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A filter-based computational homogenization method for handling non-separated scales problems

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Résumé — In this work, a computational homogenization framework based on filters is proposed to handle homogenization with arbitrary scale separation. Classical homogenization is extended by using low-pass filters instead of averaging operators, leading to a naturally nonlocal elastic framework, where the kernel function is fully constructed by means of computations on a unit cell describing the microstructure. An associated Finite Element Framework is proposed to deal with heterogeneous structures containing inclusions with characteristic length of the same order than loading fluctuation wavelength. **Mots clés** — Homogenization, Non-separated scales, Filter-based homogenization.

1 Introduction

Classical homogenization assumes separation of scales. This assumption is only valid when the characteristic fluctuation wavelength of an applied strain field over a given microstructure is supposed to be large compared with the scale of the microstructure. Otherwise, the scales are considered as *nonseparated* and the overall effective behavior at a given point depends on the strain states at other points in the neighborhood, defining a nonlocal effective behavior. Several families of methodologies have been proposed to handle lack of scale separation [1, 2, 3, 4]. The objective of this work is to provide a new computational homogenization method able to handle arbitrary scale separation.

2 Mesoscopic description of mechanical fields by numerical filters

In [5, 6], a framework for homogenization able to handle arbitrary scale separation has been proposed by replacing averaging operators by numerical filters (Gaussian, or least-square-based).

First, we define two scales, one scale associated to fine scale strain and stress fields $\varepsilon(\mathbf{x})$ and $\sigma(\mathbf{x})$, and another (upper) scale called "Mesoscale", associated to strain and stress fields denoted by $\hat{\varepsilon}(\mathbf{x})$ and $\hat{\sigma}(\mathbf{x})$, respectively, and called "Mesoscopic" strain and stress fields. These fields are related to each other through the following relations :

$$\hat{\boldsymbol{\varepsilon}}(\mathbf{x}) = \mathcal{F}(\boldsymbol{\varepsilon}(\mathbf{x})), \quad \hat{\boldsymbol{\sigma}}(\mathbf{x}) = \mathcal{F}(\boldsymbol{\sigma}(\mathbf{x})),$$
(1)

where $\mathcal{F}(.)$ is a linear operator, acting as a low-pass filter on the fine scale fluctuations. Associating \mathcal{F} with a characteristic length *h* related to the fluctuations observation at the mesoscale, the following properties are assumed for \mathcal{F} :

$$\lim_{h \to 0} \mathcal{F}^{h}(\varepsilon(\mathbf{x})) = \varepsilon(\mathbf{x}), \quad \lim_{h \to \infty} \mathcal{F}^{h}(\varepsilon(\mathbf{x})) = \langle \varepsilon(\mathbf{x}) \rangle.$$
(2)

In [6], we introduced a least-square-based filter in the form :

$$\mathcal{F}(\mathbf{\hat{\epsilon}}_{ij}(\mathbf{x})) = \sum_{p=1}^{P} M^{p}(\mathbf{x})\hat{\mathbf{\hat{\epsilon}}}_{ij}^{p},$$
(3)

where $M^p(\mathbf{x})$ are piece-wise polynomial basis functions (e.g. finite element shape functions) and $\hat{\mathbf{\epsilon}}_{ij}^p$ are coefficients, interpreted as the nodal values of the mesoscopic strain field at some nodes of a coarse grid

associated with the mesoscopic mesh (see [6] for more details), for each component ij. These values are assumed associated with a compatible mesoscopic strain field.

Given the fine scale strain field $\varepsilon(\mathbf{x})$ on a discrete fine mesh composed of *N* nodes \mathbf{x}^m , m = 1, ..., N, the unknown coefficients $\hat{\varepsilon}_{ii}^p$ are found by minimizing the following functional :

$$U = \sum_{m=1}^{N} \left(\sum_{p=1}^{P} M^{p}(\mathbf{x}^{m}) \hat{\mathbf{\varepsilon}}_{ij}^{p} - \mathbf{\varepsilon}_{ij}(\mathbf{x}^{m}) \right)^{2}.$$
 (4)

Following [5], we then introduce the following split of microscopic strain into a filtered (mesoscopic) part and a remaining fluctuation $\tilde{\epsilon}(\mathbf{x})$:

$$\boldsymbol{\varepsilon}(\mathbf{x}) = \hat{\boldsymbol{\varepsilon}}(\mathbf{x}) + \tilde{\boldsymbol{\varepsilon}}(\mathbf{x}). \tag{5}$$

Let us consider a unit cell characterizing the microstructure defined in a domain $\Omega \in \mathbb{R}^D$, *D* being the dimension of the space, with boundary $\partial \Omega$. We define the following localization problem on the unit cell for non-separated scales : assuming known an applied (non-constant) mesoscopic strain field $\hat{\epsilon}(\mathbf{x})$, find $\epsilon(\mathbf{x})$ satisfying :

$$\nabla \cdot (\mathbf{\sigma}(\mathbf{x})) = 0 \text{ in } \Omega \tag{6}$$

and

$$\mathcal{F}(\mathbf{\epsilon}(\mathbf{x})) = \hat{\mathbf{\epsilon}}(\mathbf{x}) \text{ in } \Omega$$
 (7)

with

$$\sigma(\mathbf{x}) = \mathbb{C}(\mathbf{x}) : \varepsilon(\mathbf{x}) \tag{8}$$

where $\mathbb{C}(\mathbf{x})$ is a fourth-order elasticity tensor. Condition (7) is an extension of the classical averaging condition of homogenization in the case of separated scales. It can be interpreted as follows : the filtered part of the compatible strain field satisfying (6)-(8) must match $\hat{\epsilon}(\mathbf{x}) \forall \mathbf{x} \in \Omega$. An iterative scheme has been proposed in [6] to enforce this condition.

3 Mesoscopic homogenized model

In this framework, we have shown in [5] that the constitutive law at the meso scale is given by :

$$\hat{\sigma}(\mathbf{x}) = \int_{\Omega} \hat{\mathbb{C}}(\mathbf{x}, \mathbf{y}) : \hat{\varepsilon}(\mathbf{y}) d\mathbf{y}, \quad \hat{\mathbb{C}}(\mathbf{x}, \mathbf{y}) = \mathcal{F}\left\{\mathbb{C}(\mathbf{x}) : \hat{\mathbb{A}}(\mathbf{x}, \mathbf{y})\right\},$$
(9)

where $\hat{\mathbb{C}}(\mathbf{x}, \mathbf{y})$ is a nonlocal elastic tensor defined in Ω . Note that the constitutive law (9) is general for linear filter operators satisfying conditions (2), and then remains valid when \mathcal{F} is chosen e.g. as a Gaussian filter. Another remark is that in contrast to classical nonlocal elasticity [1], the present nonlocal elasticity operator *does not have translational invariance*, i.e. $\hat{\mathbb{C}}(\mathbf{x}, \mathbf{y}) \neq \hat{\mathbb{C}}(\mathbf{x} - \mathbf{y})$. This constitutes a key feature of the the model to continuously define mesoscopic constitutive laws for arbitrary scale separation.

A discrete framework can be formulated as follows. Using (3), we define $\hat{\epsilon}(\mathbf{x})$ in the form

$$\hat{\mathbf{\epsilon}}_{ij}(\mathbf{x}) \simeq \sum_{p} M^{p}(\mathbf{x}) \hat{\mathbf{\epsilon}}_{ij}^{p}$$
(10)

where the nodal values $\hat{\varepsilon}_{ij}^p$ are defined on a coarse grid discretizing the structure at the mesoscopic scale and M^p are interpolations functions. Using the filter operator \mathcal{F} defined by (3), we obtain the following relationships :

$$\hat{\boldsymbol{\sigma}}(\mathbf{x}) = \sum_{p} \hat{\mathbb{C}}^{p}(\mathbf{x}) : \hat{\boldsymbol{\varepsilon}}^{p}, \quad \hat{\mathbb{C}}^{p}(\mathbf{x}) = \mathcal{F}\left\{\mathbb{C}(\mathbf{x}) : \hat{\mathbb{A}}^{p}(\mathbf{x})\right\},$$
(11)

and

$$\hat{\mathbb{A}}^{p}(\mathbf{x}) = M^{p}(\mathbf{x})\mathbb{I} + \Psi^{p}(\mathbf{x}) - \mathcal{F}\left(\Psi^{p}(\mathbf{x})\right),$$
(12)

where $\Psi^{p}(\mathbf{x})$ are transformation tensors associated to each node p of the coarse mesh on the unit cell, defined by :

$$\Psi_{ijkl}^{p}(\mathbf{x}) = e_{ij}^{p,(kl)}(\mathbf{x}),\tag{13}$$

where $e^{p,(kl)}$ is the strain solution field obtained by solving on the unit cell an elementary problem (see details in [6]) and where $\chi^{p,(kl)}(\mathbf{x})$ is a non-uniform eigenstrain prescribed over the support of $M^p(\mathbf{x})$ and defined as

$$\chi^{p,(kl)}(\mathbf{x}) = \frac{M^p(\mathbf{x})}{2} \left(\mathbf{v}_k \otimes \mathbf{v}_l + \mathbf{v}_l \otimes \mathbf{v}_k \right)$$
(14)

where \mathbf{v}_i are the base vectors of a Cartesian coordinate system. Then the local strain field can be relocalized by the relationship :

$$\boldsymbol{\varepsilon}(\mathbf{x}) = \sum_{p} \hat{\mathbb{A}}^{p}(\mathbf{x}) \hat{\boldsymbol{\varepsilon}}^{p}.$$
(15)

4 Numerical examples

The methodology is illustrated in the following example. A heterogeneous structure, as depicted in Figure 1 (b), is subjected to 4 points bending. The unit cell described in Fig. 1 (a) is used to compute the nonlocal constitutive operators described in section 3. Results in Figures 2 and 3 show that the proposed method allows reproducing both the simplified model (mesoscopic model) computed on a coarse grid, but also provides a good approximation for local fields, which can be obtained by post-treatment through localization rule (15). We also show the limits of classical homogenization methods and extended versions, in such situations when scales cannot be separated.

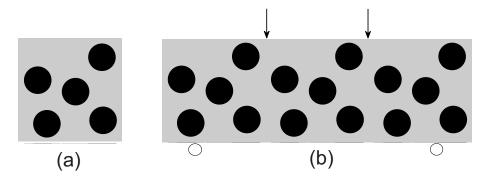


FIGURE 1 - (a) Unit cell; (b) heterogeneous structure subjected to 4 points bending.

Références

- [1] A.C. Eringen, D.G.B. Edelen. *On nonlocal elasticity*, International Journal of Engineering Science, 10:233-243, 1972.
- [2] V. Kouznetsova, M.G.D. Geers, W.A.M. Brekelmans. Multi-scale second-order computational homogenization of multi-phase materials : a nested finite element solution strategy, Computer Methods in Applied Mechancs and Engineering, 193 :5525-5550, 2004.
- [3] S. Forest, K. Sab. *Cosserat overall modelling of heterogeneous materials*, Mechanics Research Communications, 25(4):449-454, 1998.
- [4] T.-H. Tran, V. Monchiet, G. Bonnet. A micromechanics-based approach for the derivation of constitutive elastic coefficients of strain-gradient media, International Journal of Solids and Structures, 49:783-792, 2012.
- [5] J. Yvonnet, G. Bonnet. A consistent nonlocal scheme based on filters for the homogenization of heterogeneous linear materials with non-separated scales, International Journal of Solids and Structures, 51:196-209, 2014.
- [6] J. Yvonnet, G. Bonnet. Nonlocal/coarse graining homogenization of linear elastic media with non-separated scales using least-square polynomial filters, International Journal for Multiscale Computational Engineering, 12(5):375-395, 2014.

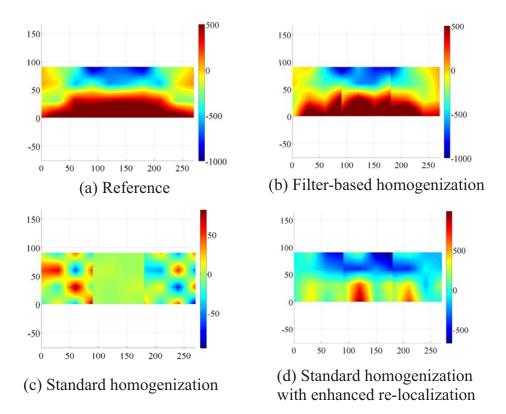


FIGURE 2 – Stress fields obtained at the mesoscopic scale (on the coarse grid) : comparisons between several models.

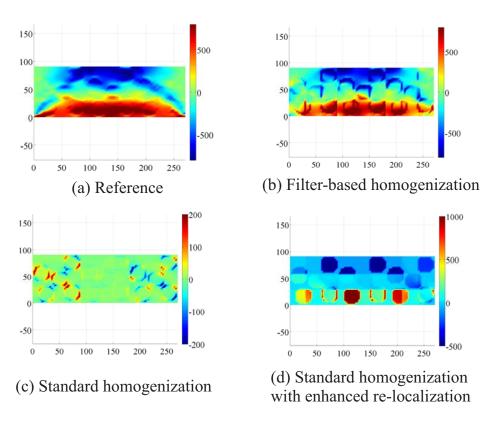


FIGURE 3 – Stress fields obtained at the microscopic scale (on the finest grid) : comparisons between several models.