High power PCB-embedded inductors based on ferrite powder

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17/5/17



Embedding of magnetics for power electronics

Proposed Embedding Technique

Results

Conclusion











Embedding of magnetics for power electronics

Proposed Embedding Technique





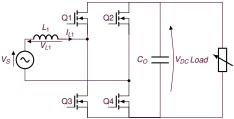


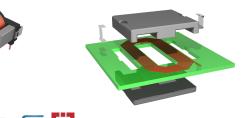


Passives for power electronics

- Main role: energy storage
- example:
 - 1 kW converter @ 100 kHz
 - 10 mJ charge/discharge per cycle
- → They are large
- → Large impact on efficiency
- Embedding in PCB to save space



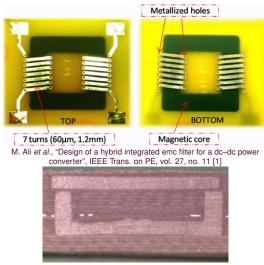




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Embedding of solid cores





- Machine a cavity in laminate
- Insert core in stack-up
- ✓ Use of high-performance materials
- X Few shapes available
- X Machining difficult
- X Brittle materials

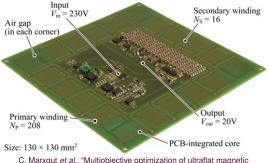
R. Perrin *et al.*, "2 MHz high-density integrated power supply for gate driver in high-temperature applications," APEC 2016 [2]



Embedding of laminated cores



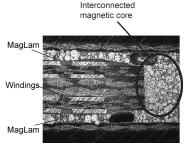
- Thin magnetic layers
 - Permalloy
 - Amorphous material
- More compliant
- Easier to machine
- ✓ Suited to flat geometry
- X Need to isolate layers
- X Complex for high power



C. Marxgut *et al.*, "Multiobjective optimization of ultraflat magnetic components with pcb-integrated core," IEEE Trans PE, vol. 28, no. 7 [3]



Embedding of flexible cores



E. Waffenschmidt *et al.*, "Design Method and Material Technologies for Passives in Printed Circuit Board Embedded Circuits," IEEE Trans. on PE, vol. 20, no. 3 [4]



D. H. Bang et al., "Ni-Zn ferrite screen printed power inductors for compact dc-dc power converter applications," IEEE Trans. on Mag. [5]

= DÉVELOPPEMENT



- Ferrite/polymer mix
 - "MagLam" Sheets
 - Polyimide/ferrite paste
- Suited to flat geometry
- ✓ Suited to complex shapes
- Mechanically compliant
- X Distributed air gap

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• Low μ_r values (\approx 10)





Embedding of magnetics for power electronics

Proposed Embedding Technique

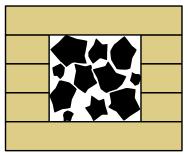


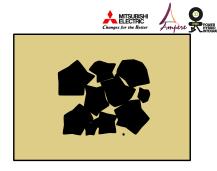






Embedding of ferrite powder in PCB





(a)

(b)

- Open cavities in a stack of pre-preg sheets
- fill cavities with ferrite powder
- laminate pre-preg to compact powder and infiltrate resin

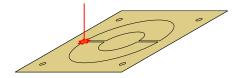






- 2. Stack cut prepregs
- 3. Press stack at low temp. (70 °C)
- 4. Remove from press
- 5. Trim bridges
- 6. Fill with ferrite powder
- Complete stack and laminate (195°C)
- 8. Drill and plate vias
- 9. Pattern copper

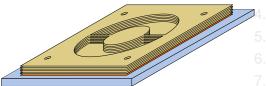






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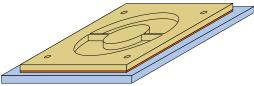
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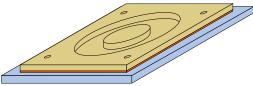






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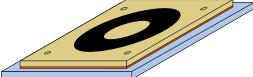






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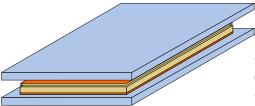




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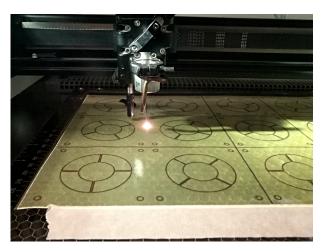
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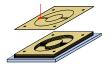




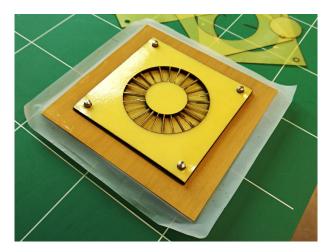




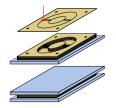












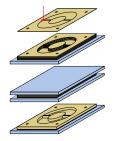






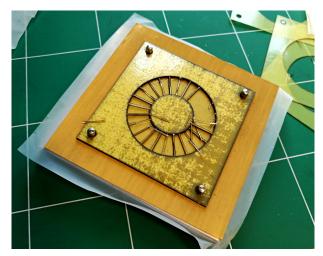




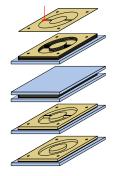




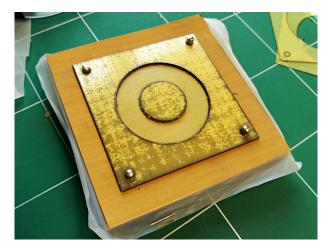




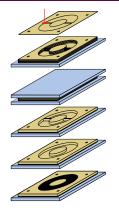










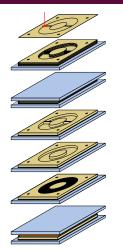












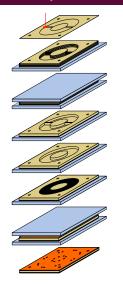




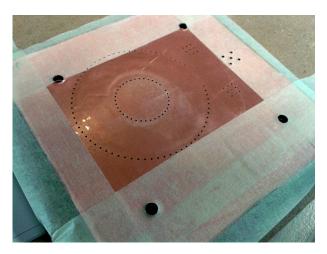




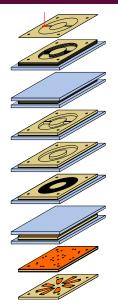




















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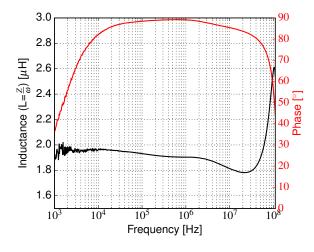








Electrical measurements



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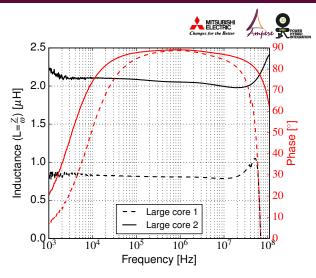
"Small core"

- Intern. Dia. 6 mm
- Outer Dia. 19 mm
- \approx 1.4 mm thick
- 16 Turns
- MnZn ferrite
- → μ_r = 28





Electrical measurements

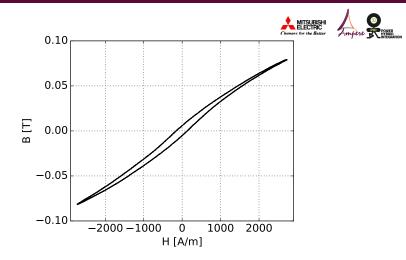


"Large" cores

- Intern. Dia. 25 mm
- Outer Dia. 50 mm
- $\blacktriangleright~\approx$ 1.4 mm thick
- 22 Turns
- MnZn ferrite
- $\rightarrow \mu_r = 9 \text{ or } 24$



Electrical measurements – 2

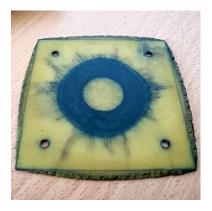


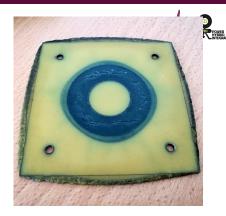
Measured at 100 Hz, power limited by test setup





Powder residues





Recto

VOLE DÉVELOPPEMENT /-MICTONEWS

Verso

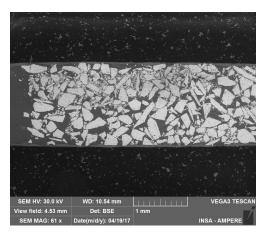
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- Powder residues remain despite cleaning (brush) before lamination
- Powder used contains large (500 μ m) but also much smaller particles
- Dark grey ring caused by laser cutting, not ferrite.





- Clean limit of ferrite area
- Measured density 3.36 g/cm³
 - Consistent with datasheet
- Good penetration of resin
 - No voids
- Particle distrib. not uniform
 - Small particles segregated
 - Might be due to tapping

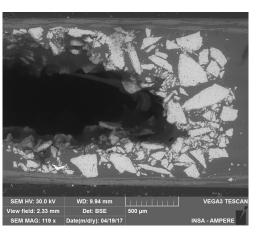






Microsections - 2





Often poor penetration of resin

- "Dry" areas
- Particles fall during cut-off
- Might be due to:
 - Trapped air
 - Process control
 - Resin flowing outwards





- μ_B up to 28, vs. 7.2 to 17 reported in literature for "ferrite in polymer"
- $\blacktriangleright\,$ Distributed airgap \approx 3.5 to 4 %
- Need for proper measurement of losses
 - Used powder not intended for power applications (Ferroxcube FMS250)

- Ferrite residues due to small particles ("dust")
- High particles density achieved
- Issues with resin infiltration
- Process relies on many pre-preg sheets





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Manufacturing process:

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Conclusion













New embedding solution for magnetics

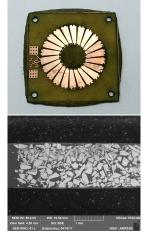
- Suited to many core shapes
- Better than existing "ferrite in polymer"

Presentation of manufacturing process

► All details in the paper (if any missing, please contact me)

Scale-up would require:

- Better powder (controlled granulometry and dispensing)
- Design rules (max ferrite volume, etc.)
- ► The availability of thick prepreg sheets (≈ 1 mm)
- Reliability testing









- M. Ali, E. Labouré, F. Costa, and B. Revol, "Design of a hybrid integrated emc filter for a dc–dc power converter," *IEEE Transactions on Power Electronics*, vol. 27, no. 11, pp. 4380–4390, 2012.
 - R. Perrin, B. Allard, C. Buttay, N. Quentin, W. Zhang, R. Burgos, D. Boroyevich, P. Preciat, and D. Martineau, "2 MHz high-density integrated power supply for gate driver in high-temperature applications," in *Applied Power Electronics Conference and Exposition (APEC)*, (Long Beach, United States), Mar. 2016.
 - C. Marxgut, J. Muhlethaler, F. Krismer, and J. W. Kolar, "Multiobjective optimization of ultraflat magnetic components with pcb-integrated core," *IEEE Transactions on Power Electronics*, vol. 28, no. 7, pp. 3591–3602, 2013.

E. Waffenschmidt, B. Ackermann, and J. A. Ferreira, "Design Method and Material Technologies for Passives in Printed Circuit Board Embedded Circuits," *IEEE Transactions on Power Electronics*, vol. 20, pp. 576–584, May 2005.

D. H. Bang and J. Y. Park, "Ni-zn ferrite screen printed power inductors for compact dc-dc power converter applications," *IEEE Transactions on Magnetics*, vol. 45, pp. 2762–2765, June 2009.





Thank you for your attention

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