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Doppler LIDAR Developments for Aeronautics

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Detecting atmospheric hazards such as wake vortices, turbulences, wind shear or wind gusts would improve flight and airport traffic safety. Moreover, to face the current and future challenges of air traffic growth in terms of environment, safety and costs, one of the major challenges is to increase runway throughput by optimizing the distance separation between aircraft. These are some of the issues, among others, addressed by Doppler LIDARs. This powerful technique can provide remote air speed data and is being deployed on the ground or in flight.

The paper presents some of the recent Doppler LIDAR developments at ONERA. Some insight into state-of-the-art technology is provided, as well as perspectives for future applications in aeronautics.

Introduction

Aeronautics being the science of navigation in the air, measuring air motion remotely from a ground station or from an aircraft is therefore a major issue. In the vicinity of an airport, for instance, wind mapping may allow dangerous gusts and wind shears to be detected. Above airport runways, detecting and tracing wake vortices generated by aircraft landing and taking off can increase flight safety and optimize airport operation. From an aircraft, remote wind measurement can provide information about the dynamic state of the atmosphere that the aircraft is about to fly into. This can enable the cross-checking of classical Pitot tube measurements and improve flight security. Long-range wind measurement ahead of an aircraft could also allow severe clear-air turbulence events to be mitigated or avoided.

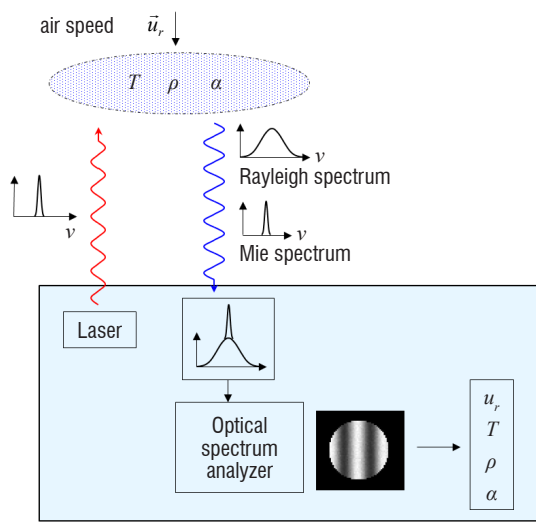
LIDAR (Light Detection and Ranging) are ideal tools for remote wind measurements. LIDARs emit beams of monochromatic light toward the desired measurement area in the atmosphere. Photons are scattered along the beam by dust particles (Mie scattering) and molecules (Rayleigh scattering) contained in the air. A very small fraction of light is 180°-backscattered toward the laser emitter, beside which a receiver is placed. Particles (and molecules) are so light that their movement perfectly follows air motion and they can be used as air speed tracers. Due to the air mass motion relative to the LIDAR emitter/receiver, backscattered light collected by the receiver is frequency-shifted by the Doppler effect by a quantity

$\Delta f = 2V_R / \lambda$, where V_R is the so-called radial wind speed (speed projected on the laser line of sight) and λ is the laser wavelength. Doppler LIDARs analyze the frequency of the backscattered signal to obtain the air speed.

This paper deals with wind LIDAR developments at ONERA for aeronautics applications. Most developments imply Doppler LIDARs, except for long-range clear air turbulence detection. In a first part, we focus briefly on high-altitude wind speed measurements. Such applications have a high potential for in-flight aeronautics, but technological issues make these developments very challenging. In a second part, we present Coherent Doppler LIDAR, which is the mainstream technology for wind speed measurement from a ground station or from low and medium altitude aircraft.

Direct Detection Doppler LIDAR

At high altitude, since particles are sparsely distributed above the atmosphere boundary layer, a LIDAR detects the signal backscattered by air molecules. The analysis is performed in the optical domain and the LIDAR is called "direct-detection" Doppler LIDAR. The spectrally broad Rayleigh-Brillouin molecular backscatter involves a receiving channel based on an optical spectral filter and a detector, which obtains the amplitude or the shift of the spectrum by flux or



Detected spectrum properties

- Central frequency (Doppler effect) \rightarrow air speed u_r
- Rayleigh broadening \rightarrow temperature T
- Rayleigh signal energy \rightarrow air density ρ
- Mie signal energy \rightarrow mixing ratio α

Figure 1 – Direct detection Rayleigh-Mie LIDAR principle

fringe pattern analysis (see Figure 1). Such systems generally require medium linewidth (<1 GHz) monomode lasers emitting at small wavelengths (UV or visible), since the backscattered signal decreases as λ^4 (λ being the LIDAR wavelength) [13].

For atmospheric science applications, Direct Detection Doppler LIDARs are used for studies in connection with climate issues, for example, aerosol transport characterization and stratosphere/troposphere mixing layer observations. Such LIDARs have long been developed by atmosphere science laboratories such as LATMOS, which was a pioneer of the technology in France (see for example [6][16][22]). Ground-based direct Detection Doppler LIDARs for high-altitude observations require high-power laser (>100 mJ/pulse), large telescopes (~ 1 m). In France these systems are installed at the *Observatoire de Haute-Provence* and the *Observatoire du Maïdo* (Reunion Island). These high-performance tools will soon be supplemented by a space-based Direct Detection Doppler LIDAR called ALADIN (Atmospheric Laser Doppler Instrument). ALADIN is the LIDAR payload of the ADM-Aeolus mission, a program launched 15 years ago by ESA. It will provide direct measurements of global wind fields from space. The purpose of the mission is to demonstrate improvements in numerical weather prediction and climate models. The LIDAR operates in the UV (355 nm) [45]. The optical receiver combines a "Mie" channel (Fizeau interferometer analyzing winds from low-altitude aerosols and clouds) and a "Rayleigh" channel (double edge Fabry-Perot interferometer analyzing air molecules). The system is currently being qualified and should be launched in 2017.

In the field of aeronautics, airborne Direct Detection Doppler LIDARs are tested to evaluate the possibility of short-range turbulence detection and mitigation. ONERA has built a short-range ground prototype demonstrating the feasibility of robust and daytime measurements with a Michelson fringe-imaging technique for Doppler analysis [14]. Similar developments have been made and promoted until their demonstration in flight throughout the EU project AWIATOR [48] [56], which used the Fabry-Perot fringe-imaging technique.

Another strong concern calling for Direct Detection LIDARs in aeronautics is the long-range detection of clear air turbulences (CAT). Aircraft experience turbulence when they encounter a vertical airflow that varies on the horizontal length scales in the range of 30 m to 2 km for large commercial aircraft. Vertical airflow on these scales is associated with two distinct physical mechanisms: wave breaking caused by shear instabilities in clear air (Kelvin-Helmholtz instability) and convective updraughts and downdraughts in and around clouds and thunder storms. Clear-air turbulences are difficult to observe because of their relatively low occurrence. The physical phenomenon has been, up to now, poorly understood and they are not well predicted. ONERA has been involved in two projects aimed at collecting and analyzing turbulence data: the MMEDTAC project [27] aimed at acquiring turbulence data with the LATMOS ground-based Rayleigh LIDAR located at the *Observatoire de Haute-Provence*. The DELICAT project involved a Rayleigh LIDAR assembled by the DLR/IPA, installed on board the NLR Citation aircraft for in-flight data acquisition [36]. Both of these projects were based on measuring the density fluctuations that are linked to strong vertical winds in atmospheric layers with high stability, rather than measuring the wind speed itself. It must be noted that, with this method, the atmosphere stability characterized by the Brunt-Väisälä frequency is assumed to be constant at the scale of measurement. The principle is to measure the amplitude fluctuations of the LIDAR signal due to a fluctuation in the molecule contribution to the backscattered signal. Particle contribution must thus be rejected, to avoid interference and spurious detections. Flying the system onboard adds extra complexity, since an agile filter is required to remove Mie scattering that is Doppler shifted by the varying aircraft speed. Particle signal rejection was performed by an optical filter based on polarization separation, which assumes that at the flight test altitude (30,000ft) particles are essentially polarizing ice crystals and ashes. CAT detection was considered to be positive only in areas with a low-level particle signal. The estimation of relative fluctuations of the backscatter signal is assumed to not be modified in the presence of low-level particle scattering due to a well-mixed aerosol layer, the ratio between aerosol and molecular backscattering remaining constant inside this layer. Although it was not possible to ensure that the atmosphere was totally free from aerosols, both projects enabled likely CAT data to be collected. New algorithms performing CAT retrieval have been developed for these two systems and will be used for future work on CAT characterization [28].

Rayleigh LIDAR involves cumbersome lasers and optics and complex key technology (e.g., agile filters), which explains why the technique is still at the level of demonstration for airborne sensors. Technology maturation is necessary to comply with aeronautics size and consumption constrains. However, since it relies on molecule scattering, Rayleigh LIDAR would be a reliable concept for operational sensors to detect atmospheric hazards at any altitude with reasonably easy certification procedures.

High power coherent Doppler LIDAR

Unlike direct detection LIDARs, coherent detection LIDAR rely solely on the presence of particles. Particles are dense in the lower atmosphere, *i.e.*, from the ground up to a few kilometers, especially in the atmospheric boundary layer. At low altitudes, remote sensing of the air speed is also an important issue. Indeed, during landing and take-off, a minimal distance separation between aircraft is

necessary, in order to avoid the risk of encountering the wake vortex from a preceding aircraft. Wake vortices are two coherent counter-rotating flows created behind the aircraft wings and they induce a potentially dangerous rolling moment to the following aircraft. ICAO wake turbulence separation minima defined forty years ago are being redefined, in order to take into account airport traffic increase. Indeed, the strength and lifetime of wake vortices vary a lot with weather conditions. Their dissipation rate varies depending on the atmospheric turbulence level. They can also be transported out of the way towards incoming traffic by cross-winds. Other air disturbances, such as wind gusts or rapid change of the incoming wind direction, are also detrimental to the airport traffic flow. Thus, anticipating these phenomena in the vicinity of airports is key information for air traffic optimization and safety.

Wake vortex locations and trajectories, wind turbulence level or wind maps can be used during certification or flight tests. They can be provided by long range-range resolved Doppler LIDAR or Radar, which measure the wind speed with a high spatial resolution [31][54]. Such sensors have been evaluated for airport safety and re-categorization purposes within the framework of various projects, such as CREDOS, FIDELIO, SESAR or UFO [19][20][55].

Not only airport safety, but also flight tests of new air vehicles, manned or unmanned, could benefit from accurate knowledge of air dynamics disturbances in the vicinity of airports. Due to recent progress in fiber lasers and amplifiers, 1.5 μm fiber LIDAR technology is becoming a serious candidate for lightweight, compact, eye-safe airborne systems. Demonstrators have been developed and flight-tested for new avionics or certification aids [3][51].

In this chapter, we review recent LIDAR achievements at ONERA and report on performance and field test results for two types of coherent Doppler LIDARs: ground based range resolved LIDAR and an airborne true air speed sensor.

In coherent detection LIDAR, the spectrally narrow Mie backscatter from aerosols and cloud particles is analyzed via the mixing of the backscattered signal and a reference wave (local oscillator) to produce a radio frequency beat note, which can be temporally analyzed with a standard photodiode. The mixing also enhances the detection sensitivity, thanks to the optical product of the signal beam and the reference beam, and enables very low signal amplification. Compared to the direct detection LIDAR, the receiving channel of the coherent detection LIDAR is much simpler.

Although the technology has been used for decades, over the last ten years a renewed interest has arisen thanks to the availability of fiber components developed for the telecommunication market. Indeed, LIDAR based on fiber technology are low-cost and resilient to vibrating environments. When emitting around 1.5 μm , they can benefit from telecom industry components with a large market at competitive costs and increased reliability. They offer simplified maintenance procedures compared to free-space technology and enable compact system designs. It is thus well suited to on-the-field operation for other domains besides aeronautics, such as defense, security or space [5][9][18].

Range-resolved wind LIDAR

Range resolution can be achieved with frequency modulation (FMCW) or pulsed emission. Whatever the technique, the fiber laser architecture based on a Master Oscillator Fiber Power Amplifier (MOFPA) offers the advantage of versatility: FMCW emission, pulse shape, duration, repetition rate and frequency characteristics can be varied from pulse to pulse at 100s of kHz rates. This unique "smart pulse" feature provides multifunction capability and perspectives for applications, such as pilot aid, with simultaneous ranging and ground velocity measurement or anemometry and velocity, gas detection with multi-wavelength DIAL LIDAR (Differential Absorption LIDAR), simultaneous DIAL-Doppler LIDARs, etc.

A typical coherent fiber LIDAR set up is depicted in Figure 2. The master oscillator is a continuous laser diode. Its output is split using a 50/50 fiber coupler. The transmitter channel goes through an acousto-optic modulator (AOM), which shapes the pulse and eventually sets an intermediate frequency (IF). It is then amplified through a fiber pre-amplification stage and a filter (BPF) and a booster stage. At the output of the booster stage, the beam is polarized, quasi-single mode, and its temporal shape is optimized for efficient coherent detection. A passive fiber pigtail (1) is used to connect to the polarization beam splitter (PBS). The polarization beam splitter enables the transmitter channel and the receiver channel to circulate thanks to a quarter wave plate. Up to the beam splitter, all components are fibered. At that point, for high-peak-power emissions, a Brillouin effect may occur in fibers and free space optics are used (Paragraph 2 elaborates on the Brillouin effect). At the telescope output, the signal beam is emitted into the atmosphere boundary layer. The signal backscattered from natural aerosols is coupled to the fiber-beam splitter pigtail (2) and mixed with the local oscillator using a fiber coupler. The electric signal of the photodetector (DET)

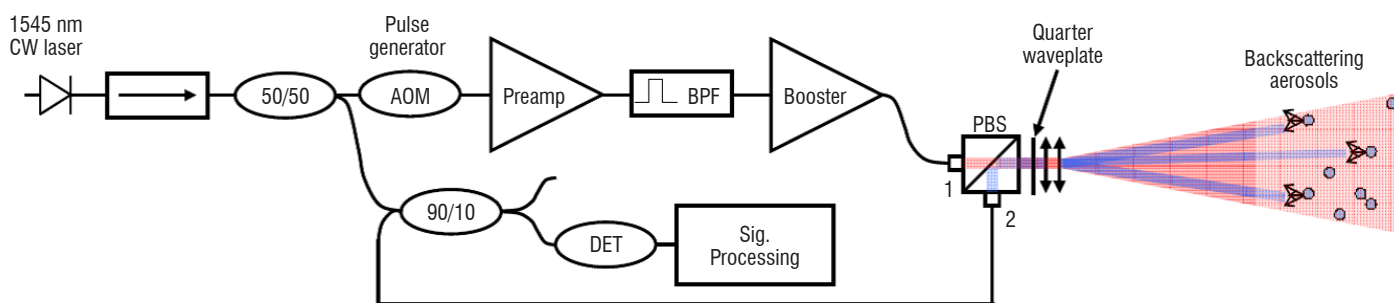


Figure 2 – MOFPA coherent fiber LIDAR setup

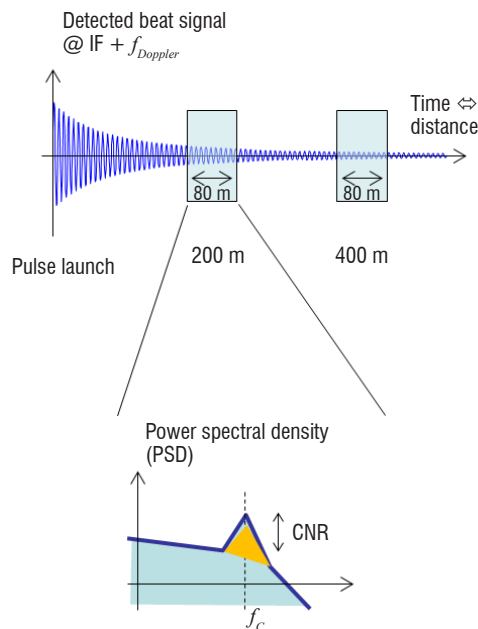


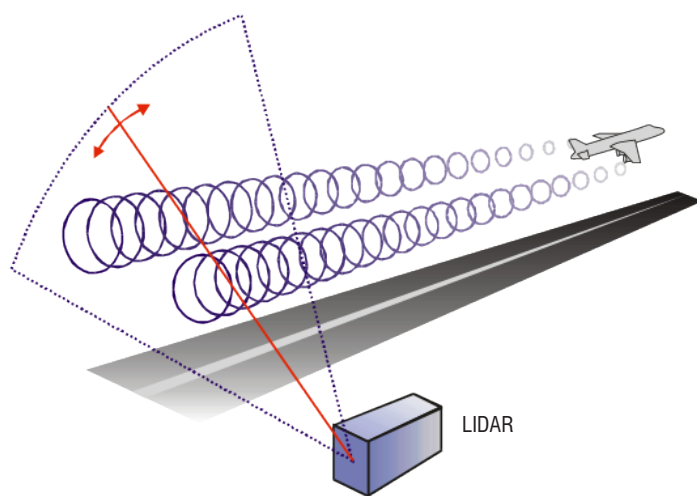
Figure 3 – signal detection

is digitized and processed in real time. The detected signal is split into temporal (or spatial) bins, which are Fourier transformed (see Figure 3). The maximum frequency of the spectrum f_c is estimated with a suitable algorithm (maximum, centroid, etc.). Each bin is thus defined by its spatial coordinates and its central frequency enabling, for example, wind map reconstructions.

Most systems emit at around 1545 nm, which corresponds to high gain in erbium doped fibers and a good atmospheric transmission. The monostatic set-up (single pupil for transmitter and receiver channels) sketched here is convenient for small-size scanning systems.

Wake vortex monitoring

For wake vortex monitoring from the ground, e.g., above runways, measured tangential velocities are high when the LIDAR scanning pattern is in a plane perpendicular to the aircraft path (Figure 4 left). The wake vortex LIDAR signature shown in Figure 4, right, is typical with four patches of positive negative velocities around the vortex



cores. Wake vortex positions can be traced from scan to scan and their trajectory retrieved.

The detailed principle and results achieved at ONERA can be found in [55]. Since 2009, operational use of ONERA technology has occurred thanks to technology transfer to a SME, Leosphere. Commercial LIDARs are deployed for windmill prospection and wind turbine monitoring. They are also operated in a number of airports to analyze wake vortex parameters and their dependency on weather and aircraft characteristics. Improvement of the technology is ongoing jointly at ONERA and Leosphere and progress has been made on the hardware and software. Recent achievements in signal processing are described in the following paragraph.

Signal processing for wake vortex characterization

The main sought features of a wake vortex are its strength, characterized by its circulation, and its position. In the literature, two notable families of algorithms aimed at obtaining these features from the LIDAR velocity spectra can be found. The first one [4] is a non-parametric method, based on extracting the positive and negative velocity envelopes using a spectrum threshold that depends on the Signal-to-Noise ratio (SNR) and the aircraft category, and thus needs to be adapted by the user. In the velocity spectra, every velocity value encountered by the laser pulse in the measurement volume is represented. The maximum (and minimum) velocity is the velocity of the wake vortex's field line tangent to the laser beam. The extrema of each velocity spectrum gives the wake vortex envelope (positive and negative). These envelopes provide the vortex positions (located where the positive envelope has its maximum, and the negative envelope has its minimum). To compute the circulation, various methods are exploitable, such as integrating these envelopes at the range of the vortex core between 5 and 15 meters. In this case, the circulation is called Γ_{5-15} .

The second family gathers the algorithms, making use of estimators such as the maximum likelihood estimation on the spectra from a Wake Vortex analytical model [24], or as the maximum of a correlation function between the radial velocities and a vortex model. A new method based on a hybrid algorithm has been developed during PhD work jointly supervised by ONERA, Leosphere and Supelec [26]. The purpose is to accurately and precisely estimate the circulations

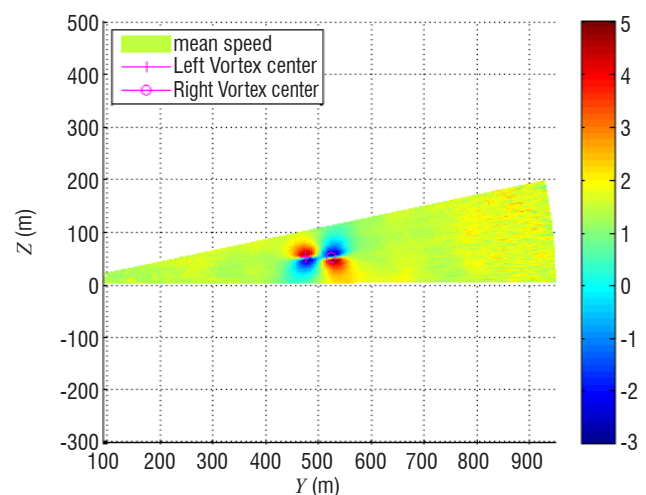


Figure 4 – LIDAR scanning pattern for lateral wake vortex detection, (left) scan pattern for CREDOS and SESAR campaigns; (right) LIDAR measurement and display of average wind field, perturbed by the wake vortex, projected on LIDAR line-of-sight

with a processing time as short as possible, so as to make this algorithm exploitable for operational projects. This is why a method has been set up to evaluate its precision and its robustness. The results of tests on simulated scenarios of different aircraft vortices and different weather conditions show that this algorithm is able to precisely locate wake vortices and to accurately estimate their circulation: the root mean square error is below 5%. In order to model the complex old vortex in the ground effect, large eddy simulations performed by UCL have been used. In this case, the error reaches 20%.

High spectral brilliance all fibered sources and SBS mitigation

The assets of fiber lasers are their high efficiency enabling a wall plug efficiency of 10% to 15%; their size – the volume of a coherent 2 W fiber laser is the size of a thick book – and their reliability due to spliced connectors.

ONERA has developed specific know-how in high-peak power, narrow linewidth pulsed fiber lasers and amplifiers. The additional laser power provides increased coherent LIDAR capability in the range and scanning of large areas, as well as better system resistance to adverse weather conditions.

In order to reach long ranges within a short acquisition time, coherent wind LIDARs require high-power (~kW), narrow-linewidth (few MHz) pulsed laser sources with nearly Fourier transform limited pulse duration (~1 μs). Eyesafe, all-fiber laser sources based on MOPFA (master oscillator, power fiber amplifier) architecture offer many advantages over bulk sources, such as low sensitivity to vibrations, efficiency and versatility. In the MOPFA coherent fiber LIDAR set up shown in Figure 2, the pulses are amplified in a sequence of fiber amplifier stages with increasing pump power and core size, which are separated by isolators and band-pass filters. MOPFA designers seek fibers with low numerical aperture (NA), which is favorable to single-mode guiding and low amplified spontaneous emission (ASE), in order to achieve high system efficiency.

Narrow linewidth pulsed MOPFA are usually limited in peak power by nonlinear effects arising in the fiber, such as Stimulated Brillouin Scattering (SBS) to a few 10s-100s Watts in standard fibers [7]. In standard single-mode fibers, the SBS threshold is reached when the peak power length product reaches about 80 W.m. The high-power density generates acoustic waves in the fiber core, which acts as a grating. The light transmitted by the fiber saturates, and part of this

light is backscattered by the grating. In fiber amplifiers, the backscattered light may be amplified in the active fiber generating high-peak-power backscattered pulses potentially harmful for upstream components [33].

The strength of the Brillouin nonlinearities in a fiber can be quantified by the intensity length product:

$$B = g_B \frac{\int_0^L P(z) dz}{A_{eff}} = \frac{g_B P(L) L_{eff}}{A_{eff}} \quad (1)$$

where g_B is a Brillouin gain, L is the fiber length, A_{eff} is the effective area of the fundamental mode, $P(z)$ is the signal power distribution along the fiber, and L_{eff} is the effective length. For a passive fiber the effective length is equal to the fiber length and for an active fiber the effective length depends on the fiber gain along the fiber [30]. From (1) it appears that there are three ways to act on the nonlinearities.

Increase in the mode area

The first way is to increase the fundamental mode effective area. Large-Mode-Area (LMA) fibers, with a large core diameter and low numerical aperture (NA) may be used to increase the mode area, but the fiber tends to guide higher-order transverse modes degrading the beam quality. A good spatial quality is crucial for many applications. For instance, in a coherent detection LIDAR when the beam quality factor M^2 equals 1.7 we expect the Carrier-to-Noise Ratio (CNR) to decrease by 3 dB [12]. The most efficient doped fibers today are based on the Erbium-Ytterbium codoping of phosphosilicate glasses. This composition has two important limitations. First, the core refractive index is quite large and special pedestal structures are needed to reduce the NA to 0.09 and limit the proportion of higher-order transverse modes. A second limitation is that the core itself is usually inhomogeneous with a central dip in the refractive index profile resulting in a poor beam spatial quality.

To go beyond this core diameter limit, IPHT and ONERA have built 40 μm core diameter multifilament-core fibers (MFC) to amplify high-peak-power pulses [8]. In this technology, the fiber core is replaced by a microstructured core composed of 37 Erbium-Ytterbium doped filaments surrounded by fluorine doped silica (Figure 5). It was shown that this structure behaves as an effective singlemode fiber, since the light only perceives an average index value for the structured core.

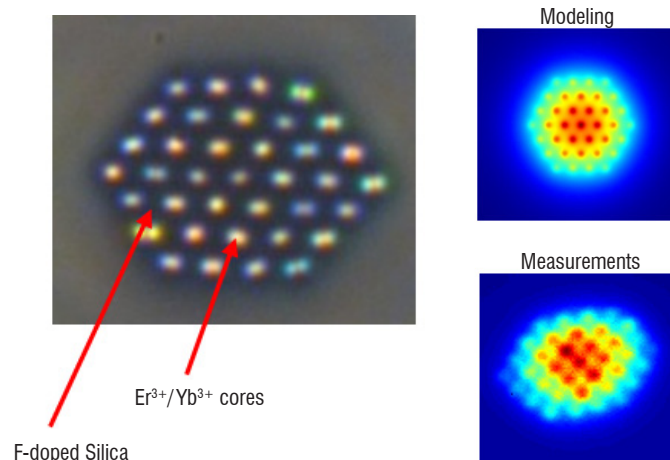
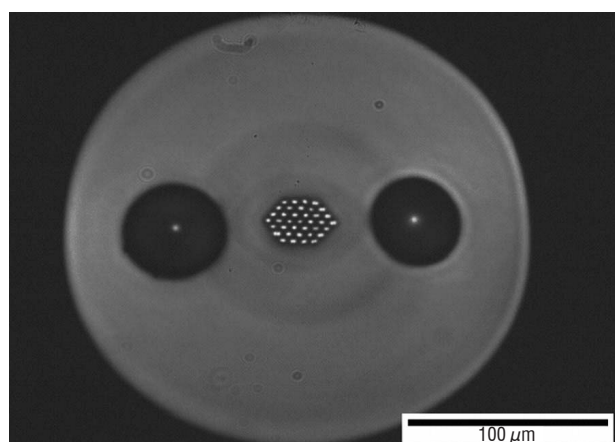


Figure 5 – Left, middle: View of the multifilament core fiber cleave. Right: mode field distribution

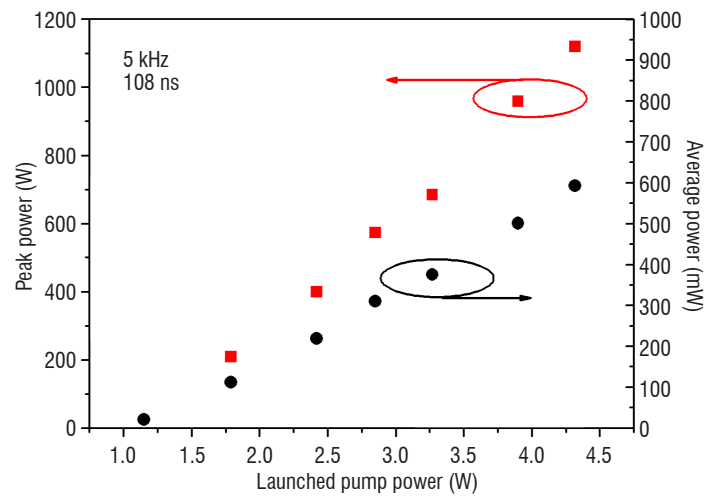
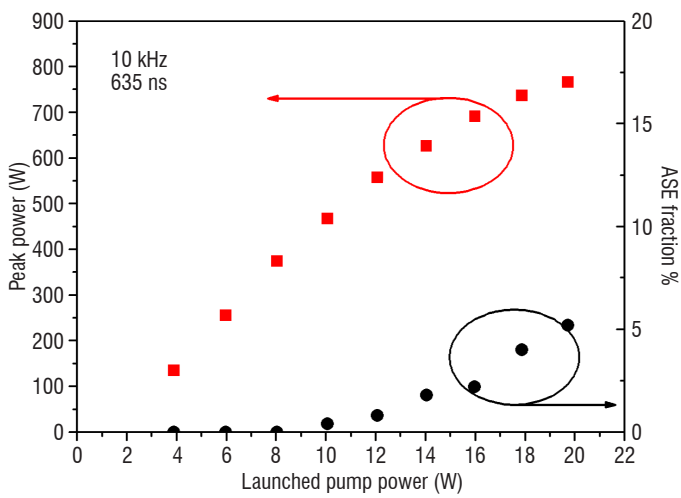


Figure 6 – Pulse peak power with respect to launched pump power in the pulsed setup. Left: pulse duration = 635 ns; PRF = 10 kHz. The ASE fraction in total power is shown on the right axis. Right: pulse duration = 108 ns; PRF = 5 kHz. The average power is shown on the right axis

Pulses with 940 W peak power, 1 μ s duration and 1 MHz laser linewidth were achieved. The beam quality is good with $M^2 \sim 1.3$. However, this laser setup was not all-fiber and MFC fiber fabrication and integration in all-fiber lasers systems are challenging.

Another method to increase the core size while preserving a good beam quality is to change the core composition. We have tested phosphoaluminosilicate glass fibers (PAS). It has been previously demonstrated that the simultaneous codoping with alumina and phosphorous results in the reduction of the refractive index, leading to lower NA cores [2][53]. We have tested a double cladding PAS Erbium-Ytterbium doped fiber with a 30 μ m diameter core with a pedestal and 300 μ m inner cladding. The core NA is 0.09 with respect to the pedestal. This fiber can be highly doped and we managed to make an efficient power amplifier with a short piece of fiber only 2 m long. When the pump power is increased, the pulse peak power increases steadily up to a 770 W peak power corresponding to a 650 ns pulse energy of 450 μ J (Figure 6 left). The ASE fraction in the total output power is 6% at that point, and the slope efficiency is 23%. For 108 ns pulses, the peak power is increased up to the SBS threshold at 1120 W (Figure 6, right). The ASE fraction is then below 1%.

Strain distribution

A second way to decrease the Brillouin effect is to minimize the integral of the power over the fiber length. By definition, this term is also equal to the product of the fiber output power and the effective length L_{eff} . In a standard fiber, the entire fiber length contributes to the Brillouin reflectivity at the same characteristic frequency. A strain gradient applied along the fiber can be used to make each fiber segment contribute to different frequencies and spread the reflected light spectrum [17], thus allowing a higher optical peak power in the fiber before reaching the Brillouin threshold.

We have recently developed a high-power single-frequency all-fiber MOPFA using high reliability passive components and this strain technique. This MOPFA was used in the first experimental demonstration of a fiber laser based wind LIDAR with a range greater than 10 km [46]. We have been able to spread the light reflected by a 25 μ m core fiber resulting in an increase by more than 3 dB in the SBS threshold. Without the strain gradient, SBS limits the pulse peak power to 300 W (200 μ J per 600 ns pulses). The M^2 is measured to be less than 1.3 in both axes. With the strain gradient applied to the doped fiber, peak power up to 630W was achieved (350 μ J per 550 ns pulses) (see Figure 7).

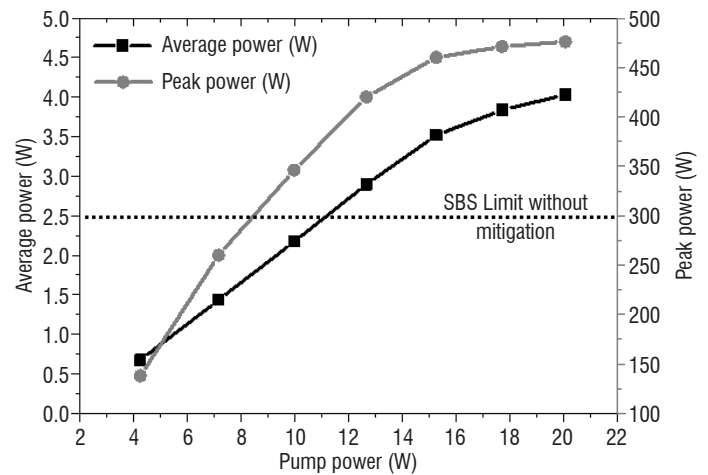


Figure 7 – Changes in the average power and peak power out of the high-power amplifier implementing the fiber straining technique. The dotted line corresponds to the amplifier maximum peak power without strain implementation

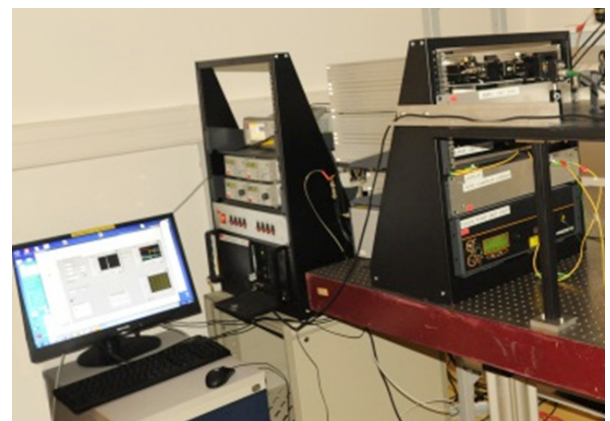


Figure 8 – The fiber laser integrated engineering model of HEPILAS for CO₂ monitoring from space

Since then, this technique has been applied to design HEPILAS, a high power laser emitting at 1579 nm, for space applications (see Figure 8). The aim of this ESA project was to study a proof of concept for monitoring CO₂ from space with a Differential Absorption LIDAR (DIAL) based on an all-fiber laser. 1.7 kW peak power was obtained for 150 ns pulses with excellent beam pointing stability.

A factor of 3 gain was obtained with a modest value of strain, thereby ensuring that the fiber lifetime was compatible with a 5 year duration space mission. The laser was also designed to withstand 10 kRad radiation, thanks to iXfiber radhard active fiber [10].

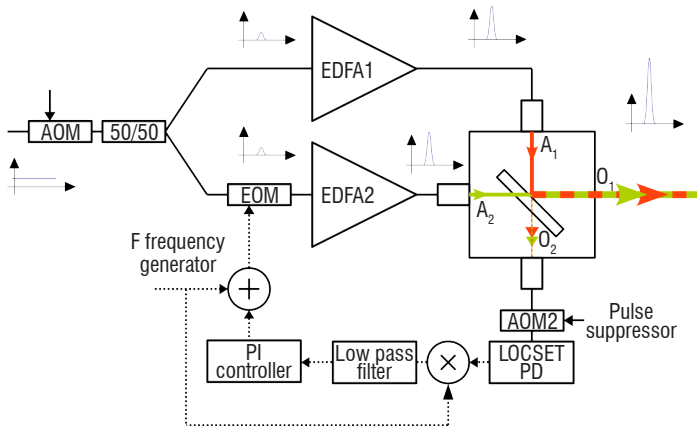


Figure 9 – Coherently combined pulsed amplifier setup. AOM, acousto-optic modulators; EDFA, erbium doped fiber amplifiers; PD, photodiode. The input signal is split into two beams, amplified separately in two EDFAs, combined into output O1, and sent into the atmosphere. A coherent pulse combination at output O1 is maintained through the minimization of output O2 by the LOCSET phase control system [49] modified for pulse operation. A signal leak between the pulses is used for phase measurement. The pulse suppressor before LOCSET PD is necessary to avoid the PD saturation by the high pulse power [35]

Coherent combination

The third strategy to tune equation (1) is to coherently add up the energy emitted by several fibers limited by SBS, while preserving the good beam quality. Coherent Beam Combination (CBC) allows the output power of MOPFA sources to be improved by adding the outputs of single amplifiers. To achieve this, two or more amplifiers seeded by the same pulsed oscillator are coherently combined into a singlemode beam. To achieve high CBC efficiency, the phase differences are compensated using a controller. We have recently demonstrated the CBC of two amplifiers in 100 ns-pulse regime, limited to 95 and 123 W respectively, resulting in a peak power of 208 W [35]. Beam quality and spectral linewidth were maintained. This source has been successfully tested in a LIDAR configuration [37]. The setup of the CBC of two pulse amplifiers is shown in Figure 9.

In particular, we demonstrated that the pulse operation CBC phase controller does not impair the LIDAR performances. Indeed, the source of Figure 9 has been used as a Booster in a LIDAR Setup with 240 ns pulse duration. We have compared the LIDAR performances when running (A) one amplifier at full power, (B) two amplifiers at half power and (C) two amplifiers at full power. The time recorded estimated wind speed is shown in Figure 10. The Power spectral densities (PSD) of each recorded time evolution are reported in Figure 11.

The extracted noise floors (0.21 m/s for Mode A, 0.19 m/s for Mode B and 0.08 m/s for Mode C) show that no performance degradation is

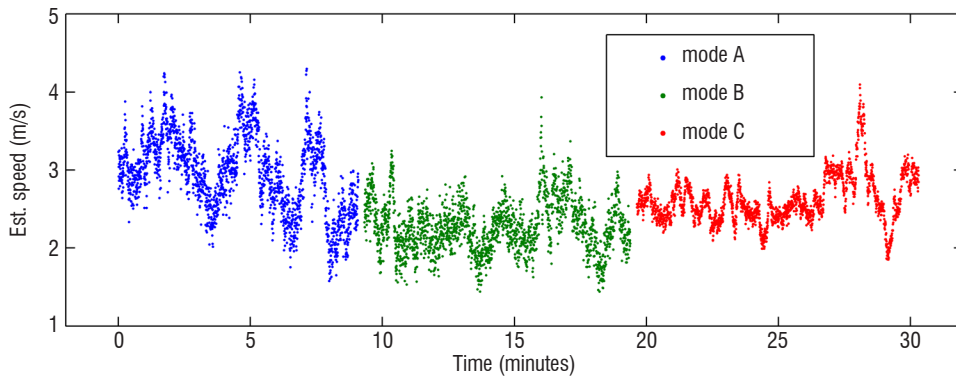


Figure 10 – Estimated wind speed, as recorded by the wind LIDAR in Configurations A, B and C

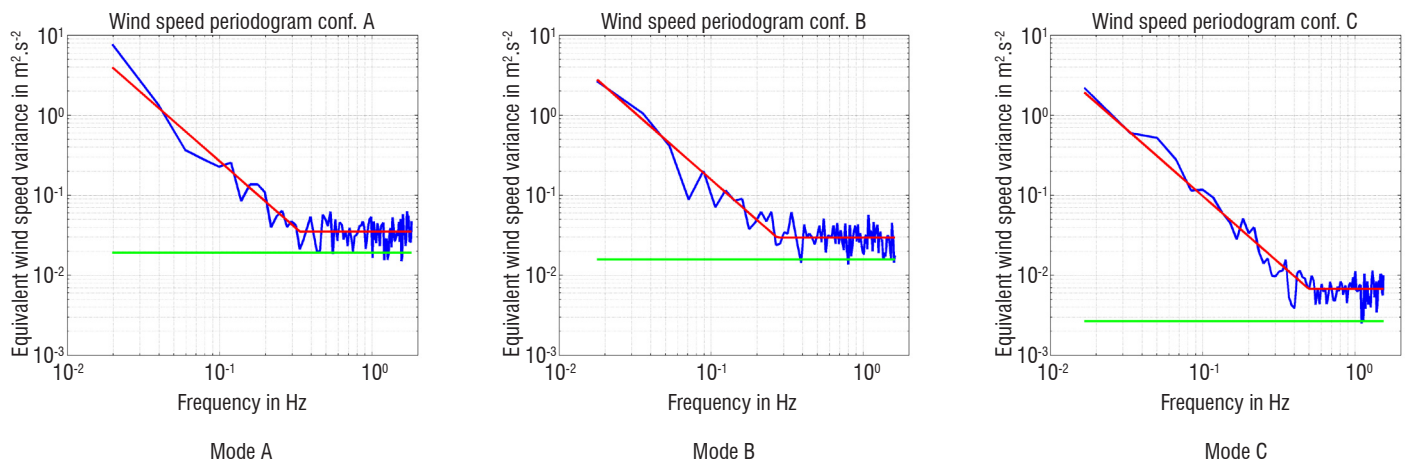


Figure 11 – LIDAR performance comparison at 150m – Instrument noise floor comparison; blue: PSD of estimated wind speed from Figure 8; red (low freq.): $\alpha f^{-5/3}$ Kolmogorov law (α fitted to data); red (high freq.): LIDAR noise floor fitted to data; green: LIDAR theoretical noise floor from estimated CNR (Cramer-Rao bound)

measured when using CBC. When both amplifiers are run at full power, the expected LIDAR performance improvement is reached. In all cases, the LIDAR performance is very close to its optimum value, given by the Cramer-Rao bound. These results show the compatibility of coherent beam combination with coherent wind LIDAR. Potentially, tens to hundreds of those amplifiers can be combined by this technique.

Long-range LIDAR measurements

These novel, high spectral brightness, all-fibered sources have been used in various LIDAR configurations to achieve record ranges and EDR measurements [38]. The ONERA wind LIDAR system LICORNE (shown in Figure 13) is a mobile platform dedicated to field tests of new lasers, components, architecture or signal processing for coherent LIDAR. Sample results are illustrated in Figure 12 in a fixed line-of-sight configuration: the wind-speed spectrogram shows that ranges beyond 15 km are achieved with 0.1 s averaging time.

The CNR and the estimated wind-speed are obtained after averaging frequency spectra over 1024 pulses, corresponding to 0.1 s acquisition time. The CNR map for vertical scan shown in Figure 13 (top left) illustrates the measurement capability inside the boundary layer up to 1200 m, and inside a cloud layer between 1500 and

2000 m. A horizontal scan of Figure 13 (top right) shows the range limit of 11 km.

High-power lasers enable the design of fast scanning LIDARs that are required for long-range wind mapping at airports. During the UFO European project, a 1.5 μm high-power pulsed fiber amplifier was integrated into a Leosphere Windcube 200S[®] (see Figure 14 left). A two-month campaign was performed at Toulouse-Blagnac airport in April to May 2014, in order to assess the LIDAR performances. A variety of other sensors were also deployed (Thales: 2D Electronic Scanning X-Band RADAR, Vertical X-Band RADAR, Leosphere: vertical 1.5 micron Doppler wind profiler) to study a Wake-Vortex Advisory System for weather-dependent distance separation concepts [52].

The scanning LIDAR was configured in order to perform wind and EDR measurements every km along the glide path in less than one minute. A sequence of several horizontal scanning patterns, as illustrated in Figure 14, ensures the theoretical accuracy of wind and EDR retrievals and the fastest update rate possible along the glide path and around the airport. Typical accumulation times of 0.16 s were used per line of sight, in order to allow the measurement range of the Windcube scanning LIDAR up to 10 km.

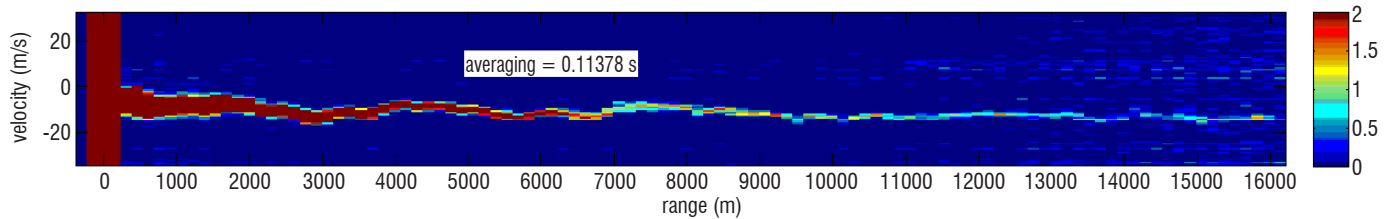


Figure 12 – Wind-speed spectrograms versus range. Color scale is the power spectral density in 0.1 s average time

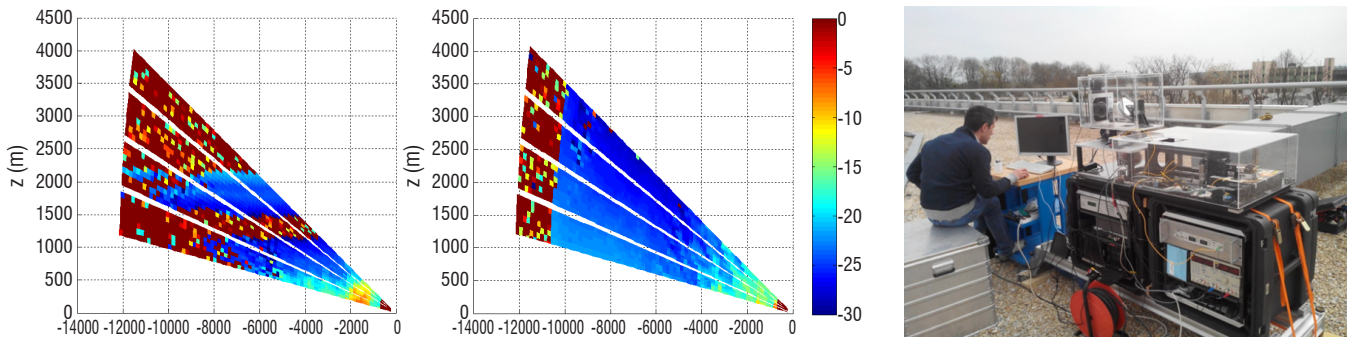


Figure 13 – Measurement in the scanning configuration: left: CNR map for a vertical scan; middle: CNR map for an azimuthal scan; right: ONERA LICORNE LIDAR



Figure 14 – left: ONERA high-power laser installed in the modified Windcube 200S[®]; middle: PPI scan for airport measurements; right: raw-wind data (radial wind speed) collected at Toulouse Blagnac airport. Data range up to 10 to 12 km

Wind mapping

Coherent LIDAR measures the radial velocity of the wind, i.e., its projection along the instantaneous line-of-sight of the LIDAR. For wind monitoring, it is desirable to know the local magnitude and direction of the wind. The Velocity Azimuth Display (VAD) technique is a method that has been used for decades for vertical wind profiling with Doppler radars [34].

The principle is described in Figure 15, where the remote wind sensor performs a vertical conical scan of the atmosphere, assuming a locally homogenous wind. Due to the angular dependence of the wind projection along the measurement axis, the Doppler velocity shift of a homogenous wind follows a sine curve.

The principle of VAD can also be extended for the wind field reconstruction of horizontal scans obtained by a long range wind LIDAR. Under the same assumption of a locally homogenous wind, the regression of a truncated sinusoid can be processed from radial wind data, corresponding to a small area of the LIDAR scan. Components of the wind vector are obtained through an ordinary least-square algorithm, as illustrated in Figure 16.

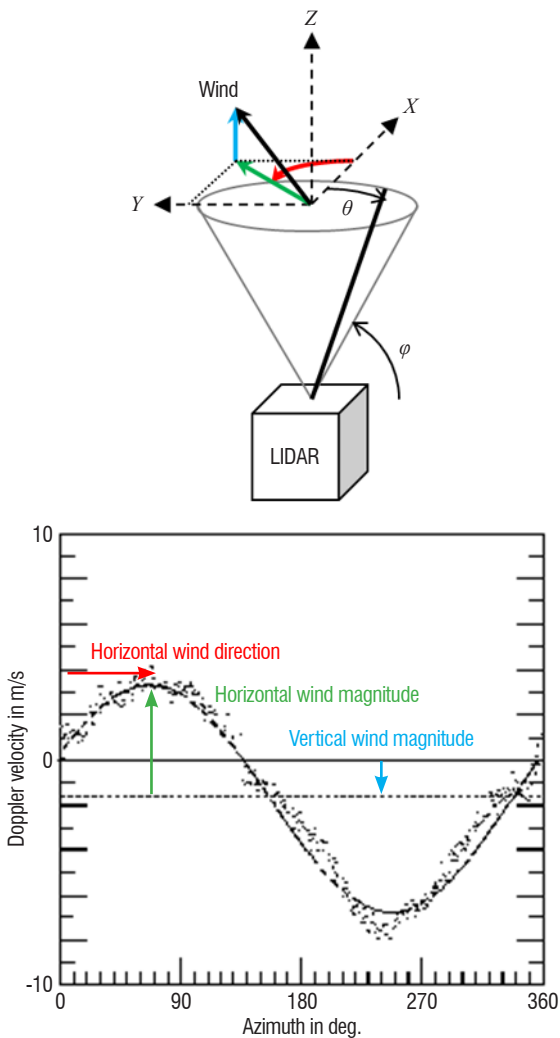
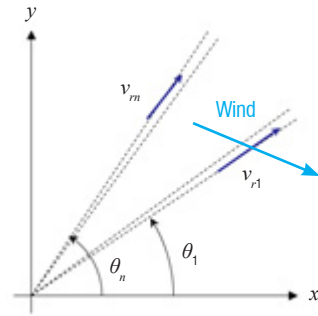


Figure 15 – Velocity Azimuth Display (VAD) principle: The horizontal wind direction is given by the maximum of the sinusoid (red), the horizontal wind magnitude is proportional to the amplitude of the sinusoid (green), and the vertical wind magnitude is proportional to the sinusoid offset (blue). The local vertical component is independent of the scanning angle.



$$\begin{bmatrix} v_{r1} \\ \vdots \\ v_{rn} \end{bmatrix} = M \begin{bmatrix} v_x \\ v_y \end{bmatrix} \quad M = \begin{bmatrix} \cos \theta_1 & \sin \theta_1 \\ \vdots & \vdots \\ \cos \theta_n & \sin \theta_n \end{bmatrix} \cos \phi \quad \begin{bmatrix} \hat{v}_x \\ \hat{v}_y \end{bmatrix} = (M^T M)^{-1} M^T \begin{bmatrix} v_{r1} \\ \vdots \\ v_{rn} \end{bmatrix}$$

Figure 16 – VAD principle applied to wind mapping. ϕ is the elevation angle of the LIDAR axis and θ_i are the azimuth angles

By applying the above to various spatial bins of the LIDAR scan, one can obtain a wind vector map in the x-y plane from radial velocity data, such as that shown in Figure 17. The same principle can be applied with various elevation angles, in order to obtain the 3D wind vector.

In order to evaluate the quality of the wind vector reconstruction, dual LIDAR field tests have been performed. Long-range LICORNE LIDAR has been measured in horizontal scans, while a commercial Leosphere Windcube® profiler measured the wind profile on a vertical directly above the LIDAR, providing data for comparison. Figure 18 shows the experimental set up. The range between the two LIDARs

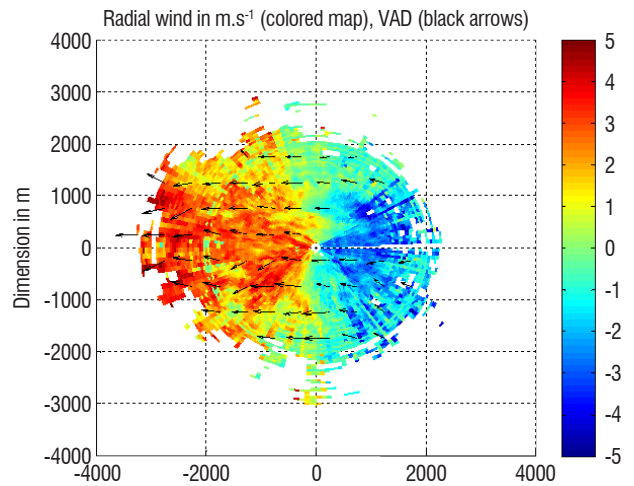


Figure 17 – 2D VAD applied to LICORNE LIDAR data. Black arrows indicate the reconstructed wind vector direction and amplitude

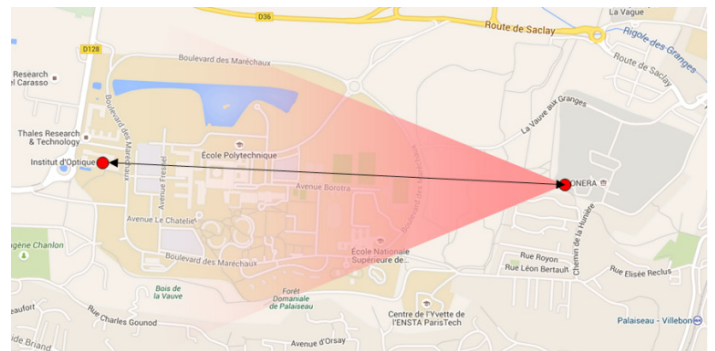


Figure 18 – Experimental set up: location of the profiler (red spot on the left), location of LICORNE (red spot on the right). The pink area is the horizontal scan pattern

was 2100 meters. The LICORNE horizontal scan pattern covered $\pm 15^\circ$. Given the necessary elevation angle of 15° (in order to avoid trees around ONERA), the horizontal scan pattern was 540 meters above the wind profiler location.

The transverse component of the wind located above the Windcube has been reconstructed and both vector data have been compared in magnitude and direction. When the wind is laminar enough, good agreement between both LIDARs is found, as illustrated by Figure 19.

Under turbulent conditions, the wind vector reconstruction is more difficult. However, an interesting feature of the LIDAR is that it can also remotely obtain the state of turbulence of the atmosphere as described in Paragraph "Obtaining the Eddy dissipation rate (EDR)". Under operational conditions, when the scanning LIDAR is used as a stand-alone system, obtaining the EDR is a technique that can thus assess the quality of the wind vector reconstruction.

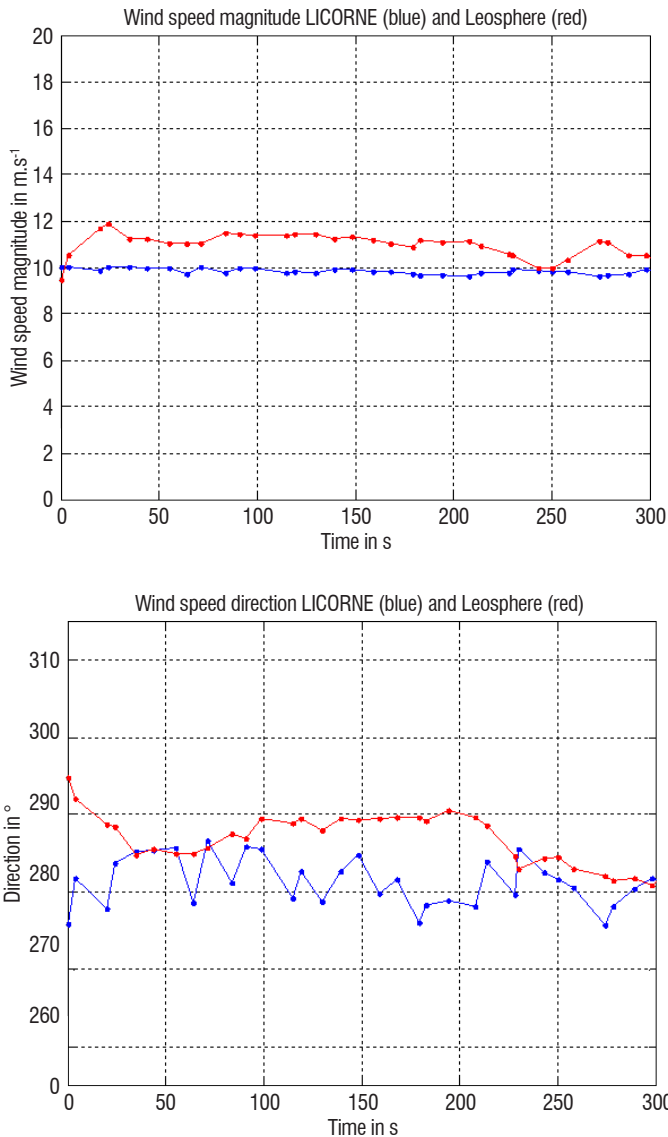


Figure 19 – Example of obtaining the transverse wind component. Top: wind speed magnitude; down: wind speed direction. Blue line: reconstructed from scanning LIDAR LICORNE; red line: measured by the Windcube® profiler

Obtaining the eddy dissipation rate (EDR)

Wake vortex decay will be quicker with high atmospheric turbulence. Theoretical analyses show that the decay time of wake vortices is proportional to the cubic root of the eddy dissipation rate (EDR).

Coherent Doppler LIDAR are commonly used to measure wind fields. They can also provide information about wind field spatial statistics and then yield an estimation of the turbulence Eddy Dissipation Rate. EDR retrieval from LIDAR data remains a relative new topic, especially for addressing operational purposes, such as air traffic applications.

Several authors have performed a review of atmospheric turbulence estimates from Pulsed LIDAR wind measurements [42][47]. Doppler LIDARs can provide information about wind field spatial statistics and then yield an estimation of the turbulence or Eddy Dissipation Rate [4][23][25]. The estimation can be made from the:

- Doppler Spectrum width,
- Velocity Variance or
- Velocity Structure function.

In the spatial domain, the EDR ε appears, for example, in the second order radial velocity structure function $D_v(s)$ defined by:

$$D_v(\bar{s}) = (V(\bar{r}) - V(\bar{r} + \bar{s}))^2 \quad (2)$$

where $V(\bar{r})$ is the radial velocity measured at range \bar{r} from the LIDAR, \bar{s} is a distance and the average is done on a spatial area. The structure function $D_v(\bar{s})$ can be estimated either along the LIDAR axis (the wind longitudinal structure function $D_{LL}(s)$) or along a transverse direction (the wind azimuthal structure function $D_{NN}(s)$). For a scanning LIDAR, the azimuthal structure function $D_{NN}(s)$ method is preferred according to Chan's analysis [15]. This procedure enables a much better resolution than the effective LIDAR range resolution.

Furthermore, there is a direct relationship with the velocity energy spectrum E , leading to the following expression:

$$D_{NN}(s) = C_{NN} \cdot \varepsilon^{2/3} \cdot s^{2/3} \quad (3)$$

where $C_{NN} = \frac{27\Gamma(\frac{1}{3})}{55} \frac{4}{3} C \approx 2.67$ and C is the universal Kolmogorov

constant [40][41]. The EDR value expressed as the cubic root of ε in $m^{2/3}.s^{-1}$ is then obtained by fitting the 2/3 slope of Equation (3) for the structure function D_{NN} obtained from wind data. The estimation of D_{NN} from LIDAR data requires further processing as proposed by Frehlich [25], in order to take into account LIDAR filtering. LIDAR filtering includes the effects of pulse length and signal analysis length.

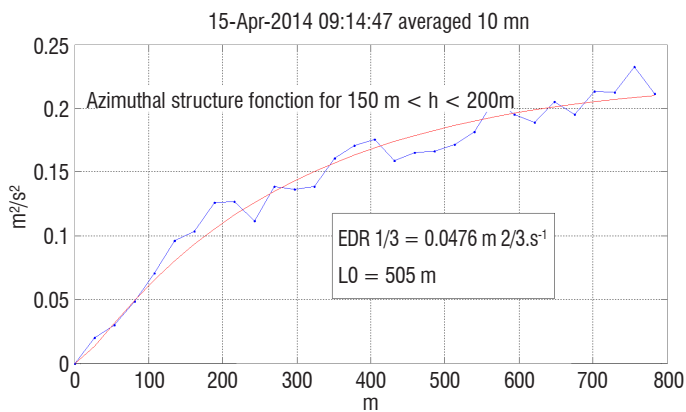


Fig. 20 – EDR measurement: example of a structure function fit for measurement points between 150 and 200 m averaged over 10 min

Figure 20 shows an example of the velocity structure function fit (red) for measurement points (blue) every 50 m in altitude and averaged over 10 min. This EDR value corresponds to quiet air.

Figure 21 shows EDR estimates for 2014, April 24th. The EDR values range from 0.0002 to 0.04 m^2/s^3 , yielding $EDR^{1/3}$ values between 0.06 and 0.35 $m^{2/3}/s$, such values corresponding to moderate to medium turbulence levels.

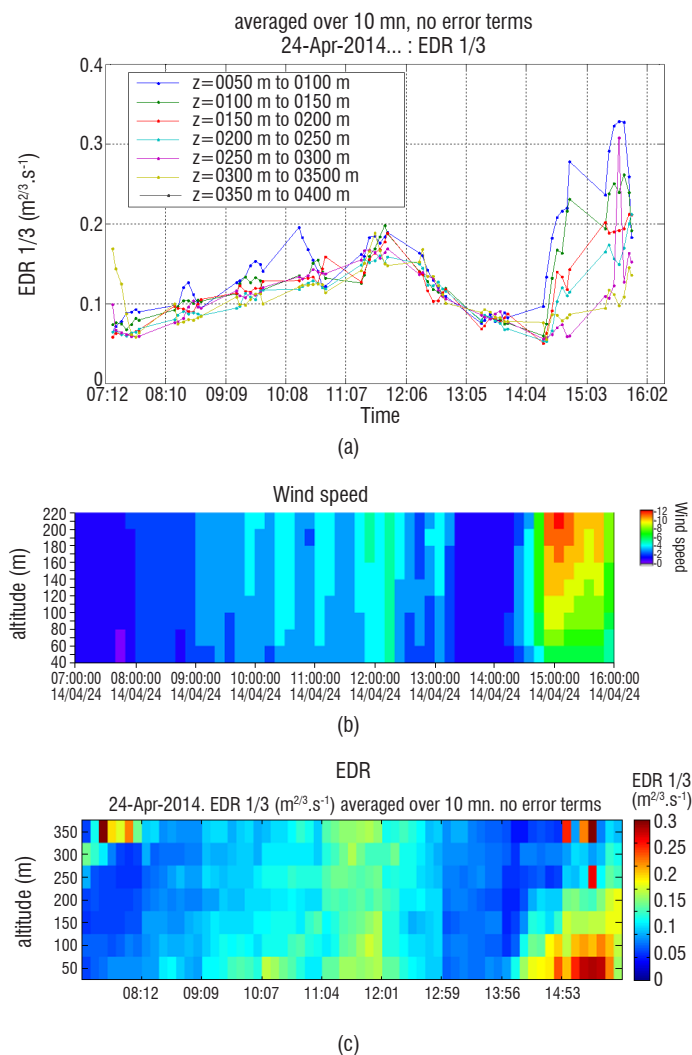


Figure 21 – April 24th, 2014 measurements. (a) EDR as a function of time for different altitudes; evolution of wind speed (b) and EDR (c) in a color scale displayed versus time (horizontal axis) and altitude (vertical axis)

Measurements show a slow increase in the EDR values from 8 to 12 am, then return to calm air at 1:50 pm before the event of a more turbulent period between 2:00 to 4:00 pm. The increase in the EDR in the morning is mainly due to the growth of the convective planetary boundary layer forced by solar radiation, whereas the increase in the afternoon is due to the increase in the horizontal wind speeds. The displays show that high wind speed in the upper layer creates a turbulent layer close to the ground.

These tests demonstrate that wind turbulence characterization is possible over large areas using a range resolved wind LIDAR.

Airborne coherent LIDAR demonstrator

Airborne remote airspeed sensing with coherent LIDAR has a number of applications, such as navigation & pilot aid (e.g., for helicopters), air data system calibration or flight test instrumentation. In addition to size and consumption constraints, reliability in order to reduce maintenance cost is one of the main design drivers for airborne systems. The maturity level for operational systems based on direct detection LIDARs (Paragraph 4) is around TRL2-3, whereas coherent detection LIDAR maturity is around TRL4-5 or higher. For airborne sensors, good laser efficiency is an important feature and is an asset of the fiber technology. Plug efficiencies around 10% are obtained with a continuous fiber laser emitting 5 W at 1.5 μm . Multi-watt fiber airspeed LIDAR demonstrators are being designed and tested throughout the world [1][3][29][51].

Vibration

One of the main assets of fiber technology is its resilience in a shaking environment, which makes the fiber LIDAR an excellent candidate for operation in flight. Demonstrators are tested on the ground in a vibrating environment at ONERA before flight tests. The LIDAR performances are tested on reference Doppler targets and on wind.

In this example, the LIDAR is a new high-power demonstrator built at ONERA/DOTA in 2016, which will be flight tested this year. The LIDAR sensor head is installed on an electromagnetic shaker and aimed at the Doppler target (rotating disk, see Figure 22). The excitation corresponds to the main vibration lines recorded during a strong shake of an aircraft.

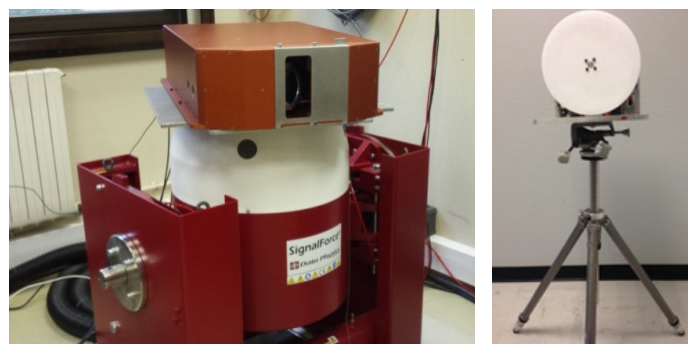


Figure 22 – left: LIDAR sensor head installed on the shaker; right: rotating disk used as the reference Doppler target

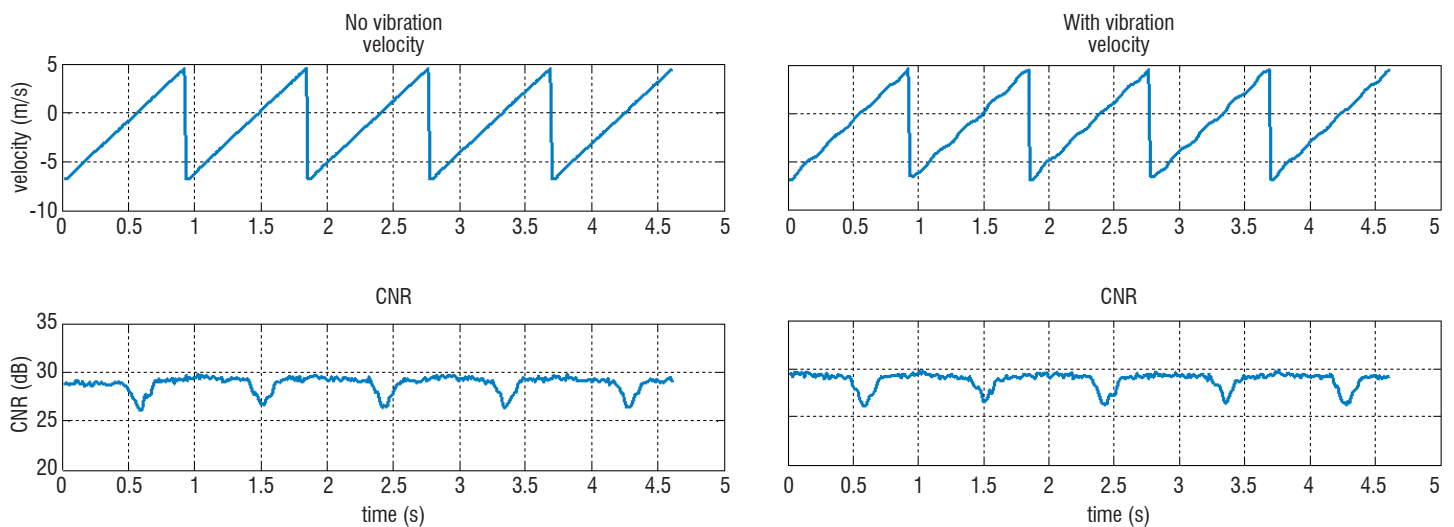


Figure 23 – left: without vibration; right: with vibrations; top: target radial velocity as a function of time (the modulated signal in the figure on the right is due to the LIDAR’s own velocity component); bottom: CNR as a function of time (dips occur when the laser crosses the center of the target with a lower albedo)

A scan of the laser beam along a diameter of the rotating target (0.6° in 1 s) enables the reflectance inhomogeneity to be smoothed. Figure 23 displays the LIDAR output signal: target radial velocity (top) and CNR profiles (bottom).

The average CNR value, 29 dB remains unchanged with and without vibrations. This indicates that the vibrations do not degrade the mixing efficiency and that the system design is resilient to vibrations even under turbulent conditions.

True air speed

Measuring the true air speed (TAS) non-intrusively in the free stream region in front of an aircraft is useful to complement the air data system. A short-range LIDAR providing local air speed at a few tens of meters from the aircraft allows a precise and remote measurement of the air speed outside the range of the flow disturbance from the aircraft: it is able to give the velocity in real time with no in-flight calibration, using autonomous onboard equipment and without *a priori* assumptions regarding the atmosphere. The LIDAR is aimed through a dedicated window, which avoids protruding equipment on the aircraft skin.

For rotary wing aircraft or UAV, even close-to-zero air speed values are measured, securing the vehicle also in hover flight. Such anemometer probes for true air speed measurements with high velocity precision have already been flight tested. In 2003, DALHEC, a 3-axis wind LIDAR, was built and flown onboard a Dauphin helicopter [11]. It was dedicated to True Air Speed measurements at medium range (30-100 m), away from rotor flow perturbations. The purpose was to evaluate the technology with regard to air speed accuracy, essentially at low speed.

Doppler LIDAR is also useful during certification procedures. Indeed, the calibration of an aircraft air data sensor requires cumbersome procedures, including specific equipment and costly dedicated flight

tests. Calibrations of the pitot static system and vanes using a laser anemometer have increased accuracy compared with those obtained with conventional techniques, such as a towed cone, tower-fly-by, or a pacer aircraft.

An airborne proof-of-concept measuring the air speed radial component (single axis LIDAR) ahead of an aircraft has been fly tested even at high altitude using a high-power fiber laser [51]. The LIDAR developed within the framework of the AIM2 European project, aimed at developing a 4-axis fiber anemometer to measure the full air speed vector. The purpose of the demonstrator was to assess the in-flight airspeed calibration of True Air Speed (TAS), Angle-Of-Sideslip (AOS) and Angle-Of-Attack (AOA). Its performances have been tested during aircraft maneuvers, a functionality that is not possible with the towed cone.

It should meet the following requirements:

- TAS dynamic: $50 \text{ m/s} \leq V_x \leq 200 \text{ m/s}$
- TAS accuracy: $\leq 1 \text{ m/s}$
- Angle dynamics: $-20^\circ \leq \text{AOS} \leq +20^\circ$; $-2^\circ \leq \text{AOA} \leq +15^\circ$
- Angle accuracy: 0.5°
- Measurement frequency: 16 Hz.

The LIDAR measures the air speed along the laser line-of-sight and the time-multiplexed 4 axes are used for speed reconstruction, assuming a homogeneous flow at the short focus distance of 50 m (see Figure 24).

The system is fully fibered ensuring good reliability against vibrations and the latest commercial fiber components.

A power spectral density is computed every $2.6 \mu\text{s}$ and, in order to improve the signal-to-noise ratio, each spectrum is averaged using 13 ms of signal acquired along each LIDAR axis. The system computes the 4 radial speeds every 100 ms and converts them into a 3D air speed vector in the aircraft reference frame.

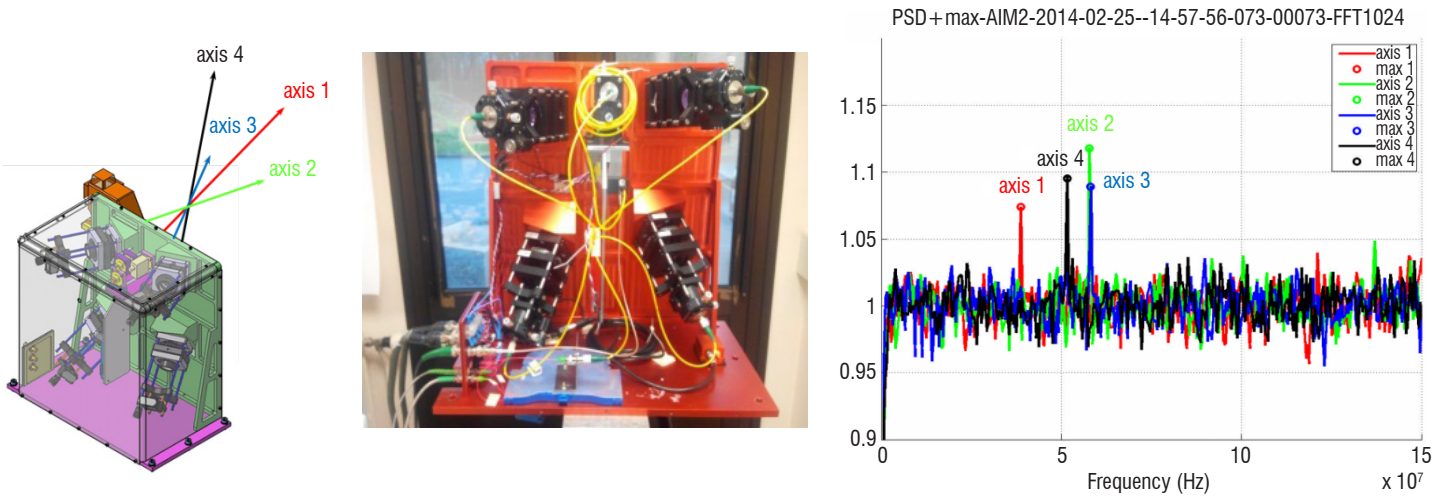


Figure 24 – right & middle: Sensor head with 4 Doppler measurement axes; left: Power Spectral Density for each axis and frequency maximum detection



Figure 25 – AIM2 installed onboard a P180

The LIDAR was installed onboard the Piaggio 180 and aimed through a passenger window fitted with an optical grade window (Figure 25). Having no protruding part facilitates flight procedures.

The system was flight tested at the Genova airfield in 2014 [3]. Reconstruction and graphical comparisons of True Air Speed, Angle-Of-Sideslip and Angle-Of-Attack with the aircraft Flight Test Instrumentation (FTI) have been performed in the LIDAR sensor head reference frame and are shown on Figure 26. Data have been analyzed during various maneuvers: Multiple ground tracks, rollercoaster pull up, level acceleration, and flat turn.

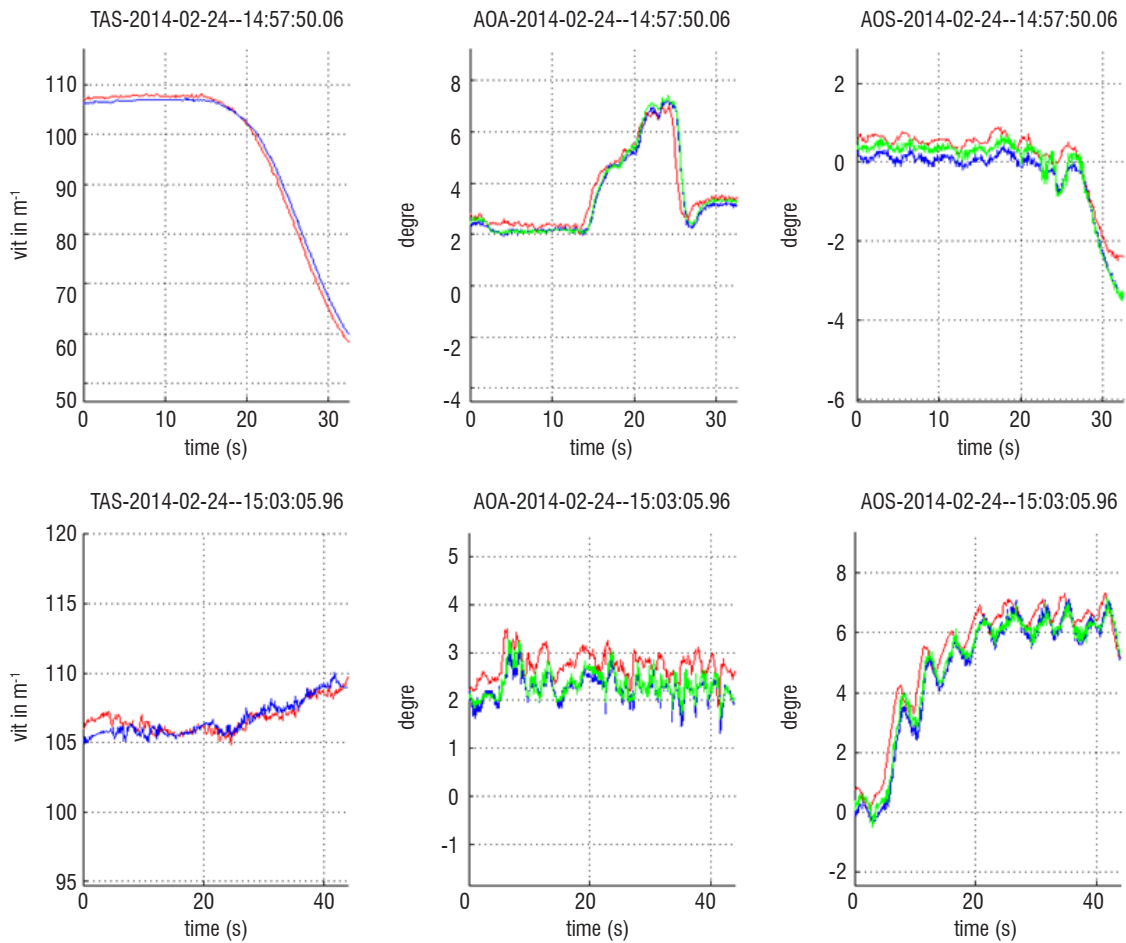


Figure 26 – LIDAR (red) and FTI data (green & blue) flight data – top: rollercoaster pull up – bottom: flat turn; left: TAS; middle: AOA; right: AOS

All bias between the LIDAR and the FTI data sets was within specifications demonstrating a very good agreement showing that fiber LIDAR technology has matured enough to provide a powerful technique for onboard air data calibration. The technology offers a significant capability in size reduction and could also be envisaged for UAV flight tests in a near future.

Conclusion

ONERA range resolved wind LIDARs based on new high-power, high-spectral-brightness, all-fibered sources have been used in various LIDAR configurations to demonstrate performance and evaluate technology maturity. We have investigated eyesafe high-peak-power sources using various SBS mitigation techniques to overcome nonlinear optics limitations. Using these sources, record ranges have been obtained in field tests. Improved algorithms for real-time wake vortex characterization, new EDR algorithms have been applied to wind measurement and validated with simulations.

High-power fiber lasers with optimized coherent LIDAR architectures offer new perspectives for applications related to airport safety and aircraft navigation, not to mention other fields of applications such as defense, security or space.

Operating an airborne LIDAR at cruise altitude would be of interest for clear air turbulence detection. However, the technology needs to mature in order to meet size and costs constraints. Nonetheless, at lower to medium altitude, coherent Doppler LIDARs based on fiber technology offer a rich panel of onboard functionalities. They can complement pitot vanes to increase air data system reliability and flight safety or to optimize the certification cycle, saving time and cost. Probing airspeed at longer ranges than the present air demonstrators using more powerful fiber lasers would enable new capabilities to be implemented, such as gust detection in a broad range of altitudes, providing anticipated warning against air dynamics hazards. They would also help in the design and certification of new air vehicles (fixed wing, rotary wing, UAV, airship, etc.) and ease their integration into air traffic. Their assets include increased reliability and resilience to vibration and low power consumption. Moreover, new designs taking advantage of the fiber architecture intrinsic multifunction capability could provide enhanced survivability of air vehicles in degraded atmospheric environments ■

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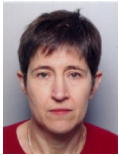
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