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Bayesian Sparse Estimation of Migrating Targets for Wideband Radar

STÉPHANIE BIDON, Member IEEE JEAN-YVES TOURNERET, Senior Member IEEE University of Toulouse France

LAURENT SAVY ONERA France

FRANÇOIS LE CHEVALIER, Senior Member, IEEE Delft University of Technology The Netherlands

Wideband radar systems are highly resolved in range, which is a desirable feature for mitigating clutter. However, due to a smaller range resolution cell, moving targets are prone to migrate along the range during the coherent processing interval (CPI). This range walk, if ignored, can lead to huge performance degradation in detection. Even if compensated, conventional processing may lead to high sidelobes preventing from a proper detection in case of a multitarget scenario. Turning to a compressed sensing framework, we present a Bayesian algorithm that gives a sparse representation of migrating targets in case of a wideband waveform. Particularly, it is shown that the target signature is the sub-Nyquist version of a virtually well-sampled two-dimensional (2D)-cisoid. A sparse-promoting prior allows then this cisoid to be reconstructed and represented by a single peak without sidelobes. Performance of the proposed algorithm is finally assessed by numerical simulations on synthetic and semiexperimental data. Results obtained are very encouraging and show that a nonambiguous detection mode may be obtained with a single pulse repetition frequency (PRF).

Authors' addresses: S. Bidon, Institut Supérieur de l'Aéronautique et de l'Espace DEOS, 10 av. E. Belin, 31055 Toulouse cedex 4, FRANCE. E-mail: (sbidon@isae.fr). J.-Y. Tourneret, IRIT - ENSEEIHT – TéSA, 2 rue Camichel, BP 7122, 31071 Toulouse cedex 7, FRANCE. L. Savy, ONERA, DEMR, Chemin de la Hunière et des Joncherettes, BP 80100 FR-91123 Palaiseau cedex, France. F. Le Chevalier, TU Delft, EEMCS Building, Mekelweg 4, 2628 CD Delft, The Netherlands.

I. INTRODUCTION

Radar systems transmitting a train of pulses at constant pulse repetition frequency (PRF) are subjected to two types of ambiguities: range ambiguities when the PRF is too large to ensure that all echoes are received within the pulse repetition interval (PRI), and velocity ambiguities when the PRF is less than the Doppler spectrum width of the echoes [1]. The unambiguous range R_a and velocity v_a are linked by the fundamental relation

$$R_a v_a = c\lambda_c/4$$

with *c* the speed of light and λ_c the radar wavelength. It shows that one cannot increase the ambiguous range without decreasing the ambiguous velocity, and reciprocally, one cannot increase the ambiguous velocity without decreasing the ambiguous range. Therefore, in many radar applications, range and velocity of a target cannot be retrieved simultaneously without ambiguities [2]. In other words, when choosing the PRF, it is often not possible to comply with the Nyquist sampling criterion to measure both range and velocity of a target.

Radar designers have used different techniques to remove ambiguities and then reconstruct the observed scenario unambiguously. Most of them consist in transmitting several bursts with different PRFs and remove ambiguities via an implementation of the Chinese remainder theorem, e.g., [3]. Nevertheless, these methods entail several drawbacks.

On the other hand, wideband radar systems may offer an alternative and elegant solution to the problem of ambiguity removal [4]. Indeed, let us assume from now on that a low PRF (i.e., there are no range ambiguities but many velocity ambiguities occur) with a wide instantaneous bandwidth is considered. Due to the subsequent high range resolution, fast moving targets are prone to migrate during the coherent processing interval (CPI) leading to a range-velocity coupling. The received digitized signal can then be seen as a set of coherent observations in adjacent narrowband channels whose analog counterparts would be identical but whose (slow-time) sampling period would increase with the subband [5, 6]. Since a low PRF is under consideration, this means that on each subband the same signal is observed but with a linearly increasing aliasing phenomenon. From these undersampled observations, one may wonder if the signal can be reconstructed unambiguously. Hence, the problem of target detection in case of a constant low PRF wideband waveform arises naturally as a compressed sensing problem.¹

Compressed sensing or compressive sampling (CS) is a recently new signal processing paradigm that states that

¹We stress out here that we do not discuss in this paper the problem of sampling rate in the fast-time. This is also of great concern since for wideband waveform the number of samples in this dimension may be very high. Nonetheless, this work is concerned only with the problem arising when the slow-time domain is undersampled.

a sparse signal can be fully reconstructed from sub-Nysquist observations [7, 8]. It is generally a two-part problem where on one hand the undersampling scheme is studied and on the other hand reconstruction algorithms are designed to fully recover the low-rate observed signal. CS constitutes thus a genuine breakthrough and has been investigated in many domains of application; radar is obviously one of them [9-14]. In the case of our low PRF wideband signal, the observed data are naturally undersampled so that one is left here with the unambiguous reconstruction of the observed scenario. Assuming compressibility of the signals of interest (i.e., the targets), the reconstruction problem appears then as an ill-posed problem. So far, $\ell_{p>0}$ -norm minimization approaches have been mostly used to estimate the target scene in various radar applications: see [12,15] and references therein. Note also the ℓ_1 penalized least squares method applied to wideband signal in [16]. We propose here to regularize the estimation problem via a fully Bayesian approach where not only a sparsity inducing prior is used to describe the signals of interest but also the estimation process is led via a Monte-Carlo Markov chain (MCMC). A Bayesian framework has been favored in this work due to several advantages it has been offering [17]. Firstly, instead of providing only an estimate of the radar scenario, other parameters are also estimated (i.e., thermal noise power, average target power, level of sparsity). Moreover, not only point estimates are obtained but full posterior distributions are estimated which may be of interest to obtain measures of confidence for the estimates. Furthermore, in our case, only a few parameters have to be tuned by the radar operator. As introduced later, these parameters have a direct physical meaning, which renders the tuning comprehensible.

The remainder of the paper is organized as follows. In Section II, the conventional data model for a low PRF wideband signal is presented. Particularly, the signature of interest is interpreted as a bidimensional cisoid whose undersampling increases linearly with the subband. Then in Section III, assuming a clutter-free scenario, a hierarchical Bayesian model is presented where a sparse promoting prior is assumed to favor a sidelobeless representation of the targets. Minimum mean square error (MMSE) and maximum a posteriori (MAP) estimators are derived accordingly. Performance of the Bayesian estimators is then assessed in Sections IV and V via synthetic data and experimental data collected from the PARSAX radar system [18]. Section IV concludes with a discussion on upcoming extensions to this work.

II. SIGNAL MODEL FOR WIDEBAND RADAR

In this section, the data model for a wideband radar system is introduced. A particular focus is put on the scatterer signature that is shown to be the undersampled version of a virtual but well-sampled signal.

A. Radar System and Received Signals

The system under consideration is a pulsed-Doppler radar with wideband waveform. The radar sends a series of *M* pulses with PRF $f_r = 1/T_r$ where T_r is the PRI. By wideband we mean that the bandwidth *B* is nonnegligible compared with the carrier frequency $f_c = c/\lambda_c$. Furthermore, the range migration of each scatterer is assumed to be negligible within the duration T_p of a single pulse but may be significant during the whole CPI, viz

$$vT_p \ll \delta_R$$
 and $vMT_r \gg \delta_R$

where v is the (constant) radial velocity of the scatterer and $\delta_R = c/(2B)$ is the range resolution. A low PRF is considered so that no-range ambiguities occur but the maximal Doppler frequency is aliased, i.e., $2v_{\text{max}} f_c/c >$ $1/(2 T_r)$ where v_{max} represents the maximum target velocity expected for a scatterer.

Usually with narrowband radar, detection is performed range gate by range gate. Nevertheless, in case of a wideband waveform, moving targets migrate so that detection is more conveniently performed on low range resolution (LRR) segments consisting of the returns collected on *K* adjacent range gates [5, 19, 20]. Samples to be processed can thus be represented by a $K \times M$ matrix where the first and second dimensions refer, respectively, to the fast- and slow-time. However, the data model can be more conveniently expressed after applying a range transform (a simple fast Fourier transform (FFT)) on the fast-time. Thus, it is assumed in the following that the samples are expressed in the fast-frequency/slow-time domain.

In absence of clutter and in case of multiple scatterers in the scene, the $K \times M$ data matrix can finally be expressed as

$$Y = \sum_{t=1}^{N} \alpha_t A_t + N \tag{1}$$

where *N* is the receiver noise and *N*, α_t , and A_t represent, respectively, the number of scatterers, the *t*th complex amplitude, and signature. The receiver noise is assumed to be spectrally white on both dimensions and is modeled by a white Gaussian random signal with power σ^2 . The signature A_t is detailed in the next section.

Note that in the remainder of the paper, an equivalent vector notation is also used for (1), i.e.,

$$\mathbf{y} = \sum_{t=1}^{N} \alpha_t \boldsymbol{a}_t + \boldsymbol{n} \tag{2}$$

where each *KM*-length vector involved is the row-vectorization of its clearly identifiable matrix counterpart.

B. Scatterer Signature

1) Conventional Expression: The scatterer signature A involved in (1) has been studied earlier in e.g., [5, 19–21] and was shown to be the product of a two-dimensional

(2D) cisoid with cross-coupling terms. More precisely, the (k, m)th element of the matrix A can be expressed by

$$[A]_{k,m} = \exp\left\{j2\pi \left(-\tau_0 \frac{B}{K}k + \frac{2vf_c}{c}T_rm\right)\right\} (2D\text{-}cisoid)$$

$$\times \exp\left\{j2\pi \frac{2v}{c}\frac{B}{K}T_rkm\right\} (cross-coupling terms)$$
(3)

where τ_0 designates the initial round-trip delay of the scatterer. The 2D-cisoid in (3) is a conventional term that involves the usual range frequency $-\tau_0$ and the Doppler frequency $2v f_c/c$ associated, respectively, with the sampling periods B/K and T_r . The cross-coupling terms are specific to the wideband waveform and model the range migration. It is worth noticing that, aside from the system parameters, these terms depend only on the radial velocity v. More information may therefore be retrieved about the scatterer velocity in the case of a wideband waveform when compared with a narrowband waveform. Moreover, measuring velocity via range migration is unambiguous contrary to Doppler frequency measurement.

A simple and straightforward way to exploit this additional information is to sum coherently the samples of the target signature (3). The resulting estimated amplitude vector is given by [5, 22]

$$\hat{\boldsymbol{\alpha}}_{\mathrm{CI}} = \frac{\boldsymbol{a}^{H}\boldsymbol{y}}{\|\boldsymbol{a}\|_{2}^{2}} \tag{4}$$

and can be implemented efficiently via a Keystone-like transform [21, 23]. Unlike a conventional Doppler processing, the coherent integration (4) allows the gain on the target peak to be preserved [24]. However, high sidelobes remain at ambiguous velocities rendering the processing inadequate in case of a multitarget scenario. We propose hereafter a novel interpretation of (3) to more deeply exploit the information brought by the range migration.

2) Towards a Sparse Representation:

a) Interpretation of the scatterer signature: To go one step further with the expression of the scatterer signature, we rewrite the expression (3) as follows

$$[\mathbf{A}]_{k,m} = \exp\left\{j \ 2\pi \left(-\tau_0 \frac{B}{K}k + \frac{2vf_c}{c}T_{r,k}m\right)\right\}$$
(5)

where

$$T_{r,k} = \left(1 + \frac{B}{Kf_c}k\right)T_r.$$
(6)

Looking carefully at these two expressions, it appears that for a given subband k, the scatterer signal is a 1D-cisoid with the same Doppler frequency as in (3) but with a subband-dependent sampling period $T_{r,k}$ which increases linearly with the subband index. As a low PRF has been previously assumed, this means that aliasing on the slow-time occurs and increases with the subband index too. This phenomenon is illustrated in Fig. 1 where a 1D-sine has been represented K times but with a linearly



Fig. 1. Observation and resampling of a cisoid. Solid line represents analog version of cisoid with frequency $2vf_c/c$. Circle markers represent observed data with period $T_{r,k}$. Square markers represent samples of cisoid obtained with thinner period \bar{T}_r independent of subband index k.

increasing sampling period (circle markers). As can be observed, the higher the subband index, the slower the observed sine.

b) Shannon reconstruction: According to the Shannon reconstruction theorem [25], each element $[A]_{k,m}$ can be written via the following interpolation formula

$$[\mathbf{A}]_{k,m} = \sum_{\bar{m}=-\infty}^{+\infty} [\bar{\mathbf{A}}]_{k,\bar{m}} \operatorname{sinc} \left\{ \pi \left(m \frac{T_{r,k}}{\bar{T}_r} - \bar{m} \right) \right\}$$
(7)

where \bar{T}_r is a sampling period that complies with the sampling theorem, i.e.,

$$\frac{2v_{\max}f_c}{c} < \frac{1}{2\bar{T}_r} \tag{8}$$

and \bar{A} is the 2D-cisoid with frequency pair $(-\tau_0, 2vf_c/c)$ and sampling periods $(B/K, \bar{T}_r)$

$$[\mathbf{A}]_{k,\bar{m}} = \exp\left\{j \ 2\pi \left(-\tau_0 \frac{B}{K}k + \frac{2vf_c}{c}\bar{T}_r\bar{m}\right)\right\}.$$
 (9)

For a given subband k, the signal (9) corresponds to the same 1D-cisoid as in (5) but this time with a constant sampling rate $\bar{f}_r = 1/\bar{T}_r$ chosen large enough to avoid aliasing. Such samples are represented in Fig. 1 with square markers. Interestingly, the virtual samples $[\bar{A}]_{k,\bar{m}}$ in (9) correspond to data that would be received by a narrowband radar (no range migration) with virtual sampling period \bar{T}_r . By defining a new sampling period, one defines also a new ambiguous velocity $\bar{v}_a = cf_0/(2\bar{f}_r)$ larger than the initial ambiguous velocity v_a . Thus, if one had access to samples $[\bar{A}]_{k,\bar{m}}$ and taking into account the condition (8), one would have a nonambiguous mode. In the remainder of this paper, we are interested in estimating such samples. However, prior to that, it is worth noticing that the formula (7) involves for each subband k an infinite number of samples $\{[\bar{A}]_{k,\bar{m}}\}_{\bar{m}\in\mathbb{Z}}$. To make the estimation

possible, we use a truncated version of (7), viz

$$[\bar{A}]_{k,m} \stackrel{\Delta}{=} \sum_{\bar{m}=0}^{\bar{M}-1} [\bar{A}]_{k,\bar{m}} \operatorname{sinc} \left\{ \pi \left(m \frac{T_{r,k}}{\bar{T}_r} - \bar{m} \right) \right\}$$
(10)

with \overline{M} the number of virtual pulses considered. It is chosen to ensure that for each subband, (10) is actually an interpolation and not an extrapolation formula, namely

$$\bar{M} \ge \left\lceil M \left(1 + \frac{B}{f_c} \frac{K - 1}{K} \right) \frac{T_r}{\bar{T}_r} \right\rceil \tag{11}$$

where $\lceil \cdot \rceil$ denotes the operator that rounds towards plus infinity. Note that \overline{M} could be chosen as a subband-dependent parameter. However, for the sake of simplicity this route is not taken here.

Applying the truncated-interpolation formula (10) to each scatterer involved in the received signal (1) yields

$$[Y]_{k,m} = \sum_{\bar{m}=0}^{\bar{M}-1} [\bar{\Lambda}]_{k,\bar{m}} \operatorname{sinc} \left\{ \pi \left(m \frac{T_{r,k}}{\bar{T}_r} - \bar{m} \right) \right\} + [N]_{k,m}$$
(12)

where $\bar{\Lambda}$ is a $K \times \bar{M}$ matrix representing the N scatterers sampled virtually on the slow-time at \bar{T}_r , i.e.,

$$\bar{\mathbf{\Lambda}} = \sum_{t=1}^{N} \alpha_t \bar{\mathbf{A}}_t.$$

A row-vectorized version of (12) gives then

$$y = T\bar{\lambda} + n \tag{13}$$

where $\bar{\boldsymbol{\lambda}}$ is the vector notation for $\bar{\boldsymbol{\Lambda}}$ and T is a

 $KM \times K\overline{M}$ block-diagonal matrix $\begin{pmatrix} T_0 & 0 \\ \ddots & \\ 0 & T_{K-1} \end{pmatrix}$ whose

block T_k is an $M \times \overline{M}$ interpolation-matrix defined by

$$[\mathbf{T}_k]_{m,\bar{m}} = \operatorname{sinc}\left\{\pi\left[m\frac{T_{r,k}}{\bar{T}_r} - \bar{m}\right]\right\}.$$

c) Expression in the fast-time/slow-frequency: In (13), the $K\bar{M}$ -length vector $\bar{\lambda}$ entails the virtual but well-sampled signatures (9) of the N scatterers present in the observation. As underlined before, if one could have access to this vector, targets could be detected unambiguously. However, estimating $\overline{\lambda}$ from (13) is an ill-posed problem as $M \ll \overline{M}$. A common way to regularize this problem is to enforce sparsity on the unknown vector $\overline{\lambda}$ while minimizing the distance between the observation y and the model $T\bar{\lambda}$. However, this approach cannot be applied directly as $\overline{\lambda}$ does not have a sparse nature (it is a sum of 2D-cisoids). A solution consists in expressing $\bar{\lambda}$ in the fast-time/slow-frequency domain where sparsity can be invoked as each scatterer is then ideally represented in this domain by a single peak located around $(-\tau_{0,t}, 2v_t f_c/c)$. Reformulating accordingly the estimation problem leads to

$$y = Hx + n \tag{14}$$

with

$$\boldsymbol{H} = \boldsymbol{T} \boldsymbol{F}^{-1} \tag{15a}$$

$$\boldsymbol{x} = \boldsymbol{F}\bar{\boldsymbol{\lambda}} \tag{15b}$$

where F is the matrix that transforms $\overline{\lambda}$ from the fast-frequency/slow-time domain to the fast-time/slow-frequency domain. More precisely, the matrix F is given by

$$\boldsymbol{F} = \boldsymbol{F}_{K}^{-1} \otimes \boldsymbol{F}_{\bar{M}} \tag{16}$$

where \otimes represents the Kronecker tensor product and F_{Δ} is the $\Delta \times \Delta$ discrete Fourier transform matrix, i.e.,

$$\boldsymbol{F}_{\Delta}(\delta_1, \delta_2) = \frac{1}{\sqrt{\Delta}} \exp\left\{-j2\pi \frac{\delta_1 \delta_2}{\Delta}\right\}; \delta_{1,2} \in \{0, \dots, \Delta-1\}.$$

Note that in the CS literature, T is often referred to as the measurement or sensing matrix while F^{-1} is the sparsifying or representing dictionary (the dictionary is complete here as F^{-1} is a square matrix). Nonetheless, the matrix T involved in (14) is neither a random matrix nor is optimized to decrease the mutual coherence with the representation matrix [26]. Instead, T stems from our reconstruction design and does not claim any optimality.

To illustrate that the vector x in (14) is a good candidate to give a sparse representation of the targets, it is interesting to consider a no-basis mismatch case arising when the scatterer frequencies correspond to the frequency points defined by the matrix F in (16), i.e., when there exists $(k_t, \bar{m}_t) \in \{0, ..., K - 1\} \times \{0, ..., M - 1\}$ such that

$$\left(-\tau_t, \frac{2\upsilon_t f_c}{c}\right) = \left(\frac{-k_t}{K} \times \frac{K}{B}, \frac{\bar{m}_t}{\bar{M}} \times \bar{f}_r\right).$$
(17)

When (17) is verified it is straightforward to show that x has exactly N non-zero elements with value $\sqrt{K\bar{M}}\alpha_t$. In light of this remark, the regularization principle based on sparsity can therefore be invoked to solve the problem (14). As stated earlier in Section I, sparsity on x is enforced in this work by assigning an appropriate prior promoting sparsity for each element of the vector. We present in the next section the whole Bayesian model adopted for the estimation problem. It is an extension of a former model used for deconvolution of seismic data [27] and for magnetic resonance force microscopy imaging [28] to the case of complex radar data.

III. HIERARCHICAL BAYESIAN MODEL AND ESTIMATION

A. Hierarchical Bayesian Model

Starting from the observation vector *y* and the linear system in (14), a hierarchical Bayesian model is proposed where prior probability distributions are assigned to the unknown model parameters. As done conventionally, these priors are chosen to reflect our degree of knowledge or uncertainty about the unknowns while ensuring mathematical tractability when deriving the posterior



Fig. 2. Graphical representation of proposed Bayesian model.

distributions. The whole model is represented in the direct acyclic graph of Fig. 2 and described hereafter from the bottom to the top of the graph.

Remark 1 (Notations: vector norm). For $p \in \mathbb{N}^*$ and $\mathbf{x} \in \mathbb{C}^m$ the *p*th norm of \mathbf{x} is defined by $\|\mathbf{x}\|_p$ $= \left(\sum_{i=1}^m |x_i|^p\right)^{1/p}$. If p = 0, the norm is defined as the number of non-zero vector elements, i.e., $\|\mathbf{x}\|_0 = \# \{i \in \{1, \ldots, m\} | x_i \neq 0\}$.

1) Likelihood: As stated in Section II, the thermal noise n is assumed to be a white Gaussian noise, denoted as $n \sim CN(0, \sigma^2 I_{KM})$ with I_{ξ} the $\xi \times \xi$ identity matrix. In other words, when x and σ^2 are known, the observation vector is Gaussian distributed, i.e., $y|x, \sigma^2 \sim CN(Hx, \sigma^2 I_{KM})$. The likelihood is then given by²

$$f(\mathbf{y}|\mathbf{x},\sigma^2) \propto \frac{1}{\sigma^{2KM}} \exp\left\{-\frac{\|\mathbf{y} - \mathbf{H}\mathbf{x}\|_2^2}{\sigma^2}\right\}$$
(18)

where \propto means proportional to.

2) *Parameters:* The next level of our model consists in defining the prior probability density functions (pdfs) of the thermal noise power σ^2 and the $K\bar{M}$ -length vector \mathbf{x} .

a) Prior of σ^2 : On the mathematical point of view, a convenient prior for σ^2 is an inverse-Gamma pdf which belongs to the family of conjugate priors with respect to (wrt) (18) [29]. This pdf is denoted by $\sigma^2 |\gamma_0, \gamma_1 \sim I \mathcal{G}(\gamma_0 \gamma_1)$ and is given by

$$f(\sigma^2|\gamma_0,\gamma_1) \propto \frac{e^{-\gamma_1/\sigma^2}}{(\sigma^2)^{\gamma_0+1}} \mathbb{I}_{[0,+\infty)}(\sigma^2)$$
(19)

where $\mathbb{I}_A()$ denotes the indicator function of the set A (i.e., $\mathbb{I}_A(x)=1$ if $x \in A$ and $\mathbb{I}_A(x)=0$ otherwise), γ_0 and γ_1 represent, respectively, the scale and shape parameters of the distribution. Then, with an adequate choice for the values of (γ_0, γ_1) , the mean and variance of $\sigma^2 | \gamma_0, \gamma_1$ can be set in accordance with our degree of prior belief about the thermal noise level [30]. For instance, in case of finite

mean m_{σ^2} and variance v_{σ^2} , one has

$$\gamma_0 = \frac{m_{\sigma^2}^2}{v_{\sigma^2}} + 2$$
 (20a)

$$\gamma_1 = m_{\sigma^2} \left(\frac{m_{\sigma^2}^2}{v_{\sigma^2}} + 1 \right). \tag{20b}$$

Particularly for radar applications, the thermal noise power level is often known with a good accuracy as it consists mainly of the receiver thermal noise [1, 31]. Thus, it is reasonable to use (20). Note that the case of a noninformative prior, i.e., when $(\gamma_0, \gamma_1) = (0, 0)$, has been presented in [6] and it also gave good performance for the studied scenario.

b) Prior of x: Assigning a prior pdf to x is a critical step in the design of our model. For complex data and given the likelihood function (18), a Bernoulli-complex Gaussian distribution appears to be suitable to enforce sparsity in the vector x and to ensure simplicity of the resulting posterior distribution [27, 32, 33]. To be more specific we have assumed that the elements of x, denoted by $x_i = [x]_i$ for $i = 0, ..., K\overline{M} - 1$, are a priori independent and such that

$$f(x_i|w, \sigma_x^2) = (1-w)\,\delta(|x_i|) + w\,\frac{1}{\pi\sigma_x^2}\exp\left\{-\frac{|x_i|^2}{\sigma_x^2}\right\}$$
(21)

with $w \in [0, 1]$ and $\sigma_x^2 > 0$. The pdf (21), denoted by $x_i | w, \sigma_x^2 \sim \text{Ber CN}(w, 0, \sigma_x^2)$, is tantamount to assuming that, at the *i*th frequency point of analysis, there is no scatterer in the data with a probability (1 - w), while with a probability w there is a scatterer with power³ σ_x^2 . We stress here that compared with other sparsity inducing priors such as a Laplacian prior [34], samples generated according to (21) can be exactly equal to 0 and that the probability of having a zero element is controlled by the value (1 - w). Recalling the assumption of independence of the x_i s, the prior distribution of x is given by

$$f(\boldsymbol{x}|w,\sigma_x^2) = (1-w)^{n_0} \left(\frac{w}{\pi\sigma_x^2}\right)^{n_1} \\ \times \exp\left\{-\frac{\|\boldsymbol{x}\|_2^2}{\sigma_x^2}\right\} \prod_{i/x_i=0} \delta(|x_i|) \quad (22)$$

where $\delta()$ is the Dirac delta function and

$$n_1 = \|\mathbf{x}\|_0$$
 and $n_0 = K\bar{M} - \|\mathbf{x}\|_0$. (23)

As both the occupancy level *w* and the scatterer power σ_x^2 are not known, another level is defined in the hierarchical model as detailed hereafter.

²Note that throughout the paper, constant parameters (e.g., the matrix H) are not systematically written in the conditional terms for notational convenience.

³It is observed later that σ_x^2 can be indeed seen as the postprocessing scatterer power.

3) Hyperparameters:

a) Prior of w: A uniform distribution is chosen for the weight *w*, denoted as $w \sim U_{[0,1]}$, i.e.,

$$f(w) = \mathbb{I}_{[0,1]}(w)$$
 (24)

reflecting the absence of knowledge about w.

b) Prior of σ_x^2 : Concerning the power level σ_x^2 and according to (21), an inverse-Gamma prior is suitable for further derivation (the same remark was made for the prior of σ^2). It is denoted as $\sigma_x^2 | \beta_0, \beta_1 \sim \mathcal{IG}(\beta_0, \beta_1)$ and is given by

$$f\left(\sigma_x^2 \middle| \beta_0, \beta_1\right) \propto \frac{e^{-\beta_1/\sigma_x^2}}{\sigma_x^{2(\beta_0+1)}} \mathbb{I}_{(0,+\infty)}\left(\sigma_x^2\right)$$
(25)

where β_0 , β_1 are, respectively, the shape and scale parameters. They correspond to the last level of the hierarchical model and are considered as constants set by the radar operator. To choose conveniently their values and thus incorporate adequately prior information about σ_x^2 in the model, the following remarks are appropriate. Firstly, according to (21), one has

$$\mathcal{E}\{|x_i|^2 | x_i \neq 0\} = \sigma_x^2$$
(26)

where \mathcal{E} {} is the mathematical expectation. In absence of basis mismatch (17), one also has

$$\mathcal{E}\{|x_i|^2 | x_i \neq 0\} = K\bar{M} \times \mathcal{E}\{|\alpha_t|^2\}$$
(27)

indicating that $\sigma_x^2/(K\bar{M})$ can be seen as the average scatterer power $\mathcal{E}\{|\alpha_t|^2\}$ before processing. Furthermore, since β_1 is a scale parameter, it is straightforward to show that $\sigma_x^2/(K\bar{M})|\beta_0, \beta_1 \sim \mathcal{IG}(\beta_0, \beta_1/(K\bar{M}))$. Hence, when the radar operator has reliable information about the target power $\mathcal{E}\{|\alpha_t|^2\}$ —e.g., via the radar equation [1]—that can be transposed in terms of finite mean $m_{\sigma_x^2/(K\bar{M})}$ (i.e., $\beta_0 > 1$) and variance $v_{\sigma_x^2/(K\bar{M})}$ (i.e., $\beta_0 > 2$), the shape and scale parameters of (25) can be chosen as follows

$$\beta_0 = \frac{m_{\sigma_x^2/(K\bar{M})}^2}{v_{\sigma_x^2/(K\bar{M})}} + 2$$
(28a)

$$\beta_1 = K\bar{M} \, m_{\sigma_x^2/(K\bar{M})} \left(\frac{m_{\sigma_x^2/(K\bar{M})}^2}{v_{\sigma_x^2/(K\bar{M})}} + 1 \right).$$
(28b)

When less or no reliable information is available about the target power, a flat prior can be chosen instead. For instance, when β_0 , $\beta_1 \rightarrow 0$, the pdf reduces to a noninformative Jeffrey's distribution [30]. A moderately informative prior is considered later for the numerical simulations allowing for a wide range of target powers. This completes the description of our hierarchical model.

B. Bayesian Estimation

Given the Bayesian model described by the set of equations (14), (18), (19), (21), (24), and (25), we propose to derive two conventional Bayesian estimators for the parameter of interest x, namely the MMSE and the MAP

estimators [29, 35]. They are respectively defined as the mean of the posterior distribution and the argument that maximizes this distribution. For the parameter of interest x, they are thus defined as follows

$$\hat{\mathbf{x}}_{\text{MMSE}} = \int \mathbf{x} f(\mathbf{x}|\mathbf{y}) d\mathbf{x}$$
(29a)

$$\hat{\boldsymbol{x}}_{\text{MAP}} = \arg\max f(\boldsymbol{x}|\boldsymbol{y}).$$
 (29b)

Both rely on the posterior distribution f(x|y) that, according to our hierarchical model, is given by (see the Appendix)

$$f(\mathbf{x}|\mathbf{y}) \propto \frac{B(1+n_1, 1+n_0)\Gamma(\beta_0+n_1)\prod_{i/x_i=0}\delta(|x_i|)}{\left(\beta_1+\|\mathbf{x}\|_2^2\right)^{\beta_0+n_1}\left[\|\mathbf{y}-\mathbf{H}\mathbf{x}\|_2^2+\gamma_1\right]^{KM+\gamma_0}}$$
(30)

where B(.) and $\Gamma()$ are the Beta and Gamma functions, respectively.

Looking at (30), it seems intractable to derive analytically the MMSE or MAP estimators (29). Moreover, the pdf of $\mathbf{x}|\mathbf{y}$ (30) does not correspond to a known distribution, making the generation of samples according to $\mathbf{x}|\mathbf{y}$ not straightforward. We propose therefore to use a common simulation method known as MCMC [29]. More precisely, a multistage Gibbs sampler is implemented [29]. Given our data model, it consists in generating iteratively samples ($\sigma^{2(n)}, w^{(n)}, \sigma_x^{2(n)}, \mathbf{x}^{(n)}$) that are distributed according to their respective conditional posterior distributions. After a burn-in period, denoted as N_{bi} samples, each subsequence $\theta^{(n)4}$ is distributed according to the posterior distribution $\theta|\mathbf{y}$. Collecting enough samples, say a number of N_r , the MMSE and MAP estimators of \mathbf{x} can then be approximated as

$$\boldsymbol{x}_{\text{MMSE}} \stackrel{\Delta}{=} \frac{1}{N_r} \sum_{n=1}^{N_r} \boldsymbol{x}^{(n+N_{bi})}$$
(31a)

$$\hat{\boldsymbol{x}}_{\text{MAP}} \stackrel{\Delta}{=} \arg \max_{\{\boldsymbol{x}^{(n+N_{bi})}\}_{n=1}^{N_r}} f(\boldsymbol{x}^{(n)}|\boldsymbol{y}).$$
(31b)

Note that while the posterior pdf of x (30) is too complex to obtain a closed-form expression of the MAP estimator (29b), its expression is necessary to derive (31b) with the sampler. The four iterative steps of our MCMC method are detailed in the next section and summarized in Fig. 3.

1) Gibbs Sampler: The Gibbs sampler considered in this work generates iteratively each chain parameter θ according to its posterior distribution. This distribution can be easily obtained from the joint posterior pdf of σ^2 , \mathbf{x} , w, $\sigma_x^2 | \mathbf{y}$ whose expression follows from the Bayes theorem

⁴The notation θ designates successively σ^2 , w, σ_r^2 and x.

 $\begin{array}{l} \text{Require: } y, H(\text{i.e., } \bar{M}, \bar{f}_r), (\gamma_0, \gamma_1), (\beta_0, \beta_1) \\ \text{Ensure: } \hat{\sigma}^2_{\text{MMSE, }}, \hat{w}_{\text{MMSE, }}, \hat{\sigma}^2_{\text{MMSE, }}, \hat{x}_{\text{MMSE, }}, \hat{x}_{\text{MAP}} \\ \{ \text{Initialization} \} \\ w^{(0)} \sim \mathcal{U}_{[0,1]} \\ \sigma_x^{(0)} \sim \Pi \mathcal{G}(\beta_0, \beta_1) \\ x^{(0)} \sim \Pi_{i=0}^{K\bar{M}-1} \mathcal{B}er \, \mathcal{CN} \left(w^{(0)}, 0, \sigma_x^{2^{(0)}} \right) \\ \{ \text{Iterations} \} \\ \text{for } n = 1 \text{ to } N_{bi} + N_r \text{ do} \\ \sigma^{2^{(n)}} \sim f(\sigma^2 | \boldsymbol{y}, \boldsymbol{x}^{(n-1)}) / *step 1* / \\ w^{(n)} \sim f(w | \boldsymbol{x}^{(n-1)}) / *step 2* / \\ \sigma_x^{2^{(n)}} \sim f(\sigma_x^2 | \boldsymbol{x}^{(n-1)}) / *step 3* / \\ x^{(n)} \sim f(x | \boldsymbol{y}, w^{(n)}, \sigma_x^{2^{(n)}}, \sigma^{2^{(n)}}) / *step 4* / \\ \text{end for} \\ \{ \text{Estimators} \} \\ \hat{\theta}_{\text{MMSE}} = \frac{1}{N_r} \sum_{n=1}^{N_r} \theta^{(n+N_{bi})} \\ \hat{x}_{\text{MAP}} = \arg \max_{\boldsymbol{x}^{(n>N_{bi})}} f(\boldsymbol{x}^{(n)} | \boldsymbol{y}) \end{array}$

Fig. 3. Multi-stage Gibbs sampler. Initialization step given as example: convergence of sampler can be reached independently of initial conditions [29].

$$f(\sigma^{2}, w, \boldsymbol{x}, \sigma_{x}^{2} | \boldsymbol{y}) \propto f(\boldsymbol{y} | \boldsymbol{x}, \sigma^{2}) f(\boldsymbol{x} | w, \sigma_{x}^{2}) f(w) f(\sigma_{x}^{2}) f(\sigma^{2})$$

$$\propto \frac{e^{-[\|\boldsymbol{y} - \boldsymbol{H}\boldsymbol{x}\|_{2}^{2} + \gamma_{1}]/\sigma^{2}}}{\sigma^{2(KM + \gamma_{0} + 1)}} \mathbb{I}_{(0, +\infty)}(\sigma^{2})$$

$$\times \frac{e^{-[\beta_{1} + \|\boldsymbol{x}\|_{2}^{2}]/\sigma_{x}^{2}}}{(\sigma_{x}^{2})^{\beta_{0} + n_{1} + 1}} \mathbb{I}_{(0, +\infty)}(\sigma_{x}^{2})$$

$$\times (1 - w)^{n_{0}} w^{n_{1}} \mathbb{I}_{[0, 1]}(w)$$

$$\times \prod_{i/x_{i}=0} \delta(|x_{i}|). \qquad (32)$$

Since (19), (21), (24), and (25) have been carefully selected among a family of conjugate priors, the Gibbs moves associated with (32) are simple to implement.

a) First move: Using (32), the conditional posterior distribution of $\sigma^2 | \mathbf{x}, w, \sigma_x^2, \mathbf{y}$ is given by

$$f(\sigma^2|\mathbf{y}, w, \mathbf{x}, \sigma_x^2) \propto \frac{e^{-\left[\|\mathbf{y} - H\mathbf{x}\|_2^2 + \gamma_1\right]/\sigma^2}}{\sigma^{2(KM + \gamma_0 + 1)}} \mathbb{I}_{(0, +\infty)}(\sigma^2)$$

where one recognizes the following inverse-Gamma distribution

$$\sigma^{2}|\mathbf{y}, w, \mathbf{x}, \sigma_{x}^{2} \\ \sim \mathcal{IG}(KM + \gamma_{0}, \|\mathbf{y} - \mathbf{H}\mathbf{x}\|_{2}^{2} + \gamma_{1})$$
 /* step 1 */

b) Second move: Looking at (32), it is straightforward to show that

$$f\left(w \left| \boldsymbol{y}, \boldsymbol{x}, \sigma_x^2, \sigma^2 \right) \propto (1-w)^{n_0} w^{n_1} \mathbb{I}_{[0,1]}(w)$$

One recognizes a Beta distribution with parameters $(1 + n_1, 1 + n_0)$, i.e.,

$$w|y, x, \sigma_x^2, \sigma^2 \sim Be(1+n_1, 1+n_0)$$
 /* step 2 */

according to which it is easy to sample.

c) Third move: According to (32), the conditional distribution of $\sigma_x^2 | \mathbf{y}, \mathbf{x}, \sigma^2, w$ is

$$f\left(\sigma_x^2 \middle| \boldsymbol{y}, \boldsymbol{x}, \sigma^2, w\right) \propto \frac{e^{-\left[\beta_1 + \|\boldsymbol{x}\|_2^2\right]/\sigma_x^2}}{\left(\sigma_x^2\right)^{\beta_0 + n_1 + 1}} \mathbb{I}_{[0, +\infty)}\left(\sigma_x^2\right)$$

from which one recognizes an inverse-Gamma distribution, i.e.,

.

$$\sigma_x^2 | \boldsymbol{y}, \boldsymbol{x}, \sigma^2, w \sim \mathcal{IG} \left(\beta_0 + n_1, \beta_1 + \|\boldsymbol{x}\|_2^2 \right) \quad /* \operatorname{step} 3 * / .$$

d) Fourth move: The last move of the Gibbs sampler consists of generating samples according the conditional distribution of the $K\bar{M}$ -length vector $\boldsymbol{x}|\boldsymbol{y}, \sigma^2, w, \sigma_x^2$ given by

$$f(\mathbf{x}|\mathbf{y}, \sigma^2, w, \sigma_x^2) \propto \exp\left\{-\frac{\|\mathbf{y} - \mathbf{H}\mathbf{x}\|_2^2}{\sigma^2} - \frac{\|\mathbf{x}\|_2^2}{\sigma_x^2}\right\}$$
$$\times (1 - w)^{n_0} \left(\frac{w}{\sigma_x^2}\right)^{n_1} \times \prod_{i/x_i=0} \delta(|x_i|)$$

where $n_1 = ||\mathbf{x}||_0$. We proceed as in [27, 28] where the Gibbs move is decomposed into univariate simulations which is tantamount to generating the vector \mathbf{x} element-by-element. Following the same path as in [27, 28], one can show that the *i*th element of \mathbf{x} is distributed according to a Bernoulli-complex Gaussian distribution with parameters (w_i, μ_i, η_i^2) , i.e., for $i \in \{0, \dots, K\bar{M}-1\}$

$$f\left(x_{i} \mid \boldsymbol{y}, \sigma^{2}, w, \boldsymbol{x}_{-i}, \sigma_{x}^{2}\right) = (1 - w_{i})\delta(|x_{i}|) + w_{i}\Phi\left(x_{i} \mid \mu_{i}, \eta_{i}^{2}\right)$$
(33)

where x_{-i} is the vector x whose *i*th element has been removed and the function $\Phi(.|\mu_i, \eta_i^2)$ denotes the univariate complex Gaussian pdf with mean μ_i and variance η_i^2 , i.e.,

$$\Phi(x_i | \mu_i, \eta_i^2) = \frac{1}{\pi \sigma_x^2} \exp\left\{-\frac{|x_i - \mu_i|^2}{\eta_i^2}\right\}$$

The variance and mean involved in (33) are given by

$$\begin{cases} \eta_i^2 = \left\{ \frac{1}{\sigma_x^2} + \frac{\|\boldsymbol{h}_i\|_2^2}{\sigma^2} \right\} \\ \mu_i = \frac{\eta_i^2}{\sigma^2} \boldsymbol{h}_i^H \boldsymbol{e}_i \end{cases}$$

where h_i is the *i*th column of H and e_i is equal to

$$e_i = y - \sum_{j \neq i} x_j h_j$$

The weight w_i in (33) is defined so that the equality sign holds in (33), i.e.,

$$w_i = \frac{w \frac{\eta_i^2}{\sigma_x^2} \exp\left\{\frac{|\mu_i|^2}{\eta_i^2}\right\}}{(1-w) + w \frac{\eta_i^2}{\sigma_x^2} \exp\left\{\frac{|\mu_i|^2}{\eta_i^2}\right\}}$$

To summarize, the fourth Gibbs move is defined as follows

$$\forall i \in \{0, \dots, K\bar{M} - 1\}, \\ x_i | \mathbf{y}, \sigma^2, w, \mathbf{x}_{-1}, \sigma_x^2 \sim Ber \mathcal{CN}(w_i, \mu_i, \eta_i^2). /* \operatorname{step} 4 * /$$

Remark 2 (Details of implementation). Note that to update efficiently the coordinate x_i at the *n*th iteration of the Gibbs sampler, we proceed as in [28, Appendix B]. By doing so, the computationally intensive matrix product Hxis derived only once at the initialization of the sampler (n = 0). Also given the particular nature of $H = TF^{-1}$ (15a), the product $F^{-1}x^{(0)}$ is firstly performed via an FFT and an inverse FFT on, respectively, *K* and \overline{M} points. Then, the block-diagonal nature of the matrix *T* is taken into account to avoid unnecessary null-products when computing $T \times [F^{-1}x^{(0)}]$.

IV. NUMERICAL SIMULATIONS

The performance of the proposed estimators \hat{x}_{MAP} and \hat{x}_{MMSE} defined in (31) is firstly assessed with synthetic radar data generated according to (1). Results are compared with that of an ℓ_1 penalized least squares approach which is more conventional when dealing with sparse recovery. More specifically, the ACAMP (adaptive complex approximate message passing) method has been chosen [14, 36, 37]. ACAMP is an iterative thresholding technique that uses a few computations per iteration and offers an adaptive way to optimally set its threshold parameter [14].

A. Simulation Parameters

1) Reference Scenario: The received signal entails N = 10 scatterers whose velocities and initial positions satisfy the no-basis mismatch assumption (17). The scatterers actually represent five targets since three of them are extended in range. For each scatterer, the signal-to-noise ratio (SNR) prior to processing is defined as

$$SNR_t = \frac{\mathcal{E}\{|\alpha_t|^2\}}{\sigma^2} \frac{\|\boldsymbol{a}_t\|_2^2}{KM}.$$

Location and SNR of each scatterer is represented in Fig. 4. Note that the considered SNRs are below the thermal noise level and that the gain of integration is $10 \log_{10}(KM) \approx 24$ dB. Also, the argument of the amplitude α_t for t = 1, ..., N is drawn from a uniform distribution in $[0, 2\pi)$. Other parameters of interest describing the radar scenario are depicted in Table I.

2) Processing Parameters: To process the wideband radar signal with our Bayesian method several parameters need to be adjusted. The virtual sampling frequency $\overline{f_r}$ is chosen 1) high enough to ensure that a target with maximum velocity v_{max} can be estimated without aliasing, and 2) not too high to limit the computational load that is related directly to the length of the vector x to be estimated. A good compromise it thus to set $\overline{f_r}$ equal to the Nyquist rate [38] which is tantamount to considering that



Fig. 4. Locations and SNRs of synthetic targets. Range resolution is $\delta_R = 15$ cm and ambiguous velocity is $v_a = 15$ m/s.

TABLE I Scenario Parameters for Synthetic Data

carrier	$f_c = 10 \text{ GHz}$
bandwidth	B = 1 GHz
PRF	$f_r = 1 \text{ kHz}$
# pulses	M = 32
LRR segment	K = 8
noise power	$\sigma^2 = 1$

TABLE II Processing Parameters for Synthetic Data

$(\gamma_0, \gamma_1) = (3, 2)$
$(\beta_0, \beta_1/(K \bar{M})) \approx (2.33, 1.33)$
$v_{\rm max} = 22.5 {\rm m/s}$
$\bar{f}_r = 3 \text{ kHz}$
$\bar{M} = 106$
$N_{bi} = 50$
$N_r = 200$

an equality sign holds in (8), i.e., $\bar{f}_r = 4v_{\text{max}}f_c/c$. Then, the number of virtual pulses \overline{M} is chosen 1) high enough to ensure that (10) corresponds to an interpolation formula, and 2) not too high to limit the length of the vector x. Again, a good compromise is to consider that an equality sign holds in (11), i.e., $\overline{M} \approx \left[M \left(1 + B/f_c \right) \right] \overline{f_r}/f_r$. This way, the observation times of both the received and reconstructed signals are identical. Since the values of \bar{f}_r and \bar{M} are now fixed, the interpolation-transform matrix H(15a) is completely defined. Turning then to the values of the hyperparameters (γ_0, γ_1) and (β_0, β_1) involved in the priors of σ^2 (19) and σ_x^2 (25), we use the relations (20) and (28) with $(m_{\sigma^2}, v_{\sigma^2}) = \sigma^2(1, 1)$ and $(m_{\sigma_z^2/(K\bar{M})}, v_{\sigma_z^2/(K\bar{M})}) = \sigma^2(1, 3)$. The resulting numerical values correspond to a rather informative prior for the thermal noise level (which is reasonable for most radar applications) and a moderately informative prior for the average scatterer power (allowing for a wide range of SNRs). Parameters of interest for the processing are gathered in Table II.

B. Performance

1) Range-Velocity Maps and Histograms: Fig. 5 depicts range-velocity maps of the amplitudes estimated from our Bayesian estimators, the ACAMP algorithm, and a simple coherent integration previously defined in (4). Note that, for a given estimator \hat{x} , the amplitude vector is defined here by $\hat{a} = \hat{x} / \sqrt{K \bar{M}}$. Fig. 5(a) shows the limit of using a coherent integration in case of a multitarget scenario since velocity sidelobes are quite high. For instance, though the isolated scatterer around range bin 4 can be well inferred, the target located at range bins 1-2 cannot be clearly distinguished from the sidelobes of the other targets. On the other hand, Figs. 5(b) to 5(d)highlight the interest of using a sparse recovery approach in that case. Indeed, the three CS estimators (MMSE, MAP, ACAMP) of x give a satisfying sparse representation of the target scene. In particular, no false alarm occurs at the location where sidelobes are expected for a conventional coherent integration. As can be observed (and confirmed by intensive simulations in Section IV-B.2) the MMSE estimator tends to better estimate the target amplitude followed successively by the MAP estimator and the ACAMP method (which mostly underestimates⁵ the target amplitude). Moreover, for all of these methods, a small amount of non-zero elements that do not correspond to a true scatterer are present. These false alarms are very low for the MMSE (they are even not visible here given the lowerbound of the colorbar), a little bit higher for the ACAMP, and finally more pronounced for the MAP estimator. These preliminary remarks are in favor with the MMSE estimator that better estimates the migrating targets with a few and low false alarms.

As underlined before, our Bayesian algorithm not only provides a point estimate of x but gives additional information. In particular, histograms and MMSE estimates for σ^2 , w, σ_x^2 can be estimated. They are represented in Fig. 6 and are in accordance with the scenario parameters. Note, that even when the prior is flat, the posterior distribution is clearly tightened around a reliable MMSE estimate. In particular, the estimated level of occupancy is $\hat{w}_{\text{MMSE}} = 1.45\%$ while the true level of occupancy is $N/(K\bar{M}) = 1.18\%$. In the same vein, the average power of the scatterers present in the scene is $N^{-1}\sum_t \sigma^2 SNR_t \approx -5.3$ dB while the estimated one is $\hat{\sigma}_{x,\text{MMSE}}^2/(K\bar{M}) \approx -4.5$ dB. Note also, the accurate estimation of the thermal noise level $\hat{\sigma}_{\text{MMSE}}^2 \approx 0.97$.

2) Error of Estimation and Computational Complexity: The performance of our Bayesian estimators (29) is further investigated by means of Monte-Carlo simulations. Herein, moduli of the target amplitude are kept fixed while their argument as well as the noise are drawn randomly. The performance metric under consideration is the mean absolute error (MAE) defined for an *L*-length vector $\boldsymbol{\theta}$ and

⁵This is not unconventional for ℓ_1 -type solver using a soft thresholding function. Note in particular that no debiasing technique has been applied to the ACAMP method [39].



Fig. 5. Range-velocity map (modulus of complex amplitude only, in decibels). (a) Coherent integration. (b) MMSE estimation. (c) MAP estimation. (d) ACAMP estimation.





Fig. 6. Prior and empirical posterior pdfs. Circle markers represent prior pdfs. Dashed lines represent MMSE estimates. (a) Prior and posterior pdfs of σ^2 . Plain line represents true value for σ^2 . (b) Prior and posterior pdfs of σ_x^2 . (c) Prior and posterior pdfs of w.

Fig. 7. Performance estimation of studied CS estimators. (a) MAE of \hat{x} (in decibels). (b) Simulation time per Monte-Carlo run. (c) MAE of target-subvector of \hat{x} (in decibels). (d) MAE of zero-subvector of \hat{x} (in decibels).

its estimator $\hat{\theta}$ by

$$MAE = \frac{1}{L} \mathcal{E}\{\|\boldsymbol{\theta} - \hat{\boldsymbol{\theta}}\|_1\}.$$

Since the no-basis mismatch hypothesis is assumed (17), the vector \mathbf{x} can be split into a zero-subvector and a target-subvector. The MAEs of \hat{x} and its two subvectors are depicted in Fig. 7 wrt the unfolding parameter v_{max} . A general trend can be observed from these three CS estimators: the zero-subvector is slightly better estimated when increasing unfolding, while the contrary is observed for the target amplitude estimation. Then, considering a fixed v_{max} and the whole vector \hat{x} , the lowest MAE is given by the MMSE estimator, followed successively by the MAP and the ACAMP methods. Considering now the subvectors, it is worth noticing that 1) the MMSE estimator has always the lowest MAE, 2) the MAP estimator better restitutes the target-subvector than the ACAMP method, and 3) an opposite behavior is observed for the zero-subvector: the ℓ_1 -norm error of the ACAMP method is lower than that of the MAP estimator and is near to that of the MMSE estimator. Finally, Fig. 7(b) compares the simulation time of both Bayesian and deterministic approaches (for an unoptimized Matlab code). As expected, the greater the unfolding parameter v_{max} , the longer the simulation time of each method. Besides, the good performance of the MMSE technique has to be counterbalanced by its increased computational complexity compared with the ACAMP method.

3) Robustness Towards Grid Mismatch: Before closing this section, a robustness analysis is finally conducted. Grid mismatch is introduced for the Doppler frequency of each simulated scatterer. More specifically, a constant shift $\delta_{\bar{m}}$ is applied for t = 1, ..., N as follows

$$\frac{2v_t f_c}{c} = \frac{\bar{m}_t + \delta_{\bar{m}}}{\bar{M}} \bar{f}_r$$

so that the no-basis mismatch assumption (17) is no longer verified. We follow then the path of [40] and estimate the MAE between the estimate \hat{x} and the vector x which is now incompressible in the dictionary F^{-1} defined in (16). As can be noticed from Fig. 8, the greater the frequency mismatch, the greater the MAE of the three CS estimators. The MMSE estimator is the most sensitive and its worst MAE is equivalent to that of the ACAMP method. However, this result has to be taken cautiously. Indeed, due to the incompressibility of x, CS estimators split the target power over the vector indices surrounding the true target location. A metric based on a norm error between xand \hat{x} might not reflect then properly the inherent detection capability of a given method. This short analysis emphasizes essentially the need for CS approaches (either Bayesian or deterministic) to robustify the estimation towards mismatch grid and/or to design a postprocessing technique to recover the target gain in case of mismatch.



Fig. 8. MAE of CS estimators (MMSE, MAP, ACAMP) wrt Doppler frequency mismatch.

TABLE III Scenario Parameters for PARSAX Data

carrier	$f_c = 3.315 \text{ GHz}$
bandwidth	B = 100 MHz
PRF	$f_r = 1 \text{ kHz}$
# pulses	M = 64
LRR segment	K = 16
noise power	$\sigma^2 \approx 1$

V. SEMIEXPERIMENTAL RADAR DATA

A. Experimental Setup and Processing Parameters

Performance of the Bayesian estimators (31) is now assessed on experimental data collected at the Delft University of Technology (TU-Delft). Indeed, the International Research Centre for Telecommunications and Radar (IRCTR) at TU-Delft has been developing over the last years the polarimetric agile radar in S- and X-band (PARSAX) [18]. This system situated on the rooftop of a 100m-high building is continuously upgraded. Recently, data acquired via an S-band linearly frequency modulated continuous waveform (LFMCW) with a bandwidth of B = 100 MHz has been showing a good dynamic range. Though the associated range resolution ($\delta_R \approx 1.5$ m) is not as high as thought previously in this paper, fast ground moving targets still may migrate of a few range cells during the CPI.

Since no cooperative targets are available in the data, a semiexperimental scenario is under consideration here, i.e., synthetic targets are injected under condition (17) in a presumed free-target region of the PARSAX data. As our Bayesian model assumes that the noise n is white, an ad-hoc prefiltering operation is performed to filter the clutter after target incorporation. It consists of a simple projection on the noise subspace assuming that the clutter has a Gaussian-shape spectrum with adequate bandwidth. The same reasoning as in Section IV-A is then followed to fix the processing parameters of our Bayesian estimators albeit

TABLE IV Processing Parameters for PARSAX Data		
σ_x^2 prior	$(\beta_0, \beta_1/(K\bar{M})) \approx (2.2, 1.2)$	
max. velocity	$v_{\rm max} = 55 \text{ m/s}$	
virtual PRF	$ar{f_r}pprox 2.4~ m kHz$	
virtual # pulses	$\bar{M} = 161$	
burn-in	$N_{bi} = 50$	
Gibbs-iterations	$N_r = 200$	



Fig. 9. Semiexperimental data. Range resolution is $\delta_R \approx 1.5$ m and ambiguous velocity is $v_a \approx 45.25$ m/s. (a) Coherent integration prior to target injection and clutter filtering (in decibels). (b) True target map.

1) the expected maximum velocity is fixed to $v_{\text{max}} = 55$ m/s to ensure that it is clearly larger than the ambiguous velocity $v_a \approx 42.25$ m/s;

2) the variance of $\sigma_x^2 | \beta_0, \beta_1$ has been increased to $v_{\sigma_x^2/(K\bar{M})} = 5$ as it leads to better performance estimation.

Note also that prior to target injection, the experimental data have been normalized so that the thermal noise level is approximately equal to $\sigma^2 \approx 1$. Parameters of interest for the simulation can be seen in Tables III, IV. A representation of the semiexperimental scenario is also depicted in Fig. 9. In particular, location and density of



Fig. 10. Range-velocity map (modulus of complex amplitude only, in decibels). (a) Coherent integration. (b) MMSE estimation. (c) MAP estimation. (d) ACAMP estimation.



Fig. 11. Prior and empirical posterior pdfs. Circle markers represent prior pdfs. Dashed lines represent MMSE estimates. (a) Prior and posterior pdfs of σ^2 . Plain line represents a priori mean value of σ^2 . (b) Prior and posterior pdfs of σ_x^2 . (c) Prior and posterior pdfs of *w*.

scatterers in the scenario have been chosen to represent vehicles on a freeway during a heavy traffic time.

B. Results

Range-velocity maps obtained from the Bayesian estimators (29) are depicted in Fig. 10 and compared as in the previous section to the amplitude map estimated with the ACAMP method [14]. The target scene recovered by a simple coherent integration (4) is also depicted. The later is clearly highly challenged in dense target environments so that it is hard to tell where the targets are. Note furthermore in Fig. 10(a) the deep notches located not only at the zero-velocity but also at the ambiguous velocities $\pm v_a$. They indeed have been created by the clutter prefiltering operation. This ad-hoc filter does not allow-at least for now given the current bandwidth of the PARSAX system-target at the ambiguous velocities to be detected. Concerning the CS estimators, same comments can be made as for the purely synthetic data. The MMSE, MAP, and ACAMP estimates of x give an adequate sparse representation of each scatterer: the MMSE technique gives the best target scene representation; a few false alarms can still be observed for the MAP estimator; the ACAMP method tends again to underestimate target amplitudes.

Histograms and MMSE estimates in Fig. 11 show that the estimation of the thermal noise level, i.e., $\hat{\sigma}_{\text{MMSE}}^2 \approx 1.23$, may have been slightly erroneous while normalizing the experimental data. This might explain why a better estimation of x is obtained when the prior of the scatterer power $\sigma_x^2/(K\bar{M})$ has a larger variance (recall that its mean has been adjusted to $\sigma^2 = 1$ in the simulation). Note that the estimated level of occupancy is $\hat{w}_{\text{MMSE}} \approx 0.74\%$ which seems reasonable given that the true level is now $N/(K\bar{M}) = 0.66\%$. Finally, the average power of the scatterers present in the scene is $N^{-1}\sum_t \sigma^2 SNR_t \approx -7.8$ dB while the estimated value is $\hat{\sigma}_{x,\text{MMSE}}^2/(K\bar{M}) \approx -6.8$ dB.

VI. CONCLUSION AND PERSPECTIVES

In case of a low PRF wideband waveform, we have interpreted the target signature as the undersampled version of a virtual but nonaliased bidimensional cisoid. Within a compressive sensing framework, we have proposed accordingly a new Bayesian algorithm able to give an adequate representation of multiple scatterer echoes. By adequate, we mean that each scatterer is represented by a single peak without sidelobe (under the no-basis mismatch assumption). Furthermore, this peak is localized unambiguously in velocity and range at the true velocity and initial round-trip delay of the scatterer. Ambiguity is actually removed thanks to the additional information brought by the range migration. Performance of the Bayesian method (especially, the MMSE estimation) obtained with synthetic and semiexperimental data is very encouraging.

The price to pay with the proposed method is its computational complexity, which might be reduced using other MCMC methods or variational Bayes algorithms. Upcoming work may also include an extension of our hierarchical Bayesian model to handle grid mismatch (e.g., via the introduction of small perturbations on the dictionary matrix) and colored noise. Modeling colored noise could be an alternative to the ad-hoc filtering technique proposed in this paper to remove clutter from the experimental data. Finally, the proposed Bayesian estimators would deserve to be fully integrated in a whole compressed sensing detection scheme.

APPENDIX. POSTERIOR DISTRIBUTION OF x | y

We derive in this Appendix the posterior distribution of x given the observation y. First, note that according to the Bayes theorem, the posterior pdf can be rewritten as

$$f(\boldsymbol{x}|\boldsymbol{y}) \propto f(\boldsymbol{y}|\boldsymbol{x})f(\boldsymbol{x}). \tag{34}$$

Then integrating the likelihood (18) over σ^2 given the prior (19) yields

$$f(\mathbf{y}|\mathbf{x}) = \int f(\mathbf{y}|\mathbf{x}, \sigma^2) f(\sigma^2) d\sigma^2$$

$$\propto \int \frac{e^{-[\|\mathbf{y} - \mathbf{H}\mathbf{x}\|_2^2 + \gamma_1]/\sigma^2}}{(\sigma^2)^{KM + \gamma_0 + 1}} d\sigma^2$$

$$\propto [\|\mathbf{y} - \mathbf{H}\mathbf{x}\|_2^2 + \gamma_1]^{-(KM + \gamma_0)}$$
(35)

Furthermore, the marginal distribution of x is given by

$$f(\mathbf{x}) = \iint f(\mathbf{x} | w, \sigma_x^2) f(w) f(\sigma_x^2) dw d\sigma_x^2$$

$$\propto \int (1 - w)^{n_0} w^{n_1} \mathbb{I}_{[0,1]}(w) dw$$

$$\times \int \frac{e^{-[\|\mathbf{x}\|_2^2 + \beta_1]/\sigma_x^2}}{(\sigma_x^2)^{n_1 + \beta_0 + 1}} \mathbb{I}_{[0,+\infty]}(\sigma_x^2) d\sigma_x^2 \times \prod_{i/x_i = 0} \delta(|x_i|)$$

$$\propto \frac{B(1 + n_1, 1 + n_0) \Gamma(\beta_0 + n_1)}{(\beta_1 + \|\mathbf{x}\|_2^2)^{\beta_0 + n_1}} \prod_{i/x_i = 0} \delta(|x_i|)$$
(36)

Finally plugging (35) and (36) in (34) yields the expression (30) of the posterior distribution of x|y.

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Stéphanie Bidon (M'08) received the engineer and master degrees from ENSICA, Toulouse, in 2004 and 2005, respectively, and the Ph.D. degree from INP, Toulouse, in 2008.

She is now with the Department of Electronics, Optronics and Signal of ISAE (Institut Supérieur de l'Aéronautique et de l'Espace, Toulouse) as an assistant professor.

Her research interests include digital signal processing particularly with application to airborne radar.

Jean-Yves Tourneret (SM'08) received the ingénieur degree in electrical engineering from the Ecole Nationale Supérieure d'Electronique, d'Electrotechnique, d'Informatique, d'Hydraulique et des Télécommunications (ENSEEIHT) de Toulouse in 1989 and the PhD degree from the National Polytechnic Institute from Toulouse in 1992.

He is currently a professor in the university of Toulouse (ENSEEIHT) and a member of the IRIT laboratory (UMR 5505 of the CNRS). His research activities are centered around statistical signal and image processing with a particular interest in Bayesian and Markov chain Monte Carlo methods. He has been involved in the organization of several conferences including the European Conference on Signal Processing (EUSIPCO) in 2002 (as the program chair), the International Conference ICASSP'06 (in charge of plenaries), and the Statistical Signal Processing Workshops SSP'12 (for international liaisons). He has been a member of different technical committees including the Signal Processing Theory and Methods (SPTM) committee of the IEEE Signal Processing Society (2001-2007, 2010-present). He has been serving as an associate editor for the *IEEE Transactions on Signal Processing* (2008-2011).





Laurent Savy is currently senior advisor of radar systems at ONERA Radar & Electromagnetism Department since 2007. He started at Thomson Radar Application Centre in 1989, in advanced studies in signal processing. From 2000-2006, he was also with Thales Airborne Systems, responsible for the advanced studies team in the radar technical directorate. His field of interest concerns new concepts in radar and signal processing.

Dr. Savy is author of several papers and patents, in particular regarding STAP (space time adaptive processing) and ATR (automatic target recognition).



François Le Chevalier is in charge of the Chair "Radar Systems Engineering" at Delft University of Technology, The Netherlands, and Scientific Director of Thales Air Operations Division in Rungis (94), France.

A French pioneer in adaptive digital beamforming and STAP radar systems demonstrations, his current research activities include space-time coding for active antenna systems, and wideband unambiguous radar systems. He has been active in- or chairing- the Technical Program Committees of most IEEE International Radar Conferences since Brest, 1999, has recently chaired the Technical Program Committee of EURAD 2012, Amsterdam, and will be the Honorary Chair of SEE/IEEE International Radar Conference in France, 2014.

An author of many papers, tutorials, and patents in radar and electronic warfare, Prof. Le Chevalier is the author of *Radar and Sonar Signal Processing Principles* (Artech House, 2002), editor of *Non-Standard Antennas* (Wiley, 2010), and co-author of *Principles of Modern Radar: Advanced Techniques* (Scitech, IET Publishing, 2012).