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# An 850 nm SiGe/Si HPT with a 4.12 GHz maximum optical transition frequency and 0.805A/W responsivity

ZERIHUN GEDEB TEGEGNE<sup>1</sup>, CARLOS VIANA<sup>1</sup>, MARC D. ROSALES<sup>1,2</sup>, JULIEN SCHIELLEIN<sup>1</sup>, JEAN-LUC POLLEUX<sup>1</sup>, MARJORIE GRZESKOWIAK<sup>1</sup>, ELODIE RICHALOT<sup>1</sup> AND CATHERINE ALGANI<sup>3</sup>

*A  $10 \times 10 \mu\text{m}^2$  SiGe heterojunction bipolar photo-transistor (HPT) is fabricated using a commercial technological process of 80 GHz SiGe bipolar transistors (HBT). Its technology and structure are first briefly described. Its optimal opto-microwave dynamic performance is then analyzed versus voltage biasing conditions for opto-microwave continuous wave measurements. The optimal biasing points are then chosen in order to maximize the optical transition frequency ( $f_{\text{Topi}}$ ) and the opto-microwave responsivity of the HPT. An opto-microwave scanning near-field optical microscopy (OM-SNOM) is performed using these optimum bias conditions to localize the region of the SiGe HPT with highest frequency response. The OM-SNOM results are key to extract the optical coupling of the probe to the HPT (of 32.3%) and thus the absolute responsivity of the HPT. The effect of the substrate is also observed as it limits the extraction of the intrinsic HPT performance. A maximum optical transition frequency of 4.12 GHz and an absolute low frequency opto-microwave responsivity of 0.805A/W are extracted at 850 nm.*

**Keywords:** Microwave photonics, Si-based devices and IC technologies

## I. INTRODUCTION

Short distance communications encourage the development of optoelectronic components on Silicon. In particular ultra-low-cost silicon based optoelectronics is highly desirable for Radio-over-Fiber applications within buildings and houses [1]. SiGe phototransistors are potential candidates for light detection that were proposed for the first time in 2003 [2, 3] to be integrated in the standard SiGe heterojunction bipolar transistor (HBT) technology. Since then, several laboratories have integrated such devices in various SiGe BiCMOS industrial technological process such as TSMC [4], IBM [5] and AMS [6]. Microwave phototransistors have the advantage to combine a PIN photodiode with an HBT, thus lowering the output impedance and making easier the match to the other components of the electronic circuits. Indeed, it avoids the need of a transimpedance amplifier as previously studied based on InP/InGaAs heterojunction bipolar photo-transistor (HPTs) [7, 8] and are recently with SiGe HPTs as well [6, 9, 10].

There is a continuous need to verify the ability of the phototransistor integration in newer commercial SiGe technological process offering faster operating frequencies but also to improve the performance of the HPT without modification of the technology vertical stack of layers. Based on different technological approaches, the performances of SiGe HPTs were studied by numerous publications as shown in Table 1. In [4] and [5], the HPTs frequency response is measured through their time domain optical impulse response at 850 nm via fast Fourier transform (FFT). A cutoff frequency as high as 5.3 GHz was demonstrated. In [3, 11] and [12] the frequency response is extracted directly from opto-microwave continuous wave measurements. It is noticeable that the two methods applied on similar technologies, i.e. [5, 11], provide very different results and may be related to the non-discrimination of the various mechanisms involved in the phototransistor using time domain measurements. In this paper, we will focus on opto-microwave measurements that we trust to be more accurate.

SiGe HPTs have been used for digital optical receiver circuits [13], photo oscillators [14] and more recently a transmission of a 60 GHz WiFi signal operating at 3 Gbps [15]. They provide a novel approach in order to combine high speed HBTs with low cost microwave phototransistors directly in SiGe bipolar and BiCMOS technologies. To optimize the speed of the phototransistor, [16] identified the fastest and slowest illuminated regions of the structure based on physical simulations. References [17, 18] investigated their opto

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Table 1. SiGe HPT performance state from publications.

Process technology	References	DC responsivity (A/W)	Cutoff frequency
TSMC	[4]	0.43*	3 GHz (pulse)
Atmel	[3]	1.49†	0.4 GHz (OM)
IBM	[5]	N/A*	5.3 GHz (pulse)
AMS	[11]	0.93*	0.14 GHz (OM)
IBM	[12]	2.4*	0.518 GHz (OM)

Pulsed: extracted from the impulse response also called FFT transformation. OM: extracted from opto-microwave continuous wave measurements.

\*At 850 nm optical wavelength.

†At 940 nm optical wavelength.

electric compact circuit modeling. M. D. Rosales *et al.* [19] verified through an opto-microwave scanning near-field optical microscopy (OM-SNOM) that the distance between the base, emitter, and collector contacts and the optical window influences the dynamic characteristics of the phototransistor. However, no optimization of the phototransistor speed has been performed in terms of the optical probe position over the device and DC biasing conditions, simultaneously. Moreover, there is no information about the optical transition frequency ( $f_{Topt}$ ) of SiGe HPTs.

This paper investigates the maximum optical transition frequency of a SiGe HPT fabricated in an 80 GHz SiGe<sub>2</sub>RF Telefunken GmbH SiGe Bipolar technological process. The optimum biasing points are analyzed to maximize the  $f_{Topt}$  and an OM-SNOM over the surface of the HPT is done at optimal DC bias to determine the most sensitive as well as the fastest regions of the HPT.

## II. SiGe/Si HPT STRUCTURE UNDER TEST

The SiGe HPT was fabricated using the existing SiGe Telefunken technological process for RF bipolar transistors used in wireless communication, which consists in double HBTs based on polysilicon. The minimum emitter size on the layout is of  $0.8 \times 1.4 \mu\text{m}^2$  for vertical NPN HBT transistors which provides actual size after processing of  $0.5 \times 1.1 \mu\text{m}^2$  due to lateral spacers. This technology exhibits electrical  $f_T$  up to 80 GHz and  $f_{max}$  up to 90 GHz. This enables circuits working above 10 GHz and potentially up to 60 GHz in some configurations [20]. The general scheme of the HBT cross-section is shown in Fig. 1.

The process parameters of the standard SiGe<sub>2</sub>RF HBT technology are not modified to design the phototransistors. This ensures compatibility with the technological process and potential integration of complete opto-electric radio frequency (OE-RF) circuits.

The basic HPT structure is designed by extending simultaneously the emitter, base, and collector layers of the reference HBT [9]. The optical window is set by designing the metal layer of the emitter contact away from the central region. To improve the optical penetration, the superficial silicon oxide and nitride layers at the defined optical window are removed by using a reactive-ion etching (RIE) step available in the process design kit for pads definition. A cross-section of the phototransistor structure is given in Fig. 2. The light path goes through the polysilicon of the emitter before entering the Si emitter, SiGe base, and Si collector regions. This HPT is essentially one large HBT whose emitter metallization was removed on the top. The optical opening size of the phototransistor emitter is  $10 \times 10 \mu\text{m}^2$ . The total emitter size is  $11.3 \times 9.2 \mu\text{m}^2$  and the total collector dimension is  $16.5 \times 10.6 \mu\text{m}^2$ . The base

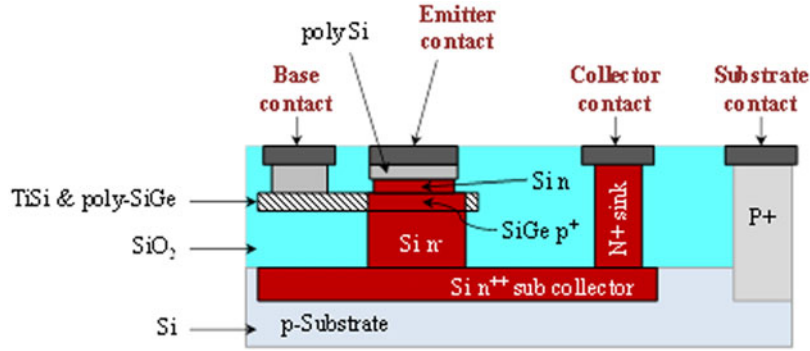


Fig. 1. Schematic cross-section of SiGe<sub>2</sub>RF technology from Telefunken.

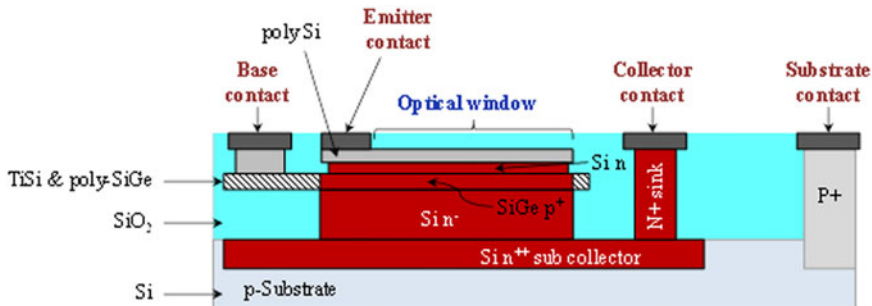


Fig. 2. Simplified schematic cross-section of an extended Emitter Base Collector HPT.

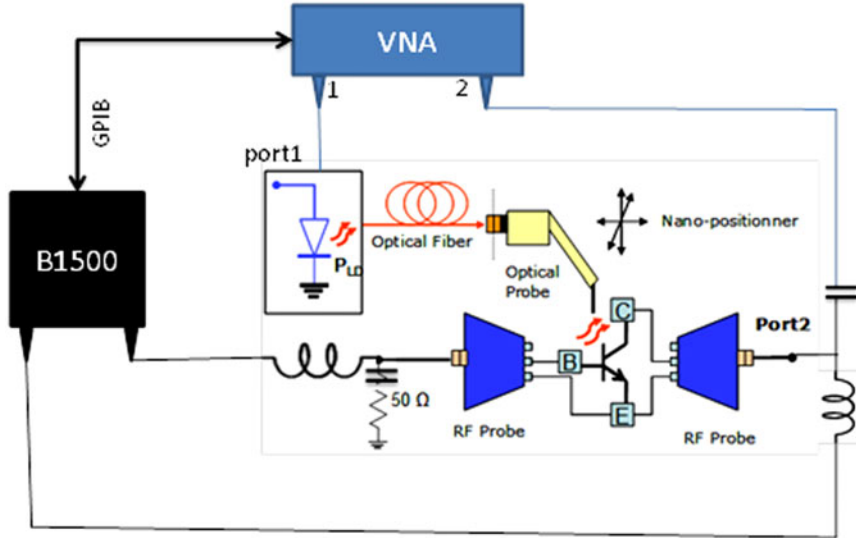


Fig. 3. On wafer opto-microwave measurement bench setup.

profile is a  $\sim 40\text{--}80$  nm thin abrupt SiGe layer with Ge content in the range of 20–25% and with high  $p$ -doping in the range of  $10^{19}\text{ cm}^{-3}$  as inferred from static measurements and physical simulation comparison with earlier 50 GHz SiGe HBT generation [3, 16]. The collector is typically 300–400 nm thick and low doped. A  $p+$  guard ring which is connected to the ground is surrounding the substrate region and creates a homojunction at the interface with the substrate.

### III. MEASUREMENT BENCH SETUP

Figure 3 shows the on-wafer test setup used to measure the HPT opto-microwave performances. It makes use of an 8753ES 40 GHz vector network analyzer (VNA) from Agilent. Port 1 of the VNA directly modulates a 10 Gbps 850 nm multimode vertical cavity surface emitting laser (VCSEL) from Philips ULM photonics. We prefer to use a multimode light source to characterize our device for greater ease and availability but also as it is better consistent with the practical conditions of use of the HPT in home area network (HAN) applications where multimode sources and multimode fibers are largely deployed at 850 nm [1]. The directly modulated optical signal is connected to a 90/10 optical

splitter. The 10% output of the optical power feeds a power meter for monitoring, while the 90% output is injected into the phototransistor through a focusing lensed fiber vertically placed above the HPT optical window. The VCSEL is biased so as to provide a 2.38 mW optical beam at the end of the lensed fiber. The optical probe is mounted on a three axes nano-positioner used to optimize the optical coupling to the HPT.

A tilted mirror is used to monitor the height of the optical probe above the optical window of the HPT through the microscope as shown in Fig. 4. This distance is set at  $50\ \mu\text{m}$  from the surface to align the optical window within the beam waist of the lensed fiber.

The optical probe scans a  $60 \times 60\ \mu\text{m}^2$  surface above the HPT including the  $10 \times 10\ \mu\text{m}^2$  optical window with a  $2\ \mu\text{m}$  step ( $\pm 20$  nm). For each position, S-parameters of the optical link are measured in the (50–20 GHz) frequency range using the VNA. This characterization provides a complete OM-SNOM view of the HPT under test.

The HPT is mounted in a common emitter configuration topology with two  $100\ \mu\text{m}$ -pitch GSG pads in order to perform on wafer microwave measurements. The base is biased through an external bias tee loaded with  $50\ \Omega$  which is the standard normalization load in microwave applications. This  $50\ \Omega$  value is also important as well for intrinsic HPT

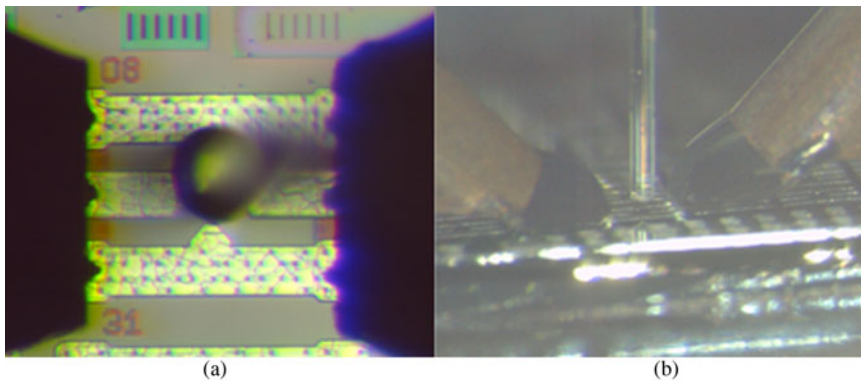


Fig. 4. (a) Top view of the fiber probe spot illuminating the phototransistor, with RF probes at the extremities of GSG access lines; (b) side view through the tilted mirror of the fiber probe illuminating the phototransistor.

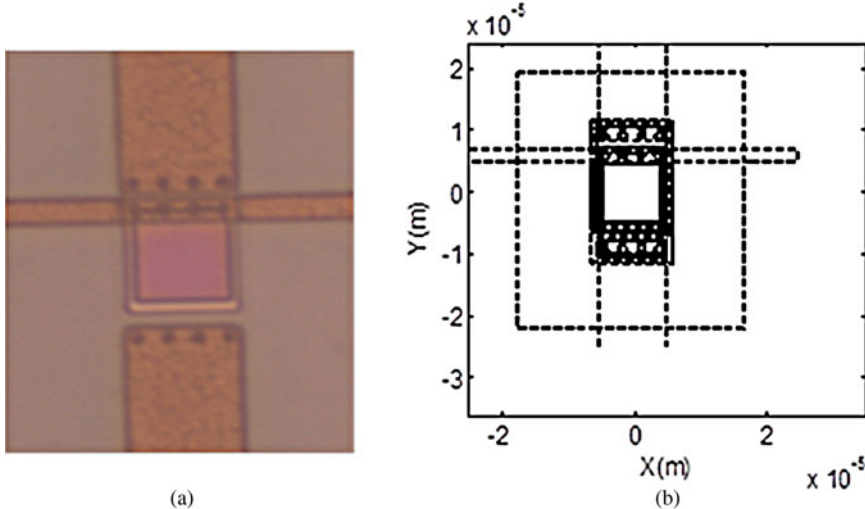


Fig. 5. (a) Top view of the phototransistor; (b) layout of the phototransistor and optical probe coordinate axes centered at the HPT optical window center.

characterization according to [21, 22] on InP/InGaAs. The collector is connected to the port 2 of the VNA and biased through the internal bias tee of the VNA. An Agilent B1500 semiconductor parametric analyzer is used to monitor and to generate the biasing levels required for the HPT.

A proper de-embedding technique is required to extract the behavior of the HPT from the pads, interconnections, and probes effects. There are three techniques suited for an on-probe opto-microwave de-embedding: adapter removal,  $T$ -matrix approach, and ghost removal technique [21, 23].

The adapter removal technique is applied to study a device-under-test (DUT) composed of the VCSEL, the lensed fiber, the SiGe HPT under test, and the RF probes.

The ghost removal sets the DUT to include the VCSEL, the fiber, and the SiGe HPT until only its pad. The measurement of the SiGe HPT with this technique requires four measurement steps and then a two steps post-processing. The DUT in the  $T$ -matrix system is composed of the VCSEL, the fiber, the SiGe HPT, and its GSG probes. It requires three measurement steps according to [21, 23], the first one being a short-open-load-thru (SOLT) calibration at the K-connector's probe planes, and the second one being the extraction of the probe characteristics through a SOLT GSG calibration substrate. The third step consists of the measurement of the full DUT. We preferred to use the  $T$ -matrix technique as it involves less measurement steps, procedures that are mathematically easier to implement and a lower number of connector-level calibrations [21].

Figure 5(a) shows the microscopic picture of the phototransistor where the ground (left and right) and signal (up and down) lines are clearly visible. The base contact is taken from the top side, the collector contact from the bottom side, and the emitter contact is connected at its left and right side to the ground. The layout is accordingly sketched in Fig. 5(b) which defines the optical probe coordinates with its origin given at the center of the HPT optical window.

#### IV. EXPERIMENTAL RESULTS

The S-parameters measurement allows determining the opto-microwave properties of the phototransistor. The opto-microwave

gain of the phototransistor, known as the  $50\ \Omega$  responsivity of the HPT, can be extracted from the transmission parameter ( $S_{2,1}$ ) [2, 22]. The optical transition frequency ( $f_{Topt}$ ) is defined as the frequency at which the  $50\ \Omega$  opto-microwave gain of the HPT mode is equal to the  $50\ \Omega$  low frequency gain of the PD mode ( $V_{be} = 0\ \text{V}$ ). Thus,  $f_{Topt}$  is extracted from these two S-parameter mode measurements.

It is important to determine the best region for optical coupling in order to optimize both the speed and the responsivity of the device. It is also important to optimize its DC biasing level accordingly. Performing an OM-SNOM at various DC biasing conditions could be an ideal way of characterizing the HPT structure. However, due to the limitation of computer memory and measurement time, we prefer to perform OM-SNOM once the biasing conditions have been optimized.

We first perform the opto-microwave measurement of the HPT by setting the optical probe at a given position of the optical window (seeking the maximum gain as much as possible) in order to fix the DC bias. Preliminary results of  $f_{Topt}$  as a function of the base voltage at various collector-emitter voltages are extracted and shown in Fig. 6. For this optical

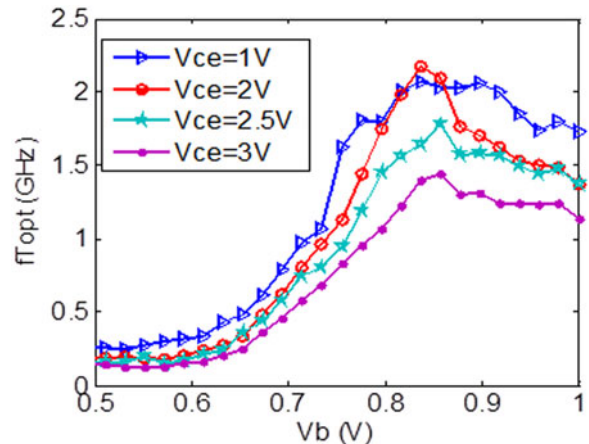


Fig. 6. Optical transition frequency as a function of  $V_{be}$  and  $V_{ce}$  at non-optimal position of the optical probe.

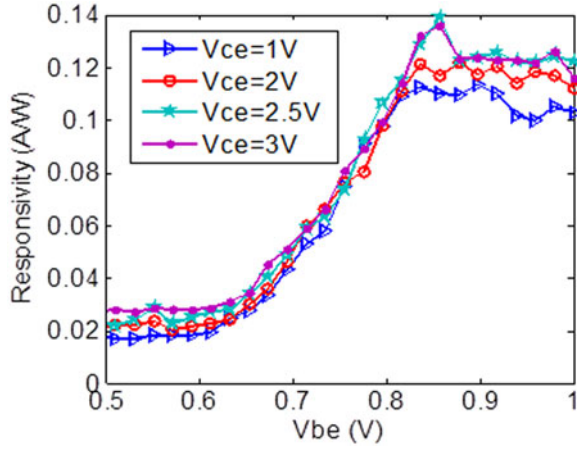


Fig. 7. Responsivity at 50 MHz as a function of  $V_{be}$  and  $V_{ce}$  at non-optimal position of the optical probe.

probe position, a maximum  $f_{T_{opt}}$  of 2.2 GHz is obtained at  $V_{be} = 0.857$  and  $V_{ce} = 2$  V. The low frequency responsivity at 50 MHz versus  $V_{be}$  and  $V_{ce}$  is then given in Fig. 7. A high responsivity is achieved above  $V_{be} = 0.837$  V when  $V_{ce} = 1$  and 2 V, and at  $V_{be} = 0.857$  V when  $V_{ce} = 2.5$  and 3 V.

The experimental OM-SNOM of the HPT is then performed both in the photodiode mode and in the phototransistor mode at the optimum biasing conditions in terms of  $f_{T_{opt}}$  deduced from the previous result: at a fixed collector-emitter voltage of 2 V and a fixed base-emitter voltage of 0.857 V in phototransistor mode, and 2 V  $V_{ce}$  and short circuited base emitter in the photodiode mode. Figure 8 shows the OM-SNOM view of the  $50 \Omega$  low frequency opto-microwave gain (at 50 MHz), i.e.  $50 \Omega$  responsivity. The optical beam is assumed to have a Gaussian profile along  $x$ - and  $y$ -axes.

The resulting opto-microwave response is thus the correlation between the optical window and the Gaussian profile of the beam. The *Erf* function is then used to model this gain and to fit with the measurement [19]. However, since the substrate

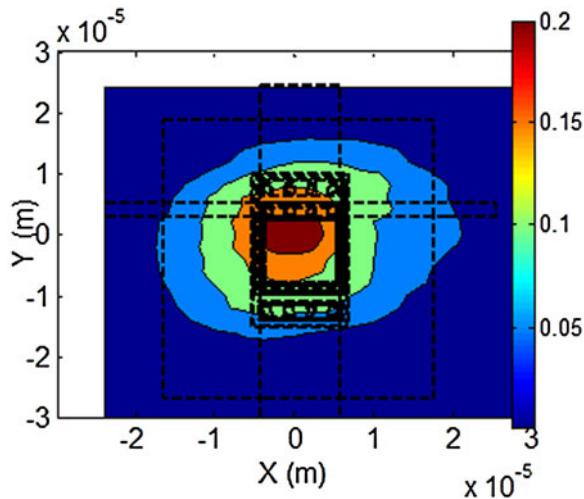


Fig. 8. OM-SNOM view of the  $50 \Omega$  opto-microwave gain at 50 MHz in phototransistor mode, with the HPT layout superimposed, at  $V_{ce} = 2$  V and  $V_{be} = 0.857$  V.

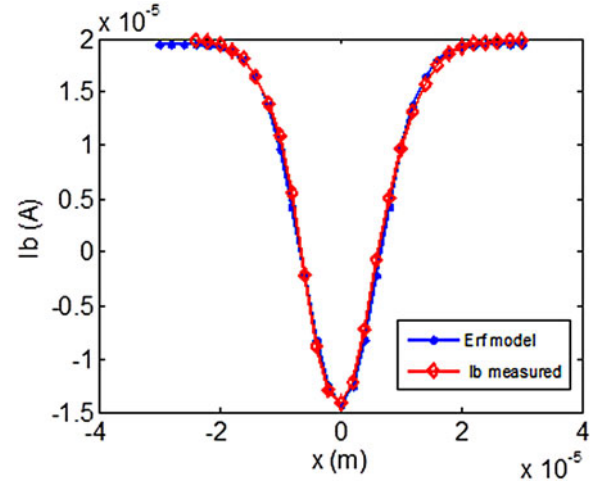


Fig. 9. Slice of the OM-SNOM view of the base current versus  $x$  position at  $y = 0$  m with measurement results (diamonds) and adjusted model (circles) at  $V_{ce} = 2$  V and  $V_{be} = 0.857$  V.

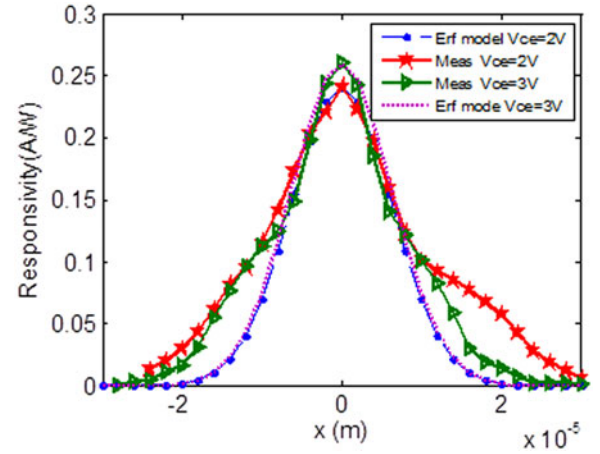


Fig. 10. Slice of opto-microwave responsivity at 50 MHz as a function of  $x$  position ( $y = 0$  m) at  $V_{ce} = 2$  and 3 V ( $V_{be} = 0.857$  V). Bold lines are measured values. Light and dotted lines are *Erf* models.

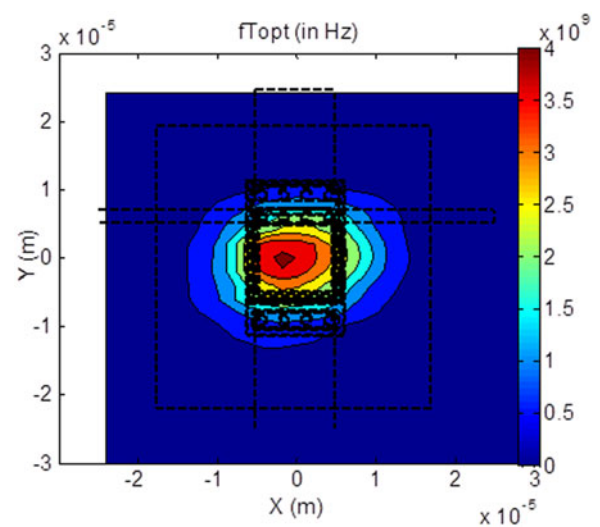


Fig. 11. OM-SNOM view of the optical transition frequency at  $V_{be} = 0.857$  and  $V_{ce} = 2$  V, with the HPT layout superimposed.

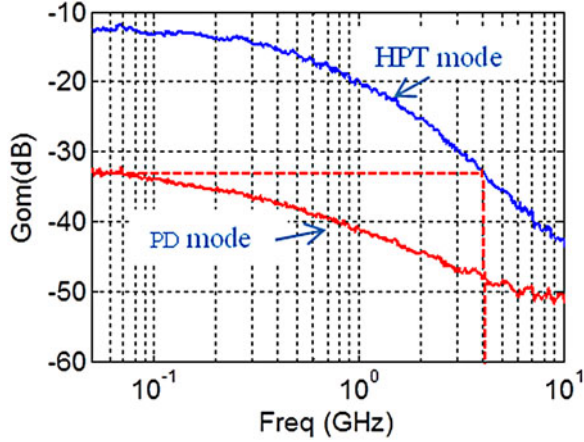


Fig. 12. Opto-microwave gain of the photodiode and phototransistor modes at  $x = 0$  and  $y = 0$  m (peak position of  $f_{T_{opt}}$ ) at  $V_{be} = 0.857$  and  $V_{ce} = 2$  V.

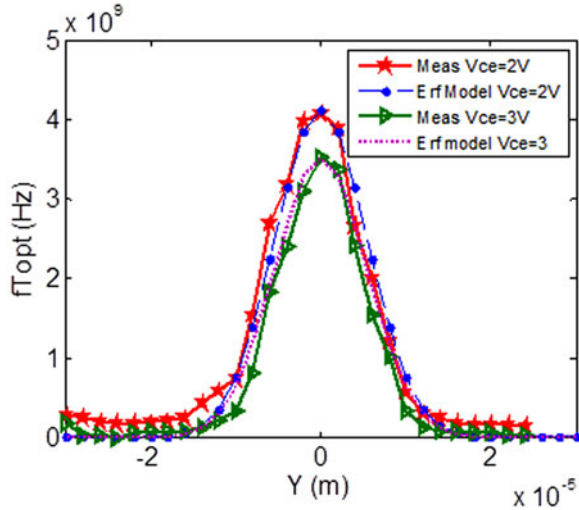


Fig. 13. Slice of optical transition frequency at  $x = 0$  m.

photodiode created by the  $n+$  sub-collector and the  $p+$  ground ring (shown in Fig. 1) is photosensitive at 850 nm, fitting the *Erf* model with respect to the low frequency responsivity is not the right way to extract the optical beam parameters. Indeed, we prefer to fit the model with respect to the base current of the HPT measured in the phototransistor mode as it is independent from the substrate photocurrent. The comparison of the so-extracted model and the measurements is given in Fig. 9. It can be noticed that the photocurrent induced in the base is opposite to the dark current and create a negative sign of  $I_b$  at the peak injection.

The OM-SNOM view of the gain is symmetrical along  $x$ - and  $y$ -axes as shown in Fig. 8. This is also illustrated on the

$x$ -axis cross-section given in Fig. 10. From the adjusted model, we estimate that the power shape of the beam is circular with a full width half maximum diameter of  $28 \mu\text{m}$ . This beam size is larger than the HPT window size. An optical coupling rate of 32.3% between the lensed fiber and the HPT window is then deduced.

The dynamic behavior of the phototransistor over the surface of the structure is analyzed through the optical transition frequency  $f_{T_{opt}}$ . Figure 11 shows the OM-SNOM view of  $f_{T_{opt}}$  as a function of the lensed fiber position. The  $50 \Omega$  opto-microwave gain at the peak detection position is plotted in Fig. 12 for both photodiode and phototransistor modes. The opto-microwave cutoff frequency in phototransistor mode,  $f_{-3dB,hpt}$  is measured to be 0.42 GHz. The measured  $f_{T_{opt}}$  curve is symmetrical with respect to the  $x$ - and  $y$ -axes and has a peak at the center of the optical window,  $x = y = 0 \mu\text{m}$ . Its peak value is 4.12 GHz.

## V. DISCUSSION

The measured opto-microwave gain is well fitted with an *Erf* function in the  $-5 \mu\text{m} < x < 5 \mu\text{m}$  range as shown in the cross-section given in Fig. 10. This indicates that the opto-microwave gain is actually only affected by the coupling ratio in this specific region. At the center of the optical window, a raw  $0.26\text{A/W}$  (resp.  $0.241\text{A/W}$ ) responsivity is measured when  $V_{ce} = 3$  V (resp. 2 V). Taking into account the 32.3% coupling ratio of the lensed fiber to the HPT, an absolute responsivity of  $0.805\text{A/W}$  is then extracted when  $V_{ce} = 3$  V. We also observe an optical gain of 20 dB as shown in Fig. 12 compared with a DC current gain ( $\beta$ ) of 300. It indicates that we benefit from the phototransistor internal amplification property beyond its equivalent photodiode mode operation. An application of this device was shown in [15] with a 3 Gbps data transmission.

The *Erf* function model does not fit well for  $|x| > 5 \mu\text{m}$ . In this case the measured gain is higher than what is predicted from the model curve. This region presents a very low  $f_{T_{opt}}$  as can be seen in Fig. 13, with no specific dependency of the responsivity on the position when moving the fiber across the optical window. This can be explained by the contribution of the Si substrate which absorbs light at 850 nm.

A maximum  $f_{T_{opt}}$  of 4.12 and 3.5 GHz is measured at the peak position when  $V_{ce} = 2$  and 3 V, respectively. According to Fig. 13, the  $f_{T_{opt}}$  curve versus the fiber position follows the same *Erf* function variation as the opto-microwave gain. At both extremities, its value is very low and could be attributed to the substrate detection. This indicates that  $f_{T_{opt}}$  follows the coupling efficiency variation law into the HPT and is then mostly limited by the substrate effect on the photodiode mode. Table 2 provides a summary of the SiGe HPT performances at 850 nm.

Table 2. SiGe HPT Performances.

Vce (V)	Vbe (V)	Relative responsivity (A/W)*	Coupling ratio (%)	Absolute responsivity (A/W)*	$f_{-3dB}$ (MHz)	$f_{T_{opt}}$ (GHz)
2 V	0.857 V	0.241	32.3	0.743	420	4.12
3 V	0.857 V	0.26	32.3	0.805	350	3.51

\*At 50 MHz.



## VI. CONCLUSION

This paper presents a SiGe HPT of  $10 \times 10 \mu\text{m}^2$  optical window developed in an existing 80 GHz SiGe HBT technology without modifying the vertical stacks and layers. The optimal DC biasing has been extracted in order to maximize the  $50 \Omega$  opto-microwave gain and the optical transition frequency  $f_{T_{opt}}$  of the device. An OM-SNOM characterization has been conducted to understand the behavior of the SiGe HPT. A detailed description of the experimental bench setup was provided and use of a direct modulated optical signal to avoid discrepant measurements as seen with SiGe HPTs in the literature. For an optimum DC bias of  $V_{ce} = 2$  and  $V_{be} = 0.857$  V, an  $f_{T_{opt}}$  of 4.12 GHz, a 3 dB cutoff frequency of 420 MHz in HPT mode and an absolute responsivity of  $0.805 \text{ A/W}$  at 50 MHz have been experimentally demonstrated. This phototransistor can be used in further opto-microwave applications where the operating frequency could lie in the 1–10 GHz range where integration to Si integrated circuits and cost are the main issues.

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