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# Simulation-based study about the lifetime and incident light properties dependency of the optically triggered 4H-SiC thyristors operation

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**Abstract**—We investigated a methodology to design light-triggered thyristors thanks to TCAD. The simulation model accuracy, especially the holding current and the minimum incident light intensity to turn-on, were compared with experimental results. The influence of SiC epitaxial layer lifetime and the incident light properties (wavelength and intensity) on the optically triggered 4H-SiC thyristor characteristics have been studied by simulation. We considered the wavelength dependency of quantum efficiency, penetration depth and photon energy. The holding current and turn-on time depends on the lifetime. The minimum intensity to turn-on the device significantly depends on the wavelength. This intensity becomes less than 0.003 times when the wavelength changed from 380 nm to 325 nm. In addition, the breakover voltage is affected by the constant incident light even if the intensity is tiny.

**Index Terms**—optically triggered thyristor, simulation model, wavelength dependency, minimum intensity

## I. INTRODUCTION

Silicon carbide (SiC) is an attractive material for manufacturing low on-resistance, high-voltage power devices. SiC thyristors are dedicated to the applications that exceed more than 10 MVA (megavolts-ampere) conversion power, especially high-voltage direct current (HVDC) electric power transmission system and power converters in smart grid [1-2]. This device already has been commercialized as engineering sample [3]. In the recent years, the 15-18kV class SiC light triggered thyristors, using 266 nm UV-C (Ultraviolet C) pulse laser, have been developed [4-5]. Dheilly et al. reported the demonstration of direct light triggering by 330-340 nm wavelength UV-A LEDs [6]. The main advantage of the optical gate driving provides galvanic isolation simplifying device driver circuitry, and it will contribute to realize the small thyristor with high reliability by preventing erroneous arc firing due to electromagnetic noise.

Compared to other power devices, designing thyristors are somewhat more challenging. The simulation model is essential to device design and circuit design. However, the facility of simulation convergence strongly depends on the meshing

quality (structure discretization quality) and designers must face to the trade-off between the calculation cost and the convergence rate. It is difficult to calculate the thyristor characteristics due to the abundance of a number of layers. Therefore, few articles on the simulation modeling were published. Mnatsakanov et al. investigated the turn-on process based on the 18kV class thyristor simulation models [7]. Meyer et al. evaluated the resistance to inductive parasitic, using the circuit simulation including a thyristor with 250 nm wavelength optical source [8].

In this study, we developed the 10kV class 4H-SiC optically triggered thyristor simulation model and evaluated the influences of the drift-layer lifetime  $\tau_{\text{drift}}$  and incident light properties (wavelength  $\lambda$  and intensity  $I_0$ ) on the static and dynamical characteristics. The model accuracy was compared with experimental results.

## II. DEVICE STRUCTURE AND PHYSICAL MODELS

The device was modeled thanks to Synopsys TCAD (Technological Computer Aided Design) Sentaurus™. The basic 4H-SiC parameters were taken from the literature: dielectric constant [9], bandgap [10] and bulk mobility [11]. Incomplete ionization was ignored to simplify the model and improve the convergence in optical turn-on simulation.

### A. Device structure and optical source

Several 10kV class 4H-SiC optically triggered thyristors shown in Fig. 1 were fabricated for measuring the breakdown voltage and dynamical characteristics. The thyristors were

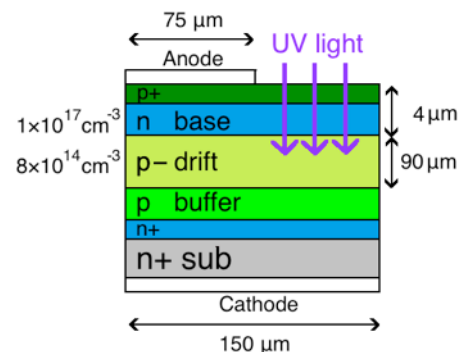


Fig. 1. Cross section of an optically triggered thyristor for measuring the breakdown voltage and dynamical characteristics.

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formed by a p<sup>-</sup> drift-layer which thickness is equal to 90 μm and a thin n base-layer. The top of the device cells were formed by p<sup>+</sup> layer. We made circular holes in the anode electrode for optical gate (optical window). The 365 nm wavelength UV-A LEDs, which has advantages in term of the size and cost compared to UV-C laser, were used to turn-on.

In the simulation, the same structure was modeled in two dimensions and the anode current simulated by solving model equations in cylindrical coordinates. The center axis is the right side of device in Fig. 1. The sizes of optical window and anode electrode are  $1.8 \times 10^{-4}$  cm<sup>2</sup> and  $5.3 \times 10^{-4}$  cm<sup>2</sup>, respectively. Area factor was set at 1.0. The monochromatic optical source was set to be uniformly irradiated to the optical windows.

### B. Lifetime

The minority carrier lifetime is an important factor of bipolar device (forward characteristics of pin diode [12], turn-off characteristics of gate turn-off thyristor [13]). Variety p-type SiC lifetimes that are measured by the microwave photoconductance decay (μ-PCD) are reported: 0.1-1.6 μs [14] and 10 μs [15]. We defined the doping dependence of the lifetime by Scharfetter relation shown in eq. 1, and we dealt with  $\tau_{\max}$  as a fitting parameter ( $\tau_{\text{drift}}$  is  $\tau_{\max}$  at drift layer).  $N_{\text{ref}}$  is set  $3.0 \times 10^{17}$  cm<sup>-3</sup> while  $\gamma$  set 0.3 [16].

$$\tau = \tau_{\max} \left\{ 1 + \left( \frac{N_{\text{total}}}{N_{\text{ref}}} \right)^{\gamma} \right\}^{-1} \quad (1)$$

### C. Avalanche Recombination

Impact ionization coefficients are critical value for simulate the breakover voltage. Accordingly, the avalanche recombination model was considered. Variety fitting parameters are reported [17-24]. We used Niwa's parameter [23] based on Okuto-Crowell model [25] shown in eq. 2 (simplified by  $T = 300$  K).  $\alpha$  is ionization coefficient,  $E$  is field intensity, and  $a$ ,  $b$ ,  $\delta$  are fitting parameters. The parameters for electrons are below:  $a = 8.19 \times 10^9$  V<sup>-1</sup>,  $b = 3.94 \times 10^7$  V/cm, and  $\delta = 1.0$ .

$$\alpha(E) = a \exp \left[ - \left( \frac{b}{E} \right)^{\delta} \right] \quad (2)$$

### D. Refractive index

The penetration depth  $\alpha^{-1}$  of light depends on imaginary part of complex refractive index (extinction coefficient  $k$ ). Equation 3 shows the Beer-Lambert law. The intensity of an electromagnetic wave inside a material  $I(z)$  fall off exponentially from the surface. Equation 4 is the relationship between penetration depth  $\alpha^{-1}$  and extinction coefficient  $k$ .  $\lambda$  is the wavelength of the light. The relationship between  $\lambda$  and the absorption coefficient  $\alpha$  were estimated [26] by using optical measurement result and the real part of complex refractive index  $n$  of 6H-SiC [27]. (Absorption coefficient  $\alpha$  is a reciprocal of penetration depth  $\alpha^{-1}$ .) We used the real part of complex refractive index  $n$  of 4H-SiC in [28] and the

imaginary part of complex refractive index  $k$  was calculated from square root of the absorption coefficient  $\alpha^{1/2}$ . Fig. 2 shows the wavelength dependency of the penetration depth  $\alpha^{-1}$ , comparing the accurate value shown in [26] and our fitting to  $\alpha^{1/2} - \lambda$  graph shown in same reference. In our fitting,  $\alpha^{-1}$  is 126.6 nm at 365 nm wavelengths. It is enough to radiate the light to n-base layer.

$$I(z) = I_0 \exp[-\alpha z] \quad (3)$$

$$\alpha^{-1} = \frac{\lambda}{4\pi k} \quad (4)$$

### E. Quantum efficiency

Quantum efficiency is the conversion efficiency from a photon to one electron hole pair. The step-function quantum yield model was used. This model is explained that the quantum yield is set to one when the excitation energy is greater than or equal to the bandgap energy, otherwise it is set to zero [29]. Nevertheless, some papers reported that the quantum efficiency regarding 365 nm wavelength laser radiation is 1% order. D. M. Brown, et al., showed the measurement results, analytical calculation results, and temperature dependency of quantum efficiency that were converted from the responsivity of 6H-SiC n<sup>+</sup>-p-p<sup>+</sup> photodiode [30]. The value of 4H-SiC Cr-SiC Schottky [31] and p-n<sup>-</sup>-n<sup>+</sup> photodetector [32] are also reported. The indirect optical

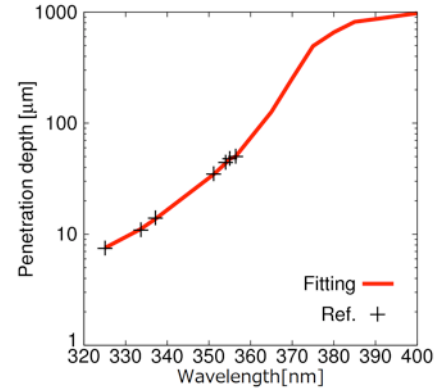


Fig. 2. Wavelength dependency of the penetration depth  $\alpha^{-1}$ . The cross-mark is the value shown in [26]. The red line is fitting from  $\alpha^{1/2} - \lambda$  graph shown in same reference.

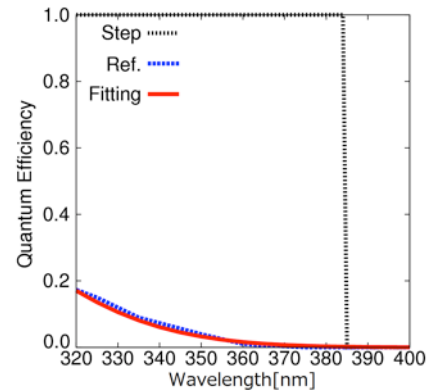


Fig. 3. Wavelength dependency of the quantum efficiency, comparing the value in [32], fitting result, and the step-function model.

excitation occurs within the long wavelength (295-385 nm) and this excitation process is a reason of low quantum efficiency [31].

We changed the scaling factor (default is 1) of step-function model depending on each wavelength, to reproduce the realistic quantum efficiency. The quantum efficiency was varied from 1.1 % (365 nm) to 60 % (265 nm) with rough approximation by Gauss function. Fig. 3 shows the quantum efficiency, comparing the measurement value in [32] and our fitting. The value from step-function model with no scaling was also shown in Fig. 3.

### III. RESULTS AND DISCUSSIONS

We simulated both static and dynamic characteristics. To keep the correspondence with the actual static/dynamic characteristic measurement condition, the device temperature was kept at 300 K and a 500-k $\Omega$  series resistance had been introduced between the voltage source and the thyristor anode electrode. To avoid the capacitive displacement current that causes the undesired turn-on, the time change rate limit of voltage source was set at 1 V/s.

#### A. The lifetime dependency of characteristics

The static output characteristics  $I_a$ - $V_{ak}$  were simulated and we estimated the lifetime dependency. Fig. 4(a) shows the simulated  $I_a$ - $V_{ak}$  characteristics. In this figure, the breakover voltage is 11 kV and reverse breakdown voltage is 450 V. The actual measured breakover voltage is 9.5 kV. The incomplete ionization and edge termination structure did not consider in this simulation. Those are one of the reasons of the difference between simulation and experimental results. (The simulated value considering incomplete ionization becomes 9.8 kV.) Fig. 4(b) shows the simulated optically turn-on and turn-off characteristics. The value of voltage source was swept from 0 V to 400 V, and the strong incident light (intensity  $I_0$  was 3800 W/cm<sup>2</sup>, pulse duration  $t_d$  was 0.1  $\mu$ s, turn-on/turn-off fronts was 1 ns, and wavelength  $\lambda$  was 365 nm) was applied when the voltage become 300 V to turn-on. When we applied 300 V, the 1  $\mu$ m order space-charge region appeared in the n base-layer caused by the reverse bias at p-n junction. Turn-on occurred by the optical generated electron-hole pair, then, snap-back occurred ( $V_{ak}$  become lower even if we increased the value of voltage source from 300 V to 400 V). Finally, the voltage decrease 400 V to 0 V to turn-off. When the anode current falls below the ‘‘holding current’’ due to reducing applied anode voltage, the turn-off process began. When the p-drift-layer lifetime  $\tau_{drift}$  was set at 0.4  $\mu$ s for electrons, the holding current was 0.30 mA (0.57 A/cm<sup>2</sup>), and the holding voltage was 3.1 V. The on-state voltage once the device has been fully turned-on were 3.05-3.11 V in Fig. 4, and these simulated values fit well with experimental data.

Fig. 5 shows the comparison between the simulated holding current and the experimental result. The holding current reduced by half when the lifetime varied from 0.40 to 0.50  $\mu$ s. Some papers discussed the relationship between the holding current of 4H-SiC thyristor and the lifetime [33-34]. The n base-layer minority carrier concentration, which contributes to

keeping on-state and decides the value of holding current, is controlled by the lifetime. The measured holding current was 0.38 mA (0.72 A/cm<sup>2</sup>), and the simulation reproduced this value well when we use  $\tau_{drift} = 0.4 \mu$ s. We applied this value in the simulation as a rough estimation instead of the result of lifetime measurement methods that are represented by  $\mu$ -PCD. In addition, we also simulated the lifetime dependency of breakover voltage. The breakover voltage had no significant lifetime dependency.

Fig. 6 shows the simulated  $I_a$ - $t$  characteristics when the turn-on process occurred by the incident light. The time axis shows the elapsed time after the optical pulse kick-started.  $V_{ak}$

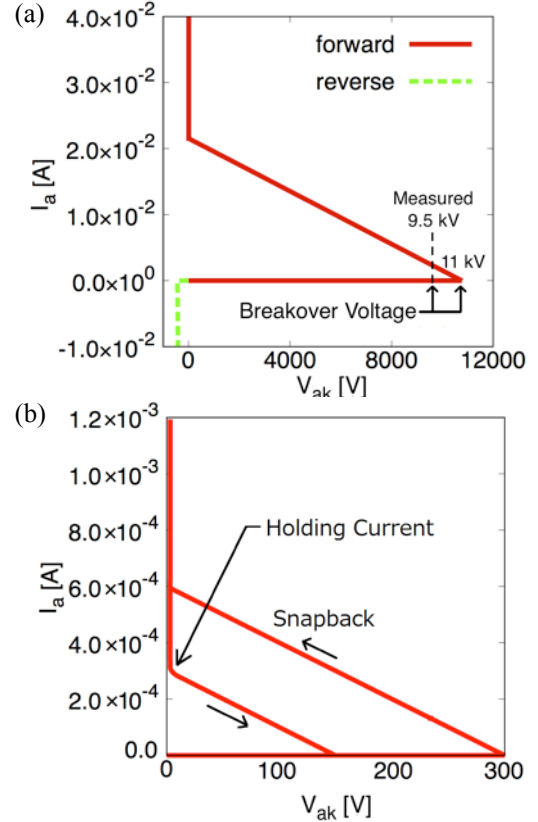


Fig. 4. Output characteristic simulation results (a) without incident light (b) with incident light ( $I_0 = 3800$  W/cm<sup>2</sup>, duration is 0.1  $\mu$ s) at  $V_{ak} = 300$  V.

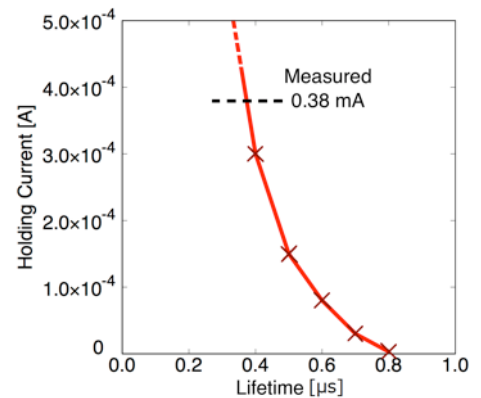


Fig. 5. Holding current simulation result. The applied voltage decrease 400 V to 0 V to turn-off. An experimental result is also shown.

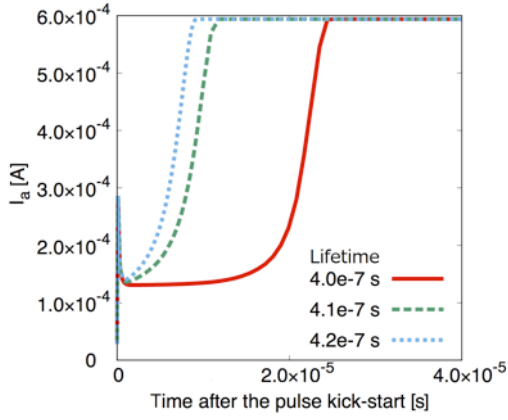


Fig. 6. Simulation result of  $I$ - $t$  characteristics with variety lifetime.  $V_{ak}$  is 300 V. The incident light intensity is  $3800 \text{ W/cm}^2$  and duration is  $0.1 \mu\text{s}$ . The horizontal axis shows the elapsed time after starting the light irradiation.

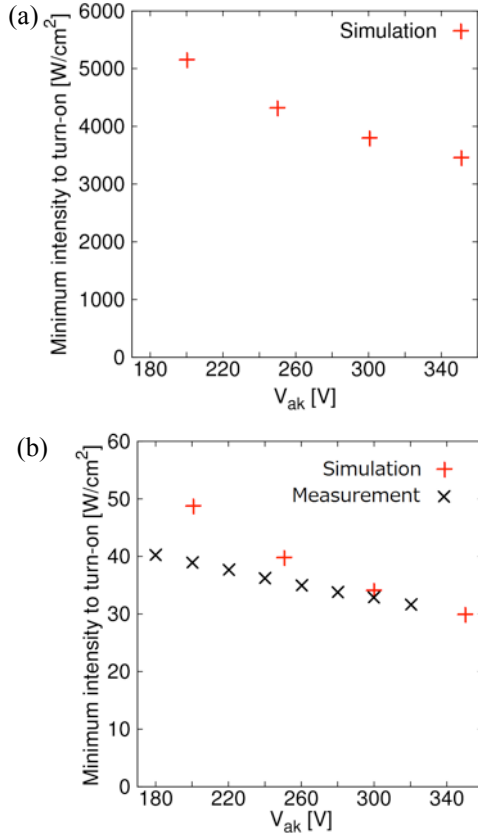


Fig. 7. Minimum intensity of optical pulse to turn-on. The pulse duration is set at (a)  $0.1 \mu\text{s}$  (b)  $15.4 \mu\text{s}$ . The wavelength is  $365 \text{ nm}$ .

was set at  $300 \text{ V}$  and the same strong incident light with Fig 4(b) was used:  $I_0 = 3800 \text{ W/cm}^2$ ,  $t_d = 0.1 \mu\text{s}$ , and  $\lambda = 365 \text{ nm}$ . We also showed the lifetime dependency of the turn-on time in Fig. 6. The lifetime varied from  $\tau_{drift} = 0.40 \mu\text{s}$  to  $0.42 \mu\text{s}$ . The initial current spike coming from the initial carrier optical generation [7, 35]. The turn-on time is  $23 \mu\text{s}$  when  $\tau_{drift} = 0.40 \mu\text{s}$ . Comparing between  $\tau_{drift} = 0.40 \mu\text{s}$  and  $\tau_{drift} = 0.41 \mu\text{s}$ , the turn-on time reduced by half even if the lifetime extended only  $10 \text{ ns}$ . This result shows the importance of the controlling balance between carrier generation and recombination to start the turn-on fast. Note that the long lifetime increases the

minority carrier in the drift layer, which cause the tail current.

### B. Light irradiation response

The minimum optical power required to trigger the thyristor is an important factor to reduce the energy loss of the thyristor upon turn-on. Fig. 7 shows the simulated minimum incident light illumination intensity to turn-on,  $I_{0min}$  at  $V_{ak} = 200\text{-}350 \text{ V}$ . The wavelength  $\lambda$  was  $365 \text{ nm}$  and the pulse duration  $t_d$  was set at (a)  $0.1 \mu\text{s}$  and (b)  $15.4 \mu\text{s}$ . We also measured  $I_{0min}$  using  $\lambda = 365 \text{ nm}$  UV-A LED.  $t_d$  was set at  $15.4 \mu\text{s}$ . The values of intensity, which are incident optical power density at the surface of optical window, were estimated from the LED current and the spatial arrangement of LEDs. Comparing with experimental results shown in Fig. 7(b), the simulation obtained well results closer to actual value in the range of  $V_{ak} = 300\text{-}350 \text{ V}$ . The simulated value was  $I_{0min} = 34.0 \text{ W/cm}^2$ , and measured value was  $I_{0min} = 32.9 \text{ W/cm}^2$  at  $V_{ak} = 300 \text{ V}$ . According to Fig. 7,  $I_{0min}$  become lower when the applied voltage become higher. The electric field originated in  $V_{ak}$  helps the injection of the optically generated hole carriers from p+ emitter to thin n-base and wide p-drift region. Then the total amount of photo-generated hole which necessary to turn-on are decreased by the carrier injection rate increasing. This explains the relationship between  $I_{0min}$  and  $V_{ak}$ . On the other hand, The multiple value of  $t_d$  and  $I_{0min}$  is about  $5 \text{ W} \cdot \text{s/m}^2$  at  $V_{ak} = 300 \text{ V}$  even if the  $t_d$  was extended more than 100 times. This constant shows the rough relationship between  $t_d$  and  $I_{0min}$ . We notice that we used the ideal light source and ignored the time dependence of the intensity in this simulation.

The wavelength dependency of  $I_{0min}$  is salient than the applied voltage dependency. Fig. 8 shows the wavelength dependence of  $I_{0min}$ . The wavelength was set within a range of  $\lambda = 325\text{-}400 \text{ nm}$ , and only one-photon excitation phenomena was considered in the simulation model. The applied voltage was  $V_{ak} = 300 \text{ V}$  and pulse duration was  $t_d = 15.4 \mu\text{s}$ . The experimental result with  $\lambda = 365 \text{ nm}$  was also shown in this figure (same value as Fig. 7(b)). According to simulation result in Fig. 8,  $I_{0min}$  become less than 0.003 times when the wavelength changed from  $380 \text{ nm}$  to  $325 \text{ nm}$ . The turn-on process did not occur at  $\lambda > 385 \text{ nm}$  wavelength. In our measurement, the turn-on phenomena also not occur in  $\lambda = 400 \text{ nm}$ . These tendencies can be explained by considering three phenomena:

- The quantum efficiency is large at short wavelength. In our parameter, shown in Fig. 3, the quantum efficiency is  $0.31 \%$  at  $380 \text{ nm}$ ,  $1.1 \%$  at  $365 \text{ nm}$  and  $14 \%$  at  $325 \text{ nm}$ . This wavelength dependency is the main reason of the significant  $I_{0min}$  wavelength dependency. The quantum efficiency is directly related to the quantity of photo-excited non-equilibrium carriers. If the amount of these carriers is larger than the “critical charge”, the turn-on finally occurs [7].
- The penetration depth steeply decreases at short wavelength. According to Fig. 2, the penetration depth is  $126 \mu\text{m}$  at  $\lambda = 365 \text{ nm}$ , and  $7.25 \mu\text{m}$  at  $\lambda = 325 \text{ nm}$ .



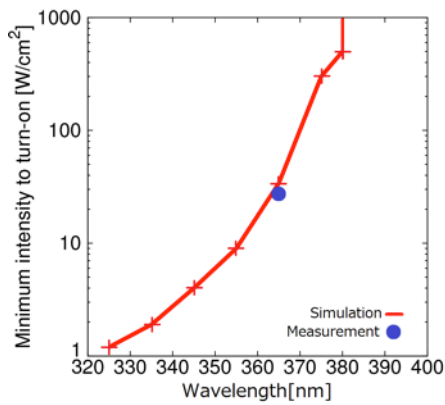


Fig. 8. Wavelength dependency of the minimum intensity to turn-on. An experimental result is also shown by blue dot. The pulse duration is set at 15.4  $\mu$ s.

However, due to the anode  $p^+$  layer and the n base layer are thin, this wavelength dependency does not affect to  $I_{0min}$  in a range of  $\lambda > 325$  nm.

- Excitation energy is not enough at  $\lambda > 385$  nm, hence, there is no way to excite the carriers even if the intensity is strong. The energy of a photon  $hc/\lambda$  is 3.22 eV at 385 nm, and the 4H-SiC bandgap  $E_g$  is 3.23 eV at 300 K [10]. The Franz--Keldysh effect was not considered in our simulation. This effect will affect the long-wavelength side limit [36].

In addition, we simulated the lifetime dependency of  $I_{0min}$ . The lifetime has no significant effect to decide  $I_{0min}$ .

The low intensity UV-A light has no influence on turn-on. However, it negatively affects the breakover voltage. Fig. 9 shows the simulated wavelength dependency of breakover voltage. The constant weak incident light always irradiated (not pulsed) and others simulation conditions are same as Fig. 4(a). The light intensity  $I_0$  varied in the range of 0.1-10  $\mu$ W/cm<sup>2</sup>, and this intensity is less than 1/1,000,000 times of  $I_{0min}$  that was shown in Fig. 7(b). Note that the UV-A emission from fluorescent lamp at a distance of 20 cm is  $I_0 = 10$   $\mu$ W/cm<sup>2</sup> order [37]. When we applied the light with  $\lambda > 385$  nm ( $hc/\lambda < E_g$ ), the breakover voltage was not changed by UV-A light (11 kV). However, in the case of the  $\lambda = 360$  nm, the breakover voltage became 8.9 kV under the  $I_0 = 0.1$   $\mu$ W/cm<sup>2</sup>. Moreover, the thyristor almost lost the blocking ability in the range of  $\lambda < 360$  nm when  $I_0 = 10$   $\mu$ W/cm<sup>2</sup>. These results show the importance of the UV light shielding.

In this study, all the dynamic calculations are made for the voltage of 400 V for the purpose of comparing with the experimental results. To modeling and discuss the turn-on operation in higher voltage, the model should be checked the correctness considering the large current density and the experimental evidence of sensitivity to incident light.

#### IV. CONCLUSIONS

We developed the 10kV class 4H-SiC optically triggered thyristor simulation model, and we evaluated the influence of the drift-layer lifetime  $\tau_{drift}$  and incident light properties (wavelength  $\lambda$  and intensity  $I_0$ ) on the static and dynamical characteristics. The model accuracy, especially the holding

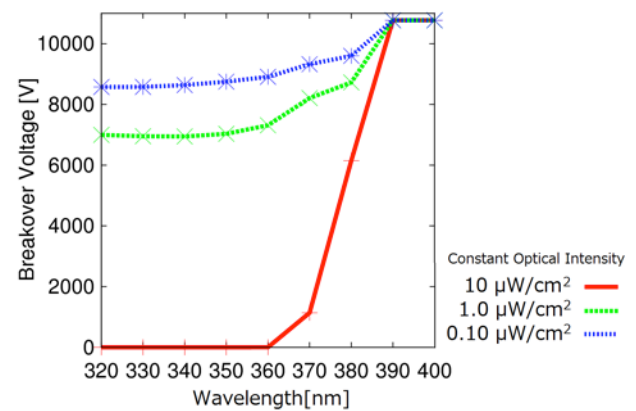


Fig. 9. Wavelength dependency simulation result of the breakover voltage. The slope of applied voltage is 1 V/s. The incident light irradiated constant.

current and the minimum incident light intensity to turn-on, was compared with experimental results.

The holding current and turn-on time depends on the lifetime. In our simulation, the holding current reduced by half when the lifetime varied from 0.40 to 0.50  $\mu$ s, and the turn-on time reduced by half when the lifetime varied from 0.40 to 0.41  $\mu$ s. The minimum incident light intensity to turn-on  $I_{0min}$  significantly depends on the incident light wavelength. The measured  $I_{0min}$  is 32.9 W/cm<sup>2</sup> at the pulse duration 15.4  $\mu$ s,  $V_{ak} = 300$  V. And the simulation reproduced the experimental result well. In our simulation,  $I_{0min}$  become less than 0.003 times when the wavelength changed from 380 nm to 325 nm, due to the wavelength dependency of the quantum efficiency. On the other hand, the low intensity UV-A light has no influence to turn-on, however, it is affect to breakover voltage degradation.

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