

# Stress distribution correlated with damage in duplex stainless steel studied by synchrotron diffraction during plastic necking

Y. Zhao <sup>a,\*</sup>, L. Le Joncour <sup>a</sup>, A. Baczmański <sup>b</sup>, E. Gadalińska <sup>c</sup>, S. Wroński <sup>b</sup>, B. Panicaud <sup>a</sup>, M. François <sup>a</sup>, C. Braham <sup>d</sup>, T. Buslaps <sup>e</sup>

<sup>a</sup> ICD-LASMIS, Université de Technologie de Troyes (UTT), UMR CNRS 6281, 12 rue Marie Curie, CS 42060, 10004 Troyes, France

<sup>b</sup> AGH- University of Science and Technology, Faculty of Physics and Applied Computer Science, al. Mickiewicza 30, 30-059 Krakow, Poland

<sup>c</sup> Institute of Aviation, Materials and Structures Research Center, al. Krakowska 110/114, 02-256 Warszawa, Poland

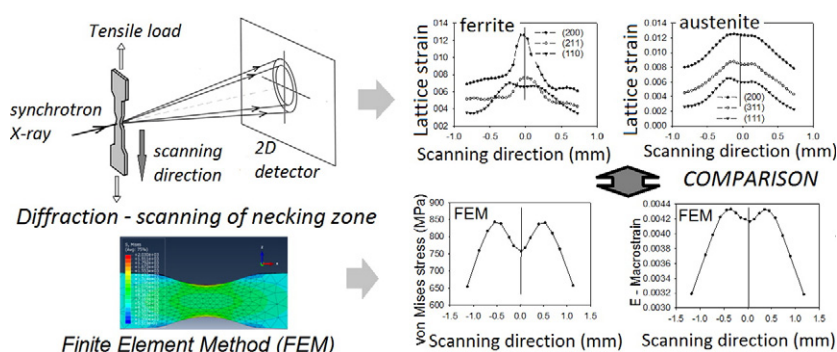
<sup>d</sup> PIMM, Arts et Métiers ParisTech (ENSAM), 151 Bd de l'Hôpital, 75013 Paris, France

<sup>e</sup> ESRF, 6, rue J. Horowitz, 38500 Grenoble Cedex, France

## HIGHLIGHTS

- Relaxation of stress in ferrite indicates damage initiation in this phase for a large deformation of duplex steel.
- The stress relaxation in ferrite depends on the grain orientation and position in the neck.
- Heterogeneous lattice strains and three-axial heterogeneous stresses are present in the necking zone.
- The softening/damage process in ferrite depends on the value of equivalent von Mises stress.

## GRAPHICAL ABSTRACT



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## ABSTRACT

The goal of this work was the determination of lattice strains distribution in two phases of duplex steel during plastic necking. Subsequently, the stress heterogeneity in the neck was studied in order to determine the reason for the damage initiation and to verify the hypothesis that the damage begins in the ferritic phase. To do this, X-ray synchrotron radiation was used to scan the 'in situ' variation of the interplanar spacings along the necking zone for samples subjected to tensile loading. A self-consistent model and FEM simulation were applied for the experimental data interpretation.

It was found that for advanced necking the phase lattice strains, especially those measured at some distance from the neck centre, show a large inversion of the loads localised in both phases compared to the undamaged state (the lattice strains in the ferrite become smaller than in the austenite). This effect indicates stress relaxation in the ferrite which is connected with the damage phenomenon. Correlation of the experimental results with the modelling shows that the value of von Mises stress is responsible for the initiation of the ferritic phase softening.

## 1. Introduction

Duplex stainless steel was discovered by Hochmann [1] during intergranular corrosion tests. This type of steel combines an excellent

\* Corresponding author.

E-mail address: yuchen.zhao@utt.fr (Y. Zhao).

resistance to corrosion with high mechanical strength due to the high content of chromium and nitrogen. The duplex steel studied in this work consists of ferrite ( $\alpha$  phase) having a bcc crystal structure and austenite ( $\gamma$  phase) exhibiting an fcc structure. Both phases possess good corrosion resistance. While the ferritic phase increases the value of yield stress, the austenitic phase improves the ductile response of the material.

Several studies of cast duplex stainless steel used in the cooling system of a nuclear power plant have been published [2,3]. This steel is subjected to a slow thermal ageing at a working temperature of 320 °C, which causes an embrittlement of the ferritic phase [4,5]. It is well-known that at temperatures below 475 °C, the spinodal decomposition of ferrite occurs [6–8].

During the deformation of duplex steel, the plastic strains are homogenous in the austenitic and more localised in the ferritic phase, where fewer slips, but with a higher magnitude, are observed [2,9–11]. SEM measurements performed for cyclic loadings show that the slip systems in the austenitic phase are activated first i.e. before the glides in the ferrite [11]. In the case of the aged duplex steel, Bugat et al. [2] observed the slip lines in the ferrite to be tortuous (following the  $\{112\}\langle 111 \rangle$  slip system and twinning along the same slip systems).

Due to the above-mentioned mechanisms, the damage process in aged duplex stainless steel is initiated mainly in ferrite, where cleavage micro cracks perpendicular to the loading direction have been shown in previous works [2,3,10]. The damage appears mainly in the regions where the strain incompatibilities are high (double or triple grain boundaries in the austenite) and/or in the intersection of the strain modes (slipping and twinning in the ferrite). The nucleation of cleavage cracks is a continuous and stable phenomenon that accelerates with the strain. The study of damage in polycrystalline materials is usually based on a direct observation of the cracks' initiation and evolution using electron microscopy [12–14] or X-ray tomography [14]. Using electron microscopy (EBSD, TEM and SEM techniques) the initiation of cracks due to a cyclic loading of duplex steel was seen in the ferritic phase [12,14]. Recently, the effect of significant lattice strain release in damaged ferrite grains was confirmed by Istomin et al. [13] using X-ray synchrotron diffraction.

To observe the mechanical behaviour inside both phases during the damage process, diffraction measurements combined with an in situ tensile test were performed [15–25]. The main advantage of the diffraction methods is that the measurements are performed selectively only for the crystallites contributing to the measured diffraction peak. When several phases are present in the sample, measurements of a separate diffraction peak allows for investigating the behaviour of each phase independently [15–25]. A comparison of the diffraction data with micromechanical models is very convenient for the study of elastoplastic properties at micro and macro scales. Both selectivity and scale considerations determine the use of diffraction technique in the present study. An analysis of the experimental data using model predictions enables understanding of the physical phenomena which occur during a sample's deformation. Moreover, the micro and macro parameters of the elastoplastic deformation can be experimentally identified.

The damage processes initiated on slip planes or particular crystallographic planes, as suggested in many works [3,26–29], may be responsible for the relaxation of the grain stresses, depending on the orientation of the crystallographic lattice. This effect was also observed by measuring lattice strains in both phases of duplex steel using the neutron diffraction method [17,20].

In this work, the effect of stress partition between phases inside and outside the necking area in plastically deformed duplex steel is studied for the first time using synchrotron radiation. An interpretation of the results was performed with help of the Finite Element Method (FEM) and elastoplastic self-consistent modelling. The FEM simulation was applied to determine the influence of the neck shape on the stress distribution, while the self-consistent model was used to predict elastoplastic deformation of the undamaged state of the material and

to show the difference between this state and the behaviour of the damaged material. In particular, a tendency of lattice strains evolution was studied and then compared with the experimental results obtained for the deformation neck.

The present work is a continuation of our previous investigation [17, 20] in which the damage process occurring in the neck was studied using neutron diffraction. Previously, the measurements of lattice strains were performed for both phases and compared with a self-consistent model accounting for the damage process. It was found that relaxation of stresses in the ferritic phase and the load transfer to the austenite occurred in the deformation neck. The observed phenomenon was explained by a model, but due to relatively large gauge volume the stress/strain heterogeneity was not studied. In the previous study [29] the preliminary results of synchrotron measurements before the sample fracture under the applied load were also presented, but the strains heterogeneity in the neck was not investigated.

The present experiment was performed using synchrotron diffraction during a tensile test for which the sample strain was controlled. Due to a small gauge volume enabling high spatial resolution of the measurements, the lattice strains were scanned along the deformation neck created during the tensile test. The main goal of this work was to observe the stress partitioning between the phases at various positions in the necking zone. As a result, the relaxation of the stress in the ferritic phase was studied and the heterogeneity of the damage within the deformation neck was described.

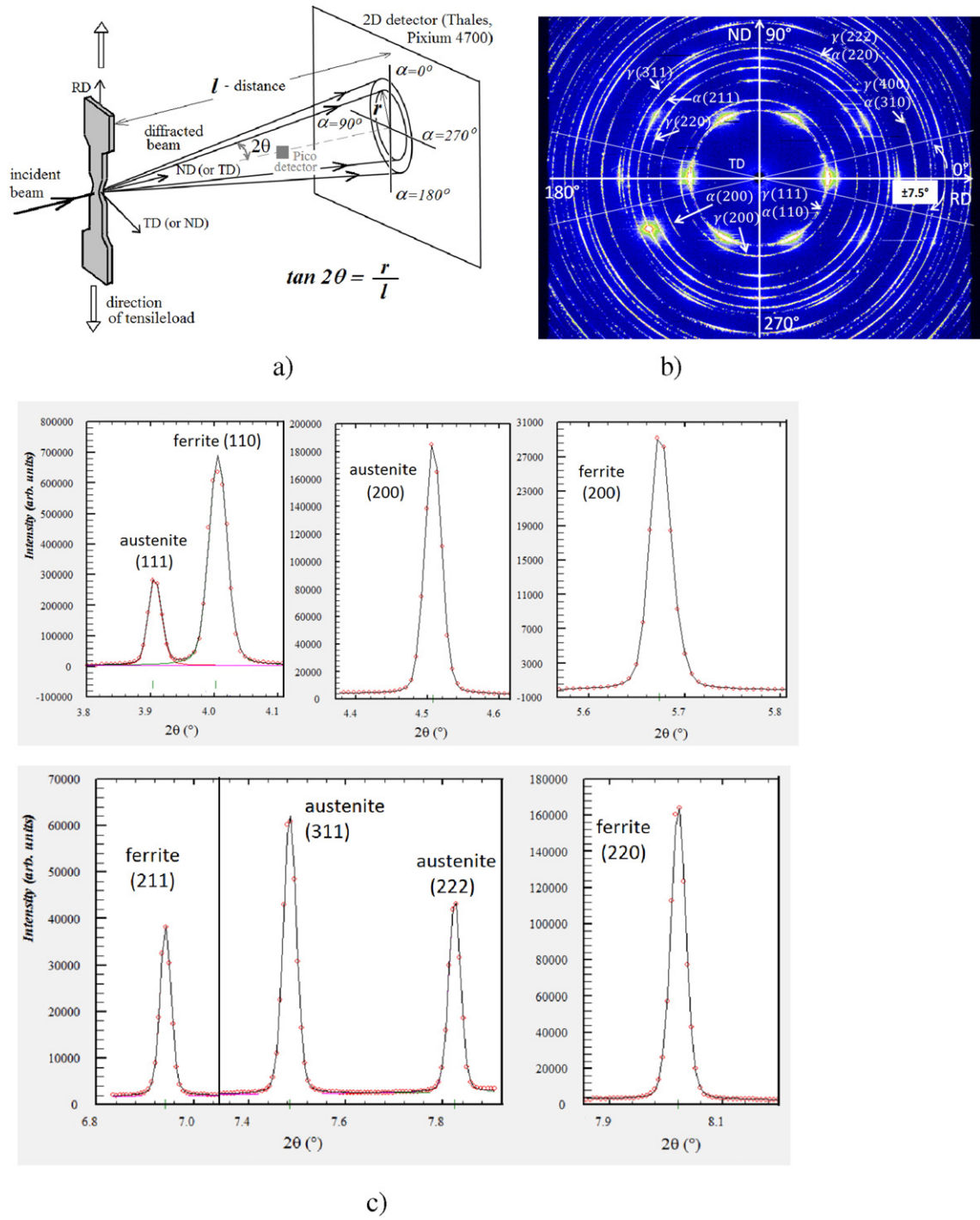
## 2. Experimental

### 2.1. Material characterisation

The present study examined an austenitic-ferritic duplex stainless steel UR45N, which was previously investigated in [17,29]. The microstructure of the studied material is constituted of a ferritic phase and austenitic phase in approximately equal volume proportions (50% austenite and 50% ferrite). EBSD maps show the elongated grains of the austenite ( $\gamma$  phase) evenly embedded in the ferritic ( $\alpha$  phase) matrix (see [17,29]). The grains of the austenite are divided into smaller crystallites with different orientations, while the grains of the ferrite possess nearly the same crystal orientation resulting from the rolling process [29]. The Orientation Distribution Function (ODF, shown in [30]) of each phase was determined from the experimental pole figures  $\{110\}$ ,  $\{200\}$ ,  $\{211\}$  and  $\{111\}$ ,  $\{200\}$ ,  $\{220\}$  measured respectively for the ferrite and the austenite, using Cr radiation on a Seifert four circles diffractometer [29].

### 2.2. Measurement configuration and treatment of the 2D diffraction patterns

The tensile tests combined with in-situ X-ray synchrotron diffraction measurements were performed in a transmission mode on the beamline ID15B at ERSF (Grenoble, France), using a monochromatic X-ray radiation with the wavelength  $\lambda = 0.14256$  Å, which was determined from a preliminary calibration performed on the CeO<sub>2</sub> reference powder [29]. The configuration of the experimental setup is shown in Fig. 1a. The diffraction pattern, recorded by a Thales 2D Pixium 4700 CCD detector [31], is presented in Fig. 1b. A Pico1 detector was placed in front of the outgoing beam in order to measure the intensity of the beam passing straight through the sample (Fig. 1a). The measurements were performed using a beam size of 100  $\mu\text{m} \times 100 \mu\text{m}$  for 'dog-bone' shape samples having a cross section of 1.5 mm  $\times$  1.5 mm in the region studied by diffraction. The samples were named respectively 'sample TD' and 'sample ND'. Sample TD was manufactured so that the transverse direction (TD) was perpendicular to the sample surface, which means that the incident X-ray beam was parallel to the TD direction during the tensile test [29]. Sample ND was machined with the normal direction (ND) perpendicular to its surface, allowing measurement with



**Fig. 1.** Experimental setup showing orientations of the samples during experiment (a), the image recorded on the 2D detector for the initial sample (b), and the integrated 1D diffraction peaks fitted by pseudo-Voigt function (c).

the incident X-ray beam parallel to the ND. The load was applied along the RD for both samples (Fig. 1a).

The recorded images were handled using diffraction patterns treatment by FIT2D [32] and Multifit [33] software. FIT2D was used to convert the received two-dimensional images into one-dimensional spectra (intensity vs. scattering angle  $2\theta$ ), while the Multifit program was applied to determine the  $2\theta$  positions of the diffraction peaks by fitting with the pseudo-Voigt function [34] (the examples are shown in Fig. 1c). Finally, the interplanar spacing  $\langle d \rangle_{\{hkl\}}$  was computed from the peak positions using the Bragg's law.

To calculate the values of  $2\theta$  angle, a simple relation  $\tan 2\theta = \frac{r}{l}$  was used, where  $r$  is the measured radius of diffraction ring acquired on the 2D detector and  $l$  is the distance between the sample and the detector (Fig. 1a). The  $l$  distance was measured comparing the radii of the diffraction rings recorded at two different positions of the detector, which was shifted by a known distance. Such a preliminary measurement was done for each sample fixed in the loading rig, prior to the tensile test. During the experiment the detector and sample were kept in a fixed position i.e.  $l$  was equal to 899.1 mm and 901.0 for the ND and TD samples, respectively. It should be emphasised that the above-

mentioned methodology is not dedicated to determining the absolute values of the interplanar spacings or lattice parameters and that the further analysis performed in this work was based on the relative changes of  $\langle d \rangle_{\{hkl\}}$  for different sample orientations (measurement of initial deviatoric stresses) or relative lattice strains with respect to the unloaded sample (in situ tensile test). Therefore, even if the value of  $l$  is measured approximately, the uncertainty of this value does not influence the relative changes of  $r$  and corresponding relative shifts of peak positions vs.  $2\theta$  angle or  $d$  - spacing.

Analysing the diffraction pattern obtained for the initial material (cf. Fig. 1b) and the patterns measured during the tensile test, it can be concluded that the studied samples exhibit a strong crystallographic texture for both phases (see also the ODFs presented in [17,29]). It was found that the positions of texture maxima does not change significantly during the tensile test, even during necking. The diffraction rings obtained for the initial sample are composed from dots representing coarse grains (the size of the grains is comparable with the size of the beam, cf. [29]). During plastic deformation the grain size (i.e. the dimension of coherent domain) decreases and the dislocation density increases, leading to smoother and more broader diffraction lines. Also, it was noticed that the crystallographic texture becomes more pronounced, causing an increase of the highest peaks and a vanishing of the lower ones. Due to the variation of peak intensity, reliable analysis was only possible for a limited number of reflections, decreasing with the progress of deformation. The reflections used in the analysis at different stages of the experiment are listed in Table 1.

### 2.3. Determination of the initial stresses

The X-ray Elastic Constants (XEC) of the studied material were calculated using the Eshelby-Kröner approach [35–37] from the measured ODFs, as well as the single crystal elastic constants of each phases given by Simons et al. [38] and Inal et al. [15]. The values of  $C_{11}$ ,  $C_{12}$  and  $C_{44}$  for the austenite are: 198 GPa, 125 GPa, 122 GPa, and the ferrite: 231 GPa, 134 GPa, 116 GPa. The average initial residual stresses present in each phase of the studied material were determined using the multi-reflection method described by Baczmanski et al. and Wronski et al. [35,36]. The interplanar spacings  $\langle d \rangle_{\{hkl\}}$  required for stress analysis were measured on the initial state of the studied samples. In the case of sample TD, the measurements for two different sample orientations with respect to the experimental setup were performed (i.e. the TD or ND was parallel to the incident beam, as shown in Fig. 1a). The spacings  $\langle d \rangle_{\{hkl\}}$  were determined in 24 different orientations of the scattering vectors by integrating the 2D pattern with a step of  $15^\circ$  over the whole range of  $360^\circ$  for the azimuth angle  $\alpha$ . Then, arithmetical mean  $\langle d \rangle_{\{hkl\}}$  spacings were calculated for symmetrically equivalent  $\alpha_n$  and  $\alpha_n + 180^\circ$  angles [29] and the deviatoric part of stress tensor was determined for each phase (to do this, the precise values of the  $d_{0,\{hkl\}}$  stress free spacings are not necessary [35,36]). In Table 2, three principal stresses measured for the initial sample TD are presented (this initial sample was measured for two orientations with respect to the experimental setup; Fig. 1a), while only one stress component was determined for the sample ND (the latter sample was measured at one orientation i.e. for the ND parallel to the incident beam; Fig. 1a).

The same types of initial stress tensors were determined in the phases of the not loaded sample TD as in our previous neutron diffraction study [29] for a similar material, but the values of the components

**Table 2**

Initial deviatoric residual stresses measured in each phase of the studied UR45N aged samples (in the case of sample TD, the stress tensor is the same as determined in [29]).

		$\sigma_{RD}$ (MPa)	$\sigma_{TD}$ (MPa)	$\sigma_{ND}$ (MPa)
Sample TD	Austenite	$134 \pm 15$	$84 \pm 15$	$-218 \pm 15$
	Ferrite	$-155 \pm 19$	$-44 \pm 19$	$199 \pm 18$
Sample ND	Austenite	$-34 \pm 11$	Not measured	Not measured
	Ferrite	$59 \pm 19$		

determined from the synchrotron experiment are significantly larger (Table 2). Moreover, a different stress state was found in sample ND. The possible reason for such disagreements is the heterogeneity of the thermal treatment leading to different initial residual stresses (heterogenous stress can be created, especially during cooling). It should also be stated that the previous neutron study was performed with a larger size of the beam, averaging the information for a large volume (ca.  $4 \text{ mm} \times 4 \text{ mm} \times 8 \text{ mm}$  [29]). To the contrary, the present results of the synchrotron experiment are much more sensitive to spatial heterogeneities because of the small gauge volume (ca.  $0.1 \text{ mm} \times 0.1 \text{ mm} \times 1.5 \text{ mm}$ ). Despite the spatial variation of the stresses in the initial sample, all the components of the stress tensor fulfil the equilibrium rule i.e. the stress component for the ferrite is opposite to the corresponding one in the austenite and both components exhibit similar absolute values. Thus, the mean stress over both phases (volume fractions 50%:50%) is close to zero, as expected in the case of the non-loaded sample.

### 2.4. In-situ tensile test during diffraction measurements

In our previous work [29] the lattice strains were measured during a tensile test performed applying the required values of the external load (the load control mode) to the sample. However, during such a test the increasing concentration of stress in the appearing deformation neck leads to an instability of deformation and an immediate fracture of the sample. Therefore, the lattice strains in the neck were not scanned with a synchrotron beam. In the present work, the sample TD and sample ND were measured in the strain control mode with strain rates respectively equal to  $2.8 \times 10^{-4} \text{ s}^{-1}$  and  $2.4 \times 10^{-4} \text{ s}^{-1}$  before an appearance of necking, and then the necks were scanned for given constant sample strains. The strain control mode enables a measurement also during a heterogenous deformation when the deformation neck is created. In this case, during a progressively increasing sample strain, the loading of the sample decreases, preventing a concentration of the large stress in the narrowest section of the neck.

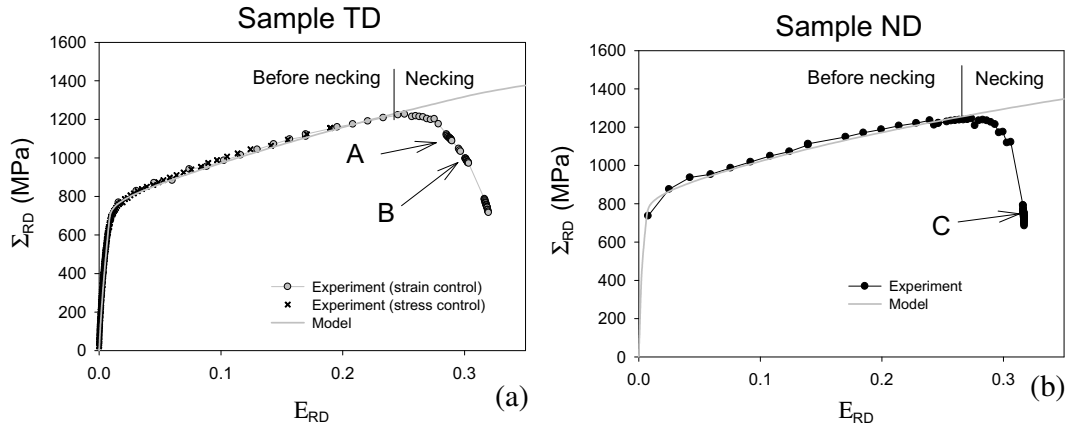
During measurements the position of grip was measured and the force subjected to the sample along RD was determined using a load cell. Then, the true stress was calculated accounting for the sample cross section evolution and the rig elasticity was taken into account in the calculation of true strain. Plots of true stress ( $\Sigma_{RD}$ ) vs. true strain ( $E_{RD}$ ) are reported respectively for the two studied samples in Fig. 2a and b. In the case of sample TD the measurements were made only during an advanced plastic deformation including the necking process and the  $\Sigma_{RD}$  vs.  $E_{RD}$  plot was completed by our previous results obtained for an identical sample (studied in [29]) but for the elastoplastic range until the appearance of necking (Fig. 2a). The curves obtained in both experiments perfectly overlap in the range of the sample strain  $1.5\% < E_{RD} < 20\%$ . As shown in Fig. 2a and b, an important reduction of the applied stress occurred at about  $E_{RD} \approx 25\%$  until the end of the test, i.e. up to the sample fracture. This stress reduction indicates appearing of a deformation neck which was seen through an optical lunette during measurements. It should be stated that starting from  $E_{RD} \approx 25\%$  the true stress as well true strain cannot be correctly estimated because of a heterogeneous sample deformation and a significant difference between the cross section within the neck and outside this region (i.e., the experimental stress from this threshold indicates relaxation of applied stress

**Table 1**

Available reflections used in the analysis performed for different stages of the experiment.

	Determination of initial stresses	In-situ tensile test and scanning of the necking zone
Ferrite	110, 200, 211, 220, 310	110, 200, 211, 220
Austenite	111, 200, 220, 311, 222, 400	111, 200, 311, 222





**Fig. 2.** Plots of true stress vs. true strain for the measured sample TD and sample ND. The indicated A, B and C points represent the stages for which scanning of necking zone was performed.

during the sample deformation, but the values  $\Sigma_{RD}, E_{RD}$  do not have a correct physical meaning).

When the neck was noticed, the sample was shifted (together with the rig) to the position enabling a diffraction measurement within the necking region (Fig. 1a). Subsequently, the scans along the necking region were performed for the stages indicated in Fig. 2a and b. In the case of the sample TD and sample ND, a few diffraction measurements were made for the early stages of the sample deformation. During tensile tests the diffraction pattern were recorded with an exposure time of 40 s separated by 15 s intervals (for which the reflected intensities were not measured). In the case of the neck scans the exposure time was equal to 10 s separated by intervals of 12 s.

Three scans of the neck were carried out at the sequence of three necking stages A, B and C, as indicated in Fig. 2, which represent different stages of evolution of the ductile damage process for the two studied samples. The scans were performed along the necking zone *N* (cf. Fig. 3b), while the X-ray beam was parallel to the TD in the case of sample TD (stages A and B) and to the ND in the case of sample ND (stage C), cf. Fig. 2. The estimation of sample thickness along the necking was based on the comparison of the outgoing beam intensity received by the Pico1 detector for the neck and for the reference sample having a known thickness equal to 1.4 mm. A schematic drawing of the setup used with the Pico1 detector is presented in Figs. 1a and 4a. The absorption law was used to evaluate the variation of the sample thickness:

$$I = I_0 e^{-\mu d} \quad (1)$$

where:  $I_0$  and  $I$  are the measured intensities of the incident and outgoing beams,  $d$  is the thickness of the sample in the scanned area, and  $\mu = 0.29 \text{ cm}^{-1}$  is the linear absorption coefficient of iron for a synchrotron X-ray energy of 87 KeV [39].

The spatial evolutions of the sample thickness along the necking zone estimated for the two samples are presented in Fig. 4b. However, the curves determined for the A and B stages cannot be compared with the one for stage C because the measurements were performed for different orientations of the incident beam with respect to the sample (TD or ND). Comparing the thickness of the deformed necks in two

directions (after tensile tests), we found that the reduction of sample thickness in the necking region was more significant in the ND than in the TD. This phenomenon can be explained by the strong crystallographic texture in both phases of the studied steel, leading to anisotropy of macroscopic plastic deformation (the elliptical cross section of the neck is shown in [17] for the round sample).

### 3. Results and discussion

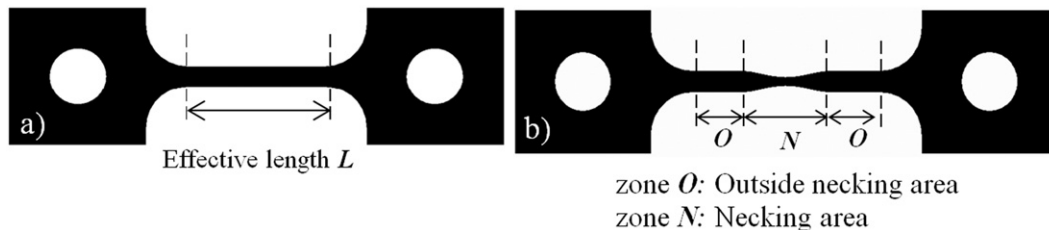
#### 3.1. Interpretation of diffraction measurements during the tensile test

The interplanar spacings were determined for the direction along the applied load (RD,  $\alpha_n = 0^\circ$  and  $180^\circ$ ) for both the studied samples. For this purpose, the intensities of the diffraction rings were integrated within 'cake shape' sectors defined by  $\alpha_n \pm 7.5^\circ$  and the mean  $\langle d \rangle_{\{hkl\}}$  spacings were calculated for symmetrically equivalent  $\alpha_n = 0^\circ$  and  $\alpha_n = 180^\circ$  angles (Fig. 1b). Next, the elastic lattice strains  $\langle \epsilon \rangle_{\{hkl\}}$  corresponding to different  $hkl$  reflection were determined from the equation

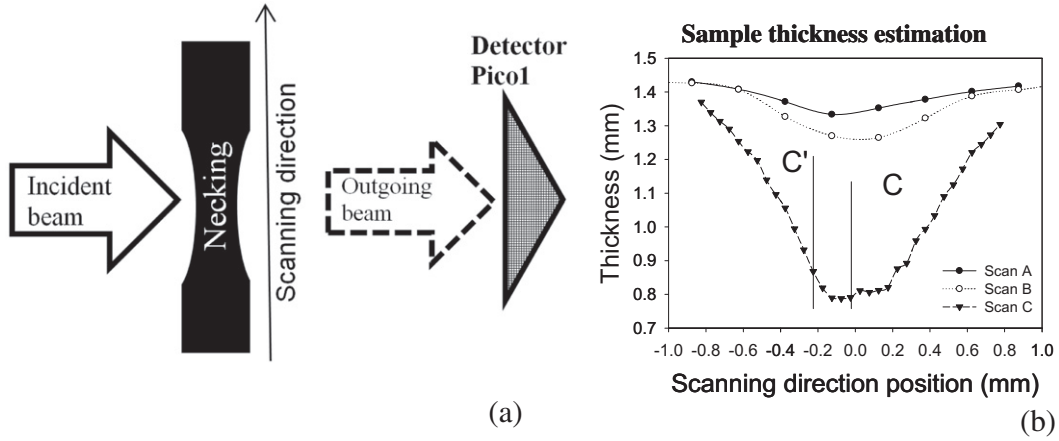
$$\langle \epsilon_{RD} \rangle_{\{hkl\}} = \frac{\langle d_{RD}^{\Sigma} \rangle_{\{hkl\}} - \langle d_{RD}^0 \rangle_{\{hkl\}}}{\langle d_{RD}^0 \rangle_{\{hkl\}}} \quad (2)$$

where:  $\langle d_{RD}^{\Sigma} \rangle_{\{hkl\}}$  is the interplanar spacings measured along the loading direction (RD) at different loads (applied stresses  $\Sigma_{11}$ ), while  $\langle d_{RD}^0 \rangle_{\{hkl\}}$  is the initial interplanar spacing measured without external load.

It should be noted that the strains considered in this work were calculated relative to the initial values of the interplanar spacings  $\langle d_{RD}^0 \rangle_{\{hkl\}}$  measured for the unloaded sample. In this way we avoided determination of the stress free interplanar spacings  $d_{0,\{hkl\}}$  for each phase which, in fact, could not be done due to the presence of the high initial stresses between the phases. Therefore, the further analysis presented in this work is based on the comparison of the elastic strain evolution occurring in the two phases, and the absolute strains or lattice spacings are not determined. Finally, the arithmetic averages  $\langle \epsilon_{RD} \rangle_{\text{phase}}$  over the lattice strains of individual  $hkl$  reflections were determined for



**Fig. 3.** Schematic drawing of the tensile test sample; the sample before tensile test (a) and the sample after the appearance of necking (b). The studied zones are indicated.



**Fig. 4.** Schematic drawing of the setup used for scanning of the necking zone  $N$  (a). The estimated sample thickness along the necking zone determined from scans A, B and C (b). The abscissa represents the positions of measurement in the scanning direction.

the sample TD (the available reflections are listed in Table 1). The mean lattice strains vs. the applied true stress are shown in Fig. 5, separately for the ferritic and austenitic phases (in the case of sample TD the results of the previous experiment performed until necking [29] are also included in Fig. 5a).

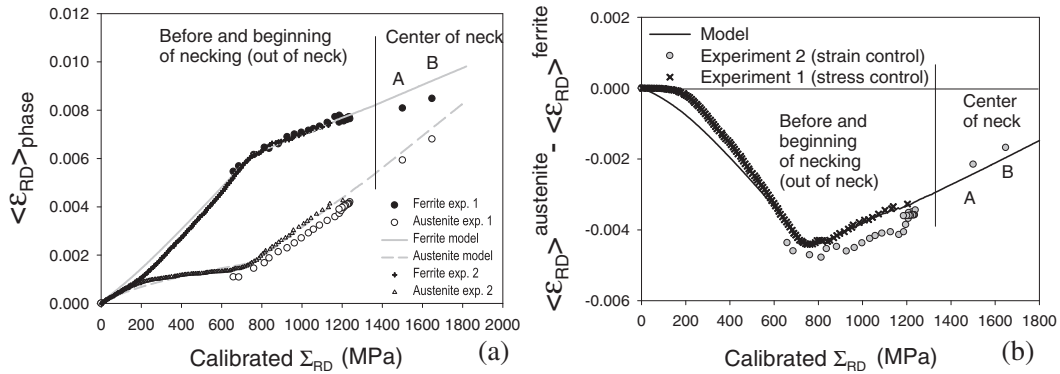
The self-consistent model of elastoplastic deformation elaborated by Lipinski and Berveiller [40,41,43,44] was used to interpret the experimental results as well as to determine the parameters of Voce law [29,42] in each phase of the studied duplex steel. In these calculations the initial orientations of crystallites, corresponding to the experimental textures [29], single crystal elastic constants given in Section 3.2 (the same as for the XEC calculation) and the initial stresses (listed in Table 2) were used as the input data for each phase. Simulations were performed for 2000 spherical grains belonging either to the ferrite (50%) or to the austenite (50%) phases. The elastic lattice strains  $\langle \epsilon_{RD} \rangle_{phase}$  and the total sample strain  $\Sigma_{RD}$  vs. the applied stress  $E_{RD}$  were calculated for different tensile loads corresponding to the experimental ones.

The lattice strains  $\langle \epsilon_{RD} \rangle_{phase}$  simulated by the self-consistent model were fitted to the experimental data (Fig. 5, part before necking), and as a result the values of the critical resolved shear stress were identified for both phases. Thus, the two thresholds  $\Gamma$  and  $\Omega$ , defined by Baczmanski and Braham [16] and Baczmanski et al. [17, 29], were identified as the yield points for the austenitic phase and for the ferritic phase, respectively. Adjusting the model results simultaneously to the experimental lattice strains and to the  $\Sigma_{RD}$  vs.  $E_{RD}$  function (Fig. 2), the critical resolved shear stresses (CRSS)  $\tau_0^{phase}$  and parameters  $\tau_1^{phase}$ ,  $\theta_0^{phase}$ ,  $\theta_1^{phase}$  characterising work

hardening for each phase were determined (for details see [29]). A very good agreement between the macroscopic behaviour predicted by the model and the experimental results was observed in the measuring range of the homogenous deformation i.e. up to about 25% of the sample strain (at this strain an unstable process caused by the necking phenomenon begins). Moreover, a good accordance between the theoretical and experimental data was obtained for the measured lattice strains (Fig. 5, part before necking). These results prove that the model correctly predicts the partition of the stresses between both phases. The parameters of Voce law determined for ferrite and austenite are presented in Table 3.

Analysing results for the aged UR45N samples, it can be concluded that the value of yield stress of the aged ferrite is much higher than that of the austenite. Thermal ageing causes the precipitation of secondary phases and spinodal decomposition of the ferrite (into  $\alpha$  and  $\alpha'$  phases) and consequently a significant increase of the hardness of the ferrite, while the mechanical properties of the austenite remains unchanged. The latter conclusions agree with those previously drawn from the diffraction study performed on a similar material [17,29].

As mentioned above, the small gauge volume measured using a synchrotron beam enables determination of a variation of lattice strain in different parts of the sample during a heterogeneous macroscopic deformation, as was done for samples TD and ND. Before the appearance of the necking phenomenon, a homogenous deformation can be assumed at the macroscopic scale. After the necking occurrence, the true stress in the measured region cannot be calculated any more due to the heterogeneous narrowing and unknown evolution of the sample cross section. Therefore, a calibration of the macrostress in the



**Fig. 5.** The evolution of phase lattice strains vs. calibrated sample stress before the beginning of necking and in the centre of the neck for the samples TD (a), deformed in the load control mode (exp. 1) and in the strain control mode (exp. 2). The difference between lattice strains in the austenite and the ferrite  $\langle \epsilon_{RD} \rangle_{Austenite - Ferrite}$  is also shown (b). The experimental results (point) are compared with the model (lines).

**Table 3**

Parameters of plastic deformation determined for the studied samples.

		Sample TD	Sample ND
$\tau_0^{phase}$ (MPa)	Austenite	150	150
	Ferrite	420	490
$\theta_0^{phase}$ (MPa)	Austenite	380	420
	Ferrite	190	150
$\tau_1^{phase}$ (MPa)	Austenite	280	280
	Ferrite	140	140
$\theta_1^{phase}$ (MPa)	Austenite	80	80
	Ferrite	40	40

diffraction volume proposed by Baczmanski et al. [17] was introduced in this study. The calibrated macrostress was determined as:

$$\Sigma_{RD}^{Calibrated} = k \langle \varepsilon_{RD} \rangle_{mean}^{Aus+Fer} \quad (3)$$

where:  $k$  is a scalar coefficient describing the relationship between macrostress  $\Sigma_{RD}^{Calibrated}$  in the diffraction gauge volume and the macrostrain  $\langle \varepsilon_{RD} \rangle_{mean}^{Aus+Fer}$ , which is equal to the mean strain for both phases:

$$\langle \varepsilon_{RD} \rangle_{mean}^{Aus+Fer} = \frac{\langle \varepsilon_{RD} \rangle_{Fer} + \langle \varepsilon_{RD} \rangle_{Aus}}{2} \quad (4)$$

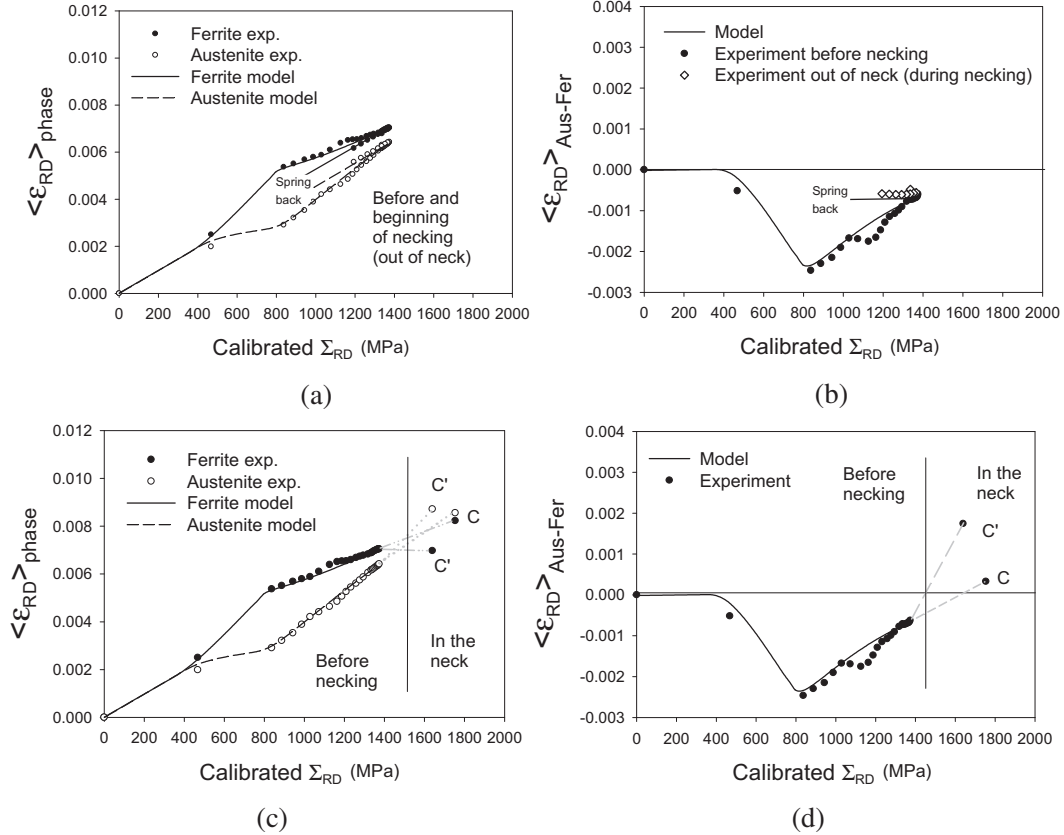
The real macrostress in the necking area is assumed to be proportional to the average elastic macrostrain  $\langle \varepsilon_{RD} \rangle_{mean}^{Aus+Fer}$  in both the elastoplastic stage and large deformation stage, even in the damage stage. Therefore, the value of  $\Sigma_{RD}^{Calibrated}$  can be calculated for the gauge within the neck from the measured  $\langle \varepsilon_{RD} \rangle_{mean}^{Aus+Fer}$  if the value of the  $k$  coefficient is known. This coefficient can be determined from the pre-

necking stages (preferable elastic range) of the sample using linear regression [17]. The inter-phase and inter-granular stresses were neglected in the stress calibration because the calculation of the average elastic macrostrain  $\langle \varepsilon_{RD} \rangle_{mean}^{Aus+Fer}$  was made considering a large number of grains having various orientations. The global inter-granular and inter-phase stress, defined as the deviations from macroscopic stress, must cancel each other out and sum to zero over a diffracted volume. This assumption was confirmed in a previous work using a self-consistent model by Le Joncour [45] and Baczmanski et al. [17].

In Fig. 5a the lattice strains in both phases are presented during the homogenous plastic deformation for the two samples TD (the first was measured in load control mode until failure, while the second one was measured during a large deformation and the necking process in the strain control mode). When the neck was created, a few measurements were made outside the neck and, next, for the point in the centre (at two states of deformation). Moreover, the difference between the mean lattice strain in the austenite  $\langle \varepsilon_{RD} \rangle_{Aus}$  and the ferrite  $\langle \varepsilon_{RD} \rangle_{Fer}$  is presented in Fig. 5b. This difference is defined by the equation:

$$\langle \varepsilon_{RD} \rangle_{Aus-Fer} = \langle \varepsilon_{RD} \rangle_{Aus} - \langle \varepsilon_{RD} \rangle_{Fer} \quad (5)$$

A very good agreement between the experimental data for both samples and model results was obtained for the pre-necking, as well as for the centre of the neck. This proves that the calibration method enabled the determination of the macrostresses in the gauge volume. It was found that the tendency of the phase strains/stresses evolution determined for the pre-necking stages continues in the centre of the neck. It should be noted that before necking as well as in the centre of the neck, the mean lattice strains in the ferrite are larger than the strains in the austenite (a negative value of  $\langle \varepsilon_{RD} \rangle_{Aus-Fer}$ ). This difference is



**Fig. 6.** The variation of phase lattice strains (a) and (c) and the difference between the lattice strain in the austenite and the ferrite  $\langle \varepsilon_{RD} \rangle_{Aus-Fer}$  (b) and (d) for the sample ND. The evolutions out of the neck (a) and (b) and in two positions in the neck (c) and (d) are shown (cf. Fig. 2b). The model's results are presented (black lines) for the pre-necking stage, while the grey lines connect the strains at the end of the pre-necking stage with the strains in the neck (for a better visualisation).

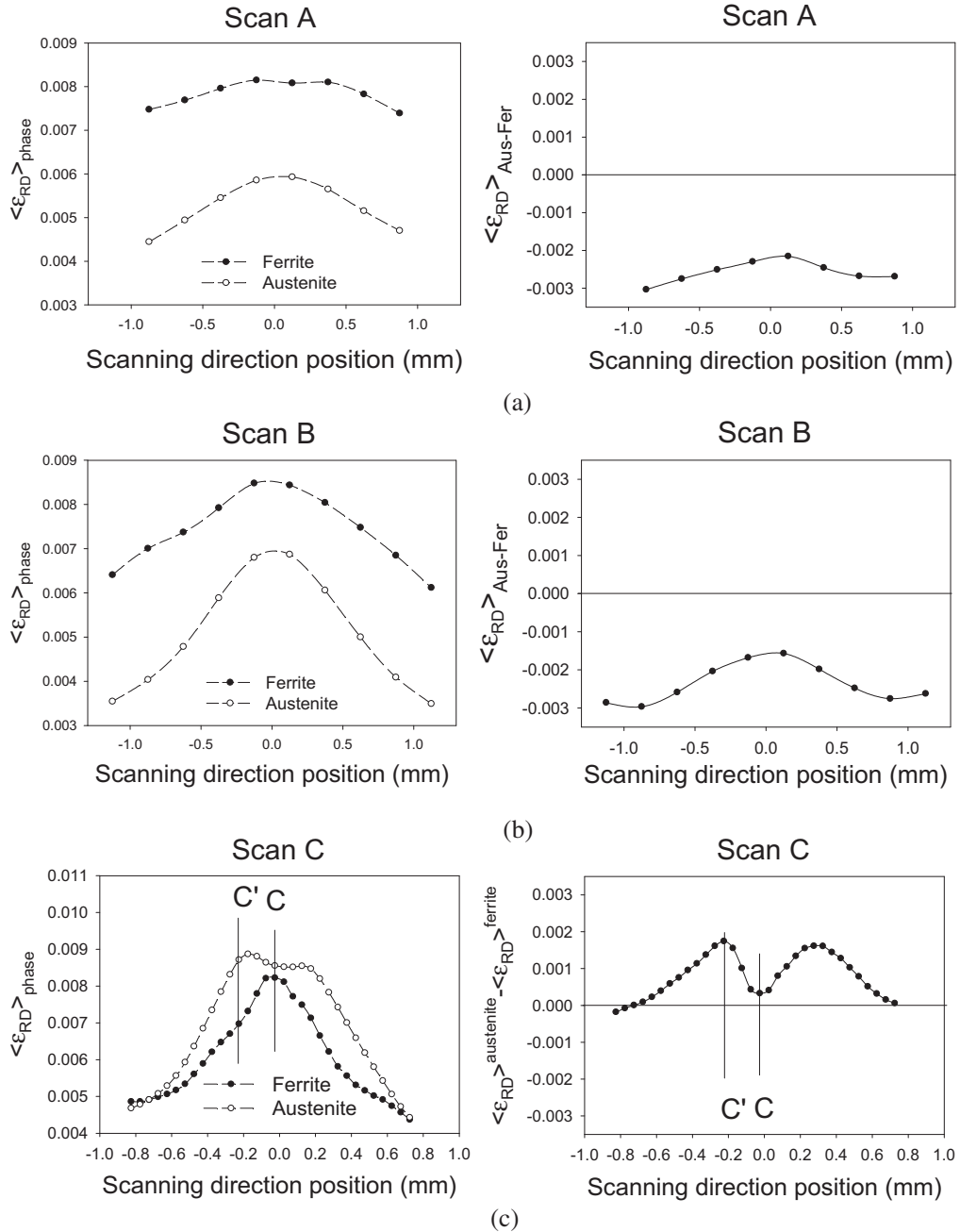
caused due to a lower yield stress of the austenitic phase, as explained in [17,29].

Next, the sample ND was measured during a tensile test and a different evolution of the phase strains was observed in comparison with the samples TD (cf. Fig. 6). In the calculations the mean lattice strains were calculated for the available reflections presented in Table 1. The initial diffraction pattern allowed us to determine one component of the initial stress tensor (along the RD, cf. Table 2). This component is different and has an opposite sign when compared with the sample TD. The model calculations were performed for the sample ND accounting for the initial stresses (Table 2) and a very good agreement between the model and the measured lattice strains was also obtained (Fig. 6). As can be seen in Fig. 2, the macroscopic dependence of a true stress vs. measured true strain was also correctly predicted by the model until the necking phenomenon. In simulations the same value of  $\tau_0^{phase}$  for the austenite

and the higher value  $\tau_0^{phase}$  for the ferrite in comparison with the sample TD (Table 3) were used.

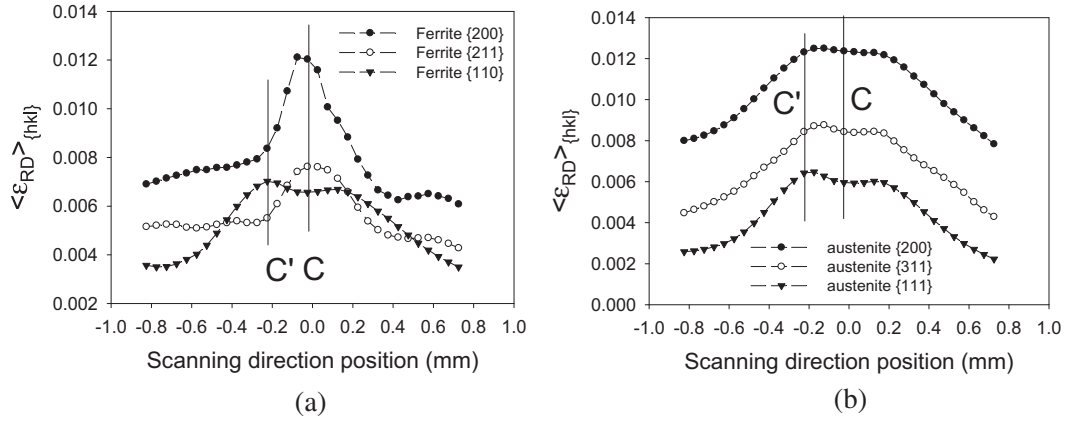
If we analyse the necking stage, we can notice the elastic spring backs of the lattice strains/stresses, determined in both phases outside of the neck i.e. in the zone O indicated in Fig. 3b. During spring back, the strains decrease linearly with the deformation progress (this effect is well observed in Fig. 6a). Simultaneously, the difference between the strains in both phases  $\langle \epsilon_{RD} \rangle_{Aus-Fer}$  stabilises - as shown in Fig. 6b. This means that during the necking stage the sample loading decreases in the zone O (out of the neck) and a plastic deformation is terminated in this region. The experimental strains for both phases, as well as the differences between them, were correctly predicted by the self-consistent model.

On the contrary, the stress in the neck does not decrease due to a narrowing of the sample section, leading to stress concentration in



**Fig. 7.** The evolution of phase lattice strains (left) and the difference between strains in the austenite and the ferrite  $\langle \epsilon_{RD} \rangle_{Aus-Fer}$  (right) as a function of position in the neck. The results for the scans in the A, B stages (sample TD) and C (sample ND) are shown respectively in panels (a), (b) and (c).





**Fig. 8.** The evolution of the lattice strains measured for different reflections in the ferrite (a) and the austenite (b) as a function of position in the neck (stage C/C' in sample ND).

this region. As shown in Fig. 6c and d, the volumes in the centre of the neck (point C) and close to the centre (point C') are subjected to a higher loading than in the pre-necking stage (both points C and C' are localised in the zone N, cf. Fig. 4b). The lattice strains in the neck centre (point C) follow the tendency of evolution before necking (Fig. 6c), and the difference between lattice strains in both phases  $\langle \epsilon_{RD} \rangle_{AUS - Fer}$  approaches to zero value (Fig. 6d). In point C', close to the centre and still in the N zone (Fig. 3b), the lattice strain is much smaller in the ferrite in comparison to that in the austenite (Fig. 6c), hence the difference between these strains  $\langle \epsilon_{RD} \rangle_{AUS - Fer}$  is large and positive (Fig. 6d). The significant heterogeneity of the stresses in the necking region will be discussed in the next section.

### 3.2. Mechanical behaviour inside the necking zone

Interesting evolutions of the lattice strains along the neck were observed analysing the diffraction data obtained from the three scans performed in the direction shown in Fig. 3a. The scans were performed for the deformation stages A, B and C as defined in Fig. 2. In Fig. 7 the lattice strains in both phases and the difference between strains in the austenite and in the ferrite  $\langle \epsilon_{RD} \rangle_{AUS - Fer}$  (Eq. (5)) are shown as a function of position in the neck. In the case of the scans done for the successive deformation stages A and B, the lattice strain in the ferrite is larger than in the austenite for the entire necking zone (negative value of  $\langle \epsilon_{RD} \rangle_{AUS - Fer}$ ). It can also be observed that in the centre of the neck the difference between the strains in both phases i.e. the absolute value of  $\langle \epsilon_{RD} \rangle_{AUS - Fer}$  decreases faster with deformation than for the other positions in the sample (compare the subsequent A and B stages in Fig. 7). This phenomenon can be easily explained due to the highest stress concentration as well as through the most advanced plastic deformation in the central region of the neck. Indeed, before the necking appearance the differences between the phase strains decreased for increasing applied stress and progressing sample deformation, as shown in Figs. 5 and 6.

To the contrary, an unexpected evolution of the difference between phase strains vs. position in the neck was determined for the scan C, for which the necking process was more advanced than in the case of stages A and B (cf. Fig. 2). The lattice strains in the centre of the neck (point C) are almost equal for both phases, while in the positions out of the centre (point C') a significant inversion of the phase strains occurred i.e. a much higher value of the strain was measured in the austenite than in the ferrite (Fig. 7c, on the right). Such strain inversion occurred over almost the whole necking zone, as was also observed by Baczmański et al. [29], when the measurements were conducted using neutron diffraction for a large volume of the neck. The transition of the load from the ferritic phase to the austenitic phase was explained by the possible damage process initiated in the ferrite. Hence, the information obtained previously from neutron diffraction measurement was confirmed using

a synchrotron measurement performed with a much better spatial resolution.

It is also interesting to discover if all the grains in the ferrite are responsible for the observed strain/stress inversion between phases. To this end, the lattice strains  $\langle \epsilon \rangle_{\{hkl\}}$  measured using different  $hkl$  reflections for both phases are presented in Fig. 8. As can be seen, the evolution of  $\langle \epsilon \rangle_{\{110\}}$  in the ferrite and all the strains in the austenite exhibit a similar variation vs. the position in the neck, while for the 211 and 200 reflections a sharp decrease of the  $\langle \epsilon \rangle_{\{211\}}$  and  $\langle \epsilon \rangle_{\{200\}}$  strains with an increasing distance from the centre is observed. This again confirms the results obtained with a neutron beam for which the important decrease of the lattice strains in the ferrite was observed for the 211 and 200 reflections close to the fracture of the sample, while the experimental lattice strains for the 110 reflection did not change significantly (cf. Fig. 10 in [29]).

It can be concluded that the ferritic grains having particular orientations and contribute to the 211 and 200 reflections, behaving differently to the other grains in the sample. As suggested in [29], the softening of the damaged grains leads to a reduction of the localised stresses and causes a transfer of the load to the other grains in the sample (mostly in the austenitic phase). However, as shown using synchrotron diffraction, this process depends on the position in the neck, therefore the reason of the determined spatial evolution of the strains in both phases should be explained.

In order to study the influence of the neck geometry on the stress and strain distributions, an FEM simulation was carried out with Abaqus CAE 6.13 software. The three-dimensional geometric model was built on the basis of the shape and dimensions of the necking zone determined for the deformed and broken sample (Fig. 7b). The simulation was performed within the elastic deformation stage of the studied material using anisotropic overall elastic constants previously determined by a self-consistent model. The overall stiffness tensor (given in Table 4) was calculated from single crystal elastic constants of each phase and accounting for the crystallographic texture.

Dynamic implicit analysis with a step time of 100 s was applied in the FEM calculations. A homogeneous uniform pressure of  $P = -80$  MPa was imposed on the two end sections of the sample (as shown in Fig. 9) to simulate the stress imposed by external loading during the tensile test. In order to balance the computation speed and the accuracy of the FEM simulation, two different mesh sizes were applied.

**Table 4**

Anisotropic elastic matrix determined using self-consistent method for experimental textures [17,29] and single crystal elastic constants given in Section 2.3.

$C_{11}$ [GPa]	$C_{22}$ [GPa]	$C_{33}$ [GPa]	$C_{12}$ [GPa]	$C_{13}$ [GPa]	$C_{23}$ [GPa]	$C_{44}$ [GPa]	$C_{55}$ [GPa]	$C_{66}$ [GPa]
261	265	252	99	112	108	84	88	74

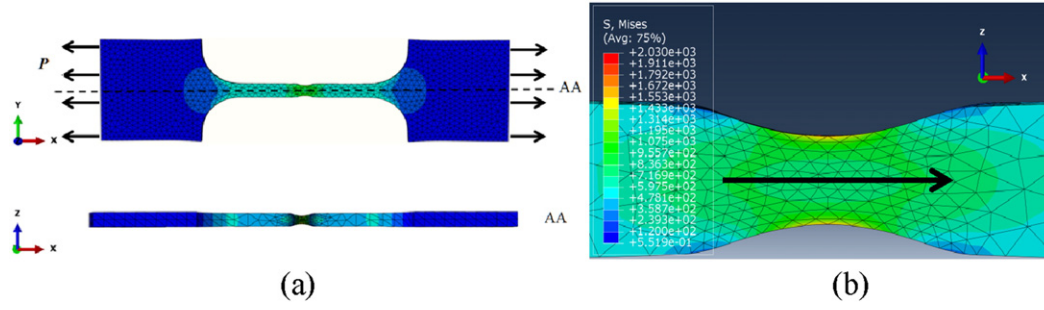


Fig. 9. Schematic drawing of a 3D model of the sample for FEM simulation (a) and spatial distribution of von Mises stress with the indicated scanning path direction (b).

On the out-necking area, the mesh with free structured tetrahedral element was used and the element seeds were assigned every 0.5 mm along the edge of the model. The same type of element was applied for the mesh of the in-necking area, but the distance between the element nodes was reduced to 0.05 mm in order to acquire a more accurate result along the necking zone. The macroscopic elastic tensor of the studied duplex steel was introduced into the model to account for elastic anisotropy of the sample. In the simulation performed in this work, mainly the influence of the neck shape on stress distribution was studied (a two-phase structure was not considered in the calculations).

The evolutions of the simulated principal stresses  $\sigma_{RD}^{FEM}$ ,  $\sigma_{TD}^{FEM}$  and  $\sigma_{ND}^{FEM}$  (shear stresses were negligible), longitudinal strain  $\epsilon_{RD}^{FEM}$  in the direction of the applied load and von Mises stress  $\sigma_{VM}^{FEM}$  as a functions of position along the neck are plotted in Fig. 10. Analysing the above plots it can be concluded that due to three-axiality of the stresses in the necking region, the maximum von Mises stress  $\sigma_{VM}^{FEM}$  and strain  $\epsilon_{RD}^{FEM}$  are not concentrated in the narrowest part of the neck but in the same distance from that place. Comparing Figs. 9 and 10 an interesting correlation was found between the difference between phase strains  $\langle \epsilon_{RD} \rangle_{AUS-Fer}$  determined from diffraction measurement and the value of von Mises equivalent stress  $\sigma_{Mises}^{FEM}$  obtained from the FEM simulation. Both quantities decrease significantly in the centre of the neck. The value of the difference between phase strains  $\langle \epsilon_{RD} \rangle_{AUS-Fer}$  increases and reaches a maximum at the distance of approximately 0.3 mm from the centre, and also the value of von Mises equivalent stress  $\sigma_{Mises}^{FEM}$  increases up to a maximum but at the distance of about 0.5 mm from the centre. Despite some disagreement concerning positions of the maxima, a good qualitative correlation between the measured  $\langle \epsilon_{RD} \rangle_{AUS-Fer}$  and simulated  $\sigma_{Mises}^{FEM}$  vs. position in the neck, indicates that the equivalent von Mises stress plays an important role in the softening of the ferrite and probably leads to the initiation of the damage process in this phase. The value of the von Mises macrostress increases at some distance from the neck centre due to three-axiality of the macrostress leading to more advanced evolution processes occurring in the phases.

Analysing the results obtained for different groups of diffracting grains, a good correlation can be seen between the lattice strains measured with all reflections available for the austenite, 110 reflection for the ferrite and calculated von Mises stress  $\sigma_{VM}^{FEM}$  as well as longitudinal

sample strain  $\epsilon_{RD}^{FEM}$  (cf. Figs. 9 and 10). Therefore, the stress distribution in the grains contributing to the above-mentioned reflections is characteristic for the shape of the deformation neck under the tensile load and can be explained by a geometrical effect, as predicted by the FEM calculations. However, the dependence of the lattice strains measured in the ferrite using 211 and 200 reflections exhibit a different dependence on the scanning position compared with the calculated von Mises stress  $\sigma_{VM}^{FEM}$  and strain  $\epsilon_{RD}^{FEM}$ . In this case, the highest measured strain is concentrated in the narrowest part of the neck and significantly decreases with the distance from this region. As previously mentioned, this effect can be caused by the damage occurring in the groups of grains contributing to the 211 and 200 reflections in the ferrite, as was previously observed using neutron diffraction [29].

#### 4. Conclusions

The main original issue of this work was the study of the stress and strain partitioning between the phases in duplex stainless steel, correlated with the damage process during the necking phenomenon. To do this, the lattice strains were scanned along the neck using in situ synchrotron diffraction during the tensile test and the experimental data were analysed using the self-consistent model and FEM simulation. A special high resolution of the synchrotron diffraction (small gauge volume) allowed studying the lattice strains evolution within the neck.

As a result, it was confirmed, that the elastoplastic deformation occurs differently for both phases of the aged UR45N stainless steel i.e. the yield stress for the austenite is much lower than for the ferrite (cf. [29]). It was found that the difference between the phase yield stresses strongly depends on the initial stresses in the phases. The initial stresses are heterogeneous in the studied material, as it was observed comparing the results obtained for the different samples.

On the basis of the performed study, the following conclusions concerning damage heterogeneity correlating with stress distribution in the deformation neck can be drawn:

- 1) For early stages of necking, the difference between the lattice strains in the austenite and the ferrite evolves more significantly in the neck centre (compared to beyond the centre) leading to an increase of

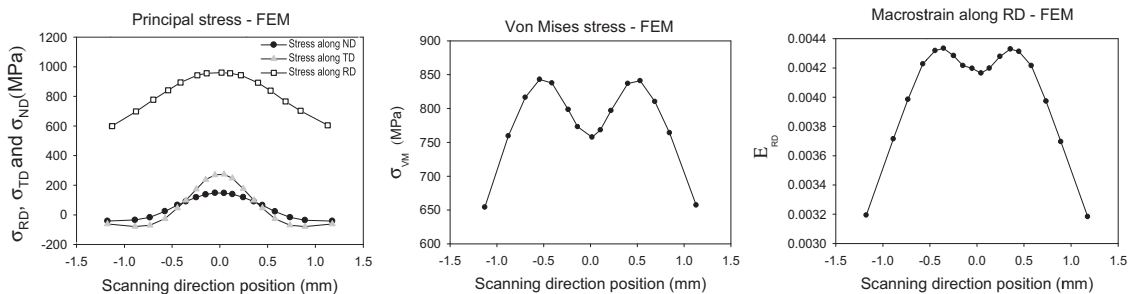


Fig. 10. Dependence of the principal stresses (a) von Mises stress (b) and longitudinal strain (c) on the position along the neck.

strains in the austenite and a decrease of strains in the ferrite. This tendency agrees with the evolution observed before necking and can be explained by the stress concentration in the narrowest region of the neck.

- 2) In the case of an advanced necking process, the mean strains in the ferrite decrease more significantly in the positions out of the neck centre, causing a load transfer to the austenite. As the result, the strains in the ferrite become lower than in the austenite for all positions measured along the neck, and the inversion in the strain partitioning between the phases is much more important than that extrapolated from the tendency before necking. These observation confirms the results obtained previously with neutron diffraction [29] and is explained by the damage process initiated in the ferritic phase.
- 3) It was observed that a stress relaxation process occurs mostly in the ferritic grains contributing to 200 and 211 reflections, and this conclusion also agrees with the previous neutron experiment [29]. Good spatial resolution of the synchrotron diffraction experiment enabled finding out that the maximum decrease of the lattice strains occurred at the distance 0.3 mm from the neck centre. This means that damage initiation depends both on the position in the neck and orientation of the grain lattice with respect to the applied load.
- 4) The spatial evolution of the lattice strains along the neck was compared with FEM simulations. A qualitative correlation between the variation of macroscopic von Mises stress and the difference between lattice strains in both phases suggest that the equivalent von Mises stress could be responsible for the processes occurring in the phases, especially for the softening (or damage) of particular grains in the ferrite.

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