppm NH<sub>3</sub> at 200°C and 250°C, respectively (Figure 10). For Temperature higher than 350°C, the ammonia over injection was factually not needed since the NO<sub>x</sub> conversion already reached 100% with ethanol. Moreover, *in situ* produced ammonia is emitted from Ag/Al (Figure 10)., as previously reported [23]. For instance, at 350°C, the WO<sub>3</sub>/Ce-Zr catalyst is virtually submitted to 400 ppm NH<sub>3</sub> from ammonia co-injection plus 150 ppm NH<sub>3</sub> from the EtOH process over Ag/Al. However, WO<sub>3</sub>/Ce-Zr then acted as an ammonia slip catalyst since approximately 50 % of this 550 ppm ammonia excess appeared converted into N<sub>2</sub>. This apparent conversion rate reached 86 % at 450°C Nevertheless, taking into account the whole temperature range, the (EtOH+NH<sub>3</sub>)/NO<sub>x</sub> ratio should to be adjusted (*i.e.* decreased) depending on the temperature to prevent ammonia emission.

Besides, over the the Ag/Al+WO<sub>3</sub>/Ce-Zr dual bed system, NO<sub>2</sub> emitted from the first catalytic bed (Ag/Al sample, Figure 5, red line) was fully converted over the downstream WO<sub>3</sub>/Ce-Zr material (SI file Figure S4). Nevertheless, the NH<sub>3</sub>-NO-NO<sub>2</sub> stoichiometry over the WO<sub>3</sub>/Ce-Zr sample did not correspond to only the fast SCR reaction, NO<sub>2</sub> appeared partially reduced into NO: at 200°C, 128 ppm

 $NO_x$  are supplementary converted into  $N_2$  in the dual-bed configuration, while 154 ppm  $NO_2$  and 285 ppm  $NH_3$  are converted.

In order to confirm that the efficiency gain observed in Figure 10 arose from a synergy effect between the two catalytic materials Ag/Al and WO<sub>3</sub>/Ce-Zr, (EtOH+NH<sub>3</sub>)-SCR experiments were performed over single Ag/Al and WO<sub>3</sub>/Ce-Zr catalysts with doubled catalytic weight (200 mg), *i.e.* with the same catalyst weight/molar flow (W/F) ratio than for the dual bed set-up. Results presented in SI file (Figure S5) indicate significantly lower deNO<sub>x</sub> efficiency in the 175-250°C temperature range over single catalysts compared with the dual-bed system. Obviously, this result illustrates the benefit of the (EtOH+NH<sub>3</sub>)-SCR process with the dual bed configuration.

Finally, the deNO<sub>x</sub> efficiency obtained in (EtOH+NH<sub>3</sub>)-SCR condition over the dual-bed system was similar to the activity observed in the most favourable fast-SCR stoichiometry over single WO<sub>3</sub>/Ce-Zr sample reported in SI file, Figure S3. This result is also better than that obtained over a patented iron exchanged ferrierite (Fe/FER) using the same set-up. In fact, results reported in [64] and in Figure S6 show that the NO<sub>x</sub> conversion in standard-SCR condition is limited from 58 to 69 % in the 200-500°C temperature range. A 2.8%Cu /FER was also evaluated and exhibited conversions close to Ag/Al in (EtOH+NH<sub>3</sub>)-SCR condition (Figure S6), without reaching the efficiency reported on the combined Ag/Al + WO<sub>3</sub>/Ce-Zr in (EtOH+NH<sub>3</sub>)-SCR condition.

To conclude, a remarkable deNO<sub>x</sub> efficiency was obtained at low temperature over Ag/Al+WO<sub>3</sub>/Ce-Zr dual bed catalysts devoted to the (EtOH+NH<sub>3</sub>)-SCR process. NO<sub>x</sub> conversion then reached 70 % at 200°C, compared with 7 % in EtOH-SCR over Ag/Al. Additionally, the deNO<sub>x</sub> efficiency of this (EtOH+NH<sub>3</sub>)-SCR process is no longer determined by the activity of the upstream oxidation catalyst (DOC) since results presented in this work were without NO<sub>2</sub> in the inlet feed stream.

#### 4. Conclusion

This work demonstrates that co-feeding ammonia and ethanol on a Ag/Al<sub>2</sub>O<sub>3</sub> catalyst enables a drastic enhancement of the NO<sub>x</sub> conversion at low temperature (175-250°C) using only NO as NO<sub>x</sub> (standard SCR condition). The (EtOH+NH<sub>3</sub>)-SCR over Ag/Al catalyst has superior NO<sub>x</sub> reduction efficiency than both NH<sub>3</sub>-SCR and EtOH-SCR in the temperature range 175-500°C. It is proposed that the hydrogen H<sup>\*</sup> species provided at low temperature by the ethanol dehydrogenation is the main responsible for the deNO<sub>x</sub> efficiency improvement, in addition to the beneficial concomitant NO<sub>2</sub> formation observed at low temperature with ethanol. Further deNO<sub>x</sub> improvement was obtained over a dual-coupled catalytic system composed of Ag/Al and a usual NH<sub>3</sub>-SCR catalyst (WO<sub>3</sub>/Ce-Zr), taking advantage of the remaining  $NH_3$  and  $NO_2$  from Ag/Al catalyst. A promising efficiency of 70% of  $NO_x$  converted at 200°C was reached, without dependence to the activity of the upstream oxidation catalyst (DOC).

The present results also have practical implications. A unique aqueous solution containing both urea (NH<sub>3</sub> carrier) and ethanol could be used for this purpose, also allowing carrying away a much higher amount of reductant species versus the conventional AdBlue solution.

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# Supplementary information file

# SI-1: Characterization of Ag/Al by TEM.

Transmission Electron Microscopy (TEM) micrographs were recorded on JEOL 2100 instrument (operated at 200 kV with a LaB<sub>6</sub> source and equipped with a Gatan Ultra scan camera). TEM experiments showed that  $Ag/Al_2O_3$  presents small silver particles, most of the particles ranging below 3 nm (Figure S1).



**Figure S1.** A: Representative TEM images obtained for Ag/Al sample; B: Corresponding silver particle sizes distribution (from the classification of the counting of approximately 150 particles).

# SI-2: Design of the IR cell for high temperature *in situ* adsorption of probe molecule.

The home-made designed cell (Figure S2) allows *in situ* treatment and high temperature adsorption of probe molecule. The design of this specific IR cell enables to collect IR spectrum of adsorbed species and gaseous compounds at the same temperature.



**Figure S2.** Design of the home-made IR cell for high temperature *in situ* adsorption of probe molecule.

# SI-3: Catalytic behaviors of WO<sub>3</sub>/Ce-Zr sample.

Before use in the dual-bed catalytic system, the  $WO_3$ /Ce-Zr sample was firstly evaluated alone with various reaction mixtures depicted in table S1. Corresponding NOx conversions depending on the temperature are depicted in Figure S3.

Table S1. Composition of the Gas mixtures of the SCR tests (total rate: 333 mL min <sup>-1</sup> ).									
Catalytic test	NO (ppm)	NO₂ (ppm)	NH₃ (ppm)	C₂H₅OH (ppm)	H <sub>2</sub> (ppm)	O2 (%)	CO2 (%)	H₂O (%)	$N_2$
Fast-NH <sub>3</sub> -SCR	200	200	400			10	10	8	
EtOH-SCR	400			1200		10	10	8	balance
(EtOH+NH₃)-SCR	400		400	1200		10	10	8	



**Figure S3.** NO<sub>x</sub> conversion in EtOH-SCR (—) and (EtOH+NH<sub>3</sub>)-SCR (—) and Fast NH<sub>3</sub>-SCR (—) over WO<sub>3</sub>/Ce-Zr catalyst ( $\triangle$ ).

(400 ppm NO, 1200 ppm  $C_2H_5OH,$  with or without 400 ppm  $NH_3,$  8 %  $H_2O,$  10 %  $CO_2,$  10 %  $O_2$  balanced in  $N_2).$ 

The NO<sub>x</sub> conversion obtained with only ethanol as reductant (blue full line, Figure S3) was very limited, with a maximum of only 7 % at 300°C. It results that WO<sub>3</sub>/Ce-Zr catalyst is not efficient to reduce NO<sub>x</sub> by ethanol. To the opposite, for the (EtOH+NH<sub>3</sub>)-SCR condition, the NO<sub>x</sub> conversion (full red line) was significant, from 13 to 70 % in the 175-450°C temperature range. Finally, this catalyst is very active in Fast-NH<sub>3</sub>-SCR condition, with NOx conversion of 53% and 90 % at 170°C and 200°C, respectively.

## SI-4: NO<sub>2</sub> emission in dual-bed configuration.



**Figure S4**. NO<sub>x</sub> conversion (full line) and NO<sub>2</sub> outlet (dotted line) over Ag/Al ( $\bigcirc$ ) and dual-bed Ag/Al+WO<sub>3</sub>/Ce-Zr ( $\Box$ ) system for (EtOH+NH<sub>3</sub>)-SCR process.

During EtOH-SCR experiments over Ag/Al<sub>2</sub>O<sub>3</sub> catalyst, significant NO<sub>2</sub> emission was recorded outlet. The addition of NH<sub>3</sub> led to a decrease in the NO<sub>2</sub> outlet concentration. However, unconverted NO<sub>2</sub> was still available. By adding a dedicated NH<sub>3</sub>-SCR sample downstream the Ag/Al<sub>2</sub>O<sub>3</sub> catalyst, a full consumption of the emitted NO<sub>2</sub> was recorded (Figure S4). Consequently, the dual-bed system takes advantage of the remaining unconverted NO<sub>2</sub> and NH<sub>3</sub> to enhance the deNO<sub>x</sub> efficiency.

## SI-5: Effect of catalytic weight in (EtOH+NH<sub>3</sub>)-SCR over dual and single bed

With the co-injection of ethanol and NH<sub>3</sub>, a remarkable deNO<sub>x</sub> activity was reached at low temperature using the dual bed configuration (red curve, Figure S5). To ensure that the efficiency gain provided by the dual bed configuration arose from a synergy effect between the two catalytic materials Ag/Al (100 mg) + WO<sub>3</sub>/Ce-Zr (100 mg), (EtOH+NH<sub>3</sub>)-SCR experiments were performed over single Ag/Al and single WO<sub>3</sub>/Ce-Zr catalysts with doubled catalytic weight (200 mg).

Figure S5 clearly shows a higher deNO<sub>x</sub> efficiency over the dual-bed system. SCR experiments performed with doubled weight over single Ag/Al or WO<sub>3</sub>/Ce-Zr materials did not allow the NO<sub>x</sub> conversion achieved over the dual bed configuration. Obviously, this result illustrates the synergetic effect denoted over Ag/Al+WO<sub>3</sub>/Ce-Zr association.



**Figure S5.** NO<sub>x</sub> conversion in (EtOH+NH<sub>3</sub>)-SCR over single Ag/Al (200 mg,  $\bigcirc$ ), single WO<sub>3</sub>/Ce-Zr (200 mg,  $\triangle$ ) or dual bed Ag/Al+WO<sub>3</sub>/Ce-Zr (100+100 mg,  $\Box$ ) system.

# SI-6: Comparison with metal exchanged zeolite catalysts.

Metal exchanged zeolite-based catalysts, devoted to NH<sub>3</sub>-SCR process, were reported to be relevant materials for the NOx abatement of mobile source. A variety of zeolites have been proposed (ZSM-5, mordenite, beta, ferrierite, Y-zeolite, chabazite,...) and in the last few years, new generations of iron or copper exchanged zeolites based on small pore materials have emerged. As a consequence, iron or copper-exchanged ferrierite (FER) samples have been evaluated in NH<sub>3</sub>-SCR in our laboratory (Figure S6).

A patented thermos-resistant Fe/FER zeolithe dedicated to NOx treatment from vehicles was evaluated in standard SCR with NH<sub>3</sub> using the same catalytic bench (same total flow rate and NOx concentration, and the same catalyst mass) [M. Seneque, X. Courtois, F. Can, D. Duprez, Top. Catal.59 (2016) 938-944]. Results reported in Figure S5 show that the deNO<sub>x</sub> efficiency is limited from 58 to 69% in the 200-500°C temperature range (NOx conversion in Fast-SCR condition reached around 97%

in the whole temperature range [Top. Catal.59 (2016) 938-944]). It clearly evidences that this ironexchanged sample is strongly dependent to the NO<sub>2</sub>/NOx inlet ratio.

In addition, a 2.8% Cu/FER was very recently prepared at the laboratory by ion exchange in a host zeolite provided by Sigma Aldrich. After hydrothermal ageing at 700°C, this sample was evaluated in standard NH<sub>3</sub>-SCR, but with a quite higher total flow rate/catalyst mass ratio (5 versus 3.33) and with 500 ppm NO in the reaction mixture. This Cu/FER sample exhibited a different behaviour compared with Fe/FER, with a limited deNO<sub>x</sub> efficiency at low temperature but a full NOx reduction from 300°C. Indeed, the NOx conversion profile was similar to that recorded over Ag/Al in (EtOH+NH<sub>3</sub>)-SCR condition. Taking into account the corresponding experimental set-up (total flow rate, catalyst weight, NO inlet concentration), the activities at 200°C are 1.67 10<sup>-5</sup> mol<sub>converted NO</sub> /min /g<sub>cata</sub> for Ag/Al in EtOH+NH<sub>3</sub> condition and Cu/FER in standard SCR condition, respectively. Consequently, the activity is 11 % higher at this temperature with the (EtOH+NH<sub>3</sub>)-SCR.



**Figure S6.** NO<sub>x</sub> conversion in EtOH-SCR (—) and (EtOH+NH<sub>3</sub>)-SCR (—) over Ag/Al sample, and in (EtOH+NH<sub>3</sub>)-SCR condition over Ag/Al+WO<sub>3</sub>/Ce-Zr dual bed system (—).

For comparison, NOx conversion obtained in  $NH_3$ -SCR over zeolite-base catalysts are also reported: patented Fe/FER (••••) and 2.8% Cu/FER (•••).

Finally, the deNO<sub>x</sub> efficiency of the (EtOH+NH<sub>3</sub>)-SCR process is significantly higher than that obtained over zeolite based catalysts, especially when a specific NH<sub>3</sub>-SCR sample is associated downstream to Ag/Al in a dual-bed configuration. This combined dual-bed system (Ag/Al+WO<sub>3</sub>/Ce-Zr) achieved a remarkable NO<sub>x</sub> conversion of 70 % at 200°C, compared to 20 % for Cu/FER sample when only NO was introduced as NO<sub>x</sub>.

#### References

- [1] R.N. Colvile, E.J. Hutchinson, J.S. Mindell, R.F. Warren, Atmos. Environ. 35 (2001) 1537-1565.
- [2] G. M. Whitesides, Angew. Chem. Int. Ed. 54 (2015) 3196-3209.
- [3] J. Kašpar, P. Fornasiero, N. Hickey, Catal. Today 77 (2003) 419-449.
- [4] D. Chatterjee, O. Deutschmann, J. Warnatz, Faraday Discuss. 119 (2001) 371-384.
- [5] W. Yang, R. Zhang, B. Chen, D. Duprez, S. Royer, Environ. Sci. Technol. 46 (2012) 11280–11288.
- [6] J. Liu, X. Li, Q. Zhao, C. Hao, D. Zhang, Environ. Sci. Technol. 47 (2013) 4528–4535.
- [7] F. Figueras, J.L. Flores, G. Delahay, A. Bourane, J.-M. Clacens, A. Desmartin-Chomel, B. Coq, A. Giroir-Fendler, Top. Catal. 39 (2006) 59-64.
- [8] F. Poignant, J. Saussey, J.C. Lavalley, G. Mabilon, J. Chem. Soc., Chem. Commun. (1995) 89-90.
- [9] L. Capek, K. Novoveska, Z. Sobalık, B. Wichterlova, L. Cider, E. Jobson, Appl. Catal. B 60 (2005) 201–210.
- [10] A. Flura, X. Courtois, F. Can, S. Royer, D. Duprez, Top. Catal. 56 (2013) 94-103.
- [11] P. Forzatti, I. Nova, E. Tronconi, Angew. Chem. Int. Ed. 48 (2009) 8366-8368.
- [12] M. Koebel, M. Elsener, G. Madia, Ind. Eng. Chem. Res. 40 (2001) 52-59.
- [13] A. Grossale, I. Nova, E. Tronconi, D. Chatterjee, M. Weibel, Top. Catal. 52 (2009) 1837-1841.
- [14] I. Nova, C. Ciardelli, E. Tronconi, D. Chatterjee, B. Bandl-Konrad, Catal. Today 114 (2006) 3-12.
- [15] Y.H. Yeom, J. Henao, M.J. Li, W.M.H. Sachtler, E. Weitz, J. Catal. 231 (2005) 181-193.
- [16] Y.H. Yeom, B. Wen, W.M.H. Sachtler, E. Weitz, J. Phys. Chem. B 108 (2004) 5386-5392.
- [17] M. Li, J. Henao, Y. Yeom, E. Weitz, W.M.H. Sachtler, Catal. Lett. 98 (2004) 5-9.
- [18] M. Li, Y. Yeom, E. Weitz, W.M.H. Sachtler, Catal. Lett. 112 (2006) 129-132.
- [19] Y.H. Yeom, M. Li, W.M.H. Sachtler, E. Weitz, J. Catal. 246 (2007) 413-427.
- [20] « Urea-SCR Technology for deNO<sub>x</sub> after treatment of Diesel Exhausts, I. Nova and E. Tronconi eds, Springer 2014 DOI 10.1007/978-1-4899-8071-7.
- [21] A. Flura, F. Can, X. Courtois, S. Royer, D. Duprez, Appl. Catal. B 126 (2012) 275-289.
- [22] Y.H. Yeom, M. Li, W.M.H. Sachtler, E. Weitz, J. Catal. 238 (2006) 100-110.
- [23] F. Can, A. Flura, X. Courtois, S. Royer, G. Blanchard, P. Marécot, D. Duprez, Catal. Today 164 (2011) 474-479.
- [24] Y.F. Tham, J-Y.C. Chen, R.W. Dibble, Proc. Combust. Inst. 32 (2009) 2827-2833.
- [25] S. Kameoka, T. Chafik, Y. Ukisu, T. Miyadera, Catal. Lett. 55 (1998) 211-215.
- [26] J. Deng, J. Wang, X. Xu, Catal. Lett. 35 (1995) 75-88.
- [27] K. Eränen, F. Klingstedt, K. Arve, L. Lindfors, D.Y. Murzin, J. Catal. 227 (2004) 328-343.
- [28] J. Shibata, K. Shimizu, Y. Takada, A. Shichi, H. Yoshida, S. Satokawa, A. Satsuma, T. Hattori, J. Catal. 227 (2004) 367–374.
- [29] X. Zhang, H. He, Z. Ma, Catal. Commun. 8 (2007) 187-192.
- [30] S. Fogel, P Gabrielsson, Appl.Catal. B 158-159 (2014) 1–10.
- [31] K-I. Shimizu, A. Satsuma, Appl. Catal. B 77 (2007) 202-205.
- [32] M. Richter, R. Fricke, R. Eckelt, Catal. Lett. 94 (2004) 115-118.
- [33] V. Houel, P. Millington, R. Rajaram, A. Tsolakis, Appl. Catal. B 73 (2007) 203-207.
- [34] V. Houel, P. Millington, R. Rajaram, A. Tsolakis, Appl. Catal. B 77 (2007) 29-34.
- [35] B. Sawatmongkhon, A. Tsolakis, S. Sitshebo, J. Rodriguez-Fernandez, M. Ahmadinejad, J. Collier, R.R. Rajaram, Appl. Catal. B 97 (2010) 373-380.
- [36] T. E. Hoost, R-J. Kudla, K. M. Collins and M. S. Chattha, Appl. Catal. B 13 (1997) 59-67.
- [37] T. Sato, S. Goto S, Q. Tang, S. Yin, J. Mater. Sci. 43 (2008) 2247-2253.
- [38] N. Apostolescu, B. Geiger, K. Hizbullah, M.T. Jan, S. Kureti, D. Reichert, F. Schott, W. Weisweiler, Appl. Catal., B 62 (2006) 104-114
- [39] G. Qi, R.T. Yang, R. Chang, Appl. Catal. B. 51 (2004) 93-106.

- [40] F. Can, S. Berland, S. Royer, X. Courtois, D. Duprez, ACS Catal. 3 (2013) 1120-1132.
- [41] A. Musi, P. Massiani, D. Brouri, J.M. Trichard, P. Da Costa, Catal. Lett. 128 (2009) 25-30.
- [42] V. Vinogradoff, F. Duvernay, M. Farabet, G. Danger, P. Theulé, F. Borget, J.C. Guillemin, T. Chiavassa, J. Phys. Chem. A 116 (2012) 2225-2233.
- [43] R. Jin, Y. Liu, Z. Wu, H. Wang, T. Gu, Chemosphere 78 (2010) 1160-1166.
- [44] Y. Amenomiya, J. Catal. 46 (1977) 326-339.
- [45] M. Amblard, R. Burch, B.W.L. Southward, Catal. Today 59 (2000) 365-371.
- [46] J.B. Peri, J. Phys. Chem. 69 (1965) 231-239.
- [47] K-I Shimizu, H. Kawabata, A. Satsuma, T. Hattori, J. Phys. Chem. B 103 (1999) 5240-5245.
- [48] T. Venkov, K. Hadjiivanov, D. Klissurki, Phys. Chem. Chem. Phys. 4 (2002) 2443-2448.
- [49] G.M. Underwood, T.M. Miller, V.H. Grassian, J. Phys. Chem. A 103 (1999) 6184-6190.
- [50] C. Börensen, U. Kirchner, V. Scheer, R. Vogt, R. Zellner, J. Phys. Chem. A 104 (2000) 5036-5045.
- [51] Y.Yu, H. He, Q. Feng, H. Gao, X. Yang., Appl. Catal. B 49 (2004) 159-171.
- [52] S. Tamm, N. Vallim, M. Skoglundh, L. Olsson, J. Catal. 307 (2013) 153-161.
- [53] A. A. Tsyganenko and V. N. Filimonov, Spectrosc. Lett. 5 (1972) 477-487.
- [54] A. A. Tsyganenko and V. N. Filimonov, J. Mol. Struct. 19 (1973) 579-589.
- [55] H. Knözinger and P. Ratnasamy, Catal. Rev. Sci. Eng. 17 (1978) 31-70.
- [56] W. El-Nadjar, M. Bonne, E. Trela, L. Rouleau, A. Mino, S. Hocine, E. Payen, C. Lancelot, C.
- Lamonier, P. Blanchard, X. Courtois, F. Can, D. Duprez, S. Roer, Micr. Meso. Mater. 158 (2012) 88-98.
- [57] H. Idriss, Platinum Metals Rev. 48 (2004) 105-115.
- [58] K. Eränen, F. Klingstedt, K. Arve, L. Lindfors, D.Y. Murzin, J. Catal. 227 (2004) 328-343.
- [59] J. Shibata, K. Shimizu, Y. Takada, A. Shichi, H. Yoshida, S. Satokawa, A. Satsuma, T. Hattori, J. Catal. 227 (2004) 367–374.
- [60] A.Y. Stakheev, P.V. Pributkov, S. Dahl, I. Gekas, G.N. Baeva, G.O. Bragina, N.S. Telegina, Top. Catal. 52 (2009) 1821-1825.
- [61] J.F. DeWilde, C.J. Czopinski, A. Bhan, ACS Catal. 4 (2014) 4425-4433.
- [62]D.E. Doronkin, S. Fogel, S. Tamm,L. Olsson, T.Khan, T.Bligaard, P. Gabrielsson, S. Dahl, Applied Catal. B 113-114 (2012) 228-236.
- [63] Y. Yeom, M. Li, A. Savara, W. Sachtler, E. Weitz, Catal. Today 136 (2008) 55-63.
- [64] M. Seneque, X. Courtois, F. Can, D. Duprez, Top. Catal.59 (2016) 938-944.