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Insights into saline intrusion and freshwater resources in coastal karstic aquifers using a lumped Rainfall-Discharge-Salinity model (the Port-Miou brackish spring, SE France)

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Abstract

The aim of this study was to develop a conceptual model of saline intrusion within coastal karst aquifers by analyzing rainfall-discharge-salinity data and to assess freshwater resources using a lumped modeling approach. In a first step, we analyzed 4 years of data (rainfall, discharge and salinity times series) of the Port-Miou brackish submarine spring in South France (400 km²). A conceptual model of the aquifer was then designed to differentiate a deep brackish reservoir and a shallower fresh one. Salinity variations at the spring are assumed to be controlled mainly by dilution originating from the fresh water in the shallower reservoir. In a second step, a lumped modeling approach was developed based on the conceptual model to simulate discharge as well as salinity over time. We proposed a reservoir-model to take into account slow and fast components in the shallower part of the aquifer and a saline intrusion in the deeper one. This Rainfall-Discharge-Salinity model was calibrated and validated for two periods of 1.5 years at a daily time step and was also tested to reproduce a multi-annual evolution of the available discharge and salinity time series. Good simulation results were obtained to reproduce water and mass budgets as well as discharge and salinity dynamics

during several hydrological cycles. The simultaneous modeling of hydrodynamics and quality data showed the robustness of the model in addition to its easy implementation. Our results led us to propose a new type of seawater mixing mechanism for brackish springs: the dilution type, in addition to the well-known Ventury suction and Head balance types. The application of the lumped model on the Port-Miou brackish spring validated the hydrogeological processes deduced from experimental data, given an initial quantification of the freshwater resources available in such complex brackish karstic aquifers.

Key words: karst, coastal aquifer, lumped model, water resources, saline intrusion, Mediterranean Sea

1 Introduction

Coastal karstic aquifers may constitute important groundwater resources, notably in the Mediterranean region (e.g. Custodio, 2010; Bakalowicz, 2015). The exploitation of such a type of aquifer calls for, first of all, an evaluation of the available freshwater. Secondly, the withdrawal must be done with a special regard to the saline intrusion processes. This requires knowledge of the hydrogeology of the aquifer. A classical scheme of seawater intrusion may represent a saltwater wedge within the aquifer, with a thick transition zone between freshwater and saltwater. But this simplified view cannot explain the presence of a large brackish submarine groundwater discharge to the ocean as observed in many places, notably in karstic areas. In these heterogeneous aquifers, the saline intrusion distribution appears more complex than when compared to porous media, due to preferential flow paths into large conduit networks.

Many authors (e.g. Stringfield and Legrand 1971; Arfib et al. 2007; Fleury et al. 2007a) have pointed out that submarine karstic springs are connected to preferential flows below sea level within karst conduits. Current karst flows are closely linked to paleo-base levels (Audra and Palmer 2013). In the Mediterranean environment, two recent main stages of karst development were identified (Mocochain et al. 2006): the Messinian salinity crisis (5.95 to 5.32 My) and the Pliocene and Quaternary period. Mediterranean sea level decreased by 1500 m during the Messinian, and by ~120 m during the last glaciation (e.g. Kominz 2001). Eustatic variations of the Mediterranean Sea impacted coastal carbonate aquifers. Karst features that form a network for groundwater flows may exist deep below the current sea level and may be connected to the current submarine springs by karst chimney-shafts (Mocochain et al. 2011). Paleo-springs that drained the karst aquifer during the low sea level stage may have been partially or totally clogged during the following transgression stage, either by marine sediments or by deposits from inside the karst (Fleury et al. 2007a, Tassy et al. 2014).

The current submarine brackish springs in the Mediterranean Sea are close to sea level (Fleury et al. 2007a). The salinity of such springs may be highly variable timewise, and is usually related variations in discharge. Main submarine karst springs are brackish, with a salinity decrease in relation with the rainfall events. Two categories of brackish coastal springs can be proposed regarding the salinity minimum. Some springs can be fresh during flood events, like the Almyros of Heraklio spring in Crete (Arfib et De Marsily 2004, Maramathas et al. 2006), the Mortola spring in France (Fleury et al. 2007d), the Blaz spring in Creatia (Bonacci and Roje-Bonacci 1997), or the Spring Creek springs in Florida (Davis and

Verdi 2014). In these cases, the saline intrusion into the karst conduit connected to the spring is limited by the water head. When the head increases in the karst conduit, the discharge rate of intruded salt water decreases, and can be reversed when a threshold is exceeded (the spring water is then fresh). The second type of brackish spring remains brackish even during high water events, as the Moraig-Toix in Spain (Fleury et al. 2007c) or Port-Miou in France (Arfib et al. 2006, Cavalera 2007). In these latter cases, freshwater discharge increases during flood events diluting the brackish water. The behavior of the aquifer is more complex since the saline intrusion seems to not be totally reduced by the head increase at the spring and in the karst network. This kind of karstic aquifer has been poorly described in literature, yet it can drain major regional groundwater resources, as is the case with the Port-Miou aquifer (400 km²) in France.

Coastal springs, as they are brackish, are not directly usable for freshwater supply. However, these springs have, at least, three main advantages. Firstly, they are the main outlet of aquifers which can drain out several hundred km². Their discharge gives a quantitative value of the flow through the aquifer, which is needed to quantify water storage. Secondly, they integrate all the processes that occur within the aquifer: the hydrodynamic functioning of the karst (head and discharge variations related to rainfall) and the saline intrusion mechanism (variations of salinity related to the hydrodynamic functioning). Thirdly, they are a major monitoring point needed for groundwater model fittings and/or validation.

Water managers need to know where to withdraw freshwater and how much. Lumped hydrological models are useful to assist the managers and give a quantitative answer to their questions. But, the modeler may have to face 2 challenges: having a sufficient knowledge of the aquifer behavior, and using a tool that produces helpful results. To do that, Voss (2011, 2012) proposed to use simple, or parsimonious, models. In fact, karst aquifers and saline intrusion in such heterogeneous media are so complex that simple modeling appears to be an efficient approach instead of the application of a distributed approach, for which parameterization remains highly uncertain. Reservoir models are an example of such simple models that are frequently used as lumped at the catchment scale to study the rainfall – discharge relationships. They have been widely applied to investigate hydrogeological functioning of karst aquifers (e.g. Rimmer and Salingar, 2006; Fleury et al., 2007b; Nikolaïdis et al., 2013; Tritz et al., 2011). Furthermore, such conceptual models were improved to simulate solute transport using mixing equations (Charlier et al., 2012; Hartmann, 2012a), showing the ability of lumped approaches to simulate water and mass balances as well as the fluxes dynamics.

The aim of our study is to develop a conceptual model of saline intrusion within a coastal karst aquifer analyzing rainfall-discharge-salinity data and to assess freshwater resources using a lumped modeling approach. The Port-Miou case study in South France is used since it is a major brackish submarine karst spring (mean discharge was higher than 7 m^3 /s in 2011), with varying salinity and since for the first time, four years of new data is available. The approach combined two steps. In a first experimental step, hydrogeological response was investigated from the analysis of rainfall-discharge-salinity time series at the spring. In a second modeling step, a lumped model was developed to simulate spring discharge and salinity at a daily time-step to quantify the fresh and saline discharges that flow through the aquifer. Model application is used to validate the previously built conceptual model and to evaluate the freshwater resources in the aquifer that are affected by seawater intrusion.

2 Study site and data

2.1 General setting

The Port-Miou coastal aquifer is located in the south-east of France (Figure 1a), along the Mediterranean Sea, in a carbonate environment (Jurassic and Cretaceous limestone, dolomite, and mixed siliciclastic-carbonate rocks). The region consists of a fold-thrust belt system (see e.g. Bestani et al., 2015 for an extensive literature review). From South to North, the Port-Miou aquifer extends over the Beausset syncline, the Sainte-Baume thrusts, the Huveaune area, and the Olympe-Aurélien thrust. The present-day structure results from poly-phase deformation events which sequentially interrupted the sedimentary basin development from Cretaceous to present (see e.g. Lamarche et al. 2012). This complex structure forms a vast fractured aquifer reaching 2000 to 3000 meters of thickness, with continuity from inland to the sea (Tassy et al. 2014).

Two main localized submarine outlets, the Port-Miou and Bestouan brackish springs, drain the aquifer to the sea in the bay of Cassis (15 km from Marseilles). They are a few meters below sea level in an early Cretaceous platform of limestones (Urgonian facies). The catchment area extends mainly over a natural landscape made of hills, karst plateau, and polje. The northern boundary of the recharge area is not well-known, but considering the geological context, the area is set to 400 km². The altitudes range from the sea to the summit of the "Sainte Baume massif" and culminates at 1148 meters. The climate is Mediterranean, with the mean annual rainfall ranging between 500 and 1000 mm. Rainfall intensities during spring

and autumn storm events may attain more than 100 mm per day, whereas droughts of long duration occur during the summer season.

2.2 Submarine caves, springs and in-situ underground laboratory

Port-Miou is one of the main coastal karst springs of Europe (Tulipano et al., 2005; Custodio, 2010; Bakalowicz, 2015). The conduit network has been explored from the outlet by cave-divers. They discovered a huge saturated sub-horizontal 20 m diameter karst conduit developing at more than 2 km inland (Figure 1b). The exploration ended at 223 meters below sea level in a karst shaft (Meniscus, 2013). This vertical shaft acts as a connection between the deeper part of the aquifer below sea-level to the surface. The submarine spring of Bestouan, one kilometer eastward, gives access to a 3 km long saturated karst conduit (Romey et al. 2014).

In the 1970's, a submarine dam was built in the saturated karst conduit of Port-Miou, 500 m inland upstream from the spring (Figure 1b). This dam stopped the direct seawater intrusion from the mouth of the submarine spring, but had no effect on the salinity of the groundwater upstream. Groundwater flows across the dam through four pipes. Downstream from the dam, the water level is controlled by sea level (head boundary). Upstream from the dam, the water level varies with the discharge rate, rising from a few centimeters above sea level at low flow to up to 3 meters when the discharge exceeds 40 m³/s (and that point, the water overflows by a spillway). Since the 2000's, the underground dam is an in-situ laboratory used to monitor the submarine groundwater discharge and the salinity of the coastal karst.

2.3 Previous studies

Brackish groundwater flows through the two sub-horizontal karst conduits of Port-Miou and Bestouan. The salinity of the water originates from seawater intrusion (Blavoux et al. 2004). Measurements during dive surveys with a CTD sensor showed that the salinity of the water remained constant along the horizontal conduits (Arfib and Douchet, 2011). It showed that the brackish water comes from the deepest zones upstream from the cave-divers exploration. Moreover, the lag time between the discharge and salinity changes at the dam at the beginning of flood events also showed that the mixing of the freshwater and the saltwater occurs far upstream from the monitoring point (Arfib et al. 2006). Upstream from the dam, there is no mixing with reversal flow from the outlet through the karst conduit. This deep saline intrusion within the karst network was also used by Gilli (2015) to discuss the mixing

of fresh and salt water in a turbulent flow within coastal karst conduits. Previous works between 2004 and 2007 (Arfib et al. 2006, Cavalera 2007, Cavalera et al. 2009) were performed during a long period of drought with few flood events. It showed that the salinity reaches a sill during the low flow periods, of about 14 kg/m^3 , when daily discharge ranged between 2 and 3 m³/s. In December 2008, the discharge of the highest flood event ever recorded at the dam was close to 50 m³/s (Tassy et al. 2010). Even if salinity decreases during high flood events, it has never decreased below 2 kg/m³, due to seawater intrusion, which never stops.

2.4 Data

Daily precipitation and potential evapotranspiration (*PET*) measurements are available at two weather stations (Météo-France, 2015) in the catchment area (Figure 1a): Plan d'Aups (elevation of 605m, north of the "Sainte Baume massif") and Castellet (elevation of 417m, on a topographic plateau between the sea and the mountainous area). The mean precipitation of the catchment is calculated combining the two stations using a rough estimate of their area of influence. As no meteorological station is available above the Plan d'Aups elevation in the mountainous area, we used this station as a representative of the surface above 500 meters (27% of the assumed catchment area), and the Castellet station for the remainder. Mean precipitation and PET are calculated as follows:

(1) P = 27%. P_{Plan d'Aups} + 73%. P_{Castellet} with P: precipitation or PET.

Water level and specific electrical conductivity (SEC) were recorded by CTD sensors at a 15 minute-time-step in the in-situ laboratory. Spring discharge Q is calculated by head differences between water levels recorded in the conduit upstream and downstream from the dam. Salinity is calculated from SEC.

Average daily discharge data is used to remove noise due to high frequency waves and tidal variations. Spring water salinity at the dam, recorded at a 15 minute-time-step, is not influenced by the tide, but average daily salinity data was also computed to have a consistent time-step with rainfall and discharge time series. Two continuous data sets are available, with missing discharge data in between due to equipment failure: Period 1 extends from Dec. 16th 2010 to Jun. 12th 2012 (545 days), and Period 2 from Oct. 21st 2013 to Dec.11th 2014 (417 days). The salinity time series is complete from 2010 to 2014. This constitutes a unique database for the study of karst submarine springs. Furthermore, a few data is available for the years 2005-2006 in Cavalera 2007 and Cavalera et al. 2009.

3 Modeling approach

3.1 Model structure

The aim of our model is to simulate the discharge and the salinity time series at the outlet of karst aquifers having deep and continuous contributions of saltwater. The model is thus a tool to quantify volumes of freshwater and saltwater that flow through the aquifer. As the modeling approach is carried out at the catchment scale, the modeling approach proposed in this paper belongs to parsimonious lumped models. The aquifer is represented as a succession of reservoirs drained by the karstic spring. The structure and the parameters of the conceptual model are presented in Figure 2 It is an adaptation of the conceptual behavior of the aquifer that will be described in the next section (Figure 8). This model is developed from a recently described and tested modeling approach with good performances on rainfall-discharge-solute data by Charlier et al. (2012).

Our model is based on 4 connected reservoirs: a SOIL reservoir that recharges the aquifer partitioned into three DEEP, SLOW and FAST reservoirs. The DEEP reservoir is characterized by brackish water, with low variations of discharge. This reservoir represents the storage function of the aquifer, with a long residence time, affected by saline intrusion. Both the SLOW and the FAST reservoirs are characterized by freshwater. The SLOW reservoir represents the storage and the long recession after rainfall events, whereas the FAST reservoir represents rapid infiltration and transfers through the aquifer during flood events. In this model, one part of the water recharge stays fresh in the aquifer, and the second part is mixed with seawater by saline intrusion in the deeper part of the aquifer. Both of these groundwater flows are then mixed close to the outlet to result in a brackish karst spring.

3.2 Governing equations

Recharge (or effective rainfall) is calculated in the SOIL reservoir from mean rainfall P and PET. If the level of the Soil Reservoir is higher than a threshold ($H_{SOIL threshold}$ parameter), then there is a recharge. The percentage of recharge flowing from SOIL to DEEP reservoir is given by the X parameter. FAST flows are activated when the water level in the SLOW reservoir becomes superior to a threshold parameter ($H_{SLOW/FAST}$ parameter). At this time, SLOW and FAST partitioning is given by the Y parameter.

Discharge Q $[L^3 T^{-1}]$ at the outlet of each reservoir is calculated as a function of the reservoir height H [L] using a linear relation:

(2)
$$Q = H_{out} \times Area$$
 with $H_{out} = H \times k$

where k $[T^{-1}]$ is a constant characterizing the recession curve of the reservoir. Once Q is calculated for each reservoir, then salinity is calculated using the following mass balance equations:

(3)
$$Q_{Spring} . Sal_{Spring} = Q_{BW} \times Sal_{BW} + Q_{FW} \times Sal_{FW}$$

$$(4) \quad Q_{Spring} = Q_{BW} + Q_{FW}$$

Where *Sal* is the salinity (M L^{-3}), with subscript Spring for the spring, subscript BW for Brackish Water, and subscript FW for Fresh Water.

In the DEEP reservoir, intruded seawater mixes with fresh water. Seawater discharge and freshwater discharge feeding this reservoir control the salinity of the deep brackish water. It can be calculated from in-situ measurements of spring salinity and discharge (equations 3 and 4, substituting BW by seawater). In the case that the discharge variations in the reservoir are low, we can assume that the salinity is constant (Sal_{BW} parameter). Deep brackish water discharge ($Q_{DEEP BW}$) is then calculated from the discharge of freshwater ($Q_{DEEP FW}$) and salinity as follows:

(5) $Q_{DEEP BW} = Q_{DEEP FW} \frac{(Sal_{SW} - Sal_{FW})}{(Sal_{SW} - Sal_{BW})}$

where Sal_{SW} is the salinity of the seawater. Knowing seawater and freshwater salinities (i.e $Sal_{SW} = 38 \text{ kg/m}^3$, and $Sal_{FW} \approx 0.5 \text{ kg/m}^3$ respectively), Sal_{BW} is the parameter that controls the deep saline intrusion contribution.

3.3 Parameterization and calibration strategy

The model inputs are the rainfall and PET, and the outputs are the simulated discharge and salinity, which were compared to the observed ones to test model performances Since we chose a lumped modeling approach, the assessment of the input signal was necessarily quite simple: precipitation and recharge rate were fixed constant for the whole recharge area. They were assumed to be well-estimated as the water budget was well-simulated. The model needs

a total of 8 parameters that may be fixed or optimised. We chose to fix a maximum of parameters, especially those that could be estimated from a previous data analysis: the constant salinity of the DEEP brackish reservoir (*Sal*_{BW}), and the three recession coefficients k_{DEEP} , k_{SLOW} and k_{FAST} using recession analysis. In order to simulate inertial functioning of the DEEP reservoir, with very low changes in discharge, k_{DEEP} has to be much lower than recession coefficient generally assessed from karstic spring hydrographs. A value of $k_{DEEP} = 1.10^{-4}$ day⁻¹ was fixed since recession of karstic springs found in the literature ranged generally between 1.10^{-2} and 1.10^{-3} day⁻¹ (e.g. Rimmer and Salingar, 2006; Fleury et al., 2007; Trizt et al., 2011; Hartmann et al., 2012a). Knowing k_{DEEP} , k_{SLOW} was fixed during low-water periods since only slow and deep components contributed to discharge. Then, k_{FAST} was fixed on the highest flood events, knowing both previously fixed recession coefficients. Finally, 4 parameters needed to be optimised: $H_{SOILthreshold}$, *X*, $H_{SLOWFAST}$, and *Y*.

A warm-up period is often used to limit the influence of parameter initialization on model performances. But this kind of approach needs a sufficiently long data set that it is not always possible. In order to avoid this problem, initial water levels in reservoirs were calculated from the first discharge value. This requires beginning during the recession period when the FAST reservoir is empty (i.e. $H_{FASTini}=0$). Then, the initial water levels in the DEEP and SLOW reservoirs ($H_{DEEP ini}$ and $H_{SLOW ini}$) were computed using the following equations:

(6)
$$H_{DEEP\ ini} = \frac{Q_{Spring\ ini}}{Area\ k_{DEEP}} \cdot \frac{(Sal_{Spring\ ini} - Sal_{FW})}{(Sal_{BW} - Sal_{FW})} \cdot \frac{(Sal_{SW} - Sal_{BW})}{Sal_{SW}}$$

(7)
$$H_{SLOW ini} = \frac{Q_{Spring ini} - Q_{DEEP BW ini}}{Area .k_{SLOW}}$$

With $Q_{DEEP BWini}$, the initial deep brackish water discharge, calculated from Equation 5. The model was calibrated against discharge and salinity data by the Particle Swarm Optimisation (PSO) method proposed by Robinson and Rahmat-Samii (2004). Optimisation of model parameters was performed using the Nash-Sutcliffe (NS) efficiency criterion for the spring discharge and salinity. Because the benchmark reference model in NS criteria is the mean observed discharge, it is well-known that it favours high values in the simulation (Moussa, 2010). Thus, in order to optimize simulations on both low and high values (recessions and flood peaks as well as dilutions and brackish water inflows), we computed NS on \sqrt{Q} (NS \sqrt{Q}) and \sqrt{Sal} (NS \sqrt{Sal}), respectively. Since the aim of the model was to simulate

both discharge and salinity, we used the mean of NS \sqrt{Q} and NS \sqrt{Sal} as the goodness of fit for the calibration procedure. The quality of the simulation is also assessed using the Root Mean Square Error on Q (RMSE Q) and Sal (RMSE Sal), on the relative error on the water balance (Er V) and on the salinity mass balance (Er M).

3.4 Sensitivity analysis

In order to assess model behaviour, a sensitivity analysis was carried out on the case study presented in this paper (Period 1 of the time series). For each of the height parameters, several discharge and salinity simulations were tested for differences of ±5%, ±10%, ±25%, and $\pm 50\%$ around the calibrated value. Results of the three NS, RMSE and Er performance criteria variations are plotted in Figure 3 and are interpreted as follows: the fewer the variation of performance criteria, the less sensitive the parameter. As expected, k_{DEEP} is the least sensitive parameter, since its value was fixed so that the discharge from the DEEP reservoir was very little influenced by rainfall events. Globally, parameters controlling flows in the fresh reservoirs (SLOW and FAST) are also less sensitive to discharge as well as salinity simulations: $H_{SOIL threshold}$, $H_{SLOW/FAST}$, Y, k_{SLOW} and k_{FAST} . The two most sensitive parameters are X and Sal_{BW} that control the contribution of brackish water. Analysing these two most sensitive parameters regarding especially the water and mass balances (Er V and Er M) results in : i) a X increase that limits the contribution of freshwater to the karst spring and increases water storage in the DEEP reservoir (which has a limited effect on Q because k_{DEEP} is very low) and consequently leads to a slight salinity over-estimation as well as to a discharge under-estimation, and ii) a Sal_{BW} increase that generates a salinity over-estimation, but also a water budget under-estimation as a consequence of the model calibration procedure performed with a combination of both variables. These first results of the model behaviour show the robustness of our conceptual approach.

4 Results

4.1 Hydrogeological behaviour

4.1.1 The climatological context

The reference weather station with decades of data in the catchment area is the Castellet station (Figure 1). The mean inter-annual rainfall over the last twenty years is 700 mm/y. Over the last ten years, the 2004-2007 period (Figure 4) had a peculiar climatological context, with a low mean annual rainfall close to 500 mm/y. In 2008 and 2009, the annual rainfall has

exceeded the mean inter-annual value. The discharge and salinity time series available for the present study are encompassed between 2010 and 2014. During this latter period, the mean annual rainfall was 826 mm/y (Figure 5), with a minimum in 2012 (585 mm/y) and a maximum in 2014 (1038 mm/y). This climatological context gives the trend of the annual recharge of the aquifer: from 2003 to 2007 the recharge was low, and then the recharge recovered a normal value from 2009 to 2014 (with a lower value in 2012), resulting in two normal years (2008 and 2009) before the beginning of the studied period.

4.1.2 Hydrodynamic response

Figure 5 shows 4 years of daily rainfall, discharge and salinity data recorded between 2010 and 2014. The spring hydrograph shows an annual pattern (seasonal variations) with large peaks corresponding to large storm-events. Table 1 gives the available main data for each year. The minimum discharge was 3 m³/s at the end of the low-flow period (end of summer or autumn). The maximum annual discharge peaks reached 37 m³/s. Mean annual discharge can be calculated for two (almost) complete calendar years: 7.2 m³/s in 2011 (rainfall close to mean inter-annual value) and 8.9 m³/s in 2014 (rainfall superior to mean). The spring is then characterized by a high base-flow value, and a typical karst-type functioning with high-flood events of relative short duration related to the rainfall. It is commonly interpreted as a two component flow: a low flow and storage in matrix (small fractures and intergranular porosity) and a conduit flow within high transmissive karst network.

Furthermore, cumulative probability plots of discharge time series (or flow duration curves) are presented in Figure 6. This is useful to illustrate data from many years in one plot. This method has been used to assess distribution of discharge time series comparing the envelop plots of several springs (Florea and Vacher, 2009), or to search for fitting straight-lines and slope variations of spring flow data (Mangin, 1975; Jeannin and Sauter, 1998). Straight lines on cumulative probability plots indicate that the data are distributed following the chosen probability law (usually log-normal law), with deviations from linearity indicating additional sources or sinks. As the discharge time series is divided in two periods (Figure 5), three plots are drawn on Figure 6: period 1 (2010-2012) in blue, period 2 (2013-2014) in red, and total available data set from 2010 to 2014 (962 days) in grey. The three plots have the same trend: the higher the discharge, the lower the slope of the plots. It is possible to identify 3 main slopes, showing a change of the hydrodynamic response for discharge lower than 5 and higher than 8.2 m³/s. According to Mangin (1975), a higher slope for the lowest discharge values shows storage inflows from previous hydrological cycles, and a lower slope for the highest

discharge values can be explained by a recharge increase (an additional source), for instance by the contribution of a fast infiltration from stream flows through sinkholes. These results show that the hydrodynamic response of the aquifer is highly non-linear.

4.1.3 Discharge and salinity relationship

The salinity time series for the whole available period is plotted in Figure 5. The previously described general trends for the hydrograph are also observed for the salinity: an annual pattern (seasonal variations) with a large drop corresponding to large storm-events. The salinity slowly increases during the low-flow period and decreases sharply during high discharge events. The minimum salinity was 1.9 kg/m³ during the highest discharge event in November 2011, whereas the maximum salinity was 13.3 kg/m³ after long recession periods. The annual average salinity ranged between 7.9 and 10.9 kg/m³ (Table 1). Salinity is plotted versus discharge in Figure 7. Three main results are detailed here-after:

- First of all, Figure 7 encloses the available daily time series between 2010 and 2014, and a data representative of the maximum salinity observed during the previous 2005 to 2007 drought period. Indeed, during the years 2004-2007, the rainfall deficit (Figure 4) led to the highest salinity of 14 kg/m³ (Cavalera et al. 2009) recorded at the Port-Miou submarine spring.

- Second of all, the general trend between discharge and salinity is very salient. For the entire period, a relationship links the salinity to the discharge. This relationship is also coherent with highest salinity data (14 kg/m³) observed in 2005-2006 during the drought period. The red line on Figure 7 shows that the groundwater salinity-discharge relationship can be roughly modeled by a simple mixing equation with two components (mass conservation equations, Eq.3 and Eq.4): salt or brackish water diluted by freshwater. This is equivalent to the mixing of a varying discharge of freshwater (with a salinity of $Sal_{FW}= 0.5$ kg/m³) with a constant discharge of saltwater. The mixing line (Figure 7) can be fitted using the salinity of local Mediterranean seawater ($Sal_{SW} = 38$ kg/m³) for a constant discharge of 1.3 m³/s, or it can be fitted considering a conceptual brackish reservoir with a constant salinity ($Sal_{BW} = 14$ kg/m³) for a constant discharge of 3.6 m³/s. Following this relationship, the salinity of the spring remains brackish even during high-discharge events (Figure 6), and reaches a steady state during long low-flow periods up to 14 kg/m³.

- Finally, the general correlation between the discharge and salinity emphasized by the red line in Figure 7 seems true most of the time, but a few data remains outside the general trend. The domain can be divided in two subareas, below or above the red line. No dots are located below the red line, meaning that for a given discharge the salinity is never fresher than the mixing model. However, a few dots are located above the general trend. These dots belong to hysteresis loops in concentration-discharge plots, due to the lag between pressure and mass transfer, which are common in karst aquifers due to the piston effect in the conduit network (Arfib et al. 2006, Valdes et al. 2006, Ford and Williams 2007, Charlier et al. 2012). During storm events, the discharge increases rapidly and pushes the brackish pre-event water (constant salinity) stored in the conduit that was explored by the cave-divers (and maybe more upstream). This pattern illustrates the stored volume in the karst conduits between the in-situ measurement point and the upstream zone of mixing of the brackish spring is not due to saline intrusion close to the outlet at the submarine spring, but from a deep mixing in the aquifer.

4.2 Rainfall-Discharge-Salinity modeling

4.2.1 Conceptual model and modeling constraints

The time series analysis showed insights on the hydrogeological functioning of the aquifer. A conceptual model of the Port-Miou aquifer is detailed herein and illustrated in Figure 8:

- The aquifer is a typical karst aquifer, with a large change in discharge due to rainfall recharge and flow in conduits. There is a fast infiltration component through karst features.

- The groundwater storage in the aquifer appears high according to the long recession flow. A slow component drains the aquifer and supplies the spring during low-flow period.

- The salinity of the water comes from a deep reservoir where saline intrusion occurs. From the salinity-discharge relationship we may hypothesize that the contribution of this reservoir is almost constant, with a constant salinity of 14 kg/m^3 .

Consequently, our conceptual model shows that saline water due to seawater intrusion is mixed in depth with freshwater in a deep brackish water reservoir. A continuous discharge from this deep brackish reservoir is mixed with freshwater coming from a shallower reservoir, having typical karst response (fast and slow components) to rainfall events.

The conceptual model (Figure 8) summarizes water flows from each involved compartment and the transfer processes that link them. In order to verify the main hypothesis about the

hydrogeological processes that were highlighted above, a modeling application is presented in the next section. The experimental step was conducted at the aquifer scale, and thus a lumped approach was chosen for the modeling step. The modeling constraints were: (i) to equally represent discharge and salinity fluctuations; (ii) to integrate the three DEEP, SLOW and FAST reservoirs; and (iii) to accurately simulate the water and mass budget. The discharge for the three reservoirs will be calculated in relationship to the recharge. It differs from the previous section, where we used a constant saltwater discharge to roughly estimate the discharge-salinity relationship (Figure 7). So in the lumped reservoirs model the discharge of brackish water will be variable according to Eq.5.

4.2.2 Model application

The model was applied on the two periods with continuous rainfall, discharge and salinity data (Figure 5): Period 1 from Dec. 2010 to Jun. 2012, and Period 2 from Oct. 2013 to Dec. 2014. Since the two time periods have different lengths, which could lead to a difficult comparison of model performances, a split-sample test (Klemeš, 1986) was conducted. This test considers that both periods should be used in turn for calibration and validation.

Parameterizations used for calibration and validation procedures on both periods 1 and 2 are given in Table 2. According to performance criteria shown in Table 3, modeling results show good accuracy on discharge and salinity simulations for calibration and validation, given the same goodness of fit regarding the NS criterion. Mean NS criterion (mean of NS \sqrt{Q} and NS \sqrt{Sal}) is 0.82 for calibration on both periods, and is 0.72 and 0.78 for validation on Period 1 and Period 2, respectively. Regarding simulations of calibration on Period 1 and validation on Period 2, the budget is globally equilibrated for flows and salinity with Er V between -1.2% and 3.0%, and Er M between 4.9% and 7.1%. Regarding procedure 2 (calibration on Period 2, validation on Period 1), an underestimation of about 20% of fluxes is observed (ErV and ErM).

Figure 9a and 9b show the simulated time series for calibration and validation procedures of Period 1 and 2, respectively. The general shape of discharge and salinity is well reproduced during high-discharge events as well as during recession periods, regardless of the period of calibration that was used. Focusing on Period 2, in February 2014 the simulated discharge is underestimated while the salinity seems well estimated, explaining the previously noticed underestimation of balances (ErV and ErM) (Table 3). During this specific period, the model highlights that the rainfall-discharge-salinity relationships changed, but returned to a general

behaviour for the next eight months. All these results validate our hydrogeological conceptual model at the catchment scale.

4.2.3 Modeling multi-annual trend

The aim of this section is to assess the model efficiency in simulating multi-annual time series. The previously calibrated model for Periods 1 and 2 was used to simulate discharge and salinity for the whole four-year period (Dec. 2010 to Dec. 2014). Measured discharge data was only available for Periods 1 and 2, with 15 months of missing data, whereas the salinity data was available for the whole period (Figure 5). Figure 10 shows rainfall, and discharge and salinity at the spring. Simulated water levels in the three DEEP, SLOW, and FAST reservoirs are also plotted. The water level of the reservoir FAST naturally decreased quickly and dried up in a few days. The water level of the reservoir SLOW did not dry up in the low-flow period, feeding continuously the spring with freshwater, so that the salinity at the spring remained inferior to 14 kg/m³. The water level of the DEEP reservoir is about 100-fold higher compared to the SLOW one, and remains more or less close to its initial level due to its strong inertial properties ($k_{DEEP}=1.10^{-4}$ day⁻¹).

As expected, both calibration procedures (Period 1 and 2) showed similar results over the whole period. Focusing on the beginning of the Period 2 (October 2013), after 15 months without discharge measurements, discharge and salinity data were very well simulated. The model is able to predict discharge and salinity not only for several months (Period 1 or Period 2) but also for at least a few years, giving efficiency results for a multi-annual trend.

5 Discussion

The aim of our study was to develop a conceptual model of saline intrusion within a coastal karst aquifer analyzing rainfall-discharge-salinity data and to assess freshwater resources using a lumped modeling approach. The application of a lumped model on the Port-Miou brackish spring validated the hydrogeological processes that were deduced from experimental data and showed its ability to reproduce water and mass budget at the spring as well as discharge and salinity dynamics during several hydrological cycles. The following discussion aims to explore four questions: (1) What is new in our modeling approach? (2) What is new about the Port-Miou case-study, analyzing the modeling results? (3) What can we learn about saline intrusion in coastal karst aquifers? (4) What can we deduce about the freshwater resources in similar contexts?

5.1 A simple modeling approach to simulate discharge as well as salinity

One original aspect of our model is the combined use of quantity and quality measurements with model simulations to characterize the hydrogeological functioning of complex karst aquifers as coastal karsts drained by brackish springs. This gives more robustness in the modeling approach, because both discharge and salinity variables are controlled by all parameters, as was illustrated in the sensitivity analysis (Figure 3). Our calibration procedure on both variables is a first step to limit the equifinality – that is the fact that acceptable simulations can be reached by many potential sets of parameterizations - which is a recurrent question during model calibration (Beven, 2006). In the case of aquifers having little internal data, the use of quantity and quality measurements may improve the realism of conceptual model structures (Charlier et al., 2012; Hartmann, 2013). This is one of the main strengths of this model which is parsimonious if we consider that only 8 parameters are needed to adequately simulate two independent time series (that is discharge and salinity). Finally, advantages of such reservoir models are their simple implementation and easy adaptation to various case-studies.

5.2 Insights on the hydrodynamic functioning of the Port-Miou aquifer

We can deduct from the conceptual scheme and the lumped model that groundwater flow is spread out in several compartments inside the aquifer, each with its own hydrogeological behavior. These compartments, viewed as reservoirs for modeling purposes (Figure 8), are all connected together to the main karst conduit of the Port-Miou spring, which has been explored by cave-divers and discharges into the Mediterranean Sea.

The conceptual model includes two reservoirs of freshwater and a third one with brackish water in depth. During recession periods, both SLOW and DEEP reservoirs - but especially the DEEP one - contributed to the discharge. The discharge of the DEEP reservoir is almost constant; consequently, it is characterized by a high storage (small water level variations compared to the saturated zone) and a very low recession coefficient. For the 4 years which were studied (Dec. 2010 to Dec. 2014), this reservoir contributes in average to 4.2 m³/s (Table 4) of the spring discharge (including the discharge of deep intruded seawater), that is about 60% of the total discharge.

The freshwater that dilutes the deep brackish water and decreases the salinity of the spring when the discharge increases, comes from the two reservoirs SLOW and FAST. They drain the last 40% of the outflow. The fast flow has a very high recession coefficient, but it needs a

threshold to be activated. In this latter case, 20 to 25% of the total effective rainfall (from Table 2: (1-X).Y) contributes to fast infiltration and to groundwater flows through karst conduits, with temporal streams losing water through sinkholes in poljes and karstic valleys. The analysis of the three reservoirs' contribution (Figure 9a and 9b) illustrates that FAST flows generated high flood events, while the sum of the SLOW component and the DEEP component is less than 8 m³/s. This discharge value was previously identified in the cumulative probability plots (Figure 6) as a breakpoint below contributions of another storage zone (lower slope for higher discharge). The maximum discharge at the spring is then highly correlated to the recharge duration and intensity, and to the water level in the SLOW reservoir. For the entire period that was studied, the FAST and SLOW flows represent in average 1.0 and 2.0 m³/s of freshwater at the spring, respectively (Table 4).

During Period 2, between December 2013 and February 2014, the model under-estimated slightly (20%) the discharge whereas the salinity is well fitted (Figures 9). Two assumptions can be proposed to explain this change: it may be due i) to the increase of the catchment area during this rainy period, or ii) to a second fast flow component of fresh and brackish water that have been neglected for parsimonious modeling.

5.3 Saline intrusion mechanism in coastal karst aquifer

Coastal karsts are specific aquifers due to conduit networks that are located below the current sea water level. Coastal karst aquifers, as with all coastal aquifers, are intruded by sea water inland that can occur by several different processes (Fleury et al. 2007a). For instance, Davis and Verdi (2014) recently illustrated that saline intrusion can flow through the coastal karst network connected to the sea, leading to a direct flow of sea water into submarine springs during backflow conditions. However, our study clearly showed that even if the seawater can flow inland at the bottom of the karst conduit open to the sea, the Port-Miou submarine spring is brackish due to saline intrusion occurring in depth within the aquifer. One of the main features of the coastal karst is that deep karst conduits can cross the saline intrusion zone. Therefore karst conduits drain a large zone of the aquifer from deep horizons to the surface. Thus, deep brackish water of more or less long resident time mixes with water from fast infiltration flow. This is achieved at the Port-Miou spring by the 2 km long karst conduit that goes down to at least 223 meters below the sea level. Previous studies (e.g. Maramathas et al. 2006; Fleury et al. 2007a) have shown that the seawater flow rate at brackish springs (inland or submarine) can increase with the total discharge of the spring because of the Venturi suction effect, or decrease when the hydraulic head in the karst

network balances the seawater inflow. These processes can be viewed on schematic plots representing saltwater discharge (Q_{SW}) *vs.* freshwater discharge (Q_{FW}) -as illustrated in Figure 11 (the plots have no scale because the mathematical laws that link both variables are not discussed): the "Venturi suction effect" has a rising slope (Figure 11a), and the "head balance process" has a decreasing slope (Figure 11b) down to $Q_{SW}=0$ when the saltwater inflow can be stopped or reversed (see for example the Almyros case study in Arfib and Marsily (2004) and Maramathas et al. (2006)). The Port-Miou case study illustrates a third case (Figure 11c): the flowrate of saltwater (seawater or brackish water) at the spring has a very low variation during all of the hydrological cycle despite big total discharge variations. In this third case, the salinity evolution of the brackish spring is mainly due to freshwater dilution. For the Port-Miou spring, there is no evidence of a decrease of the deep saltwater intrusion within the main karst conduit supplying the spring, while the submarine dam built in the 1970's across the karst conduit forces the water level to rise 3 meters above the sea level during high discharge events (for a discharge superior to 40 m³/s).

To address the mixing issue, we may consider karst as a set of storage or reservoirs, and conduit networks as connectors that link them. As saline intrusion does not encroach on all of the aquifer, some reservoirs stay fresh, whereas others are brackish. The mixing of the water from the different reservoirs results finally in brackish water that flows to the spring, with variable salinity according to the contribution of each reservoir. In the case of the Port-Miou spring, one part of the aquifer behaves as a brackish reservoir with smooth and low changes in hydraulic gradient as a porous aquifer. The mixing zone needs a certain width and a certain transit time so that the aquifer provides some brackish water with an almost constant salinity and discharge. This concept of brackish reservoir that was used for the Port-Miou conceptual model is coherent with other studied karst aquifers such as the Moraig-Toix aquifer (Fleury, 2007c).

5.4 Freshwater resources

We showed that the water head increase at the spring did not decrease the brackish water flow rate at the spring. In natural conditions, the saline intrusion process is not reversible. This results in the fact that freshwater resources are never available at the spring. Freshwater must thus be withdrawn inland.

The FAST and SLOW reservoirs can be viewed as the two components of freshwater flowing through an aquifer not influenced by saline intrusion. This compartment of the Port-

Miou aquifer can be called the upper aquifer, in contrast to the deeper one. The FAST reservoir constitutes the flow through conduits, with a very low storage, and mainly a transmissive function during flood events.

The SLOW reservoir simulates the baseflow of the upper aquifer, which stores the freshwater. Based on four years of simulation, the mean available discharge from this reservoir is around 2.0 m³/s (Table 4). We can also estimate the time needed to drain the volume of water stored in this SLOW reservoir (equivalent to freshwater without saline intrusion) above the spring outlet, using Eq.2 (with $k_{SLOW}=0.011$ day⁻¹, Table 2). Starting from a water level of 100 mm in the reservoir, i.e. the maximum level simulated with the model (Figure 10), it needs 356 days without recharge to simulate a discharge lower than 100 L/s (or 360 m³/hour) at the reservoir outlet. This freshwater is then mixed with the deep brackish water downstream from the DEEP reservoir. Once the freshwater of the upper aquifer and the brackish deep water are mixed, the freshwater is no longer available in the karst conduit supplying the spring. For water management purposes, this freshwater has to be withdrawn upstream from its connection with the karst conduit where the deep brackish water flows.

Finally, our model calculated that between 45% to 60% (Table 2) of the recharge supplied the DEEP reservoir. A large amount of groundwater is stored in this inertial part of the aquifer (very low k_{DEEP} , Table 2). Deep saline intrusion limits the availability of the freshwater resources at the brackish spring, but inland, the groundwater must be fresh.

From the preceding discussion, we can conclude that groundwater is available as freshwater resources in two target zones: (1) in the upper karst aquifer (SLOW and FAST reservoirs), upstream from the connection with the deep brackish water flowing to the spring through the karst features, (2) in the deep aquifer (DEEP reservoir equivalent to a porous aquifer behavior), upstream from the saline intrusion zone. Further work is still needed to locate the connection zone between the upper aquifer and the deep karst conduit.

As future perspectives, since a hydrogeological scheme is now well defined, a geochemical approach could help to gain insights into the water transit-times, water origin, and mixing between brackish and fresh water compartments. Chemical and isotopic tracers may be applied, using e.g. Br/Cl, δ^{18} O/²H, Rn on spring waters sampled during contrasted hydrological conditions and during flood events.

6 Conclusion

To quantify the discharge of fresh and brackish water flowing in a coastal karst aquifer, a Rainfall-Discharge-Salinity reservoir model was developed in accordance with the conceptual model built from the analysis of 4 years of in-situ monitoring of salinity and discharge at the submarine spring of Port-Miou.

On the contrary to other case studies in the Mediterranean context, where springs can be fresh when deep saline intrusion is stopped due to water head increase, our data shows that the saline intrusion can be almost constant over time. We claim that the salinity variations were mainly due to dilution of deep brackish water flows by a shallower fresh aquifer. The contribution of the deep reservoir is never stopped or reversed. Consequently, actual freshwater resources exist in this aquifer inland but are not available at the outlet. Our results led us to propose a new type of seawater mixing mechanism for brackish aquifers: the dilution type in addition to the well-known Ventury suction, and Head balance types.

In conclusion, our combined experimental and modeling approach appears to be relevant for managers to carry out a robust diagnostic of the available freshwater resources in brackish aquifers. As the presented Rainfall-Discharge-Salinity model is easy to implement, we expect it to be a generic tool, which could be tested as a first step to help characterize the hydrogeological functioning of such complex brackish aquifers.

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Table 1: Annual (calendar year) rainfall, discharge, and salinity data of the Port-Miou aquifer

	D ' (* 11 /								
	Rainfall (mm)		Discharge (m ³ /s)			Salinity (kg/m ³)			
	Le Castellet	Plan d'Aups	Minimum	Mean	Maximum	Minimum	Mean	Maximum	
2011	752	999	3.4	7.2	37	1.9	8.9	12.1	
2012	584	917	4.2* *Data from 01 days)	- 1/01/12 to 06/	24* 12/12 (164	5.3	10.9	13.3	
2013	884	1121	3.0** **Data from 1 days)	- 10/21/13 to 12	22** 2/31/13 (72	4.7	9.1	12.2	
2014	1038	1371	3.6*** ***Data from days)	8.9*** 01/01/14 to 1	36*** 2/11/14 (345	2.6***	7.9***	11.0***	
				-					
0	6	2							

Table 2: Calibration values of the model parameters: period 1 from Dec. 2010 to Jun. 2012, and period 2 from Oct. 2013 to Dec. 2014

Threshold value to activate		1 0110 0 1	renoa z
reservoir	mm	7.1	37.9
Recession coefficient for the DEEP reservoir	day ⁻¹	1.10 ⁻⁴	1.10^{-4}
Recession coefficient for the SLOW reservoir	day ⁻¹	0.011	0.011
Recession coefficient for the FAST reservoir	day ⁻¹	0.190	0.190
Percentage of recharge of the DEEP reservoir	%	59.64	45.79
Threshold value in SLOW reservoir to activate FAST flows	mm	52.7	36.8
Percentage of recharge of the FAST reservoir (when $H_{SLOW/FAST}$ is exceeded)	%	65.61	43.58
Constant salinity of the DEEP reservoir	kg/m ³	14.0	14.0
meters			
	Recession coefficient for the DEEP reservoir Recession coefficient for the SLOW reservoir Recession coefficient for the FAST reservoir Percentage of recharge of the DEEP reservoir Threshold value in SLOW reservoir to activate FAST flows Percentage of recharge of the FAST reservoir (when <i>H</i> _{SLOW/FAST} is exceeded) Constant salinity of the DEEP reservoir neters	Recession coefficient for the DEEP reservoirday ⁻¹ Recession coefficient for the SLOW reservoirday ⁻¹ Recession coefficient for the FAST reservoirday ⁻¹ Percentage of recharge of the DEEP reservoir%Threshold value in SLOW reservoir to activate FAST flowsmmPercentage of recharge of the FAST reservoir (when $H_{SLOW/FAST}$ is exceeded)%Constant salinity of the DEEP reservoirkg/m ³	Recession coefficient for the DEEP reservoirday ⁻¹ 1.10^{-4} Recession coefficient for the SLOW reservoirday ⁻¹ 0.011 Recession coefficient for the FAST reservoirday ⁻¹ 0.190 Percentage of recharge of the DEEP reservoir%59.64Threshold value in SLOW reservoir to activate FAST flowsmm52.7Percentage of recharge of the FAST reservoir (when $H_{SLOW/FAST}$ is exceeded)%65.61Constant salinity of the DEEP neterskg/m³14.0

Table 3: Model performances for calibration and validation procedures for Period 1 (from 16 Dec. 2010 to 12 Jun. 2012: 545 days) and Period 2 (from 21 Oct. 2013 to 11 Dec. 2014: 417 days).

Table 4: Mean values of observed and simulated discharge and salinity at the Port-Miou brackish spring for the whole monitoring period (Dec. 2010 to Dec. 2014) according to the two calibration procedures.

Parameter name	Signification	Unit	Observations.	Calibration on Period 1	Calibration on Period 2.
Q _{Mean}	Mean total discharge at the brackish spring	m ³ /s	7.45*	7.48	6.92
$\operatorname{Sal}_{\operatorname{Mean}}$	Mean salinity at the spring	kg/m ³	9.19	9.15	9.6
$Q_{\text{Mean_DEEP}_FW}$	Mean simulated discharge of freshwater flowing out of the DEEP reservoir	m ³ /s	n.a.	2.78	2.63
Q _{Mean_DEEP_BW}	Mean simulated discharge of brackish water flowing out of the DEEP reservoir (including the Q _{Mean_DEEP_FW} previously given)	m ³ /s	n.a.	4.34	4.11
$Q_{\text{Mean}_\text{FAST}}$	Mean simulated discharge of freshwater flowing out of the FAST reservoir	m ³ /s	n.a.	1.01	0.95
Q_{Mean_SLOW}	Mean simulated discharge of freshwater flowing out of the SLOW reservoir	m ³ /s	n.a.	2.14	1.86

* Observed discharge only available on Periods 1 and 2 (missing data from 13 Jun. 2012 to 20 Oct. 2013)

Figure 1: (a) Structural map (modified from Lamarche et al. 2012) of the Provence region (South-East France), with the location of the Port-Miou spring and its recharge area. (b) Schematic cross section of the Port-Miou karst conduit explored by cave-divers (Meniscus 2013) 2 km upstream of the sea and down to 223 m below sea-level.

Figure 2: Structure of the rainfall-discharge-salinity reservoir model devoted to a brackish spring.

Figure 3: Sensitivity analysis for model parameters (see Table 2 for parameters signification) on Period 1; plots show the variation of three performance criteria (*NS*, *RMSE* and *Er*) for differences of $\pm 5\%$, $\pm 10\%$, $\pm 25\%$, and $\pm 50\%$ of the tested parameters around the calibrated value. Note that negative NS values are not represented.

Figure 4: Annual rainfall from 1994 to 2014 at the meteorological station Le Castellet (elevation 417m); the dotted black line represents the mean annual rainfall over the1994-2014 period.

Figure 5: Rainfall, discharge and salinity time series of the Port-Miou submarine spring at a daily time step (4 years, from 12/16/2010 to 12/11/2014). Highest rainfall events produce high-flood events, with a correlated decrease of salinity.

Figure 6: Cumulative probability plot of daily discharge data at the Port-Miou spring (Period 1 and 2 referred to time series from 16 Dec. 2010 to 12 Jun. 2012, and from 21 Oct. 2013 to 11 Dec. 2014, respectively).

Figure 7: Salinity vs. discharge (mean daily data) measured at the Port-Miou submarine spring, from 16 Dec. 2010 to 11 Dec. 2014 (missing data from 06/12/12 to 10/20/13). The maximum salinity value was observed during the low flow period in summer 2005 and 2006 by Cavalera (2007). A mixing equation is fitted, for a constant discharge of brackish water (Salinity = 14g/l, Discharge =3.6 m³/s), and for a varying discharge of freshwater (Salinity = 0.5 g/l).

Figure 8: Conceptual model of the hydrogeological functioning of the Port-Miou coastal karst aquifer, showing the mixing of brackish water due to seawater intrusion in the aquifer in depth with freshwater from the shallower aquifer.

Figure 9: Simulation results for (a) calibration on Period 1 (Dec. 2010 to Jun. 2012) and validation on Period 2(Oct. 2013 to Dec. 2014), and for (b) calibration on Period 2 and validation on Period 1. Simulated discharge is split in 3 components related to the FAST, SLOW, and DEEP reservoirs.

Figure 10: Simulation results over the whole period available (Dec. 2010 to Dec. 2014) showing the water level variations in the FAST, SLOW, and DEEP reservoirs. #1 and #2 refer respectively to calibration on Period 1 and Period 2. Note the missing discharge data from Jun. 2012 to Oct. 2013.

Figure 11: Three types of relationships between Seawater discharge (Q_{SW}) and Freshwater discharge (Q_{FW}) at a karstic brackish spring for "Venturi suction effect", "Head balance process" and "Dilution".

Graphical abstract



Highlights

- *We investigate fresh and salt water mixing in coastal karst aquifers
- * Discharge and salinity data show that the brackish spring is diluted but never fresh
- * We built an original lumped parsimonious rainfall-discharge-salinity model
- * The model fits mass budgets suitably as well as discharge and salinity time series
- * We propose a new type of seawater mixing mechanism (dilution) for brackish springs

1 Figure 1: (a) Structural map (modified from Lamarche et al. 2012) of the Provence region 2 (South-East France), with the location of the Port-Miou spring and its recharge area. (b) 3 Schematic cross section of the Port-Miou karst conduit explored by cave-divers (Meniscus 4 2013) 2 km upstream of the sea and down to 223 m below sea-level.

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Deep saline intrusion

1500 m

223 bsl

500 m

recharge

SGD

8 Figure 2: Structure of the rainfall-discharge-salinity reservoir model devoted to a brackish





Figure 3: Sensitivity analysis for model parameters (see Table 2 for parameters signification) on Period 1; plots show the variation of three performance criteria (*NS*, *RMSE* and *Er*) for differences of $\pm 5\%$, $\pm 10\%$, $\pm 25\%$, and $\pm 50\%$ of the tested parameters around the calibrated value. Note that negative NS values are not represented.



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Figure 4: Annual rainfall from 1994 to 2014 at the meteorological station Le Castellet (elevation 417m); the dotted black line represents the mean annual rainfall over the1994-2014 period.





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- 52 Figure 8: Conceptual model of the hydrogeological functioning of the Port-Miou coastal 53 karst aquifer, showing the mixing of brackish water due to seawater intrusion in the aquifer in
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Figure 9: Simulation results for (a) calibration on Period 1 (Dec. 2010 to Jun. 2012) and validation on Period 2(Oct. 2013 to Dec. 2014), and for (b) calibration on Period 2 and validation on Period 1. Simulated discharge is split in 3 components related to the FAST, SLOW, and DEEP reservoirs.



a) Calibration on Period 1



Figure 10: Simulation results over the whole period available (Dec. 2010 to Dec. 2014) showing the water level variations in the FAST, SLOW, and DEEP reservoirs. #1 and #2 refer respectively to calibration on Period 1 and Period 2. Note the missing discharge data from Jun. 2012 to Oct. 2013.

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Figure 11: Three types of relationships between Seawater discharge (Q_{SW}) and Freshwater discharge (Q_{FW}) at a karstic brackish spring for "Venturi suction effect", "Head balance process" and "Dilution".

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